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Machine learning of phase diagrams†

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By starting from experimental- and *ab initio*-determined phase diagrams (PDs) of materials, a machine learning (ML) method is developed to infer the free energy function for each phase. The ML method is based on a custom two-step explore-exploit *k*-nearest neighbor strategy, which samples the multidimensional space of Gibbs free energy parameters and user-defined physical constraints into a database of millions of PDs in order to identify the target material properties. The method presented herein is 1000× to 100 000× faster than currently available approaches, and defines a new paradigm on the quantification of properties of materials and devices. As an example application, the developed methodology is combined with the most widely used thermodynamic models – the regular solution, Redlich–Kister, and sublattice formalisms – to infer the properties of materials for lithium-ion battery applications in a matter of hours, reconstructing without human bias, well-established CALPHAD formulations while identifying previously missed stable and metastable phases and associated properties. For the EC–DMC–PC systems, the ML method allows to distinguish between stable and metastable phase boundaries, while simultaneously considering the relevant phases. For the high-power density LiFePO₄ chemistry, a room-temperature metastable phase is identified. Its appearance highlights a previously unreported driving force for the transformation kinetics between lithiated and delithiated states that serves as a stepping stone to access a high-temperature eutectoid state that can be applied to engineer solid-state chemistries. For the high-energy density LiCoO₂ chemistry, a highly lithiated electronically insulating phase is thermochemically favorable, particularly at grain corners and boundaries, greatly improving the description of the experimental voltage profile, irrespective of the used baseline free energy model to describe the relevant phases.

1 Introduction

A phase diagram (PD) is a graphical construction that summarizes the thermochemical ranges of structural stability of a material.¹ It is the roadmap and the starting point to plan the processing of existing and advanced materials, and is the most elusive piece of information when an emerging chemistry is being considered.

The modern CALculation of PHase Diagrams (CALPHAD), pioneered by Meijering and Hillert^{2–4} and Kaufman and Cohen,^{5,6} is a well-established scientific field that enables the systematic prediction of the temperature *vs.* composition PDs of multicomponent chemical solutions. The long historical effort (50+ years) has resulted in a vibrant and evergrowing community amassing a wealth of databases that has been traditionally

powered through commercial software, such as Thermo-Calc,⁷ FACT-SAGE,⁸ and SOLGASMIX,⁹ and most recently through public software libraries such as *gibbs*,¹⁰ *pycalphad*,¹¹ and *OpenCalphad*.¹²

At the heart of a modern PD calculation is the optimization (fitting) of the parameters associated to the Gibbs free energy function that describes a material phase. This optimization is one of the most widely active CALPHAD research areas, as new chemistries become the focus of emerging technological applications, including for high-entropy materials,^{13–16} and in uncertainty quantification.^{17–23} Traditionally, the PD construction process combines experimental (*e.g.*, calorimetric, electrochemical, vapor pressures, and phase boundary measurements) and most recently atomistic calculations²⁴ to enable the prediction of a PD by starting from the periodic table, while simultaneously enabling a deeper understanding of the effect of bonding and solid-state physics on the properties and coexistence of phases. Conceptually, this information is directly fit to Gibbs free energy of mixing state functions (see Methods) with physically interpretable parameters through error minimization algorithms that use weighting factors to provide precedence to the dominant topological feature or material property controlling the accuracy of the fit.²⁵ Existing approaches such as Lukas,^{25,26} PARROT,^{7,27} FITBIN,⁸ and ChemOpt,²⁸ maximize the

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superposition of the Gaussian probability likelihood to a fit of a multivariable free energy function, in comparison to its experimental or first-principles counterpart.²⁷

Fundamentally, the PD optimization process starts by defining a set of Gibbs free energy functions $\{g^{(\alpha)}, g^{(\beta)}, g^{(\gamma)}, \dots, g^{(M)}\}$ of size M describing the possible physical phases of a multicomponent system $\{c_1, c_2, \dots, c_N\}$ of size N , so that for a fixed absolute temperature, a two- or P-phase equilibrium is sought, *i.e.*,

$$\begin{aligned}\mu_i^{(\alpha)}(c_1^{(\alpha)}, c_2^{(\alpha)}, \dots, c_N^{(\alpha)}, T) &= \mu_i^{(\beta)}(c_1^{(\beta)}, c_2^{(\beta)}, \dots, c_N^{(\beta)}, T) \\ &= \dots = \mu_i^{(P)}(c_1^{(P)}, c_2^{(P)}, \dots, c_N^{(P)}, T)\end{aligned}\quad (1)$$

Constraints such as mass and charge conservation are incorporated to reduce the number of degrees of freedom of the physical system.²⁹ Numerically, the optimization is implemented by applying (a) steepest descent, as described by Newton–Raphson and secant methods, *e.g.*, see ref. 9, 28 and 30, until a predefined error tolerance is reached; and (b) energy-minimizing phase fraction search strategies, which have proven their robustness for highly complex models that aim to use a large number of sublattices and their corresponding variables.³¹ Other recent contributions include convex hull solutions, as pioneered by Carter and Cahn,³² and implemented in *gibbs* by Cool, García, *et al.*¹⁰ The current speed of these calculations is a direct function of the analyzed thermochemical system, the specified numerical tolerance, and the coarseness of the discretization, leading to the computation of PDs in wall times that range from seconds to minutes by using commercial software.^{7,8,12,21,33–35}

Currently used approaches deliver a manual trial-and-error process, take from months to years to carry out, and demand specialized intuition, experience, and patience, particularly when experimental data is scarce or partially unavailable.³⁶ In this context, the possibility of deriving two or more contradictory free energy models that optimize the same PD is real, costing invaluable time and effort. Specifically, the application of CALPHAD approaches to engineer materials for lithium-ion batteries (LIBs) remains anecdotal at best,³⁷ even though relevant information for important chemistries such as LiFePO₄ (LFP) has been available since the 1990s.³⁸ The first direct CALPHAD application was only formally reported in the early 2000s,^{39–43} by using polynomial and transcendental functions to fit the excess free energy of mixing models in binary polymer mixtures. Abe and Koyama in 2011⁴⁴ and Chang, Siefert, and coworkers in 2013⁴⁵ reported CALPHAD analyses for the LiCoO₂ (LCO) system, a cathode material for high energy density applications, each with significant differences in the equilibrium potential, particularly in the large lithiation limit. In contrast, *ab initio*-based PDs have been proposed since the late 1990s, as pioneered by Van der Ven and Ceder,^{46,47} and Marianetti and Ceder.⁴⁸ The application of CALPHAD methods to model LFP was not reported until 2011,⁴⁹ and was further advanced in 2019.⁵⁰ The thermodynamic description of LFP remains disconnected from very successful and widely used kinetic and coarse-grained models^{51–53} which, in spite of these deficiencies, provide insights into the intercalation kinetics of LIBs, even though they are based on simple regular solution descriptions.

In spite of the great progress in the construction of phase diagrams, the rate of development of *physical* Gibbs free energy models remains at a pace of months to years at best, limiting a deeper understanding of the materials' thermodynamic and kinetic properties. In this paper, we propose a physics-based Machine Learning (ML) approach to describe material properties of a specified chemistry in a matter of hours, instead of months or years, as a natural extension to the well-established CALPHAD foundation. As an example application, the developed methodology is applied to optimize the properties of LIB-materials, making direct comparisons against available models and experimental data. The existence of equilibrium and metastable phases is inferred from the resulting analysis.

2 Results and discussion

To infer the parameters of the Gibbs free energy state function for each material phase directly from a PD, a two-step k -nearest neighbors (knn)^{54,55} search strategy was developed, see Section 5.3. Here, the Q -dimensional space of free energy parameters was uniformly discretized into a set of equally spaced sampling points, which was used to perform a stochastic optimization step where the distance between a sampled PD point and a target PD were used to identify the physical parameters that most closely match the experimental or numerical system of interest (see Fig. 1). This distance defines an error or loss function between the sampling point and target location. Multiple kinds of experimental data, including electrochemical data and enthalpies of formation, can be used to constrain the search and further improve the optimization of the proposed model. Rather than focus on creating an optimization routine for a few data points, as is traditionally done by the CALPHAD community,^{7,8,12,21,26,56} the proposed ML-method considers the entire range of physically possible states, with equal likelihood. The search strategy was implemented in *gibbs*.ML, an extension of the open-source software *gibbs*,¹⁰ to predict the thermodynamic equilibrium of materials. As compared to traditional CALPHAD methods, which traditionally aim to sequentially optimize the thermochemical parameters against a few key experimental data points,²⁵ the proposed approach compares the sought experimental PD against the computer-generated equivalent, irrespective of the model used to generate the PD.

Fig. 1 shows an example calculation based on 2×10^6 PDs, spanning the entirety of the space of physically accessible parameters in under 30 minutes, ~ 670 μ s per diagram. The calculation of distance, data curation, and search process took on the order ~ 45 min, for a total of 1.1 h of computing time. In comparison, the currently existing commercial software takes between 0.2 s and 15 min per diagram,^{7,8,12,21,33–35} making it unrealistic to implement ML strategies with the commercial packages.

Overall, results for the regular solution free energy of mixing model demonstrate the possibility of PD prediction within a 3% deviation with respect to the target diagram. In contrast to the performed calculations, the goodness of the fit has only



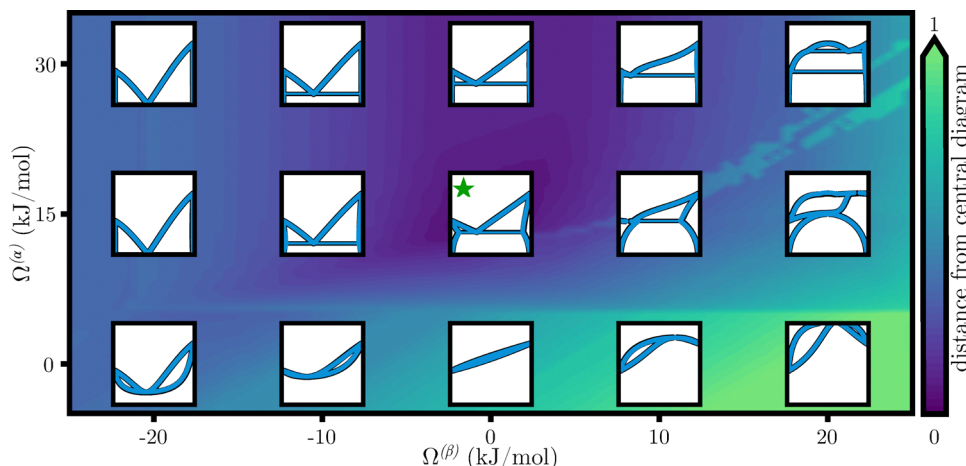


Fig. 1 Graphical depiction of the parameter space for temperature-concentration binary phase diagrams (PDs) describing two phases, α and β , through two regular solution free energy models. Each inset location shows two PDs where \blacksquare corresponds to those originally reported by Pelton and Thompson,⁵⁷ and \blacksquare corresponds to the machine learning (ML)-determined parameters. The background contour plot shows the distance (error) between a central (target) PD, \star , and the surrounding (sampling point) locations. Parameter search occurs through a PD space distance metric which emphasizes differences in solubility, invariant reactions (e.g., eutectic, peritectic), presence of stoichiometric compounds, and other underlying properties such as measurable equilibrium potentials.

recently been openly reported in CALPHAD-determined PDs,^{58–62} by formulating a vector of confidences with accuracies of at least 90% for every phase for the W + Pd system (10% normalized error),⁶³ extending this idea to weigh the prevalence of each phase, resulting in a measure of deviation in the 1–8% range, as shown for the Fe + Ti system.⁶⁴ Bayesian sampling^{17,18,20} has resulted in PDs with deviations on the order of 6%, as reported for the Cu + Mg system.

The application of *gibbs*.ML to an experimental system is summarized in Fig. 2, for ten of the most widely used organic electrolytes used in LIBs,^{39–43} as reported by Ding,⁴¹ i.e., the PC + DEC, DEC + DMC, DMC + EC, EMC + EC, PC + EC, DEC + EMC, DEC + EC, PC + DMC, PC + EMC, and EMC + DMC experimental PDs, which include two stoichiometric solid phases (three if DMC is present), and a liquid phase.⁶⁵ The Redlich–Kister excess free energy model⁶⁶ was used to optimize a third-order temperature-independent set of parameters. This calculation took less than 2.5 min to converge to a set of predicted parameters for each pair of chemistries. Six of the ten electrolyte chemistries show an error less than 3%, in excellent agreement with the experimental data. The DEC + EC system displays the largest model discrepancy on the liquidus line, as compared to Ding's prediction⁶⁵ which used a nontraditional exponential free energy of mixing function. As compared to currently used methodologies,^{7,8,12,21,56} *gibbs*.ML explores a larger space of parameters with no prejudice or bias within minutes, while the traditional optimization analyses require a sequential search of parameters that is prone to be dependent on the search path. The ML-based approach reported herein simultaneously optimizes all the parameters.

Fig. 2 shows that the ML-method enables distinguishing between phase boundary data at equilibrium and away from it, while simultaneously considering all phases present, defining an iterative technique to predict thermodynamically consistent PDs.

For the PC + DMC and PC + EMC systems, the experiment-prediction discrepancy highlights that the experimental data points below the eutectic temperature are metastable, as *gibbs*.ML only reports the equilibrium states. Removal of the metastable data improves the accuracy to 2.82% for PC + DMC and 2.045% for PC + EMC. Finally, the large discrepancy against the EMC + DMC system, as predicted by Ding,⁶⁵ is a result of *gibbs*.ML identifying the peritectic solid–solid phase transition, i.e., a polymorphic transition line, at -53°C for the DMC side of the diagram as a consequence of consistently describing the free energy phases of DMC by the automated knn search.[‡]

The most widely used Gibbs free energy CALPHAD model, the sublattice formalism,²⁴ was implemented for the technologically relevant battery material, LiFePO₄ (LFP), a pseudo-binary system. Two models found in the literature, namely: a short range order sublattice model (SRO) from Lee⁴⁹ and a long range order sublattice model (LRO) from Phan *et al.*,⁵⁰ were directly reproduced by using the experimental data reported by Dodd *et al.*,⁶⁷ see Fig. 3, column O.

Lee⁴⁹ identified the need to use multiple sublattices to successfully model LFP, while Phan *et al.*⁵⁰ extended this description to account for the long range ordering of lithium ions,⁷⁰ enabling the description of larger solubilities at higher temperatures. The direct application of the ML-method presented herein to the LRO model resulted on computation times $\lesssim 1$ h, see Fig. 3, column D, and delivers an improvement on the eutectoid temperature prediction and room temperature solubility as a result of the ability to explore the entirety of the

[‡] At room temperature, because the excess free energy of mixing is at most half the contribution of the configurational entropy, the entropy is being maximized in all the calculations, in agreement with the second law of thermodynamics. Results show that the PC + EC system displays the most stable liquid phase of the analyzed polymer chemistries, while the DEC + EC is the least stable, suggesting that the addition of solute would favor a phase transition.



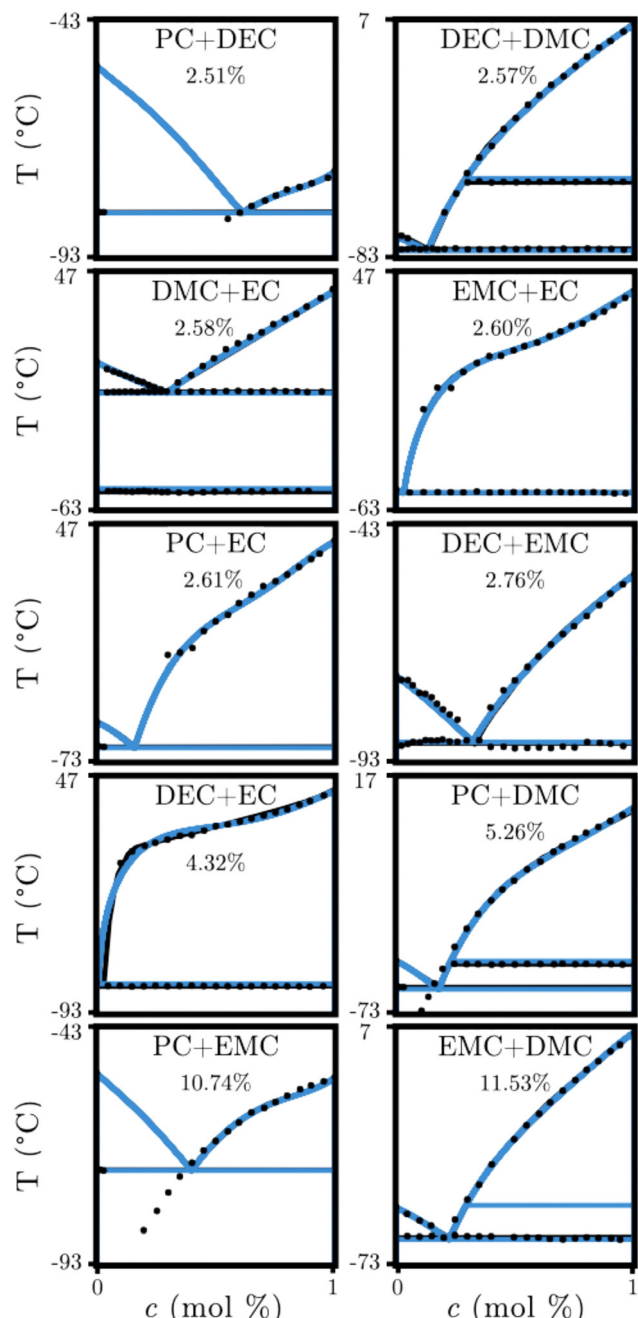


Fig. 2 Thermodynamic model-experiment comparisons for ten polymer electrolyte chemistries used in LIBs.^{39–43} • corresponds to calorimetric measurements,⁴¹ ■ corresponds to PDs reported by Ding,⁶⁵ and — corresponds to the ML-determined PDs. Deviations with respect to the literature-reported two-phase equilibria and the corresponding data are shown as percentages. Note that the largest deviations correspond to the locus of points where the equilibrium phase boundary is expected to be (PC + DMC and PC + EMC), or where newly identified phases have been found (EMC + DMC).

space of all possible PDs without the need for prior, hand-crafted search strategies. In contrast, the *gibbs*.ML optimization on the SRO sublattice formalism took on the order of 55 h and was unable to optimize the experimentally determined deep eutectoid, which is a result of the limitations imposed by the previously reported sublattice model.

Experimental results suggest that the limitations of the LRO and SRO models are a result of the temperature-dependent ferromagnetic properties,^{70–72} which are not captured by these models. To overcome these limitations, a temperature-dependent sublattice formalism, a TLRO model, was proposed, see Section 5,^{36,73} and optimized in *gibbs*.ML in 17 h. The T-LRO model matches the experimental eutectoid temperature and solubility imposed by the phase boundaries, see Fig. 3, row T-LRO. The proposed description shows that the configurational entropy increases the solubility limit,³⁶ suggesting a temperature-dependence on the phase boundaries. In contrast, the PD reported by Dodd *et al.*⁶⁷ is, for all practical purposes, a temperature-independent hand-drawn sketch based on the experimental results, see Fig. 3 (solubility increases less than $\sim 0.01\% \text{ K}^{-1}$). Column P shows a proposed improvement, naturally resulting in a deeper eutectoid while matching the experimental data within 3.68%.^{67,68}

The effect of the different sublattice models against the room temperature experimental equilibrium potentials, as reported by Yamada *et al.*,⁶⁸ and Tan,⁶⁹ is shown in Fig. 3, rightmost column. The upper-right inset highlights that the T-LRO model delivers a 100 mV improvement on the predicted equilibrium electrochemical potential; however, the two-phase region is wider than experiments by 0.05, a small over prediction that can be attributed to kinetic effects.

Even though all three models reproduce the PD within 6% uncertainty, see Fig. 3, lower right, results show that the SRO model will favor traditional spinodal decomposition kinetics, as assumed by multiple authors.^{51,52,74,75} In contrast, the LRO model predicts the formation of a metastable phase at $c \sim 0.6$ in agreement with recent experimental observations in single-crystal particles,^{76–81} and in grain boundaries.^{82,83} The analysis shows that this prediction is a result of a local Gibbs free energy minima that, at high temperatures, will result on the high temperature eutectoid phase transformation. The T-LRO model predicts a larger energy barrier that needs to be overcome to induce the formation of the metastable phase, but will persist for long periods of time if locally stabilized. This suggests that different types of intercalation kinetics have been overlooked, but are possible, particularly in the presence of chemomechanical stresses, surfaces, and interfaces.^{52,74,84} Here, an initially unstable phase can temporarily segregate into a two-phase microstructure (coexistence of metastable and stable phases), before transitioning into a stable two-phase microstructure, each microstructure displaying a characteristic segregation wavelength. Specifically, the results demonstrate that the choice of free energy model impacts the predicted characteristic, or fastest growing wavelength for segregations, $\lambda = \frac{\pi \Delta c \sqrt{2\kappa}}{g_{\max}}$, in agreement with Cahn.⁸⁵ For $\kappa = 5 \times 10^{-12} \text{ J cm}^{-1}$, as reported by Tang *et al.*,⁷⁴ the SRO sublattice model predicts $\lambda^{\text{SRO}} = 5.3 \text{ nm}$, whereas the LRO model defines $\lambda^{\text{LRO}} = 9 \text{ nm}$ and the T-LRO model states $\lambda^{\text{T-LRO}} = 6 \text{ nm}$. This suggests a faster segregation rate of larger wavelengths for the SRO model. In particular, the possibility of metastable characteristic wavelengths, $\lambda_{x < 0.6}^{\text{LRO}} = 7.1 \text{ nm}$ and $\lambda_{x > 0.6}^{\text{LRO}} = 7.0 \text{ nm}$ for the LRO model and $\lambda_{x < 0.6}^{\text{T-LRO}} = 4.7 \text{ nm}$ and $\lambda_{x > 0.6}^{\text{T-LRO}} = 4.8 \text{ nm}$ for the T-LRO model, suggest the temporary appearance of one type of



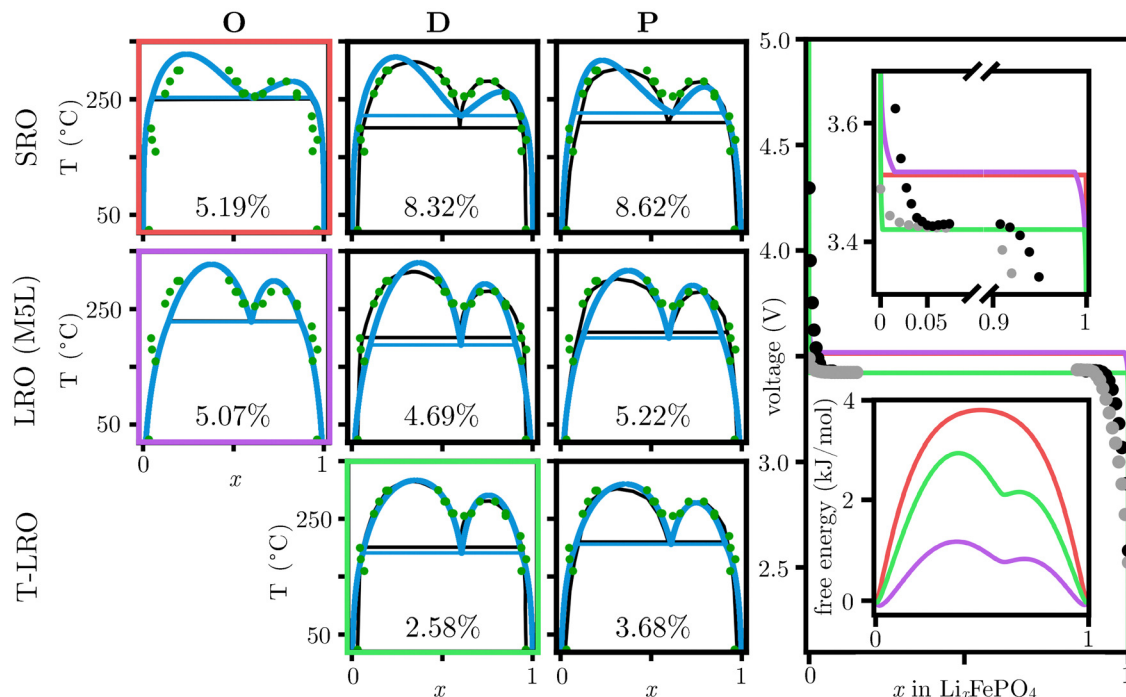


Fig. 3 Catalog of lithium iron phosphate (LFP) PDs including (1) a proposed short range order, four sublattice model by Lee, SRO, \blacksquare ,⁴⁹ (2) a long range order, five sublattice model by Phan *et al.*, LRO (M5L), \blacksquare ,⁵⁰ and (3) a temperature-dependent, five sublattice model proposed herein, T-LRO, \blacksquare corresponds to target PD. \blacksquare corresponds to the ML-determined PD. \bullet corresponds to experimental data, as reported by Dodd.⁶⁷ The deviation with respect to the experimental data is shown as a percentage. Column O shows PDs as published in the literature and reproduced herein. Column D shows a comparison against the originally reported experimental PD,⁶⁷ and column P shows a comparison against a PD with thermodynamically consistent solubility at low temperatures, in agreement with Yamada *et al.*⁶⁸ \bullet corresponds to electrostatic potential experimental data as reported by Yamada *et al.*⁶⁸ and \bullet , as reported by Tan,⁶⁹ both at room temperature. The top-right zoomed-in inset highlights the differences on the predicted voltage profiles, and the bottom-right corresponds to the predicted Gibbs free energy. While each model provides a PD that agrees within nine percent of phase diagram distance to experiments, the effects on the possible stable and metastable phases, as well as the possible energy density and kinetics of intercalation, is predicted to vary widely. Results demonstrate that the T-LRO model is quantitatively in better agreement with both PD and electrochemical data, and suggests a thermally accessible metastable phase, in agreement with Phan *et al.*⁵⁰

microstructure with a fine interlayer spacing where one of the phases displays a low lithium concentration in the lithium-rich phase for short times, to be replaced with a coarser interlayer spacing with the traditionally expected lithium-deficient and lithium-rich phases. The smaller g_{\max} value predicted by the LRO model indicates the metastable phase is expected to persist for long times, whereas the T-LRO model predicts that the eutectoid (chemically disordered) phase would be short lived because of the large driving force to phase separate into rich and lithium-deficient phases. The metastable phase description, naturally captured by *gibbs.ML*, highlights the accelerated transformation between lithiated and delithiated LFP and, as compared to existing kinetic optimization approaches,^{86–88} it demonstrates the importance to simultaneously consider the effects of the kinetic and equilibrium properties as well as incorporating high-temperature phases in emerging modeling formulations.

The application of the ML methodology to complex systems that include a combination of near room temperature experiments,^{89–93} *ab initio* calculations,^{46,47,94} and low C-rate voltage profiles^{89,92,95,96} have been compiled to develop CALPHAD-based models for the LiCoO_2 (LCO) system.^{44,45} Historically, the cobalt oxide (O1), lithium cobalt oxide (O3), and a half cobalt oxide, half lithium

cobalt oxide (H13) phases were optimized by Abe and Koyama,⁴⁴ and later by Chang and coworkers,⁴⁵ to obtain an equilibrium electrochemical potential that agrees in the $0 < x < 0.8$ range, see Fig. 4. Here, the ML-method was extended to directly include the equilibrium voltage profile in the loss function to avoid overfitting. The performed calculation was completed in $\lesssim 6$ h, see Section 5.3 for details. In addition, by starting from the original experimental and *ab initio* data, as well as the latest developments on the expected phases,^{47,48,89,97,98} a PD in the zero to 200 °C temperature range was proposed, see Fig. 4, green PD. However, while the error for the PDs is minimal (less than 5%), all three models overpredict the voltage profile in the $0.3 < x < 0.7$ range, and under predict it for $x > 0.8$.

In this context, Reimers and Dahn⁸⁹ and Ohzuku and Ueda⁹⁰ found a lattice mismatch in the $0.75 < x < 0.925$ range, while Van der Ven *et al.*⁴⁷ speculated on the possibility of a metal-insulator transition by using first-principles calculations. The latter was confirmed experimentally by Ménétrier *et al.*¹⁰⁰ Marianetti *et al.*⁴⁸ proposed that the insulating phase was a result of extrinsic impurities that energetically favor a Mott insulator. Finally, using spectroscopy, Kellerman *et al.*⁹⁸ showed that, for temperatures greater than 150 K, LCO will become insulating for

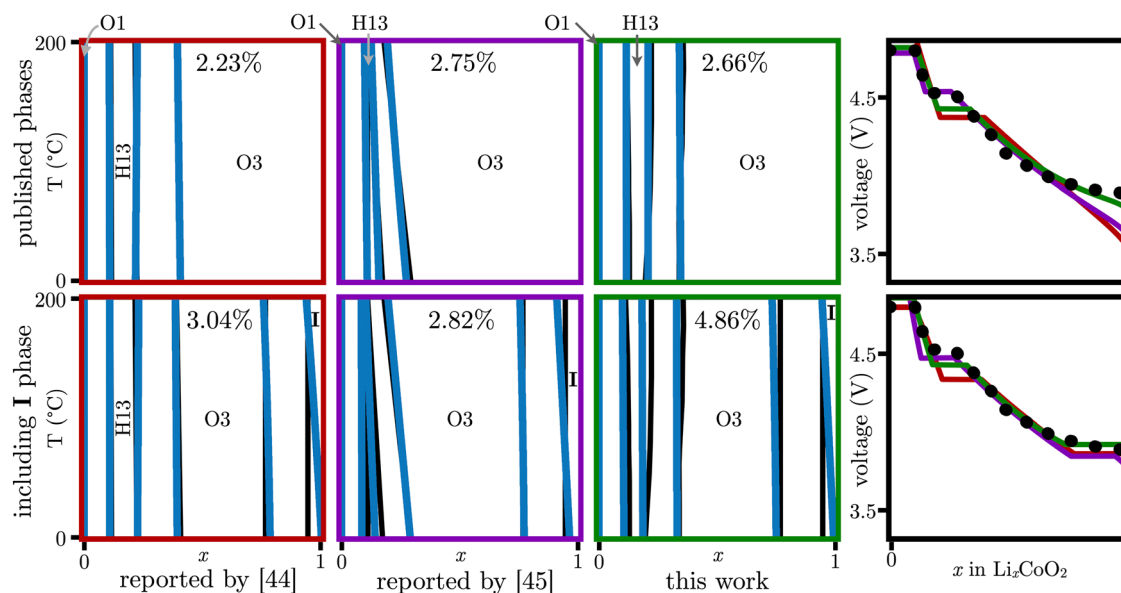


Fig. 4 Lithium cobalt oxide (LCO) PDs and equilibrium electrostatic potential (fourth column). • Corresponds to experimental equilibrium electrostatic potential,⁴⁵ — corresponds to Abe and Koyama,⁴⁴ — corresponds to Chang *et al.*,⁴⁵ and — corresponds to this work. — corresponds to the target PD for the ML-determined PD, as shown in —. In contrast to traditional CALPHAD approaches, which have reported to have inadequate experimental and theoretical data,^{44,45} in spite of the multiple reports and voltage data agreeing on its existence,^{47,48,89,97,98} the second row considers the incorporation of an electrically insulating phase and the associated experimental equilibrium voltage to capture the correct physical behavior.^{89,91,93,99}

$x > 0.85$ due to a decrease of lithium vacancies. Thus, by using a simple regular free energy model, the insulating phase referred herein as O3(I)⁸⁹ was determined, see Fig. 4, bottom row. The results suggest that the proposed insulating phase is thermochemically favorable and in great agreement with the experimental voltage profile, irrespective of the used baseline free energy model to describe the rest of the phases. Further, the addition of an insulating phase results on a shift of the free energies of mixing parameters for all the existing phases, as the optimization process includes the entirety of the composition, thermal, and electrical properties. This indicates that currently available models compromise the values of the physical parameters across all phases in an effort to compensate for the effect of an experimentally observable two-phase region, highlighted by the $0.75 < x < 0.925$ voltage plateau which was previously not considered. The predicted insulating phase favors mixing, $\Omega^{(I)} \sim -30 \text{ kJ mol}^{-1} < 0$, particularly at grain corners and boundaries. At the closing of the writing of this paper, Merryweather *et al.*¹⁰¹ reported the reversible formation of the insulating phase, further supporting the *gibbs.ML* prediction.

3 Conclusion

In conclusion, by extending the open source software, *gibbs*,¹⁰ a novel machine learning approach is presented to infer the thermodynamic state functions of a material by starting from a graphical description, a phase diagram (PD). The method presented herein is three to five orders of magnitude faster than any currently available approach, defining a new paradigm on the quantification of properties of materials and

devices. While it is common to focus on developing automated methodologies that pull away from using physical intuition, the presented ML method emphasizes the importance of using physical principles to guide the rapid development of thermodynamically consistent models that accurately capture the relevant physical phenomena, thus freeing the researcher to spend more time on the physical aspects.

As demonstrated in the ten analyzed organic electrolyte systems, missing phases and metastable experimental data were readily identified and assessed for stability and potential use, by exploring the entire space of parameters without any human bias. Further, the free energy models were reviewed and updated to identify thermodynamically stable phases. For the two analyzed cathode materials, LFP and LCO, published models were compared against their respective PDs and the electrochemical profile. The performed thermochemical and electrochemical analysis allowed to identify previously missed metastable and equilibrium phases that control the power and energy density response and to rapidly assess the validity, influence, and quality of the selected thermodynamic free energy model.

The integration of *ab initio*-based, thermodynamically consistent free energy models into advanced phase field formulations will allow to identify currently overseen physics-based microstructural evolution mechanisms, specifically those that occur in the presence of multiphysical driving forces,^{102–104} effectively removing the bottlenecks that link single-crystal phenomena with long term microstructural response. For the generality of materials, the developed methodology provides the ideal basis to understand the thermodynamic and kinetic limitations for a wide variety of applications that go well



beyond energy-related systems, including ternary and higher order, setting up the stage to dramatically advance the pace of discovery and material design. Finally, while it is beyond the scope of this paper, the methodology presented herein can be readily extended to the multiphysical, multicomponent CALPHAD description of materials and devices.

4 Methods

4.1 Thermodynamic models

For the i th phase of a binary PD, define the Gibbs free energy of mixing as³⁶

$$g^{(i)}(c, T) = g_{\text{form}}^{(i)}(c, T) + g_{\text{mix,ideal}}^{(i)}(c, T) + g_{\text{mix,ss}}^{(i)}(c, T) \quad (2)$$

The formation energy for each end member, $g_{\text{form}}^{(i)}(T) = H_{T_0}^{(i)} +$

$\int_{T_0}^T c_p^{(i)} dT - TS_{T_0}^{(i)} - T \int_{T_0}^T \frac{c_p^{(i)}}{T} dT$ where $c_p^{(i)}$ is typically approximated as a power series. If all phases have the same heat capacity, then $\Delta g_{\text{form}}^{(i)}(T) = \Delta H_{T_0}^{(i)} - T \Delta S_{T_0}^{(i)} = \Delta H^{(i)} \left(1 - T/T_m^{(i)}\right)$ relative to $g^{(s)}$ since $\Delta S_{T_0}^{(i)} = \Delta H_{T_0}^{(i)}/T_m^{(i)}$. The composition-dependent formation energy for a binary system at a given concentration is a simple rule of mixing for the two components a and b,

$$\Delta g_{\text{form}}^{(i)}(c, T) = \Delta H_a^{(i)} \left(1 - T/T_{m,a}^{(i)}\right) (1 - c) + \Delta H_b^{(i)} \left(1 - T/T_{m,b}^{(i)}\right) c \quad (3)$$

The ideal free energy of mixing is given by the configurational entropy contribution, $g_{\text{mix,ideal}}^{(i)}(c, T) = RT(c \ln(c) + (1 - c) \ln(1 - c))$, where R is the universal gas constant.

The simplest nonideal model, the regular solution model, assumes that the excess free energy of mixing, the enthalpy of mixing, to be entirely temperature-independent, and considers quadratic or binary interactions,

$$g_{\text{mix,ss}}^{(i)}(c, T) = c(1 - c)\Omega^{(i)}, \quad (4)$$

whereas the Redlich-Kister model⁶⁶ considers higher order interactions,

$$g_{\text{mix,ss}}^{(i)}(c, T) = c(1 - c) \sum_{j=0}^{L=3} L_j^{(i)}(T) (2c - 1)^j. \quad (5)$$

The interaction parameters are defined herein as linearly dependent on temperature, i.e., $L_j^{(i)}(T) = a_j^{(i)} + b_j^{(i)}T$.

Stoichiometric compounds were modeled in terms of the stable, equilibrium concentration $c_0^{(i)}$ with no free energy of mixing,

$$g^{(i)}(c, T) = \Delta g_{\text{form}}^{(i)}(T) = \Delta H^{(i)} \left(1 - T/T_m^{(i)}\right) + \Theta(c - c_0)^2 \quad (6)$$

where $\Theta = 10^8 \text{ J mol}^{-1}$ is the stability constant.

The sublattice model, as described by Sundman and Ågren,¹⁰⁵ corresponds to

$$g^{(i)}(\{y_j^{(s)}\}, T) = \sum_{j \in (1)} \sum_{k \in (2)} \cdots \sum_{l \in (S)} y_j^{(1)} y_k^{(2)} \cdots y_l^{(S)} \Delta g_{j,k,\dots,l}^{\text{form}}(T) + RT \sum_{s=1}^S \sum_{j \in (s)} n^{(s)} y_j^{(s)} \ln y_j^{(s)} + \sum_{s=1}^S \sum_{j \in (s)} \sum_{k \in (s), j \neq k} y_j^{(s)} y_k^{(s)} \times \left(\sum_{l_m \in (m), m \in \{1, 2, \dots, s-1, s+1, \dots, S\}} y_{l_1}^{(1)} y_{l_2}^{(2)} \cdots y_{l_{s-1}}^{(s-1)} y_{l_{s+1}}^{(s+1)} \cdots y_{l_S}^{(S)} \times L_{l_1, l_2, \dots, l_{s-1}, j, k, l_{s+1}, \dots, l_S}^{(s)}(T) \right), \quad (7)$$

where the s th sublattice of the i th phase corresponds to the $y_j^{(s)}$ site fraction of the j th species found on the s th sublattice, such that $c_j = \sum_{s=1}^S n^{(s)} y_j^{(s)}$. The equilibrium is determined as $g^{(i)}(c, T) = \min_{\{y_j^{(s)}\}} g^{(i)}(\{y_j^{(s)}\}, T)$. For two sublattices, s and r , each with two species, $y_a^{(s)}$ and $y_b^{(s)}$ and $y_c^{(r)}$ and $y_d^{(r)}$, eqn (7) reduces to^{36,106–108}

$$g(y_a^{(s)} y_b^{(s)} y_c^{(r)} y_d^{(r)}, T) = y_a^{(s)} y_c^{(r)} \Delta g_{a,c}^{\text{form}}(T) + y_a^{(s)} y_d^{(r)} \Delta g_{a,d}^{\text{form}}(T) + y_b^{(s)} y_c^{(r)} \Delta g_{b,c}^{\text{form}}(T) + y_b^{(s)} y_d^{(r)} \Delta g_{b,d}^{\text{form}}(T) + RT \left(n^{(s)} y_a^{(s)} \ln y_a^{(s)} + n^{(s)} y_b^{(s)} \ln y_b^{(s)} \right) + RT \left(n^{(r)} y_c^{(r)} \ln y_c^{(r)} + n^{(r)} y_d^{(r)} \ln y_d^{(r)} \right) + y_a^{(s)} y_b^{(s)} \left(y_c^{(r)} L_{a,b,c}^{(s)}(T) + y_d^{(r)} L_{a,b,d}^{(s)}(T) \right) + y_c^{(r)} y_d^{(r)} \left(y_a^{(s)} L_{a,c,d}^{(r)}(T) + y_b^{(s)} L_{b,c,d}^{(r)}(T) \right) \quad (8)$$

The equilibrium voltage, Φ , corresponds to

$$\Phi = -\frac{\mu}{z\mathcal{F}} = -\frac{1}{z\mathcal{F}} \frac{\partial g(\{p^{(i)}\}, c)}{\partial c} \quad (9)$$

where z is the valence, is Faraday's constant, and $\{p^{(i)}\}$ is the set of the phases.

4.2 Material systems

The regular solution model-based PDs were optimized after those reported by Pelton and Thomson.^{36,57,109} The α phase was set as the reference phase. The melting temperatures $T_{m,a} = 800 \text{ K}$ and $T_{m,b} = 1200 \text{ K}$ were read directly from the diagram. Four parameters were found: $\Delta H_a^{(\beta)}$ and $\Delta H_b^{(\beta)}$, with values in the 0 to 15 kJ mol^{−1} range, and mixing parameters Ω_α and Ω_β in the −25 to 35 kJ mol^{−1} range.

The solid phases in the electrolyte systems were modeled as stoichiometric compounds, and the liquid phase as a Redlich-Kister model. The melting temperatures and enthalpies of



transformation for all solid phases were taken directly from literature values.⁶⁵ The liquid phase was set as the reference phase for each material system. L_0 , L_1 , and L_2 were optimized to values in the -20 to 20 kJ mol⁻¹ range.

The LFP system was described as a sublattice model. Lee's SRO model uses four sublattices, one for each element with no mixing between the oxygen and phosphate sublattices. The iron sublattice is populated entirely by Fe²⁺ and Fe³⁺ and interacts with the lithium sublattice containing Li⁺ and vacancies due to a speculated short range ordering effect. In order for Li_xFePO₄ to be electrically neutral for $0 \leq x \leq 1$, $c_{\text{Fe}^{2+}} = c_{\text{Li}^+} = c$. Thus, eqn (7) simplifies to:

$$\begin{aligned} g^{(\text{SRO})}(c, T) = & c^2 \Delta G_{\text{Li}^+ \text{Fe}^{2+}}^{\text{form}}(T) + c(1-c) \Delta G_{\text{Va:Fe}^{2+}}^{\text{form}}(T) \\ & + (1-c)^2 \Delta G_{\text{Va:Fe}^{3+}}^{\text{form}}(T) + c(1-c) \Delta G_{\text{Li}^+ \text{Fe}^{3+}}^{\text{form}}(T) \\ & + 2RT(c \ln(c) + (1-c) \ln(1-c)) \\ & + c(1-c)(cL_{\text{Li}^+, \text{Va:Fe}^{2+}} + (1-c)L_{\text{Li}^+, \text{Va:Fe}^{3+}}) \\ & + c(1-c)(cL_{\text{Li}^+ \text{Fe}^{2+}, \text{Fe}^{3+}} + (1-c)L_{\text{Va:Fe}^{2+}, \text{Fe}^{3+}}) \\ & + c^2(1-c)^2 \sum_{j=0}^n (a_j + b_j T)(2c-1)^j \end{aligned} \quad (10)$$

The last line of eqn (10) includes the interactions between the lithium and iron sublattices in order to account for short range ordering effects. The formation energies were defined as $\Delta G_j^{\text{form}} = \Delta H_j^{\text{form}} - T\Delta S_j^{\text{form}}$.

Eqn (10) was simplified by using the electrically neutral end members as reference phases and by assuming the intra-sublattice energy of mixing to be negligible, in agreement with Lee *et al.*⁴⁹ Four inter-sublattice interaction parameters ($n = 2$ in the last line of eqn (10)) were simultaneously optimized.

Phan and coworkers,⁵⁰ used a five sublattice model (LRO), where the lithium sublattice is split into two, one holding up to 0.6 molar concentration and the other remaining at 0.4 molar concentration in order to account for long range ordering and the eutectoid in the PD. The additional sublattice results in eight end members: $G_{\text{Li}^+ \text{Li}^+ \text{Fe}^{2+}}^{\text{form}}$, $G_{\text{Li}^+ \text{Li}^+ \text{Fe}^{3+}}^{\text{form}}$, $G_{\text{Li}^+ \text{Va:Fe}^{2+}}^{\text{form}}$, $G_{\text{Li}^+ \text{Va:Fe}^{3+}}^{\text{form}}$, $G_{\text{Va:Li}^+ \text{Fe}^{2+}}^{\text{form}}$, $G_{\text{Va:Li}^+ \text{Fe}^{3+}}^{\text{form}}$, $G_{\text{Va:Va:Fe}^{2+}}^{\text{form}}$, and $G_{\text{Va:Va:Fe}^{3+}}^{\text{form}}$ that are simplified using the compound energy formalism,¹¹⁰ into four temperature-independent adjustable parameters: $\Delta G_{\text{FePO}_4^-}^{\text{form}}$, $\Delta G_{\text{LiFePO}_4^+}^{\text{form}}$, $\Delta G_{\text{adjust}_1}^{\text{form}}$, $\Delta G_{\text{adjust}_2}^{\text{form}}$, which correspond to the excess formation energy of non-neutral end members. In addition, $g_{\text{mix, xs}}^{(\text{LRO})}(c, T) = 0$. The ML-method converges in less than one hour.

The T-LRO model proposed in this paper extends Phan's LRO model to include entropic effects by introducing temperature dependence to $\Delta G_{\text{FePO}_4^-}^{\text{form}} = \Delta H_{\text{FePO}_4^-}^{\text{form}} - T\Delta S_{\text{FePO}_4^-}^{\text{form}}$ and $\Delta G_{\text{LiFePO}_4^+}^{\text{form}} = \Delta H_{\text{LiFePO}_4^+}^{\text{form}} - T\Delta S_{\text{LiFePO}_4^+}^{\text{form}}$. In total, the six adjustable parameters were optimized in 17 h. Implementation details are included in the ESI.†

The voltage reported in the rightmost column of Fig. 3 was taken directly from the original paper and was not optimized.

For the LCO system, the cobalt oxide phase (O1) was modeled as a stoichiometric compound, the lithium cobalt oxide phase (O3) as a temperature-dependent Redlich–Kister, and the half cobalt oxide, half lithium cobalt oxide phase (H13) as a sublattice model.⁴⁴ Similar to the LRO model in LFP, the H13 phase has a sublattice for cobalt, a sublattice for oxygen, and two sublattices for lithium. While the cobalt sublattice is populated with two species, Co³⁺ and Co⁴⁺, the energetic effect is assumed to be negligible. Each lithium sublattice is capable of holding half of the ions, with one sublattice completely filled before the other. Thus, in the range where H13 is stable, eqn (7) simplifies to

$$\begin{aligned} g^{(\text{H13})}([y_{\text{Li}^+}], [y_{\text{Va}}], T) = & \Delta G_{\text{CoO}_3}^{(\text{H13})}[y_{\text{Va}}] + \Delta G_{\text{LiCoO}_3}^{(\text{H13})}[y_{\text{Li}^+}] \\ & + RT([y_{\text{Li}^+}] \ln([y_{\text{Li}^+}]) + [y_{\text{Va}}] \ln([y_{\text{Va}}])) \\ & + [y_{\text{Li}^+}][y_{\text{Va}}] \sum_{j=0}^{L=2} L_j^{(\text{H13})}(T)([y_{\text{Li}^+}] - [y_{\text{Va}}])^j \end{aligned} \quad (11)$$

Since the sublattice only contains half of the possible sites for lithium, $[y_{\text{Li}^+}] = 2c$ and $[y_{\text{Va}}] = 1 - [y_{\text{Li}^+}] = 1 - 2c$.

The voltage profile reported by Chang *et al.*⁴⁵ was included in the ML method to optimize both the predicted PD and associated voltage profile, to agree with all available experimental evidence and better represent the physics of the system. The effect of the electrochemical potential was included by minimizing the error between the predicted and experimental electrochemical potential.⁶⁸

4.3 Machine learning architecture

The prediction of the material parameters was performed by developing a custom two-step explore-exploit machine learning strategy, based on the knn algorithm.^{54,55} In the first step, a dataset of PDs is generated in *gibbs.ML* by uniformly sampling the sought Gibbs free energy parameters, five sampling points for every parameter, which defines a uniform mesh in PD parameter space that embodies a dataset of almost ten million PDs for a ten-parameter model. The PDs in the generated dataset are compared against the target PD, so that the k -closest PDs are kept. k was set to 0.1% of the size of the dataset.

The second step uses a stochastic optimization with at least ten iterations on the result from the first step. Here, for each central cell location in the generated uniform mesh in parameter space, a PD was generated by randomly sampling material parameters from a multivariate normal distribution, where the mean of the distribution corresponds to the center of the sampled cell and the standard deviation corresponds to one fourth of the width of the mesh spacing. 1024 proposed solutions are tested, and the top 100 were kept for the next iteration. These 100 PDs become sampling points for the ten iteration steps of optimization. After the final iteration, all seed points were examined and only the PD



closest to the target and its corresponding material parameters is reported.§

The target and the sampled PDs were evaluated by using a distance metric, \mathcal{L} , i.e., a loss function, independent of the utilized free energy model,

$$\mathcal{L} = \sqrt[n]{\sum_{i \in \text{PD}_t} w_i \min_{j \in \text{PD}_p} \left(\frac{|c_i - c_j|}{\Delta c} + \frac{|T_i - T_j|}{\Delta T} \right)^n} + \sqrt[n]{\sum_{i \in \text{PD}_p} \min_{j \in \text{PD}_t} \left(\frac{|c_i - c_j|}{\Delta c} + \frac{|T_i - T_j|}{\Delta T} \right)^n} + \sigma_{\text{property}} \quad (12)$$

where PD_k corresponds to the set of all the normalized phase boundary concentration–temperature pairs, (c_i, T_i) , in the k th PD. The subscript p denotes the proposed or sampled PD from the dataset, whereas t denotes the target PD. $\Delta T = T_{\text{max}} - T_{\text{min}}$ corresponds to the temperature range of PD, and $\Delta c = c_{\text{max}} - c_{\text{min}}$ to the analyzed composition range. $n = 8$ was set to emphasize the difference between diagrams by weighting outliers higher. The first term in eqn (12) corresponds to the distance from every point in the target PD to the nearest point in the sampled PD, and the second term corresponds to the distance from every point in the sampled PD to the nearest point in the target PD. σ_{property} denotes an additional constraint, experimental or theoretical, that can be used to further optimize the description of the sought parameters. The contribution of the phase boundaries of the sampled PD was also weighted relative to the physical constraint imposed by σ_{property} . For example, the LCO system was optimized by comparing the root mean squared error between the predicted and target voltage profiles at the experimental room temperature.

4.4 Numerical implementation and data generation

The machine learning architecture and the free energy models presented herein were numerically implemented in the python-based open-source framework, *gibbs*,¹⁰ which uses symbolic computation to allow for rapid model development of material systems. The developed *gibbs* and *gibbs.ML* libraries use a combination of fixed and adjustable model parameters over a user-specified range of physically possible values. For the sublattice models, the physical constraint was solved by the Newton–Raphson method.

The equilibrium of each physical system was solved by using a parallelized implementation of the common tangent construction by determining the intersection of the proposed common tangent to the overall convex hull. The phase boundaries and invariant reactions were identified. *gibbs.ML* was

implemented in python 3.6.9, c++ 2017, g++ version 7.5, cuda 10.1, swig 3.0.12, and numpy 1.18.1. All calculations were run on a single Nvidia RTX 2080 Ti GPU. *gibbs.ML* constructed PDs with a resolution of 128×512 , and downsampled to a 64×64 grayscale images.

Conflicts of interest

There are no conflicts of interest to declare.

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§ While other search methodologies such as gradient descent,¹¹¹ directed random walks,^{112–114} regression,^{115,116} kernel methods,^{117,118} neural networks,¹¹⁹ exist, the proposed knn strategy defines a generalized approach that is independent of the number of phases, the selected free energy model, topology of the PD. It provides the researcher with an easy-to-use and ever extendable approach, enabling the user to focus on the physics or design at hand instead of the numerical aspects. Further, because the proposed knn search strategy samples 0.1% of volume of the space of parameters where the solution is being sought, and the search is enhanced with random sampling in the vicinity of the solution during postprocessing, the k value has no significant impact on the obtained results.



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