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PAPER

# Nonlinear microrheology of an aging, yield stress fluid using magnetic tweezers

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The large deformation mechanical response of complex fluids and soft materials provides fundamental insight into their underlying microstructure and dynamics. Additionally, associated yielding and flow processes are often central to industrial processing and end-use. By probing nonlinear rheological properties at the microscopic scale, microstructural dynamics and flow mechanisms can be more directly elucidated. In the current work, we present a simple magnetic tweezer technique for probing the nonlinear microrheology of complex fluids and soft materials. The setup is characterized in terms of the accessible stresses, the applied magnetic fields, and the measurable viscosities and shear rates. Further, we report the first use of magnetic tweezers to determine yield stresses at the microscopic scale, as well as the first comparison between bulk and micro-scale yield stress measurements. The capabilities of the technique are demonstrated on an aqueous dispersion of Laponite<sup>®</sup>: an aging, thixotropic colloidal clay of considerable scientific and practical interest. Probe trajectories in this material reflect the yield stress and strong shear-thinning behaviour observed on the bulk scale, and for sufficient clay concentrations we find good agreement for the shear yield stress obtained from bulk rheology and magnetic tweezer measurements. These unforeseeable observations illuminate the nature of the dispersion microstructure, including the characteristic size of microstructural features.

## 1 Introduction

Microrheology has become an important tool for understanding and characterizing soft materials.<sup>1</sup> The field encompasses various methods in which rheological properties are extracted from the motions of embedded microscopic probe particles.<sup>2</sup> It is especially suited for situations where bulk rheometry is not feasible, such as for rare materials or *in vivo* studies of biological fluids,<sup>3</sup> and can provide insight into materials with complex microstructure, which may exhibit different rheological behaviour at bulk and microscopic length scales.<sup>4,5</sup> Techniques for probing both linear (small deformation and deformation rate) and nonlinear (large deformation and/or deformation rate) microrheology have been developed, with the nonlinear case necessarily involving active techniques in which external forces are applied to probes.<sup>2,4,6</sup> While linear microrheology has received the most attention, nonlinear microrheology plays a key role in the flow properties of numerous important microstructured

materials, such as colloidal glasses,<sup>7</sup> electrorheological and magnetorheological fluids,<sup>8</sup> and polymer-colloid mixtures.<sup>9</sup> The bulk response and proper function of these materials is highly dependent on shear-thinning and yield stress phenomena at microscopic length scales. For example, in magnetorheological suspensions, microscopic iron-containing particles are often dispersed in viscoplastic carrier fluids, whose rheological properties prevent particle sedimentation and influence field-responsive self-assembly.<sup>10</sup>

Because of its significance in understanding the properties of structured fluids, recent work in the field has begun to investigate nonlinear microrheology for several canonical materials, and has explored relationships with bulk properties. A number of studies have examined the micro-scale viscosity of colloidal dispersions,<sup>11–14</sup> the nature of forced microstructural rearrangements and shear melting near the colloidal glass transition,<sup>7</sup> and an active microrheological method for measuring normal stress coefficients.<sup>15</sup> Additionally, yield stress measurements at the microscopic length scale were first reported by Wilking and Mason, who examined gelatin solutions using optical tweezers that were modified to exert torques on an embedded microdisk.<sup>16</sup>

In the current work, we present a magnetic tweezer technique for measuring nonlinear microrheological properties of complex fluids. The motion of embedded magnetic microparticles has been used for many years to probe such phenomena as the mechanical properties of cell protoplasm,<sup>17</sup> the elasticity of gels,<sup>18</sup> the stretching behaviour of macromolecules,<sup>19</sup> and the

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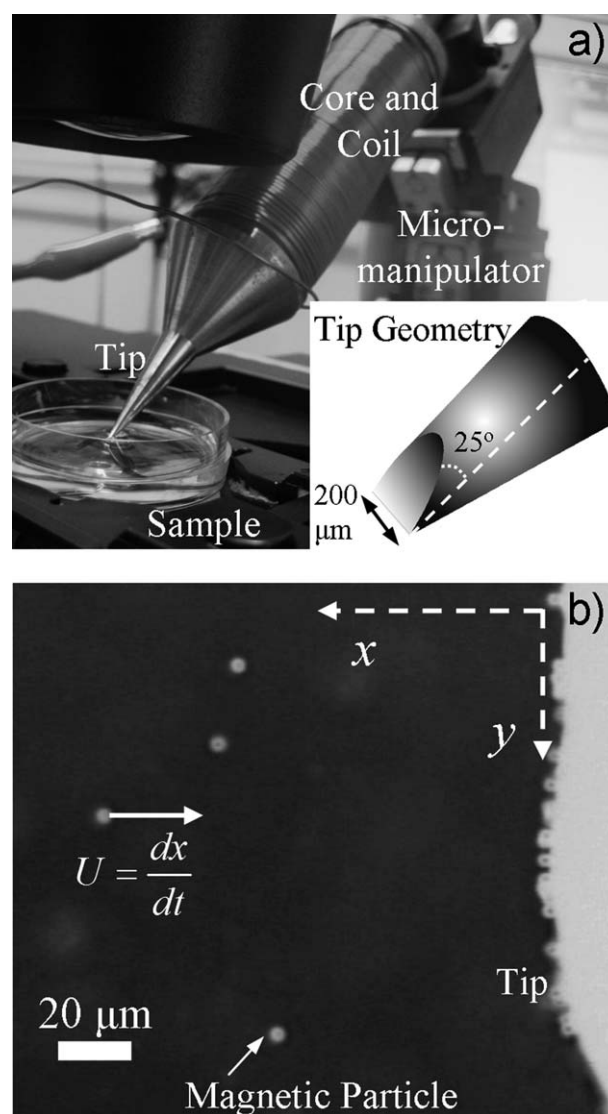
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mechano-transduction of cells.<sup>20</sup> Here we employ the single-pole design from Lammerding,<sup>21</sup> which can apply forces on the order of 10 nN on 4.5  $\mu\text{m}$  superparamagnetic particles. The dynamic range of the instrument is characterized and probe trajectories are analyzed to extract effective viscosity measurements. Additionally, we report the first use of magnetic tweezers to determine yield stresses at the microscopic scale, affording advantages to optical tweezer techniques because of simpler design and implementation. The technique is demonstrated on a typical thixotropic, aging, yield stress material,<sup>22</sup> an aqueous dispersion of the synthetic clay Laponite<sup>®</sup>.<sup>23</sup> Often used as a rheological modifier in commercial soft materials, Laponite<sup>®</sup> clay consists of nanometric disks that undergo progressive structural arrest over time when dispersed in water at concentrations as low as about 1 wt%.<sup>24–27</sup> The microstructural development results in complex and time-dependent rheology.<sup>28–32</sup> Previous work has addressed the bulk rheology and linear microrheology of aqueous Laponite<sup>®</sup> dispersions; for more thorough reviews of the current understanding of the phase behaviour, structure, and rheology, see Ruzicka *et al.*<sup>33</sup> and Rich *et al.*<sup>34</sup> We note that while the local nonlinear rheology of aqueous Laponite<sup>®</sup> dispersions has also been studied,<sup>35</sup> only probes with sizes on the order of 1 mm were used. The current work therefore presents the first truly micro-scale nonlinear rheological study of this material, as well as the first comparison to bulk nonlinear properties. We observe that the effective viscosity is strongly shear-thinning, obeying similar power-law behaviour at both the bulk and microscopic scales. Additionally, the yield stress grows approximately logarithmically with age time, exhibiting quantitative agreement between bulk and microscopic scales for concentrations  $\geq 2$  wt%.

## 2 Experimental

The magnetic tweezer device used in the present work was designed and described by Lammerding.<sup>21</sup> A rod of high magnetic permeability iron (CMI-C, CMI Specialty Products, Bristol, CT) is machined to a sharp tip of width  $\approx 200$   $\mu\text{m}$ , as shown in Fig. 1, and subsequently annealed according to the manufacturer's specifications. The highly pointed geometry results in large magnetic field gradients, leading to relatively large forces on magnetic probe particles.<sup>36,37</sup> The core metal is wrapped with about 300 turns of AWG 19 copper magnet wire over a length of 7.2 cm, leading to a wire turn density  $n$  of about  $n \approx 4200$   $\text{m}^{-1}$ . The assembly is then mounted on a manual micromanipulator (MX110, Siskiyou, Grants Pass, OR) alongside an inverted microscope (Axiovert 40 CFL, Carl Zeiss AG, Oberkochen, Germany) and the wires are connected to a DC power supply (GPS-2303, GWInstek, Taipei, Taiwan). Experiments are conducted at room temperature,  $T \approx 22.5$   $^{\circ}\text{C}$ . For a current of 1.5 A, the temperature of the tip does not rise more than about 1  $^{\circ}\text{C}$  over the time scale of a measurement ( $\sim 1$  min).<sup>21</sup> We therefore consider electrical resistance heating of the tip to be negligible. Gaussmeter measurements at the back of the core indicate that the magnetic field stabilizes within 1 s of applying a current.

Laponite RD<sup>®</sup> powder was obtained from Rockwood Additives. To prepare the clay dispersion, dry Laponite<sup>®</sup> powder is added to an aqueous buffer of pH  $\approx 10$  consisting of 1.8 mM NaOH and 4.1 mM  $\text{NaHCO}_3$ . The purpose of the buffer is to



**Fig. 1** The magnetic tweezer setup used for nonlinear microrheology experiments. (a) The magnetic tweezer device is mounted on a micromanipulator adjacent to the stage of an inverted microscope. The iron core is machined to a sharp tip, which is dipped directly into the fluid of interest. The flattened tip design, which is shown in detail in the inset, leads to locally horizontal forces when the device is held at an angle of  $45^{\circ}$  to the horizontal.<sup>21</sup> (b) Microscope view frame of the magnetic tweezer experiment. The point of the tip is flattened to a width of about 200  $\mu\text{m}$ , providing an approximately unidirectional magnetic force in the vicinity of the tip. Upon magnetization of the core, superparamagnetic probe particles (diameter  $d = 4.5$   $\mu\text{m}$ ) move towards the tip with a velocity  $U$ . The distance from a probe to the surface is given by  $x$ , while  $y$  defines the distance along the surface of the tweezer device.

maintain the dispersion pH and fix the solvent ionic strength at 5.9 mM. The dispersion is mixed vigorously for at least 1.5 h and subsequently passed through a 0.8  $\mu\text{m}$  filter, breaking apart most of the remaining aggregates with a strong shear.<sup>38</sup> This filtration marks the reference point for subsequent aging studies, in accordance with previous work on Laponite<sup>®</sup> dispersions,<sup>39</sup> and structuring of the clay progressively increases as the system ages. Petit *et al.*<sup>40</sup> demonstrated that about 7% of the initial Laponite<sup>®</sup>

concentration is lost when dispersions of about 3 wt% Laponite<sup>®</sup> are passed through 0.45  $\mu\text{m}$  filters. However, since the present study uses filters with larger pores (0.8  $\mu\text{m}$ ), it is assumed that filtration does not change the nominal concentration of Laponite<sup>®</sup>.

Immediately following filtration, superparamagnetic micro-particles of diameter  $d = 4.5 \mu\text{m}$  (M-450 Dynabeads, Invitrogen Life Technologies, Carlsbad, CA) are added at a concentration of about  $\phi \approx 0.4 \text{ vol}\%$ . The magnetic particle concentration is chosen to achieve a large number of measurable particle trajectories with approximately non-interacting particles. After vortex mixing for about 15 s, the magnetic particles are randomly dispersed in the sample. The additional rejuvenation of the sample due to vortex mixing is minimal since it is conducted immediately after filtering. A small petri dish is filled with the dispersion and placed on the microscope stage for visualization with a  $20\times$  objective (N.A. = 0.5). By adjusting the micromanipulator, the tip of the magnetic tweezer device is dipped directly into the dispersion and brought arbitrarily close to magnetic probe particles, maximizing the accessible forces on probes.<sup>36</sup> The tip is machined such that approximately horizontal magnetic fields are locally obtained when the device is positioned at a  $45^\circ$  angle to the horizontal, as pictured in Fig. 1a. The directionality of the force is confirmed by checking that particles remain in focus as they move towards the tip.

Movies of probe particle dynamics are captured with a CCD camera (KP-M1A, Hitachi, Tokyo, Japan) having a variable shutter speed between 1/60 s and 1/10 000 s set to frame integration mode. Scion Image software is used to record movies at a rate of 30 frames  $\text{s}^{-1}$ . Each video frame consists of two interlaced fields (the odd or even rows of the CCD matrix) that are exposed 1/60 s apart, requiring each frame to be de-interlaced during the movie analysis. The interlacing also results in a loss of spatial resolution in the direction perpendicular to the interlacing;<sup>41</sup> thus, particle displacements in this study are only examined in the horizontal direction (the  $x$ -direction), which is the predominant direction of motion. Movies are analyzed to obtain particle trajectories using publicly available software developed by Crocker and Grier.<sup>41</sup> Any particles that chain or cluster together are neglected in the analysis.

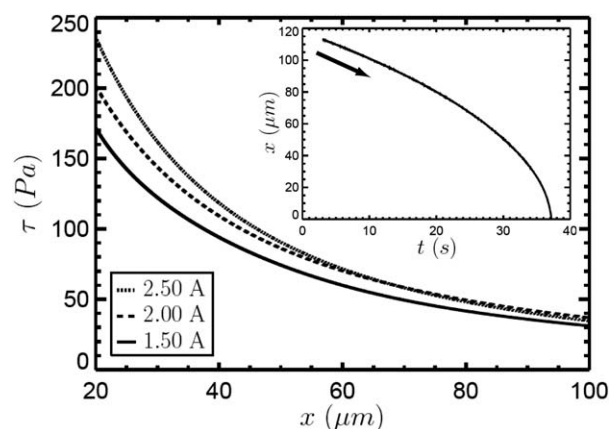
Bulk rheology measurements are made using a stress-controlled rheometer (ARG-2, TA Instruments, New Castle, DE) with a 40 mm diameter aluminium plate geometry and a 0.5 mm gap. Adhesive-backed 600 grit sandpaper (McMaster-Carr, Elmhurst, IL, RMS roughness  $\approx 6.0 \mu\text{m}$ ), is attached to each surface to minimize wall-slip. The Laponite<sup>®</sup> dispersion is prepared in the same way as in the microrheology experiments, and is introduced between the plates immediately after filtering, which is again marked as the time of zero age,  $t_w = 0$ . To help ensure a reproducible initial condition, the sample is then pre-sheared at a shear rate of  $\dot{\gamma} = 250 \text{ s}^{-1}$  for 30 s. Though the pre-shear may keep aggregates from forming and partially rejuvenate the fluid,<sup>42</sup> we find this additional rejuvenating effect to be negligible when the pre-shear is performed immediately subsequent to the filtration step. After the dispersion is allowed to age at a constant temperature  $T = 22.5^\circ\text{C}$ , continuous ramp tests are

performed to explore the yielding and shear-thinning behaviour. Starting from a value below the static yield stress, the applied shear stress is increased continuously until the dispersion has yielded, allowing the extraction of the flow curve and viscosity behaviour during yielding. The stress is ramped linearly at a rate of about  $1 \text{ Pa s}^{-1}$  over a time of 2 min, which is small compared to the age of the dispersion. We note that this protocol estimates the *static* yield stress, which is the stress required to induce flow from rest, in contrast to the *dynamic* yield stress, which is estimated by decreasing the shear rate and extrapolating the resulting shear stresses to  $\dot{\gamma} = 0 \text{ s}^{-1}$ .<sup>43</sup>

### 3 Results and discussion

#### 3.1 Calibration of magnetic tweezers

The force and the stress applied by the magnetic tweezer device on probe particles are calibrated by tracking particle motion in Trimethylsiloxy-terminated Polydimethylsiloxane (DMS-T43, Gelest, Morrisville, PA), a Newtonian liquid with kinematic viscosity  $\nu = 30,000 \text{ cSt}$  (dynamic viscosity  $\eta = 29.5 \text{ Pa s}$ ). The reported viscosity was confirmed using bulk rheology measurements. The stress applied by the tweezer device is a function of both the distance from the tip surface,  $x$ , and the current in the copper wire,  $I$ . About 30 particle trajectories  $x_i(t)$  are obtained at a given current and an average trajectory is calculated by applying a least-squares fit. The most suitable fit for the calibration experiments is provided by functions of the form  $t_{s,i} - t = P_m(x)$ , where  $t_{s,i}$  is the time at which the  $i^{\text{th}}$  particle reaches the tip and  $P_m$  is a polynomial of order  $m$  ( $m = 3-6$ ). By taking a time derivative of the fit, an expression for the average particle velocity,  $U(x)$ , is obtained, allowing calculation of the shear rate  $\dot{\gamma}(x) = 3|U(x)|/2a$  and the stress  $\tau(x) = \eta\dot{\gamma}(x) = 3\eta|U(x)|/2a$ , where  $a$  is the probe radius. The

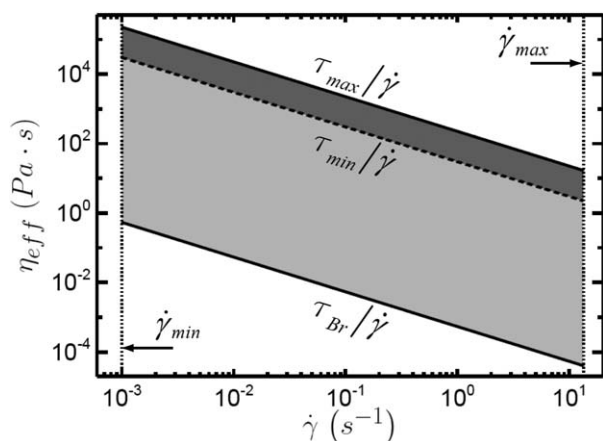


**Fig. 2** Calibration curves for the stress applied by the magnetic tweezers as a function of the distance from the tip. Results for  $I = 1.50 \text{ A}$ ,  $2.00 \text{ A}$ , and  $2.50 \text{ A}$  are shown. The stress increases as the tip is approached and stresses up to about 230 Pa are accessible close to the tip. For  $x < 20 \mu\text{m}$ , the computed stress values are highly sensitive to the order of the polynomial fit to trajectory data. The stress exhibits only weak dependence on current, suggesting that either the core or the probe particles are approaching magnetic saturation. The inset shows a typical probe trajectory in the Newtonian calibration fluid, which has a kinematic viscosity of  $\nu = 30\,000 \text{ cSt}$  ( $\eta = 29.5 \text{ Pa s}$ ).

† <http://www.physics.emory.edu/~weeks/idl/>, "Particle Tracking Using IDL", site maintained by Eric Weeks

resulting stress calibration curves for three different values of the current are plotted in Fig. 2. Here it is seen that the instrument can impose stresses on probe particles up to about 230 Pa, which provides an upper limit for measurable yield stress values. Additionally, the stress depends only weakly on  $I$  over the range explored in the present work, increasing by 10–27% (depending on  $x$ ) from  $I = 1.50$  A to  $I = 2.50$  A. The inset of Fig. 2 shows a typical probe trajectory in the Newtonian calibration fluid at a current of 2.00 A. A smooth acceleration towards the surface is observed, with  $d^2x/dt^2 < 0$  for all  $x$ , as a result of the constant viscosity and the continually increasing stress on the particle. The magnetic tweezer technique therefore provides a micro-scale analogy to the bulk continuous stress ramp described in the previous section. In Section 3.2.1, we contrast the shape of this trajectory with that in the non-Newtonian case, where effects of shear-thinning behaviour become apparent.

By combining the stress calibration with the limitations of the optical and particle-tracking setup, we construct an operating diagram of the accessible shear rates and viscosities that can be measured by the magnetic tweezer technique. This diagram is shown in Fig. 3, in which the range of accessible shear rates is bounded by the dotted lines. Assuming thermal forces are negligible compared to magnetic forces, the lower bound  $\dot{\gamma}_{min}$  is given by the spatial resolution (here about 90 nm, as determined from the apparent displacement of immobilized particles at 20 $\times$  magnification<sup>44</sup>) divided by the duration of the experiment, which in the present work is 1 min. The upper bound  $\dot{\gamma}_{max} = 3|U_{max}|/2a$  is limited by the maximum frame rate of the camera



**Fig. 3** Operating diagram for the magnetic tweezer setup showing the range of accessible shear rates and viscosities. The maximum shear rate  $\dot{\gamma}_{max} = 3|U_{max}|/2a$  is limited primarily by the frame rate of the camera (30 frames  $s^{-1}$  or 60 interlaced fields  $s^{-1}$ ), which enables particles with diameter  $2a = 4.5$   $\mu m$  to be tracked at velocities up to about  $|U_{max}| \approx 20$   $\mu m s^{-1}$  under 20 $\times$  magnification. The minimum shear rate  $\dot{\gamma}_{min}$  is given by dividing the spatial resolution (here about 90 nm) by the time over which the magnetic field is applied (here 1 min). The stress calibration in Fig. 2 allows calculation of the corresponding accessible viscosities. The dynamic range demonstrated in the present work is given by the dark shaded region, with  $\tau_{max} = 225$  Pa and  $\tau_{min} = 30$  Pa, while the lighter region is accessible at lower currents than used here. Eventually, Brownian stresses become significant, providing an ultimate lower limit to the measurable viscosities. Here this limit is calculated using the characteristic Brownian stress  $\tau_{Br} = k_B T/a^3$  at  $T = 22.5$   $^{\circ}C$  on a particle with radius  $a = 2.25$   $\mu m$ .

(30 frames  $s^{-1}$ , or 60 interlaced fields  $s^{-1}$ ), which allows particles to be accurately tracked at velocities up to about  $|U_{max}| \approx 20$   $\mu m s^{-1}$  under 20 $\times$  magnification. This highlights a potential modification that could extend the dynamic range of future realizations of the technique through the use of a high-speed camera. The range of measurable viscosities is given by the stress calibration in Fig. 2, using the relation  $\eta(\dot{\gamma}) = \tau/\dot{\gamma}$ . The dark gray area shows the dynamic range demonstrated in the present work, while the lighter region, which corresponds to smaller shear stresses, is accessible at lower currents than used here. At very low currents, the applied stress becomes comparable to the characteristic Brownian stress  $\tau_{Br} = k_B T/a^3$ . In this limit, particle diffusion out of the area of focus generally makes continual tracking of particle trajectories impossible, so that  $\tau_{Br}/\dot{\gamma}$  corresponds to an ultimate lower limit to the measurable viscosities.

Further insight into the capabilities of the technique can be gained by considering the magnetic field applied by the tweezers and the resulting magnetization of the probe particles. While it is difficult to accurately measure the magnetic field,  $B$ , at distances of 10–100  $\mu m$  away from the tip, it can be estimated by combining the calibration data with a suitable model for the particle magnetization,  $M$ . We use the Fröhlich–Kennelly equation:<sup>45</sup>

$$M(H) = H \left( \frac{1}{\chi_0} + \frac{H}{M_{sat}} \right)^{-1} \quad (1)$$

Here  $\chi_0 = 1.6$  is the linear magnetic susceptibility and  $M_{sat} = 30$  kA  $m^{-1} = 19$  emu  $g^{-1}$  is the saturation magnetization of the particles, both provided by the manufacturer.  $H$  is the magnetizing field. To proceed with analysis, a more manageable functional form for the average trajectory is required. In place of the polynomial form mentioned above, we take a simpler power law form:  $x = A(t_{s,i} - t)^\alpha$ . For  $I = 1.5$  A, least-squares fitting gives  $A = 23.1$   $\mu m$  and  $\alpha = 0.43$ . The particle velocity is then

$$U(x) = -\frac{dx}{d(t_{s,i} - t)} = -A\alpha(t_{s,i} - t)^{\alpha-1} = -A^{1-\alpha} \alpha x^{(\alpha-1)/\alpha} \quad (2)$$

where the final equality is in terms of the distance from the tip,  $x$ . The drag force is then calculated from Stokes' Law for steady viscous drag on a sphere

$$F_{drag}(x) = -6\pi\eta a U(x) = 6\pi\eta a A^{\alpha-1} \alpha x^{(\alpha-1)/\alpha} \quad (3)$$

and the magnetic force is

$$F_{mag}(x) = \mu_0 V M \frac{dH}{dx} = \mu_0 V H \left( \frac{1}{\chi_0} + \frac{H}{M_{sat}} \right)^{-1} \frac{dH}{dx} \quad (4)$$

where  $\mu_0$  is the magnetic permeability of free space and  $V$  is the particle volume. By summing the drag force and the magnetic force and assuming inertial acceleration is negligible, we obtain a differential equation that can be solved for the magnetizing field  $H$  as a function of  $x$ .

$$\mu_0 V H \left( \frac{1}{\chi_0} + \frac{H}{M_{sat}} \right)^{-1} \frac{dH}{dx} = -6\pi\eta a A^{1-\alpha} \alpha x^{(\alpha-1)/\alpha} \quad (5)$$

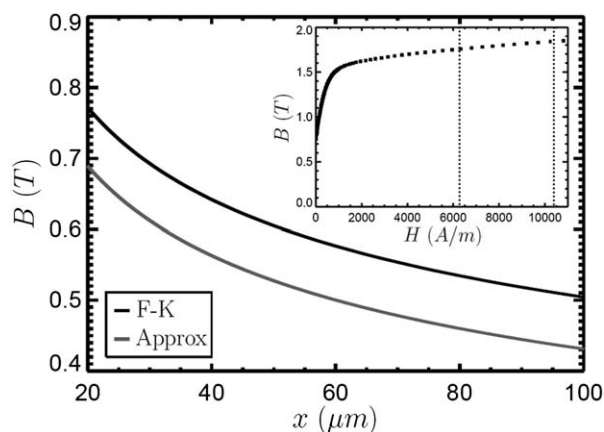
Using the condition that  $H \rightarrow 0$  as  $x \rightarrow \infty$ , eqn (5) can be integrated to obtain an expression that is explicit in  $x$  but implicit in  $H$ .

$$x = \left( \frac{M_{sat}^2 \mu_0 V \left( 2 - \frac{1}{\alpha} \right)}{6\pi\eta a A^{1/\alpha} \alpha} \right)^{\frac{\alpha}{2\alpha-1}} \left[ \frac{1}{\chi_0} \ln \left( 1 + \frac{\chi_0 H}{M_{sat}} \right) - \frac{H}{M_{sat}} \right]^{\frac{\alpha}{2\alpha-1}} \quad (6)$$

This expression is plotted in Fig. 4 (black line) in terms of the magnetic field  $B(x) = \mu_0 H(x)$  for  $I = 1.50$  A. Within  $100 \mu\text{m}$  of the tip, the magnetic field acting on magnetizable probe particles is of the order  $\sim 1$  T, which is consistent with the magnetization properties of the CMI-C core metal shown in the inset. The magnetic field decays with increasing distance from the tip, dropping by about 35% over a distance from  $x = 20 \mu\text{m}$  to  $x = 100 \mu\text{m}$ . This field gradient leads to a magnetic force on the probe particles according to eqn (4). The resulting probe particle magnetization values, calculated from eqn (1), are 28.6–29.1  $\text{kA m}^{-1}$ , so that  $M \approx M_{sat} = 30 \text{ kA m}^{-1}$ . This near-saturation provides an explanation for the marginal difference between stress calibration curves at different currents shown in Fig. 2. If  $M \rightarrow M_{sat}$ , the particle force balance results in a simpler relation between  $H$  and  $x$ .

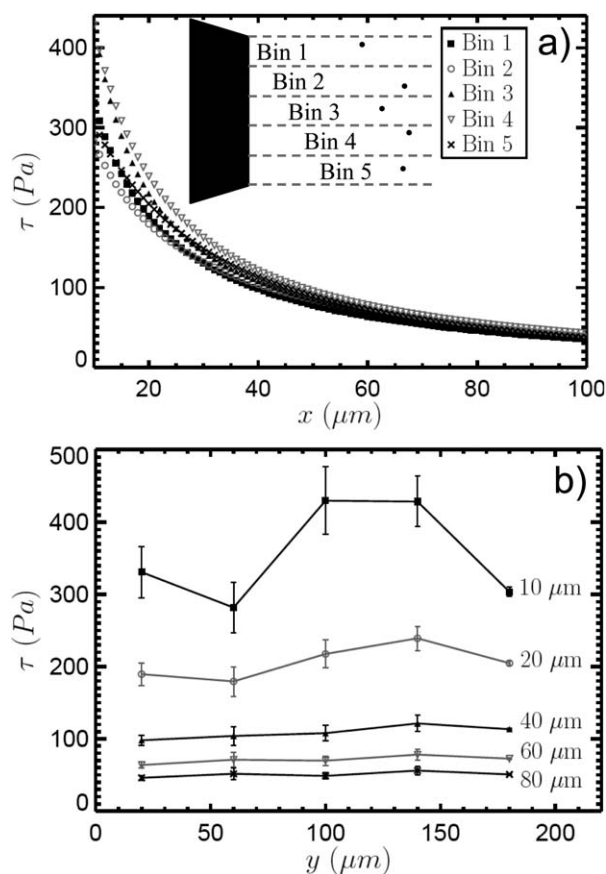
$$H = \frac{6\pi\eta\alpha^2 A^{1/\alpha}}{\mu_0 V M_{sat} (1 - 2\alpha)} x^{2-1/\alpha} \quad (7)$$

Eqn (7) is shown by the gray line in Fig. 4. Though this expression provides physical insight, Fig. 4 shows that it is not as suitable for quantitative analysis since it underestimates the field by about 15–20% compared to eqn (6). These calculations imply that larger stresses could be achieved by using probe particles with a higher saturation magnetization.



**Fig. 4** Calculation of the magnetic field as a function of distance from the tip at a current of  $I = 1.50$  A. The black line presents the result obtained from eqn (6), which uses the Fröhlich–Kennelly relation in eqn (1) to model the particle magnetization. The strength of the field is attributed to the magnetization properties of the CMI-C core metal, shown in the inset with data provided by the manufacturer. The dotted lines bound the range of  $H$  values in our experiment, where  $H = nI$  and  $n \approx 4200 \text{ m}^{-1}$  is the wire turn density of the coil. As a result of the field strengths on the order  $\sim 1$  T, the magnetization of probe particles is calculated from eqn (1) to be 28.6–29.1  $\text{kA m}^{-1}$ , which is very close to saturation. The gray line shows the calculation of the field using the approximation of probe particle saturation  $M = M_{sat}$  from eqn (7). The result is about 15–20% lower than the values obtained using the Fröhlich–Kennelly relation, though the trend is the same.

A final important consideration is the variation in the applied stress across the lateral plane of the tip (see Fig. 1b). Roughness and edge effects on the microscopic scale could lead to significant deviations at different values of  $y$ , especially when the probes are very close to the tip at small values of  $x$ . Because the coefficient of variation for the probe size is less than 5% (manufacturer information), and it has been claimed that deviations in magnetic properties are largely due to size polydispersity,<sup>46</sup> these irregularities in tip geometry are expected to be the primary source of variations in the applied stress. To explore this effect, probe particles are binned according to their position along the  $y$ -axis, as shown in the inset in Fig. 5a. For each bin  $j$ , an average trajectory is obtained by applying a least-squares fit to a polynomial as described above, allowing calculation of an average velocity function  $U_j(x)$  and a shear stress-distance calibration curve,  $\tau_j(x) = \eta \dot{\gamma}(x) = \eta |U_j(x)|/a$ . At least 5 individual trajectories are averaged per bin. The calibration curves for  $I = 2.00$  A are shown in Fig. 5a, and we find that the variation across the



**Fig. 5** Lateral variation in the applied stress across the surface of the tweezer device. (a) Stress calibration data is plotted at  $I = 2.00$  A with particle trajectories partitioned into five bins according to their positions along the  $y$ -axis, as shown in the inset. Though the applied stress becomes approximately uniform far from the tip, local variations in the tip geometry lead to deviations in the stress as the tip is approached. This is clarified in (b), where the applied stress is re-plotted as a function of  $y$  at five distances from the tip. Error bars represent the standard error between individual trajectories. In order to neglect non-uniformities in the stress across the surface, we limit our analysis to distances beyond  $x = 20 \mu\text{m}$ , where the coefficient of variation is less than 10%.

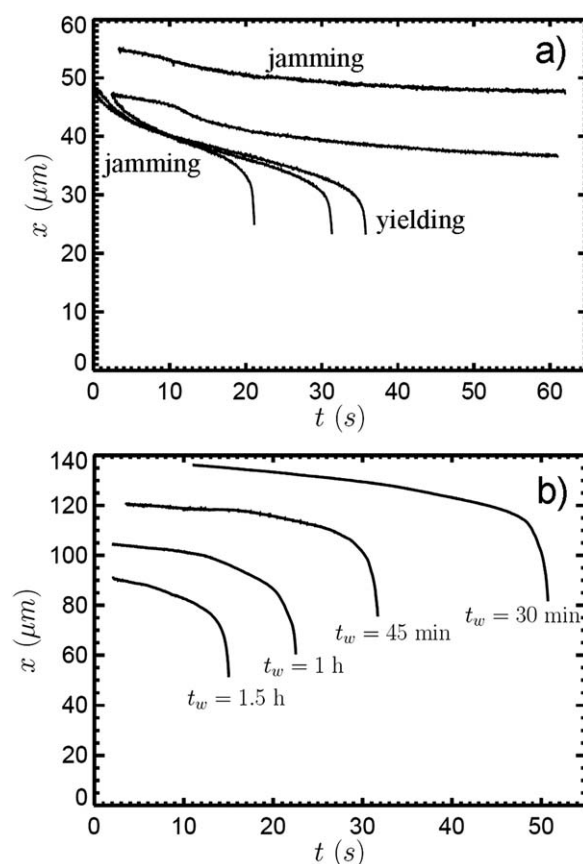
lateral plane of the tip becomes increasingly significant at closer distances. This is also seen in Fig. 5b, where the applied stress is plotted as a function of  $y$  at various values of  $x$ . Beyond a distance of  $x \approx 40 \mu\text{m}$ , the applied shear stress is essentially constant across the tip. In particular, the coefficient of variation at  $x = 20 \mu\text{m}$  is about 10%, and so we limit our quantitative experiments to distances beyond this value. This calibration indicates that improvements on this technique could be achieved by decreasing the variation across the tip through more precise micro-machining. This would increase the upper bound of practically accessible stresses while maintaining the experimental error within reasonable limits.

### 3.2 Nonlinear microrheology of an aging colloidal clay

Having discussed the instrument calibration and associated considerations, we now apply this magnetic tweezer device to the examination of the nonlinear microrheology of an aging, thixotropic, microstructured yield stress material: a colloidal clay composed of an aqueous dispersion of Laponite<sup>®</sup>. The nonlinear rheology of aqueous Laponite<sup>®</sup> dispersions has been studied at the bulk scale,<sup>30,31</sup> but has never been examined at scales below  $\sim 1 \text{ mm}$ .<sup>35</sup> In addition to shear-thinning behaviour, we present the first magnetic tweezer measurements of yield stresses at the microscopic scale. Since microstructural length scales are expected to be on the order of the probe size,<sup>47</sup> it is unclear *a priori* whether micro-scale yield stress results will match those obtained from bulk rheology.<sup>5,48</sup>

**3.2.1 Probe trajectories.** Bulk rheology experiments on aqueous Laponite<sup>®</sup> dispersions have showed a sharp decrease in viscosity at a critical applied stress (*i.e.*, the static yield stress), providing clues as to the expected shape of probe particle trajectories in our experiment.<sup>42,49</sup> If a probe particle is close enough to the tip to exceed the yield stress, we expect the viscosity in the vicinity of the particle to decrease significantly as a result of the disruption of the microstructure due to the applied stress (*i.e.*, local rejuvenation, or shear melting). This would lead to even greater mobility of the particle so that it moves more easily towards the tip to a region of even higher stress, causing an even further decrease in the local viscosity. The resulting trajectories will exhibit rapid acceleration towards the tip surface, reflecting the avalanche behaviour of thixotropic yield stress fluids described by previous authors.<sup>50</sup> In contrast, the stress on particles farther from the tip will not be sufficient to break the yield stress of the surrounding fluid, so those particles are expected to remain stationary.

Fig. 6a shows five typical probe trajectories in a 2.0 wt% Laponite<sup>®</sup> dispersion at an age time of  $t_w = 2 \text{ h}$ . The current is  $I = 2.00 \text{ A}$ . The trajectories are generally consistent with the expectations described above, with a few additional features that merit explanation. We first note that the bottom three trajectories do reach the tip surface ( $x = 0$ ); however, some data is lost because for  $x \leq 22 \mu\text{m}$ , the particles move too fast to be tracked at  $30 \text{ frames s}^{-1}$ . Therefore, some probe particles reach the tip surface during the experiment and others, which generally begin farther away, do not. The most prominent feature of the “mobile” trajectories is their rapid acceleration toward the tip upon reaching a critical separation (or stress), which in this case



**Fig. 6** Probe trajectories in Laponite<sup>®</sup> dispersions. (a) Five typical trajectories are shown in 2.0 wt% Laponite<sup>®</sup> at an age time of  $t_w = 2 \text{ h}$  with current  $I = 2.00 \text{ A}$ . Some particles, generally those beginning closer to the tip, accelerate rapidly toward the surface (“mobile” particles), moving too fast to be tracked for small  $x$ . Others remain at a finite separation over the course of the experiment (“immobile” particles). The initial slowing of both populations of probes is suggested to be a result of “jamming” of the dispersion microstructure, while the eventual rapid acceleration of mobile particles is a result of strong shear-thinning behaviour upon yielding. (b) Typical trajectories of mobile particles are shown for different age times in 1.5 wt% Laponite<sup>®</sup>. As the material ages and undergoes structural arrest, the critical separation at which the particles accelerate rapidly towards the surface decreases, indicating that the critical value of the local stress required to induce flow increases with age.

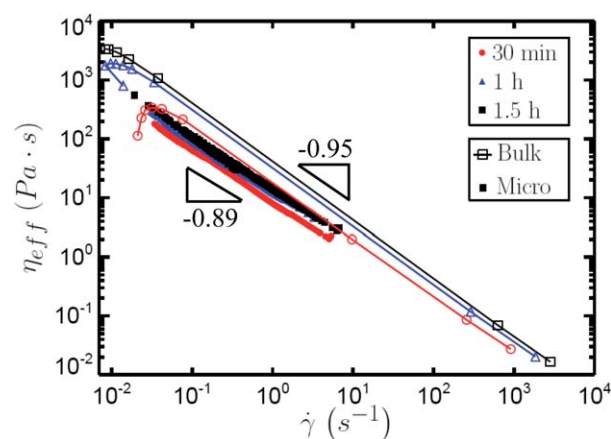
is about  $x = 32 \mu\text{m}$  (corresponding to a stress of about  $\tau = 135 \text{ Pa}$ ). This observation is in agreement with our expectations as described above, and is in contrast to the smooth trajectories observed in the Newtonian calibration fluid. Prior to this rapid acceleration there is a region in which  $d^2x/dt^2 > 0$ , indicating a slight slowing of the probe velocity. Though this behaviour is not explored in detail in this communication, our present contention is that it is a result of effective “jamming” of the dispersion microstructure, while  $d^2x/dt^2 < 0$  indicates a Newtonian or shear-thinning response. The “immobile” trajectories, while never reaching the tip surface, do exhibit measurable displacement. This slow creep and eventual plateau toward the end of the experiment indicates an elastic response and may also be a result of microstructural jamming. Whether or not creeping probes eventually break the yield stress and accelerate rapidly toward the tip depends on the balance between the

stress on the particle, which slowly increases as the particle creeps, and the rheological aging process, which results in a continual increase in the static yield stress and the effective viscosity of the unyielded state.<sup>42,51</sup> Spatial heterogeneity in the dispersion rheological properties may also play a role.<sup>34</sup> Since the material properties of the dispersion evolve with age time, it is expected that changes will be observed in the probe trajectories as the material undergoes aging. This is demonstrated in Fig. 6b, where typical trajectories of mobile particles are shown for a 1.5 wt% Laponite<sup>®</sup> dispersion at four different age times and a current of  $I = 2.00$  A. As the material ages and the microstructure develops, the static yield stress is expected to increase. As a result, we observe that the separation distance at which probes accelerate rapidly towards the surface decreases with age. Or equivalently, the critical stress of rapid acceleration *increases* with age, here going from about 30 Pa at  $t_w = 30$  min to about 60 Pa at  $t_w = 1.5$  h.

**3.2.2 Shear-thinning viscosity.** In order to extract nonlinear rheological information from the trajectories in Fig. 6 it is necessary to calculate particle velocities. Because the trajectories in Laponite<sup>®</sup> dispersions exhibit sharp features not observed in the Newtonian case, a global polynomial or power law fit as described for the calibration is insufficient for an accurate determination of the velocity at each value of  $x$ . Instead, a piecewise cubic spline is used to interpolate the data with a differentiable function. To decrease the noise in the trajectories, a smoothing algorithm is first applied using the MATLAB ‘smooth’ function with a local weighted linear least squares regression and a 1st degree polynomial model (*i.e.*, the ‘lowess’ method). Sufficient smoothing is attained by setting the span of the local regression to about 2% of the data. Subsequently, a cubic spline is applied and differentiated to obtain the particle velocity  $U(x)$ , which is related to the shear rate  $\dot{\gamma}(x) = 3|U(x)|/2a$ . Combining this with the calibration for the stress  $\tau(x)$  allows calculation of an effective micro-scale viscosity,  $\eta_{micro}$ :

$$\eta_{micro} = \frac{\tau}{\dot{\gamma}} = \frac{2a\tau}{3|U|} \quad (8)$$

The shear rate dependence of the effective viscosity for a 1.5 wt% dispersion is shown at three different age times in Fig. 7. The applied current is  $I = 2.00$  A. Here magnetic tweezer micro-rheology results (solid symbols) are compared directly with bulk rheology data (open symbols) obtained from continuous stress ramp tests. At both bulk and microscopic length scales, the effective viscosity exhibits a power law dependence on the shear rate,  $\eta_{eff}(\dot{\gamma}) \propto \dot{\gamma}^p$ . The material is very strongly shear-thinning, with  $p_{micro} \approx -0.89$  and  $p_{bulk} \approx -0.95$ . This result may reflect the open microstructure of the dispersion. At 1.5 wt% ( $\approx 0.6$  vol%), the dispersion is mostly water, so that when the microstructure is disrupted and the material begins to flow, the viscosity is expected to decrease sharply and approach that of water. The power law exponents at both length scales are essentially independent of age time, an observation we attribute to the common microstructural states realized during the aging-rejuvenation process and the (age time)–(shear stress) superposition described by Joshi *et al.*<sup>30</sup> That is, when a dispersion at long age times undergoes shear melting, it passes through many of the same states during rejuvenation as a dispersion at shorter age times.



**Fig. 7** Effective viscosity as a function of shear rate for 1.5 wt% Laponite<sup>®</sup> at three age times. Results from bulk stress ramp tests (open symbols, with lines added to guide the eye) and microrheology (solid symbols) are shown, with both exhibiting strong shear-thinning behaviour. A current of  $I = 2.00$  A is used for the magnetic tweezer experiments. The effective viscosity follows approximately a power law dependence on shear rate,  $\eta_{eff} \propto \dot{\gamma}^p$ , and the observed power law exponents are essentially independent of age time, having values of  $p_{micro} \approx -0.89$  and  $p_{bulk} \approx -0.95$ . The correspondence between the power law exponents at bulk and microscopic scales suggests commonality in the nature of the shear melting process. The magnitude of the viscosity increases with age time, but is consistently 2 to 6 times smaller on the microscopic scale, in qualitative agreement with previous work comparing the linear viscoelastic moduli of Laponite<sup>®</sup> dispersions from bulk- and micro-rheology measurements.<sup>32,34</sup>

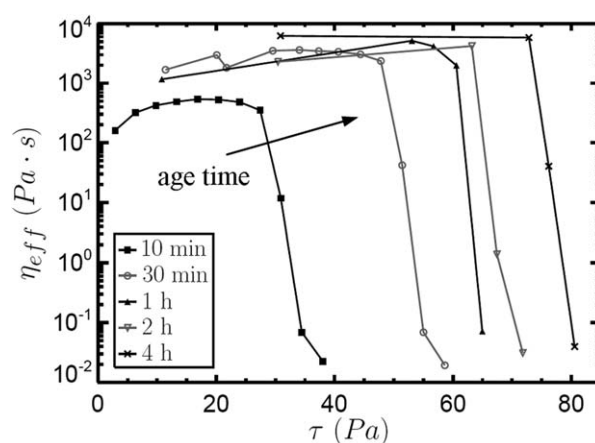
The correspondence between the power law exponents for bulk and micro-scale measurements is consistent with calculations that reveal similar shear-thinning behaviour between the micro- and macroviscosity in colloidal dispersions of spherical particles.<sup>11</sup> Additionally, it indicates that the nature of the shear melting process in Laponite<sup>®</sup> dispersions is similar at bulk and microscopic length scales. In both cases, the interactions between Laponite<sup>®</sup> platelets result in an arrested microstructure that must be disrupted, either locally or globally, for the material to flow. The observation that  $p_{micro} \approx p_{bulk}$  is in spite of fundamental differences between the character of the two flows. The bulk viscosity measurement is extracted from a viscometric shear flow between parallel plates, whereas the micro-scale viscosity is obtained from flow past a sphere. Despite the similarity between  $p$  values across length scales, the magnitude of the effective bulk scale viscosity,  $\eta_{bulk}$ , is about 2 to 6 times  $\eta_{micro}$  for all shear rates and age times. This observation is qualitatively consistent with linear rheological measurements in aqueous Laponite<sup>®</sup> dispersions, which indicate a weaker gel (lower viscoelastic moduli and longer gelation times) at microscopic length scales.<sup>32,34</sup> As in the linear case, the discrepancy is likely due to microstructural features in the dispersion, such as pores or clay particle clusters, that exhibit characteristic sizes similar to the probe size, so that microrheology reflects the mechanical properties of a slightly different structure than bulk measurements.

Before leaving this discussion, it is important to address the unsteady nature of the flows from which the viscosity data in Fig. 7 is extracted. Because the stress is continually increasing in

both the bulk and micro-scale experiments, it may be inappropriate to consider the viscosity values as steady-state measurements. For similar Laponite® systems, the stress relaxation time scale,  $\lambda$ , was measured to be on the order of  $\sim 100$  s,<sup>52</sup> which is large compared to the current shearing time scale  $1/\dot{\gamma}$ . In other words, the Deborah number,  $De$ , is large for the experiments in Fig. 7:  $De = \lambda\dot{\gamma} \gg 1$ . For this aging system with continually evolving microstructure and rheological properties, however, it is unclear how to measure bulk steady-state viscosity values in the traditional sense. In particular, if such an experiment could even reach steady-state it would likely take significant time, prohibiting the study of age-time dependence. This was demonstrated by Abou *et al.*,<sup>31</sup> who performed bulk creep tests on Laponite® dispersions of similar concentration and ionic strength as in the present study. They found that reaching steady state requires exceeding a critical shear stress and shearing for times on the order of hours. With this method, they measured steady-state viscosities over the range of shear rates  $50 \text{ s}^{-1} \leq \dot{\gamma} \leq 5000 \text{ s}^{-1}$  and found a shear-thinning power law of  $p \approx -0.6$ , which is clearly not as strongly shear-thinning as the data in Fig. 7. This discrepancy further suggests that effects of the unsteady nature of the flows may be present, and so we qualify our results as “effective” viscosities. However, because of the continuous ramping of the shear stress in both cases, the bulk and micro-scale measurements reported in Fig. 7 are still considered to be analogous to each other.

**3.2.3 Yield stress.** At higher Laponite® concentrations, the yield stress becomes a very prominent rheological feature. For example, after aging for about 1 h, dispersions with concentrations of about 2.5 wt% or more do not flow when the recipient is overturned. Bulk stress ramp tests performed on a 2.0 wt% Laponite® dispersion support the notion of a significant yield stress. Effective viscosity data for these experiments as a function of the applied shear stress is shown in Fig. 8 at five different age times. The sharp decrease in viscosity at a critical stress is indicative of a yield stress, which we estimate as the stress at which the viscosity exhibits an intermediate value between its pre- and post-yielded viscosities. We note that the viscosity values reported in the pre-yielded state ( $\sim 1000$  Pa s) may be somewhat artificial and may depend strongly on the experimental protocol, so that they do not necessarily reflect a true, high-viscosity, fluid state.<sup>53</sup>

Magnetic tweezer measurements of the yield stress at the microscopic scale are based upon the distinction between “mobile” and “immobile” probe particles as described in Section 3.2.1. Mobile particles break the yield stress and cause shear-thinning of the surrounding fluid, eventually reaching the tip. Immobile particles exhibit a slow creep, but their trajectories plateau and they remain separated from the tip. The  $x$  value that separates the shear-thinning region from the creep region can be considered a yield surface. More specifically, the yield stress,  $\tau_y$ , is bounded by the minimum stress on mobile particles and the maximum stress on immobile particles. That is, if  $x_{mobile}$  is the farthest distance from the tip for mobile particles and  $x_{immobile}$  is the shortest distance from the tip for immobile particles, then  $\tau(x_{mobile})$  and  $\tau(x_{immobile})$  are bounds on  $\tau_y$  and we take  $\tau_y$  as the average of  $\tau(x_{mobile})$  and  $\tau(x_{immobile})$ . One would expect that  $x_{mobile} < x_{immobile}$ , so that based on the calibration in Fig. 2,



**Fig. 8** Effective viscosity as a function of applied shear stress from bulk continuous stress ramp tests on 2 wt% Laponite®. Results are shown at five different age times. At a critical stress, the viscosity exhibits a sharp drop over several orders of magnitude, a phenomenon associated with a yield stress on the bulk scale. This critical stress increases with the age time. We note that because the stress in each test is ramped continuously over 2 min, the reported viscosity values do not correspond directly to steady-state measurements.

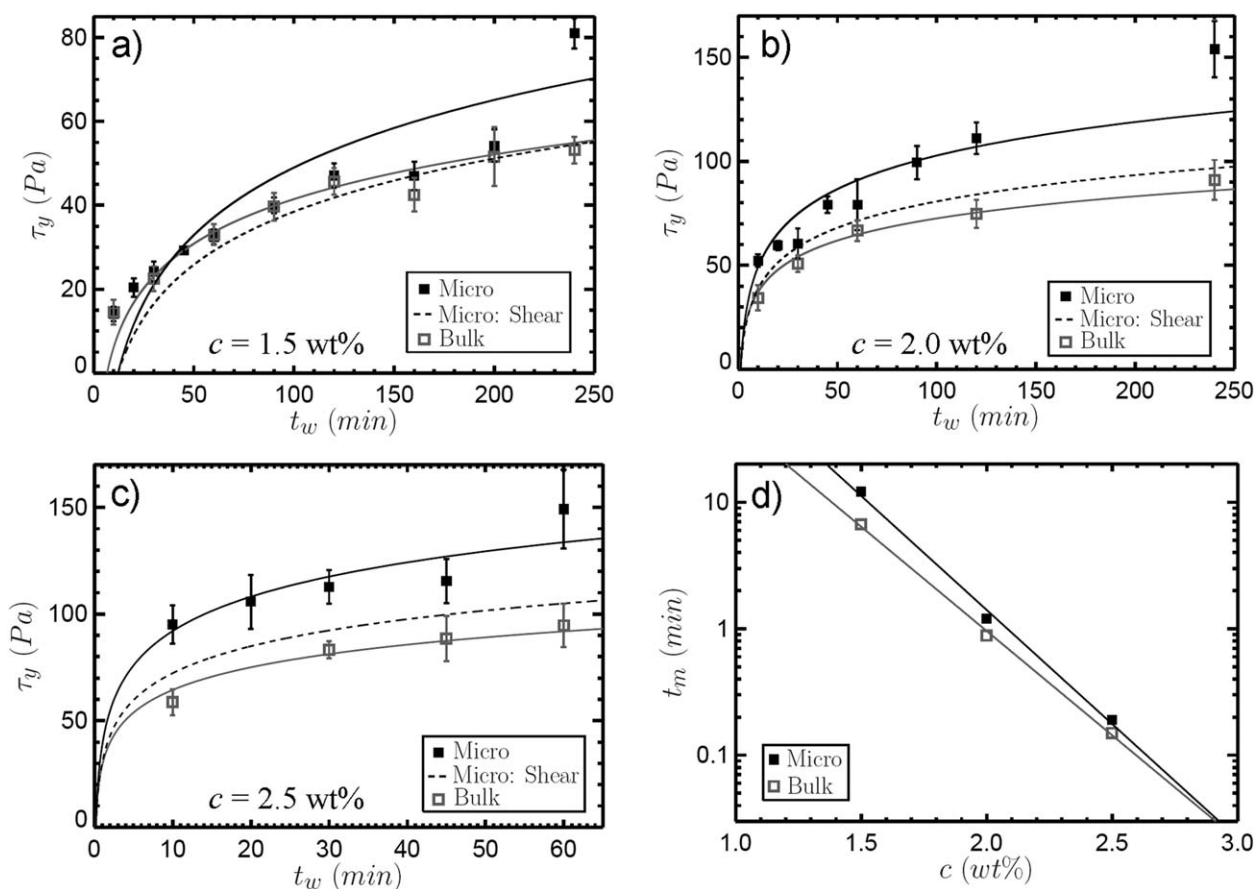
$\tau(x_{mobile}) > \tau(x_{immobile})$ . However, we typically observe  $x_{mobile} > x_{immobile}$  as a result of the creeping of immobile particles over the course of a measurement. This is demonstrated in Fig. 6a, in which one of the immobile particles eventually creeps past the initial position of a mobile particle, and yet remains far from the tip. This observation is likely a result of a small amount of aging during a single measurement, as well as spatial heterogeneity in the dispersion rheological properties. Another consequence of the creep behaviour is that the experimental time (*i.e.*, the time over which the current is applied) must be kept constant; otherwise immobile particles may creep varying distances for different experiments, resulting in inconsistent calculations of  $\tau_y$ . We maintain the experimental time at 1 min.

Yield stress measurements as a function of age time are plotted in Fig. 9 for three Laponite® concentrations. Bulk rheology data (gray open symbols) and magnetic tweezer measurements (black solid symbols) are directly compared. The reproducibility of the data is demonstrated by the error bars, which represent the standard error of measurements on three different samples at each age time. In agreement with previous work on the rheology of Laponite® dispersions,<sup>29,35</sup> as well as other microstructured aging materials,<sup>54,55</sup> the yield stress grows approximately logarithmically with age time according to the function

$$\tau_y = \beta \ln\left(\frac{t_w}{t_m}\right) \quad (9)$$

where  $\beta$  is a constant (assumed to be independent of Laponite® concentration) and  $t_m$  is interpreted as a time scale for microstructural development that can be concentration-dependent. Gray and black solid lines in Fig. 9 show least-squares fits to eqn (9) at bulk and microscopic scales, respectively, for each concentration. Eqn (9) generally provides a good fit to the experimental data, although it is a somewhat poor approximation (with coefficient of determination  $R^2 = 0.72$ ) for the magnetic tweezer data at 1.5 wt%. A power law fit was also





**Fig. 9** Comparison of yield stress measurements at bulk and microscopic scales. The age-time dependence of the observed yield stress is shown for Laponite<sup>®</sup> concentrations of (a) 1.5 wt%, (b) 2.0 wt%, and (c) 2.5 wt%. Error bars represent the standard error of measurements on three different samples at each age time. For all concentrations, the yield stress measured at both length scales grows approximately logarithmically with age time according to eqn (9), although this is a somewhat poor approximation for the micro-scale data at 1.5 wt% ( $R^2 = 0.72$  for 1.5 wt% micro-scale data). Fits to this functional form are shown by lines in black (micro) and gray (bulk). While there is good agreement between the bulk and raw microrheology data for the lowest concentration up to  $t_w = 200$  min, the raw micro-scale data provides higher values for the yield stress compared to measurements from bulk shear for 2.0 and 2.5 wt% Laponite<sup>®</sup>. However, by treating the pre-yielded material as a linear elastic solid and approximating the shear contribution to the applied stress for the microrheology experiments, quantitative agreement with the bulk yield stress measured in shear can be recovered for concentrations  $c \geq 2.0$  wt%. This approximate shear component of the micro-scale applied stress is  $\pi/4$  times (78.5%) the measured average stress based on the total force and the probe surface area in the magnetic tweezer experiment and is given by the dashed black line. The characteristic time scales  $t_m$ , which are related to microstructural development and are extracted by fitting the bulk and micro-scale data to eqn (9), decrease exponentially with Laponite<sup>®</sup> concentration, as shown in (d).

examined, with a power law exponent that is independent of length scale and concentration, but only marginal improvement in the overall quality of the fit is observed when the additional adjustable parameter is taken into account. That is, we find  $R_{adj}^2 = 0.95$  for the power law fit and  $R_{adj}^2 = 0.93$  for the logarithmic fit, where  $R_{adj}^2$  is an adjusted  $R^2$  value that corrects for the number of model parameters.<sup>56</sup> The logarithmic fits yield  $\beta$  values of  $\beta_{bulk} = 15.3$  Pa and  $\beta_{micro} = 23.2$  Pa. The fitted  $t_m$  values are plotted as a function of Laponite<sup>®</sup> concentration,  $c$ , in Fig. 9d. We observe that  $t_m$  decreases exponentially with  $c$  (*i.e.*, linearly on semi-log scale), indicating that dispersions of higher concentration undergo faster structural arrest. Additionally, as the Laponite<sup>®</sup> concentration increases, bulk and micro-scale  $t_m$  values converge.

While quantitative agreement between bulk and micro-scale yield stress data is observed for the lowest Laponite<sup>®</sup> concentration of 1.5 wt% up to  $t_w = 200$  min, the micro-scale data

systematically provides higher values for the yield stress compared to measurements from bulk shear for higher concentrations. To interpret these results, it is important to consider the differences between the flow kinematics for the bulk and micro-scale experiments.<sup>57</sup> Only shear stresses are applied in the bulk plate-plate experiment, while the fluid experiences both shear and normal stresses at the surface of magnetic probe particles. Since yield stress materials generally exhibit resistance to both shear and normal stresses, it is reasonable that an elevated yield stress might be observed from magnetic tweezer measurements. A more appropriate comparison of the data can be achieved by considering only the shear component of the stress. Without knowledge of the flow kinematics, however, an exact expression for the shear stress in the micro-scale experiment is unavailable. As an approximation, we treat the pre-yielded fluid as a linear elastic medium. In this case, the Rayleigh analogy between viscous flow and the linear elastostatics of isotropic, incompressible solids

dictates that the stress distribution around the probe sphere is the same as that for Newtonian creeping flow past a sphere,<sup>58,59</sup> for which the shear stress distribution is

$$\tau(\theta) = \left(\frac{3\eta U}{2a}\right) \sin \theta \quad (10)$$

where  $\theta$  is the inclination angle measured from the axis of the sphere velocity  $U$ .<sup>60</sup> By integrating eqn (10), the average shear stress at the surface of the sphere is found to be  $\tau_{shear} = 3\pi\eta U/8a$ , which is  $\pi/4$  times (78.5%) the average stress based on the total force (Stokes drag,  $|F| = 6\pi\eta a|U|$ ) divided by the sphere surface area,  $\tau = 3\eta U/2a$ . Using this result from linear elastic kinematics to approximate the contribution of shear stresses, we therefore shift the logarithmic fits to the micro-scale data down by a factor of  $\pi/4$ . These shifted results, shown as black dashed lines in Fig. 9, exhibit closer agreement with bulk shear yield stress data and a  $\beta$  value of  $\beta_{shear} = 18.2$  Pa. However, the correspondence between bulk and micro-scale data at 1.5 wt % Laponite<sup>®</sup> breaks down when considering only the shear contribution to the stress; the apparent agreement of the black dotted line with the bulk measurements is an artefact of the questionable fit of the magnetic tweezer data to eqn (9) at this concentration.

We note briefly that the problem of a sphere moving through the simplest model yield stress fluid, a Bingham plastic, was previously considered by Beris *et al.* using finite element analysis.<sup>61</sup> In this work, an expression is proposed that relates the yield stress to the critical applied force,  $F$ , necessary to induce flow:  $\tau_y = 0.143F/(2\pi a^2)$ . Applying this expression to our magnetic tweezer data results in micro-scale yield stresses that are about 40–50% of bulk measurements. This discrepancy is not necessarily surprising, however, since the Laponite<sup>®</sup> dispersion does not strictly obey the Bingham model, but exhibits both pre-yield elastic deformation and post-yield shear-thinning and ‘rejuvenation’ (see Fig. 6 and 7).

The correspondence, or lack thereof at low concentrations, between bulk and micro-scale rheology is related to the characteristic size of microstructural features in the dispersions, such as pores and other microstructural heterogeneities, as compared to the length scale that is probed. For dispersions of similar concentration and ionic strength, Pignon *et al.* studied the physical structure of Laponite<sup>®</sup> dispersions by combining small-angle X-ray and neutron scattering with static light scattering.<sup>47,62</sup> With this method, they obtained the scattering curve over five orders of magnitude in length scale. Their results indicate that the microstructure consists of a fractal network of loosely-connected clusters having a characteristic size of about 5  $\mu\text{m}$ . At larger length scales, the dispersion appears homogeneous. We therefore expect that probing at length scales significantly larger than 5  $\mu\text{m}$  would result in data that match bulk measurements. Results for smaller probes will primarily reflect the rheological properties on the length scale of the probe size. Since the largest microstructural length scale is on the same order of magnitude as the probe size in the present work, we do not necessarily anticipate that bulk rheology and microrheology results will match, though we might expect them to be close. It is reasonable to expect that the characteristic pore size will shrink as the dispersion concentration is increased. Such a trend in the size of

microstructural features may account for the fact that better agreement is observed between the bulk and the appropriately shear-corrected magnetic tweezer measurements for the more concentrated dispersions of 2.0 wt% and 2.5 wt%. Multiple particle tracking linear microrheology experiments in aqueous Laponite<sup>®</sup> dispersions have also suggested that the characteristic pore size decreases with age time, based on the delay in the apparent gelation time observed with decreasing probe particle size.<sup>34</sup> This could provide an explanation for the eventual increase in the micro-scale yield stress for the 1.5 wt% dispersion at the longest age time, at which point the shear contribution to the stress corresponds reasonably well with the bulk measurement.

## 4 Conclusions

Nonlinear rheology is critical to the processing and end-use of many industrially relevant materials, as well as in numerous settings in nature and biology. In many of these situations, micro-scale dynamics play a key role; however, methods for quantitatively probing nonlinear microrheology are only recently being developed. In the present work, we have discussed a simple magnetic tweezer technique for studying the nonlinear microrheology of complex fluids. The instrument can apply magnetic fields on the order of  $\sim 1$  T, leading to stresses up to about 230 Pa on 4.5  $\mu\text{m}$  superparamagnetic probe particles. Shear rates up to about  $10\text{ s}^{-1}$  and viscosities up to about  $10^5$  Pa s can be measured. The experimental error is controlled by limiting measurements to probe separations beyond 20  $\mu\text{m}$ , where the variability in the magnetic force across the tip of the tweezer device is less than 10%. Improvements to the technique and the experimental setup could be achieved through more precise machining and the use of a high-speed camera.

The technique has been demonstrated on an industrially and scientifically relevant aging and thixotropic yield stress fluid: an aqueous dispersion of the synthetic clay Laponite<sup>®</sup>. “Mobile” and “immobile” probe trajectories were observed, reflecting a distinction between probes that overcome the yield stress of the material and those that experience insufficient stress to cause flow. By analyzing “mobile” probe trajectories, the effective micro-scale viscosity was determined as a function of the shear rate. The Laponite<sup>®</sup> dispersion was found to exhibit strong shear-thinning behaviour, a feature extracted from the rapid acceleration of probes towards the tip and associated with microstructural disruption and shear melting. The shear-thinning behaviour was corroborated by bulk measurements, which exhibited similar power law results despite differences in viscosity values by a factor of about 2 to 6. Furthermore, the distinction between “mobile” and “immobile” probe trajectories has provided a basis for the first use of magnetic tweezers to directly and quantitatively measure yield stresses at the microscopic scale. When the approximate shear contribution to microrheology results is isolated, bulk and micro-scale yield stress measurements were found to agree quantitatively for Laponite<sup>®</sup> concentrations of 2.0 wt% or higher, with both exhibiting an approximately logarithmic growth with age time. The age-time dependence of the yield stress has revealed a time scale associated with microstructural development, which we have found to decrease with Laponite<sup>®</sup> concentration.

It is expected that nonlinear bulk and micro-scale rheology results will agree if probe particles are large compared to the characteristic length scale of microstructural features in the dispersion.<sup>5</sup> An interesting problem for future work would be to determine the probe size at which the bulk-micro agreement observed in Fig. 9b and 9c breaks down. This would provide insight into the microstructural length scales in those dispersions. Further, does agreement break down at all age times, or might the measurements coincide at long enough age times? Our current contention is that measurements with smaller probes in 2.0 or 2.5 wt% Laponite® would likely follow similar behaviour as the data in Fig. 9a, and that a concentration–(probe-size) superposition would exist, as in the linear rheology case.<sup>34</sup>

The methods and tools presented here will aid in the micro-scale characterization of complex fluids and soft materials, providing new insight into the microstructure and mechanical response of such materials as polymer gels, colloidal glasses, and biological tissues. Additionally, this work will enable a more complete rheological characterization of materials that are difficult to obtain in large quantities, like certain biofluids. Finally, the results of this article will further the understanding of aqueous Laponite® dispersions, which have become important model thixotropic materials in industry and in academic studies.

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## References

- 1 P. Cicutta and A. M. Donald, *Soft Matter*, 2007, **3**, 1449.
- 2 M. L. Gardel, M. T. Valentine and D. A. Weitz, in *Microscale Diagnostic Techniques*, ed. K. S. Breuer, Springer Verlag, New York, 2005, pp. 1.
- 3 D. Wirtz, *Annu. Rev. Biophys.*, 2009, **38**, 301.
- 4 T. A. Waigh, *Rep. Prog. Phys.*, 2005, **68**, 685.
- 5 J. Liu, M. L. Gardel, K. Kroy, E. Frey, B. D. Hoffman, J. C. Crocker, A. R. Bausch and D. A. Weitz, *Phys. Rev. Lett.*, 2006, **96**, 118104.
- 6 L. G. Wilson and W. C. K. Poon, *Phys. Chem. Chem. Phys.*, 2011, **13**, 10617.
- 7 P. Habdas, D. Schaar, A. C. Levitt and E. R. Weeks, *Europhys. Lett.*, 2004, **67**, 477.
- 8 M. Parthasarathy and D. J. Klingenberg, *Mater. Sci. Eng., R*, 1996, **17**, 57.
- 9 R. G. Larson, *The Structure and Rheology of Complex Fluids*, Oxford University Press, New York, 1999.
- 10 P. J. Rankin, A. T. Horvath and D. J. Klingenberg, *Rheol. Acta*, 1999, **38**, 471.
- 11 T. M. Squires and J. F. Brady, *Phys. Fluids*, 2005, **17**, 21.
- 12 A. Meyer, A. Marshall, B. G. Bush and E. M. Furst, *J. Rheol.*, 2006, **50**, 77.
- 13 I. C. Carpen and J. F. Brady, *J. Rheol.*, 2005, **49**, 1483.
- 14 I. Sriram, A. Meyer and E. M. Furst, *Phys. Fluids*, 2010, **22**, 10.
- 15 A. S. Khair and T. M. Squires, *Phys. Rev. Lett.*, 2010, **105**, 4.
- 16 J. N. Wilking and T. G. Mason, *Phys. Rev. E*, 2008, **77**, 055101.
- 17 W. Seifriz, *Br. J. Exp. Biol.*, 1924, **2**, 1.
- 18 M. Gordon, S. C. Hunter, J. A. Love and T. C. Ward, *Nature*, 1968, **217**, 735.
- 19 C. Haber and D. Wirtz, *Rev. Sci. Instrum.*, 2000, **71**, 4561.
- 20 J. Lammerding, A. R. Kazarov, H. Huang, R. T. Lee and M. E. Hemler, *Proc. Natl. Acad. Sci. U. S. A.*, 2003, **100**, 7616.
- 21 J. Lammerding, PhD Thesis, *Dept of Biological Engineering, Massachusetts Institute of Technology*, 2004.
- 22 H. A. Barnes, *J. Non-Newtonian Fluid Mech.*, 1997, **70**, 1.
- 23 Rockwood Additives: Southern Clay Products, Laponite product information, (<http://www.scprod.com/pdfs/Laponite%20brochure%20EN.pdf>).
- 24 A. Mourchid, A. Delville, J. Lambard, E. LeColier and P. Levitz, *Langmuir*, 1995, **11**, 1942.
- 25 B. Ruzicka, L. Zulian and G. Ruocco, *Phys. Rev. Lett.*, 2004, **93**, 258301.
- 26 B. Ruzicka, L. Zulian and G. Ruocco, *Langmuir*, 2006, **22**, 1106.
- 27 S. Jabbari-Farouji, H. Tanaka, G. H. Wegdam and D. Bonn, *Phys. Rev. E*, 2008, **78**, 061405.
- 28 S. Cocard, J. F. Tassin and T. Nicolai, *J. Rheol.*, 2000, **44**, 585.
- 29 A. S. Negi and C. O. Osuji, *Phys. Rev. E*, 2010, **82**, 031404.
- 30 Y. M. Joshi and G. R. K. Reddy, *Phys. Rev. E*, 2008, **77**, 021501.
- 31 B. Abou, D. Bonn and J. Meunier, *J. Rheol.*, 2003, **47**, 979.
- 32 F. K. Oppong, P. Coussot and J. R. de Bruyn, *Phys. Rev. E*, 2008, **78**, 10.
- 33 B. Ruzicka and E. Zaccarelli, *Soft Matter*, 2011, **7**, 1268.
- 34 J. P. Rich, G. H. McKinley and P. S. Doyle, *J. Rheol.*, 2011, **55**, 273.
- 35 C. Wilhelm, F. Elias, J. Browaeys, A. Ponton and J.-C. Bacri, *Phys. Rev. E*, 2002, **66**, 021502.
- 36 A. R. Bausch, F. Ziemann, A. A. Boulbitch, K. Jacobson and E. Sackmann, *Biophys. J.*, 1998, **75**, 2038.
- 37 P. Kollmannsberger and B. Fabry, *Rev. Sci. Instrum.*, 2007, **78**, 6.
- 38 D. Bonn, H. Kellay, H. Tanaka, G. Wegdam and J. Meunier, *Langmuir*, 1999, **15**, 7534.
- 39 B. Abou, D. Bonn and J. Meunier, *Phys. Rev. E*, 2001, **64**, 021510.
- 40 L. Petit, C. Barentin, J. Colombani, C. Ybert and L. Bocquet, *Langmuir*, 2009, **25**, 12048.
- 41 J. C. Crocker and D. G. Grier, *J. Colloid Interface Sci.*, 1996, **179**, 298.
- 42 D. Bonn, P. Coussot, H. T. Huynh, F. Bertrand and G. Debrégeas, *Europhys. Lett.*, 2002, **59**, 786.
- 43 Q. D. Nguyen and D. V. Boger, *Annu. Rev. Fluid Mech.*, 1992, **24**, 47.
- 44 T. Savin and P. S. Doyle, *Biophys. J.*, 2005, **88**, 623.
- 45 R. M. Bozorth, *Ferromagnetism*, Wiley - IEEE Press, 1993.
- 46 F. Ebert, P. Dillmann, G. Maret and P. Keim, *Rev. Sci. Instrum.*, 2009, **80**, 083902.
- 47 F. Pignon, A. Magnin, J. M. Piau, B. Cabane, P. Lindner and O. Diat, *Phys. Rev. E*, 1997, **56**, 3281.
- 48 M. T. Valentine, P. D. Kaplan, D. Thota, J. C. Crocker, T. Gisler, R. K. Prud'homme, M. Beck and D. A. Weitz, *Phys. Rev. E*, 2001, **64**, 061506.
- 49 R. Ewoldt, C. Clasen, A. E. Hosoi and G. H. McKinley, *Soft Matter*, 2007, **3**, 634.
- 50 P. Coussot, Q. D. Nguyen, H. T. Huynh and D. Bonn, *Phys. Rev. Lett.*, 2002, **88**, 175501.
- 51 P. Coussot, Q. D. Nguyen, H. T. Huynh and D. Bonn, *J. Rheol.*, 2002, **46**, 573.
- 52 R. Bandyopadhyay, P. H. Mohan and Y. M. Joshi, *Soft Matter*, 2010, **6**, 1462.
- 53 P. C. F. Møller, A. Fall and D. Bonn, *Europhys. Lett.*, 2009, **87**, 6.
- 54 T. S. Chow, *Polymer*, 1993, **34**, 541.
- 55 K. Chen and K. S. Schweizer, *Phys. Rev. E*, 2008, **78**, 031802.
- 56 R. G. D. Steel and J. H. Torrie, *Principles and Procedures of Statistics*, 2 edn, McGraw-Hill, New York, 1980.
- 57 T. M. Squires, *Langmuir*, 2007, **24**, 1147.
- 58 J. W. S. Rayleigh, *The Theory of Sound*, 2 edn, Dover, 1945.
- 59 W. B. Russel and P. R. Sperry, *Prog. Org. Coat.*, 1994, **23**, 305.
- 60 W. M. Deen, *Analysis of Transport Phenomena*, Oxford University Press, New York, 1998.
- 61 A. N. Beris, J. A. Tsamopoulos, R. C. Armstrong and R. A. Brown, *J. Fluid Mech.*, 1985, **158**, 219.
- 62 F. Pignon, J.-M. Piau and A. Magnin, *Phys. Rev. Lett.*, 1996, **76**, 4857.