

# Soft Matter

rsc.li/soft-matter-journal



ISSN 1744-6848



**PAPER**

Xuehua Zhang *et al.*  
Growth dynamics of surface nanodroplets during solvent exchange  
at varying flow rates



Cite this: *Soft Matter*, 2018, 14, 5197

## Growth dynamics of surface nanodroplets during solvent exchange at varying flow rates†

Brendan Dyett,<sup>a</sup> Akihito Kiyama,<sup>b</sup> Maaik Rump,<sup>c</sup> Yoshiyuki Tagawa,<sup>b</sup> Detlef Lohse<sup>c</sup> and Xuehua Zhang<sup>b,dac</sup>

Solvent exchange is a simple solution-based process to produce surface nanodroplets over a large area. The final size of the droplets is determined by both the flow and solution conditions for a given substrate. In this work, we investigate the growth dynamics of surface nanodroplets during solvent exchange by using total internal reflection fluorescence microscopy (TIRF). The results show that during the solvent exchange, the formation of surface nanodroplets advanced on the surface in the direction of the flow. The time for the number density and surface coverage of the droplets to reach their respective plateau values is determined by the flow rate. From the observed evolution of the droplet volume and of the size of individual growing droplets, we are able to determine that the growth time of the droplets scales with the Peclet number  $Pe$  with a power law  $\propto Pe^{-1/2}$ . This is consistent with Taylor–Aris dispersion, shedding light on the diffusive growth dynamics during the solvent exchange. Further, the spatial rearrangement of the droplets during coalescence demonstrates a preference in position shift based on size inequality, namely, the coalesced droplet resides closer to the larger of the two parent droplets. These findings provide a valuable insight toward controlling droplet size and spatial distribution.

Received 5th April 2018,  
Accepted 3rd May 2018

DOI: 10.1039/c8sm00705e

rsc.li/soft-matter-journal

## 1 Introduction

Droplet formation on surfaces is paramount to a growing number of fundamental and applied processes.<sup>1–4</sup> Areas of interest include breath figure templating<sup>5,6</sup> and the condensation of droplets on liquid repellent surfaces.<sup>7,8</sup> Surface droplets are also relevant for high throughput screening<sup>9</sup> and compartmentalized biological conversion in microdroplet arrays.<sup>10</sup> Once these droplets are tens to hundreds of nanometers in height and several hundred nanometers to several microns in lateral diameter, we refer to them as surface nanodroplets. To be more precise, they may be also called sessile submicron droplets.

To lay the foundation for a variety of droplet-based applications, various approaches have been explored to produce surface nanodroplets, including inkjet<sup>11</sup> and contact printing,<sup>12</sup> matrix-assisted pulsed laser evaporation,<sup>13</sup> drop splitting<sup>14</sup> and condensation.<sup>15</sup>

Among these approaches, solvent exchange provides a versatile approach for producing droplets on a substrate in contact with a surrounding phase of an immiscible liquid. The approach of solvent exchange denotes the general process of displacing a good solvent of the droplet liquid with a poor solvent within a fluid channel which accommodates the substrate. Solvent exchange has been shown to be universal, yielding femtoliter surface droplets of various liquids<sup>16</sup> and is not limited by scale.<sup>17</sup>

During solvent exchange, a pulse of temporal oversaturation of the solute is created at the mixing front,<sup>18</sup> leading to the formation of surface nanodroplets on the substrate. The oversaturation and from this the resulting droplet size can be controlled by the flow and solution conditions. However, this control of the droplet formation requires a quantitative understanding of the mechanism of solvent exchange. The work by Zhang *et al.*<sup>19</sup> highlighted the interplay between the solution chemistry and fluid dynamics for the final droplet size. It was reported that the droplet size was larger at higher flow rates, corresponding to higher Peclet ( $Pe$ ) numbers. For fixed fluid cell geometries, the final droplet volume per unit area scales with  $\propto Pe^{3/4}$ . On the other hand, for a fixed flow rate, the droplet volume scales with the channel height  $h$  with  $\propto h^3$  and thus can be modulated by modulating the channel height.<sup>20</sup> These influences can be understood by describing the mixing of the two solutions through Taylor–Aris dispersion.<sup>21–23</sup> Consequently, for given channel dimensions, it is expected that the duration of the oversaturation pulse  $\tau$  scales  $Pe^{-1/2}$ .<sup>20</sup> So far,

<sup>a</sup> *Soft Matter & Interfaces Group, School of Engineering, RMIT University, Melbourne, VIC 3001, Australia. E-mail: xuehua.zhang@ualberta.ca*

<sup>b</sup> *Department of Mechanical Systems Engineering, Tokyo University of Agriculture and Technology, Nakacho 2-24-16 Koganei, Tokyo 184-8588, Japan*

<sup>c</sup> *Physics of Fluids Group, Department of Science and Engineering, Mesa+ Institute, J. M. Burgers Centre for Fluid Dynamics and the Max Planck Center Twente for Complex Fluid Dynamics, University of Twente, P.O. Box 217, 7500 AE Enschede, The Netherlands*

<sup>d</sup> *Department of Chemical and Materials Engineering, Faculty of Engineering, University of Alberta, Edmonton, Alberta T6G1H9, Canada*

† Electronic supplementary information (ESI) available. See DOI: 10.1039/c8sm00705e



however, the growth time of droplets at different flow rates has not yet been directly measured from experiments and a quantitative correlation between the droplet growth time and the flow rate of the solvent exchange is yet to be established.

More recently, Xu *et al.*<sup>24</sup> identified universal regimes of droplet growth based on the final droplet morphology from a broad range of flow and solution conditions. It was suggested that the surface coverage and number density of droplets initially increased before a maximal surface coverage was reached. With continued droplet growth, the surface coverage remained saturated while the number density decreased. However, the dynamics of the droplet growth has not yet been examined *in situ* during the process of solvent exchange.

In this work, we employ total internal reflection fluorescence confocal microscopy<sup>25–27</sup> (TIRF) to examine the growth of surface nanodroplets. This experimental technique allows *in situ* observation of surface nanodroplets during the entire process of solvent exchange. From the superb spatial and temporal resolution of TIRF measurements we are able to determine the growth time of the droplets at different flow rates. The measurements allow for two complementary approaches to determine the growth time of droplets for a given flow rate, which both give consistent results. Furthermore, once the surface coverage is above a certain threshold, the dynamical process of droplet coalescence can clearly be revealed. The findings of this work are valuable for the design of flow conditions for desirable droplet sizes, but also may be applied to control microphase separation in general.

## 2 Experimental section

### 2.1 Chemicals and materials

1-Octanol (99%, Sigma), ethanol (AR, Chem-supply), isopropanol (AR, Chem-supply), octyldecyltrichlorosilane (OTS) (99%, Sigma), Nile-red (Sigma) were used as received without further purification. The glass substrates (high precision, 26 × 60 mm, no. 1.5H, Marienfeld) were hydrophobized using OTS by following a previously reported protocol.<sup>28</sup> The substrates were additionally cleaned by sonication in isopropanol for 15 min immediately before use.

1-Octanol was chosen as the droplet liquid. To perform the solvent exchange, two solutions were prepared. The first solution, solution A, was 5% (v/v) 1-octanol in 50% aqueous ethanol while the second solution, solution B, was 1-octanol saturated water. All the experiments were conducted at room temperature. For the measurements by confocal microscope, Nile-red was used to selectively dye the 1-octanol phase.

### 2.2 TIRF measurements of growing nanodroplets during solvent exchange

Surface nanodroplets were formed on the glass substrate that was the bottom wall of a custom-built fluid chamber as sketched in Fig. 1A. The rectangular chamber was 15 mm in width, 50 mm in length and 900 μm in height. The fluid cell was positioned on the top of the sample stage for TIRF

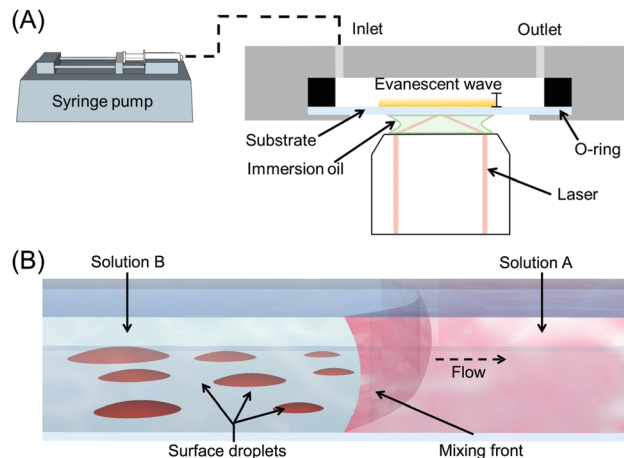


Fig. 1 (A) Schematic depiction of the setup used for TIRF measurements. (B) Schematic of surface droplet formation by solvent exchange. The good solvent (solution A, shown in red), is displaced by the poor solvent (solution B, shown in blue), leading to nanodroplet (red) nucleation and growth behind the mixing front.

measurements. During the solvent exchange, the fluid chamber was pre-filled with solution A. The second solution, solution B, was introduced into the chamber at a given flow rate to displace solution A. The flow rate was controlled by using a digital syringe pump (NE-1000, Pump Systems). The flow conditions for the solvent exchanges are listed in Table 1 and were performed in triplicate.

The process of nucleation and growth of surface nanodroplets sketched in Fig. 1B was observed in the measurements by TIRF. A Nikon N-Storm super-resolution confocal microscope (TIRF 100× 1.49 NA objective lens) was used with the samples illuminated by a continuous wave (CW) 561 nm laser. Within the NIS-Elements AR software the TIRF mirror position was adjusted until achieving TIR, determined by a simultaneous decrease in background brightness. The region of interest was collected by an Andor iXon EMCCD camera and defined as 81.9 × 81.9 μm<sup>2</sup> with ~31.2 ms exposure, resulting in a pixel calibration of 0.16 μm per pixel.

### 2.3 Data analysis

A tiff stack of the raw data from TIRF was processed frame-by-frame in self-written Matlab codes. The brightness of each

**Table 1** Flow parameters for solvent exchange to form surface nanodroplets. The mean flow velocity ( $\bar{U}$ ) is determined by  $Q = h w \bar{U}$ ; the Reynolds number by  $Re = \bar{U} h / \nu = Q / w \nu$ ; the Peclet number by  $Pe = \bar{U} h / D = Q / w D$ . Here  $\nu$  and  $D$  are the viscosity of solution B and the diffusion coefficient of the droplet liquid in solution B, respectively.  $h$  is the chamber height and  $w$  is the chamber width

$Q$ (μl min <sup>-1</sup> )	Re	Pe	$\bar{U}$ (mm s <sup>-1</sup> )
25	0.031	27.8	0.031
35	0.044	38.9	0.043
50	0.062	55.6	0.062
75	0.094	83.3	0.093
100	0.125	111	0.123
150	0.187	167	0.185



frame was adjusted by adaptive histogram equalization before segmentation and watershed transforms. Based on the binarized images, the number, size and surface coverage of droplets with time were determined. To analyse droplet coalescence, a coalesced droplet was first identified, and then the tiff image stack of this droplet at earlier time was analysed to identify its parent droplets. The size and position of the droplets were determined in each frame as the time went back to earlier and earlier stages. The change in droplet position and number was utilized to characterize the parent-child droplet relationships.

### 3 Results and discussion

#### 3.1 Size, surface coverage and number density of droplets during solvent exchange

A representative series of snapshots shown in Fig. 2 reveals the progressive nucleation of 1-octanol droplets along the surface. The flow for the solvent exchange was in a diagonal direction from the upper left to the lower right, identical to the advancing direction for the droplet formation. These TIRF images resolve droplet radii of  $\sim 200$ – $300$  nm, allowing the direct visualization of the droplet growth process from an early stage of the exchange. The interval between two sequential snapshots is  $\sim 60$ – $120$  ms. The moment of the detection of the initial droplets in the measurements is defined as time 0. The images of the droplets at the end of the solvent exchange (shown in Fig. 3) did not show any difference in terms of droplet size at different locations of the substrate. The observations suggest that the duration of the solvent exchange at a given location on the surface is not related to the flow direction. That is, the earlier formed droplets also stop growing earlier. A video of the solvent exchange with millisecond temporal resolution is available in the ESI† (Video S1).

The extended time series of TIRF images in Fig. 3 show the droplet growth during the solvent exchange from the beginning to the end at  $\sim 24$  s. For six different flow rates from  $25 \mu\text{l min}^{-1}$  to  $150 \mu\text{l min}^{-1}$ , the number density, size and surface coverage of droplets were different not only at the end of the growth process, but also exhibited contrasting dynamics during the growth process. For the slowest flow rate  $Q = 25 \mu\text{l min}^{-1}$ , the nanodroplets were clearly smaller in size and grew mostly isolated from one another for the entire solvent exchange.

At a flow rate  $Q = 35 \mu\text{l min}^{-1}$  however, the number of droplets started to decrease from several incidents of droplet coalescence from 8 s onward. At an even faster flow rate  $Q = 50 \mu\text{l min}^{-1}$ , the droplets were much more crowded on the surface than those formed for the two slower flow rates. Then at faster flow rates of  $75$ – $150 \mu\text{l min}^{-1}$ , the decrease in the number density from droplet coalescence was particularly noticeable and was evident at earlier time intervals as the flow rate was increased. Below we will refer to  $25 \mu\text{l min}^{-1}$  and  $35 \mu\text{l min}^{-1}$  as slow flow rates,  $50 \mu\text{l min}^{-1}$  as the intermediate flow rate and  $75$ – $150 \mu\text{l min}^{-1}$  as fast flow rates.

The quantitative analysis of individual droplet radius, droplet number, surface coverage and droplet volume per unit area, all as a function of time is provided in Fig. 4(A–D). The droplet base radius  $R$  as a function of time  $t$  is obviously greatly influenced by the coalescence. Fig. 4(A) shows the radius of two representative growing droplets that did not experience any coalescence in the given time window. The size of individual droplets rapidly increased first and then slowly approached a plateau. The growth time was obviously longer as the flow rate decreased from  $Q = 150 \mu\text{l min}^{-1}$  to  $Q = 75 \mu\text{l min}^{-1}$ . In the following section, the dependence of individual droplet radius as a function of time will be analysed in greater detail to precisely extract the duration of the droplet growth.

The plot in Fig. 4(B) reveals the transition of different stages in the number density of droplets corresponding to different flow rates. For slow flow rates, the initial nucleation yielded a relatively slow increase in droplet number between  $\sim 0.1$  s and 1 s. There was then a rapid increase in the droplet number until  $\sim 10$  s, beyond which the droplet number remained unchanged. For the intermediate and fast flow rates, the rapid rise in the droplet number already finished in  $\sim 3$  s and  $\sim 1$  s, respectively. After the droplet number peaked, there was a subsequent reduction due to droplet coalescence, in particular for fast flow rates. At the end of the droplet growth, the highest droplet number density was achieved at an intermediate flow rate  $Q = 50 \mu\text{l min}^{-1}$ . Interestingly, Fig. 3 also showed that the final droplet size was clearly smaller at  $Q = 50 \mu\text{l min}^{-1}$  than at  $Q = 35 \mu\text{l min}^{-1}$ . Given the droplets are effectively competing for local oversaturation, the reduced size can be attributed to the higher number density during the growth process, which leads to increased competition between neighbouring droplets.

The plot of surface coverage vs. time in Fig. 4(C) shows an early stage of fast increase and a late stage of slow increase.

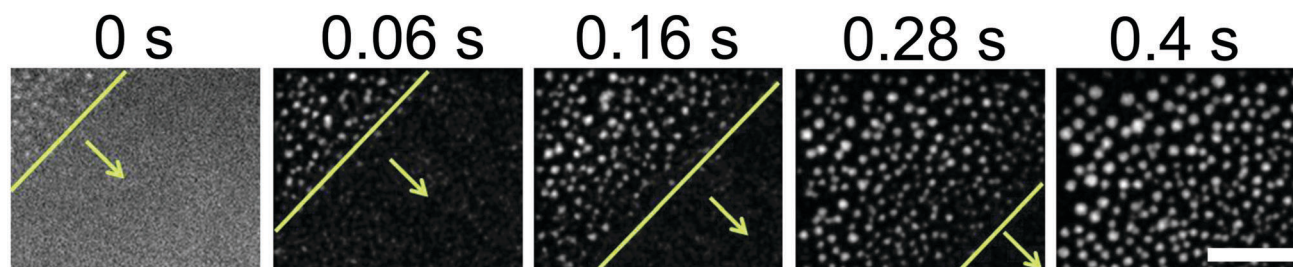


Fig. 2 TIRF images showing the formation of 1-octanol surface droplets along the flow direction during solvent exchange with a flow rate of  $150 \mu\text{l min}^{-1}$ . The arrow and tilted line emphasize the progressive nucleation across the substrate, from the upper left to lower right corners of the field of view. The time of the snapshots from left to right is  $\sim 0$  ms, 62 ms, 155 ms, 279 ms and 403 ms. Scale bar =  $10 \mu\text{m}$ .



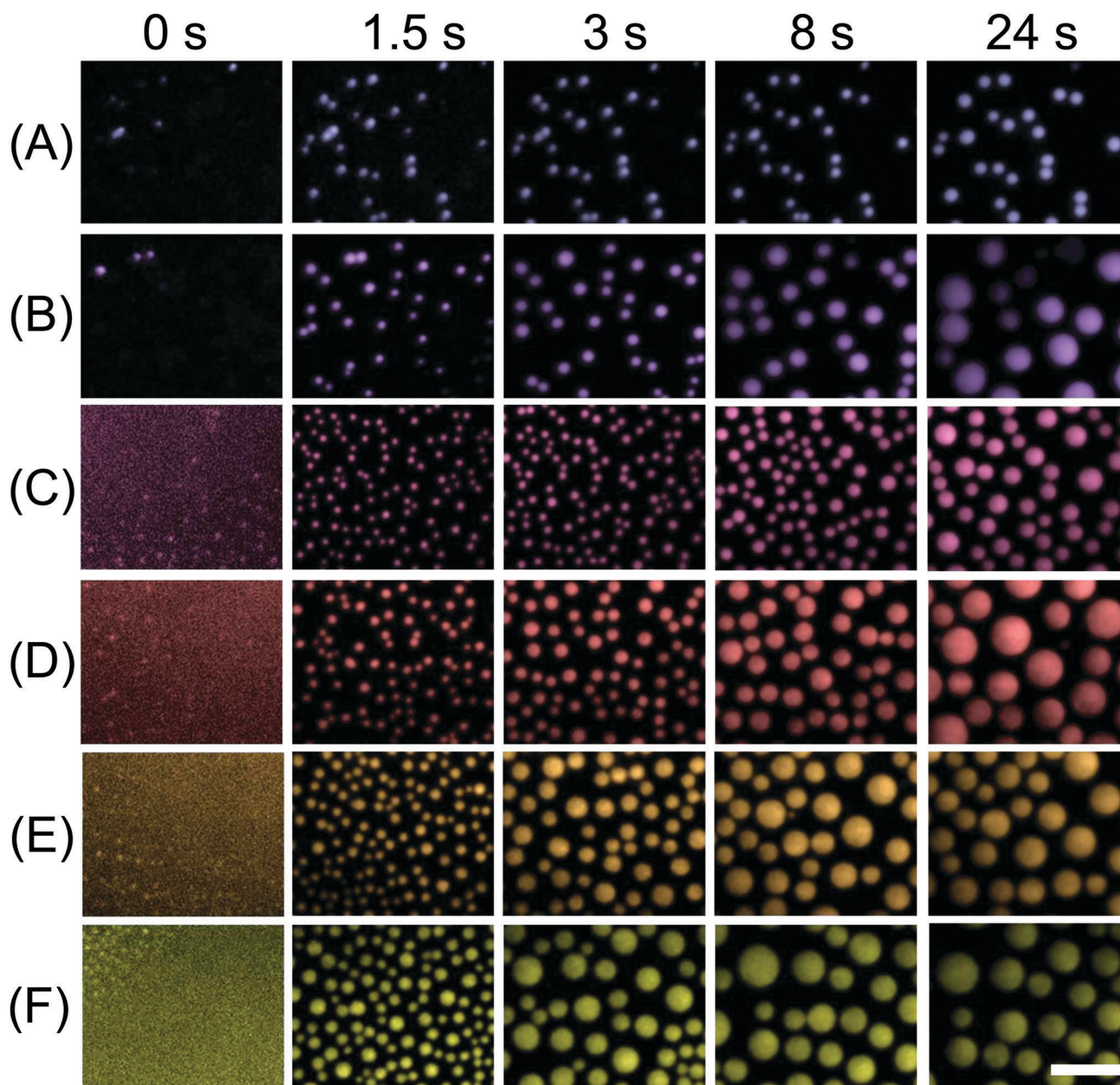


Fig. 3 Snapshots of surface droplets growing during the solvent exchange. From the top to bottom row, the flow rates, differentiated by colour, were (A)  $25 \mu\text{l min}^{-1}$  (blue), (B)  $35 \mu\text{l min}^{-1}$  (violet), (C)  $50 \mu\text{l min}^{-1}$  (pink), (D)  $75 \mu\text{l min}^{-1}$  (red), (E)  $100 \mu\text{l min}^{-1}$  (orange), (F)  $150 \mu\text{l min}^{-1}$  (yellow). For each flow rate, from left to right, the corresponding times of TIRF images were  $\sim 0$  s, 1.5 s, 3 s, 8 s and 24 s. The magnification of all the images in the panel is same. Scale bar =  $10 \mu\text{m}$ .

After the peak in droplet number at fast flow rates, the surface coverage of droplets still kept increasing. The terminal surface coverage was  $\sim 10\%$  at  $Q = 25 \mu\text{l min}^{-1}$ ,  $\sim 24\%$  at  $Q = 35 \mu\text{l min}^{-1}$  and remained to be  $\sim 37\%$  to  $\sim 45\%$  at all higher flow rates from  $50 \mu\text{l min}^{-1}$  to  $150 \mu\text{l min}^{-1}$ . The dependence of the final surface coverage of droplets on the flow rate is in agreement with what we found in ref. 24.

The coupled effects from temporal evolution of individual droplet size, surface coverage and number density led to a clear difference in the total volume of the droplets per unit surface area at different flow rates. Fig. 4D shows that the droplet

volume per unit area monotonically increases with time for fixed flow rates and with flow rate for a given duration. Below we will explain how the growth rate in droplet volume per unit area is related to the flow rate. The relation between the final total droplet volume per unit area  $V$  and the flow rate (expressed as  $Pe$ ) was devised in ref. 19, obtaining  $V \propto h^3 Pe^{3/4}$ . The explanation was based on diffusive droplet growth through a time-dependent concentration boundary layer given by the passing oversaturation pulse due to the mixing front. Extending the same idea, here we focus on the dynamics of the growth process.



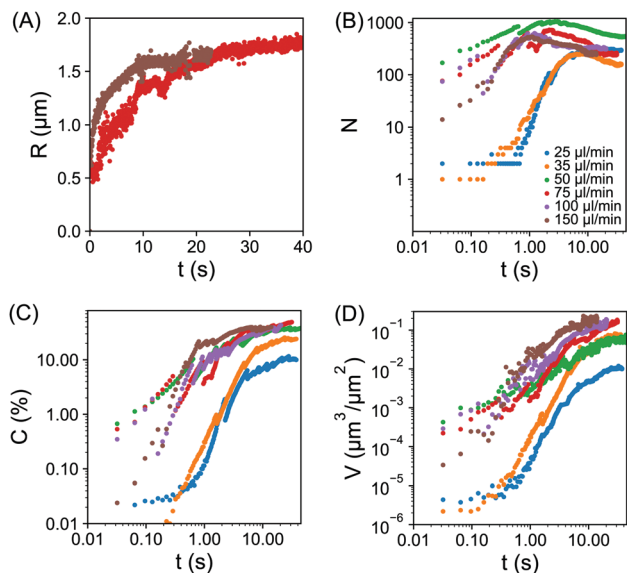


Fig. 4 (A) Plot of droplet base radius  $R$  vs. time  $t$ , for two representative growing droplets. The individual droplets did not experience coalescence in the given time window. The flow rates of the solvent exchange were  $75 \mu\text{l min}^{-1}$  (red) and  $150 \mu\text{l min}^{-1}$  (brown). For clarity, only two flow rates are shown here, results for additional flow rates are included within the ESI,† Fig. S1. (B–D) log–log plot of the number of droplets  $N$  in (B), the surface coverage  $C$  in (C), the droplet volume per unit area  $V$  in (D) all as a function of time  $t$ . The flow rate as labelled by different colors was  $25 \mu\text{l min}^{-1}$  (blue),  $35 \mu\text{l min}^{-1}$  (orange),  $50 \mu\text{l min}^{-1}$  (green),  $75 \mu\text{l min}^{-1}$  (red),  $100 \mu\text{l min}^{-1}$  (purple) and  $150 \mu\text{l min}^{-1}$  (brown). Plots B–D begin from the initial frame ( $\sim 30$  ms) prior to droplet detection.

### 3.2 Theoretical analysis of droplet growth dynamics

Assuming the droplet grows with a constant contact angle, the growth of an individual droplet is given by the diffusion equation,

$$\dot{m} = 4\pi\rho_{\text{oil}}R^2\dot{R} = 4\pi DR^2\partial_r c|_R, \quad (1)$$

where  $m$  and  $\rho$  are the droplet mass and density, respectively. Owing to the low contact angle of the droplets, we assume a scaling which would apply to a flat surface. The concentration gradient at the droplet surface  $\partial_r c|_R$ , is given by the difference between the concentration of the oil in the liquid far away from the droplet  $c_\infty$ , and the concentration at the droplet surface  $c_s$ , given by the solubility of oil and the boundary layer with the thickness  $\lambda \sim R/\sqrt{\text{Pe}}$  of the droplet in a laminar flow,  $\partial_r c|_R = (c_\infty(t) - c_s)/\lambda(t) \propto (c_\infty(t) - c_s)\sqrt{\text{Pe}}/R(t)$ . This can be integrated over time leading to

$$\int_0^{R(t)} R dR \sim \frac{Dc_s}{\rho} \sqrt{\text{Pe}} \int_{-\infty}^t \zeta(t) dt. \quad (2)$$

We now consider the shape of the oversaturation pulse,  $\zeta(t) = c_\infty(t)/c_s - 1$ , to be Gaussian,

$$\zeta(t) = \frac{c_\infty(t)}{c_s} - 1 = \zeta_{\text{max}} e^{-(t-t_0)^2/2\tau^2} \quad (3)$$

where  $\zeta_{\text{max}}$  is the maximal oversaturation and  $\tau$  is the duration of the oversaturation pulse. With the definition of the error

function,  $\text{Erf}(x) = \frac{2}{\sqrt{\pi}} \int_0^x e^{-y^2} dy$ , we then obtain

$$(R(t))^2 \sim \frac{Dc_s}{\rho} \sqrt{\text{Pe}} \zeta_{\text{max}} \tau \text{Erf}\left(\frac{t-t_0}{\sqrt{2}\tau}\right) \quad (4)$$

The shear flow in solvent exchange corresponds to a non-uniform, parabolic flow velocity distribution within the channel; with the highest velocity in the middle of the channel and a parabolically decreasing velocity approaching the channel walls. As described by Taylor–Aris dispersion,<sup>21–23</sup> the velocity profile creates enhanced concentration gradients, which in turn enhance the radial diffusion of the solute. This effectively results in a ‘smearing out’ of the concentration distribution in flow direction. Consequently, it is expected that  $\zeta_{\text{max}} \sim \text{Pe}^{1/2}$  and  $\tau \sim h^2 \text{Pe}^{-1/2}/D$ , reflecting that at a fixed position downstream for large advection velocity the blob of oversaturation will be smeared out less as less time has passed.<sup>20</sup> Thus  $\zeta_{\text{max}} \tau \sim h^2/D$ ,<sup>20</sup> resulting in

$$(R(t))^2 \sim h^2 \frac{c_s}{\rho} \sqrt{\text{Pe}} \text{Erf}\left(\frac{t-t_0}{\sqrt{2}\tau}\right) \quad (5)$$

or

$$\begin{aligned} V(t) &\sim (R(t))^3 \sim h^3 \left(\frac{c_s}{\rho}\right)^{3/2} \text{Pe}^{3/4} \left\{ \text{Erf}\left(\frac{t-t_0}{\sqrt{2}\tau}\right) \right\}^{3/2} \\ &\sim V_f(\text{Pe}) \cdot \left\{ \text{Erf}\left(\frac{t-t_0}{\sqrt{2}\tau}\right) \right\}^{3/2} \end{aligned} \quad (6)$$

where  $V(t)$  and  $V_f(\text{Pe})$  denote the volume and final volume. To verify this relation, the normalized volume  $V(t)/V_f$  versus time and its best fit to eqn (6) are shown in Fig. 5. Eqn (6) includes two fitting parameters, the pulse width  $\tau$  and the initial  $t_0$ . Here  $t = 0$  is defined as immediately prior ( $\sim 30$  ms) to the initial detection of the surface droplets. Accordingly,  $t_0 = 0$  s was fixed in all cases. The normalized volume shows a sharp increase before approaching the plateau near the final droplet volume. The experimental data are well fitted by the error function result eqn (6), particularly at the lower flow rates. However, there was some noise in the measurements which could not be avoided. The high frame rate captures intermediate stages of coalescence; the non-equilibrium morphology introduces error to the volume calculations which assumes a spherical cap. As one may expect, this is more prominent for the fast flow rates which exhibited increased droplet coalescence.

From fittings of the droplet volume as a function of time shown in Fig. 5, the oversaturation pulse duration  $\tau$  for different flow rates was obtained and plotted against  $\text{Pe}$  in Fig. 6. The plot revealed that the pulse duration indeed decreased with increases in  $\text{Pe}$ . Moreover, the fittings indicates  $\tau \sim \text{Pe}^{-1/2}$ . This result demonstrates the mixing behaviour during solvent exchange is well described Taylor–Aris dispersion.<sup>20–23</sup>

### 3.3 Growth time determined from temporal evolution of individual droplets

The growth time was also quantified by the evolution of individual droplet radii at different flow rates, as represented in Fig. 4A. Results for the additional flow rates are provided in



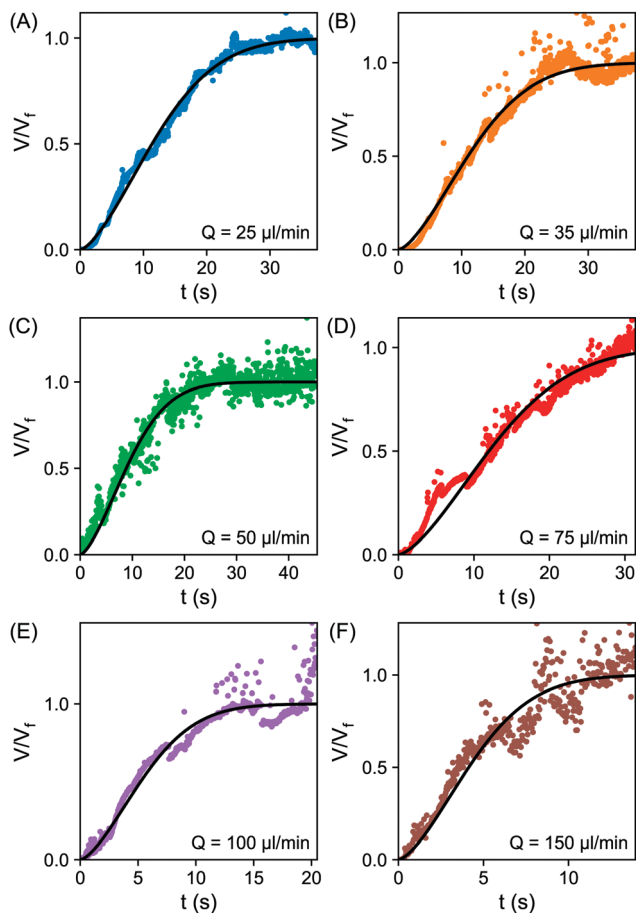


Fig. 5 (A–F) Plot of the normalized volume  $V/V_f$  vs. time  $t$  for varying flow rates; (A)  $25 \mu\text{l min}^{-1}$  (B)  $35 \mu\text{l min}^{-1}$  (C)  $50 \mu\text{l min}^{-1}$  (D)  $75 \mu\text{l min}^{-1}$  (E)  $100 \mu\text{l min}^{-1}$  (F)  $150 \mu\text{l min}^{-1}$ . The fitting to the error function eqn (6) is shown as the solid black line.

the  $\text{ESI}^\dagger$  (Fig. S1). The droplets grew to a final (plateau) droplet size  $R_{\text{max}}$ , determined by averaging values in the plateau. The corresponding growth duration, called  $\sigma$ , was estimated as the time required to achieve  $0.9R_{\text{max}}$ , as indicated by the fitting lines in Fig. S1 ( $\text{ESI}^\dagger$ ). As a result,  $\sigma$  encompasses most of the growth duration while minimizing noise from the end of the experiment, where the change in droplet size becomes increasingly minor.

The growth times  $\sigma$  of the droplets for different flow rates are plotted as a function of  $\text{Pe}$  number in Fig. 6, together with the previously identified time scales  $\tau$ , showing reasonable agreement. The fitting of the data shows good agreement with  $\tau \sim \sigma \sim \text{Pe}^{-1/2}$ . This result further confirms the scaling of growth time with the  $\text{Pe}$  number based on fitting of the droplet volume by error functions in Fig. 5. Note that the values for  $\tau$  are slightly lower than those for  $\sigma$  obtained from the direct droplet radius measurements. This is reasonable as  $\tau$  represents the time scale of the Gaussian peak width (oversaturation pulse width), not necessarily encompassing the entire growth duration.

### 3.4 Dynamics of droplet coalescence

Now we provide more analysis of the droplet coalescence, based on the data from the TIRF measurements. As demonstrated in

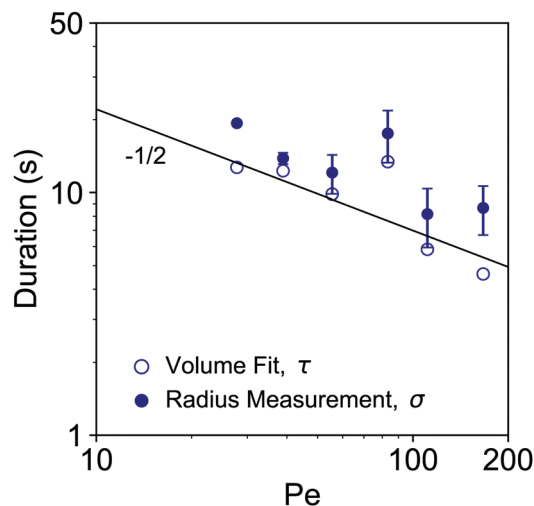
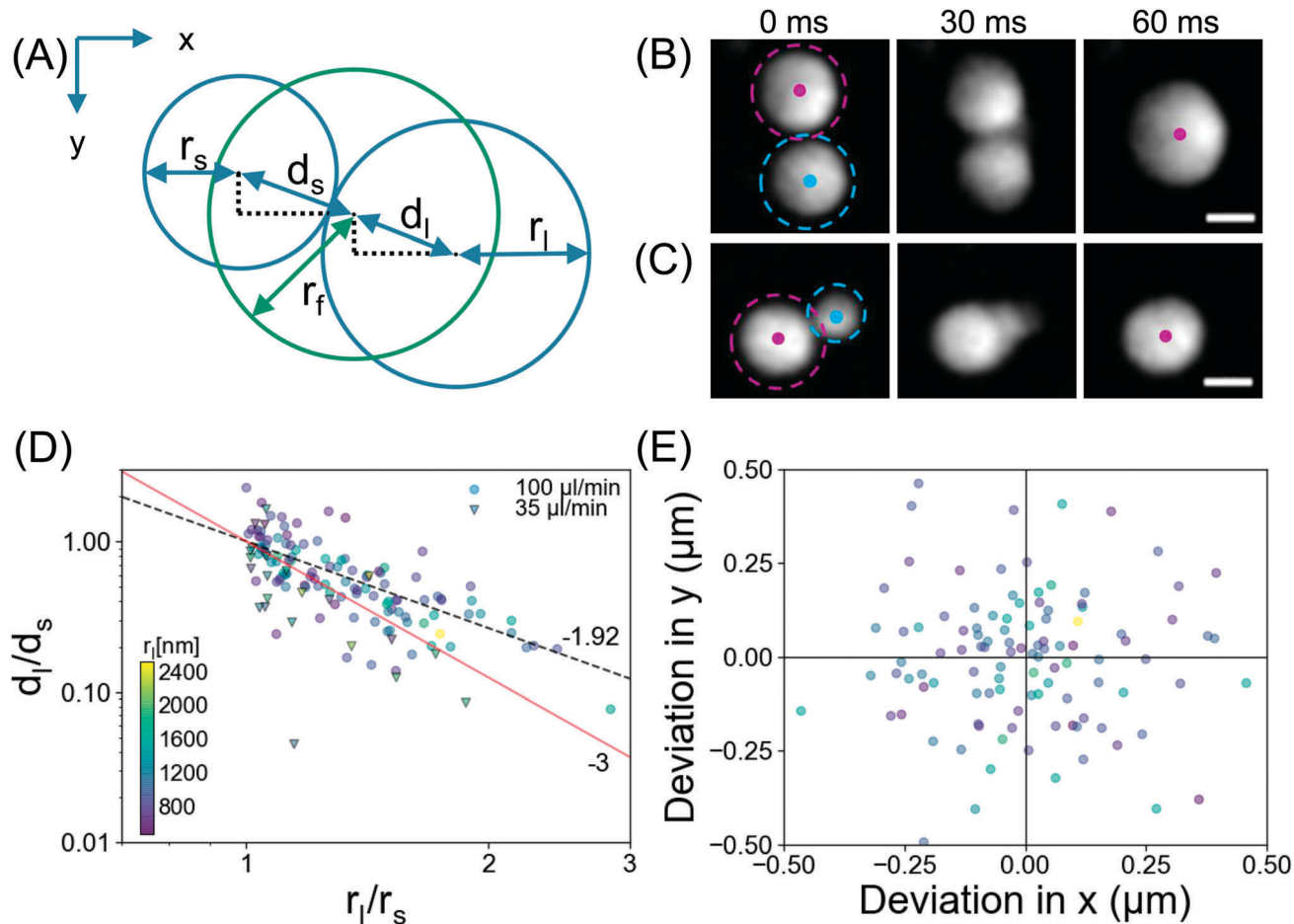


Fig. 6 log–log plot of the growth durations as a function of  $\text{Pe}$ . The growth duration was determined by two approaches. The timescale  $\tau$  obtained from the fitting of the droplet volume per unit area by error functions in Fig. 5 is labelled by open circle markers. The duration  $\sigma$  based on the temporal evolution of the individual droplet radius is labelled by the filled circle markers. The predicted slope of  $-1/2$  is shown as solid black line.

Fig. 3, after the surface coverage reaches a certain threshold, coalescence is the determinant process in droplet growth. Representative snapshots in Fig. 7B and C show two coalescence events at  $Q = 100 \mu\text{l min}^{-1}$  with an interval of 30 ms. The images reveal bridging of the droplets, as reported for larger droplets in literature.<sup>29–31</sup> Fig. 7B shows coalescence between droplets of similar sizes,  $r_s = 1.34 \mu\text{m}$ ,  $r_l = 1.57 \mu\text{m}$ . Here the final droplet position was observed to be in the middle of the two parent droplets. Fig. 7C shows coalescence between droplets of dissimilar sizes,  $r_s = 0.97 \mu\text{m}$ ,  $r_l = 1.47 \mu\text{m}$ , where the final droplet position was nearer to the larger parent droplet.

To quantify the droplet positions, the relevant centroids and sizes of the smaller, larger and final droplets during the coalescence process were determined as depicted in Fig. 7A. Assuming a constant contact angle mode (thus  $r^3 \sim V$ ), the theoretical centre of mass was determined from the radii of the parent droplets. The ratio of displacement for the large/small droplet is plotted against the size ratio of large/small in Fig. 7D. The experimental data for displacement was fitted (dashed black line) with the power law,  $d_l/d_s \sim (r_l/r_s)^{-p}$ , yielding an exponent  $p = 1.92$  (standard error = 0.18,  $R^2 = 0.68$ ). The fitting of the power law indicates that there is a coalescence preference, namely the final droplet is located closer to the larger parent. This observation resembles the behavior of microdroplets.<sup>32–34</sup> Also in our latest work, we showed that nanodroplets around the rim of a microcap demonstrated a coalescence preference with a similar exponent  $p = 2.08$ .<sup>35</sup> The coalescence preference was attributed to the balance of the capillary force ( $F = 2\pi\gamma r_{\text{min}}$ ) which brings the droplet together, against the force required to overcome the contact angle hysteresis. The strength of the latter depends on the contact area of the droplet with the substrate,<sup>36</sup> ( $F/r_n^2$ ), thus  $d_l/d_s \sim (r_l/r_s)^{-2}$ , yielding the theoretical exponent of  $p = 2$ .





**Fig. 7** (A) Schematic depiction of droplet radii ( $r$ ) and displacements ( $d$ ) during coalescence. The subscripts  $s$ ,  $l$  and  $f$  denote small, large, and final, respectively. (B) Coalescence between two similar sized droplets. The centroid of each droplet is indicated by the coloured dots. The smaller ( $r_s = 1.34 \mu\text{m}$ ) and larger ( $r_l = 1.57 \mu\text{m}$ ) droplets are encircled by purple and green, respectively. The final droplet is located evenly between the two parent droplets. Scale bar =  $2 \mu\text{m}$ . (C) Coalescence between two dissimilar sized droplets. The smaller ( $r_s = 0.97 \mu\text{m}$ ) and larger ( $r_l = 1.47 \mu\text{m}$ ) droplets are encircled by purple and green, respectively. The final droplet position is closer to the larger parent droplet. Scale bar =  $2 \mu\text{m}$ . (D) log–log plot of displacement ratio vs. parent droplet size ratio,  $d_l/d_s$  vs.  $r_l/r_s$ . The experimental data for  $Q = 100 \mu\text{l min}^{-1}$  and  $Q = 35 \mu\text{l min}^{-1}$  are shown as coloured circles and dark-edge triangles, respectively. The best experimental power law fit,  $d_l/d_s \sim (r_l/r_s)^{-p}$ , with  $p = 1.92$  (the dashed black line) and the power law from the centre of mass (CM) prediction ( $p = 3$ ) are shown (the solid red line) as comparison. (E) Deviation in final position from centre of mass prediction. The symbols in (D) and (E) are coloured by  $r_l$ .

This agrees well with the observed exponent determined here ( $p = 1.92$ ) and in ref. 35 ( $p = 2.08$ ).

To examine whether the preference in the droplet position shift is related to the direction or rate of the external flow, we define the final position from the centre of mass calculation in  $x$  and  $y$  directions as shown in Fig. 7E. Based on the experimental data for coalescence during exchange at  $Q = 35 \mu\text{l min}^{-1}$  and  $Q = 100 \mu\text{l min}^{-1}$ , we did not observe any correlation between the position shift of the droplets and the direction or rate of the flow. Therefore, the droplet coalescence seemed to be independent of the flow conditions.

## 4 Conclusions

The nucleation and growth of surface nanodroplets by solvent exchange on a homogeneous substrate was revealed by TIRF

with high temporal and spatial resolution. During the solvent exchange surface droplets nucleated along the flow direction. In subsequent droplet growth, the surface coverage and droplet number exhibited a rapid increase at early stage and reached plateaus at later stages, whose values depend on the flow rate. The duration of droplet growth, determined in two different ways, scales as  $\sim \text{Pe}^{-1/2}$ , as one would expect from Taylor–Aris dispersion. At sufficient surface coverage, droplets coalesce. The coalescence process exhibited a preference in position shift according to the relative droplet sizes. In addition, the position shift at droplet coalescence was independent of flow rate and direction. The quantitative understanding of droplet growth with time and position shifting rules will further enable the modelling of the solvent exchange process as well as aid the experimental design for controlling droplet morphology. In particular, the improved understanding of droplet growth dynamics will facilitate future use of droplet templates for





engineering functional surface structures. The findings of this work may also be applied to the understanding of microphase formation in general. Beyond this, the experimental methodology utilized herein invites future studies in areas such as the wetting behaviour of submicron droplets.

## Conflicts of interest

There are no conflicts to declare.

## Acknowledgements

We thank Hao Hao for assistance in the analysis of droplet coalescence. X. H. Z. acknowledges the support from the Australian Research Council (FT120100473, LP140100594) and from Start-up Fund from the Faculty of Engineering and funding support of Future Energy Systems in University of Alberta. We also acknowledge the RMIT MicroNano Research Facility for providing access to equipment and resources. This work was supported by the Netherlands Center for Multiscale Catalytic Energy Conversion (MCEC), an NWO Gravitation programme funded by the Ministry of Education, Culture and Science of the government of the Netherlands. Open Access funding provided by the Max Planck Society.

## Notes and references

- 1 K. Stephan, *Heat transfer in condensation and boiling*, Berlin, Springer-Verlag, 1992.
- 2 D. Beysens, A. Steyer, P. Guonoun, D. Fritter and C. M. Knobler, *Phase Transitions*, 1991, **31**, 219–446.
- 3 D. Beysens, *Physique* 7, 2006, **7**, 1082–1100.
- 4 J. Ju, H. Bai, Y. Zheng, T. Zhao, R. Fang and L. Jiang, *Nat. Commun.*, 2012, **3**, 1247.
- 5 U. H. F. Bunz, *Adv. Mater.*, 2006, **18**, 973–989.
- 6 N. Noor, J. Koll, C. Abetz, H. Notzke and V. Abetz, *Sci. Rep.*, 2017, **7**, 8050.
- 7 N. Miljkovic, D. J. Preston, R. Enright and E. N. Wang, *Appl. Phys. Lett.*, 2014, **105**, 013111.
- 8 N. Miljkovic, R. Enright, Y. Nam, K. Lopez, N. Dou, J. Sack and E. N. Wang, *Nano Lett.*, 2013, **13**, 179–187.
- 9 A. Theberge, F. Courtois, Y. Schaeferli, M. Fischlechner, C. Abell, F. Hollfelder and W. Huck, *Angew. Chem., Int. Ed.*, 2010, **49**, 5846–5868.
- 10 J. Shemesh, T. B. Arye, J. Avesar, J. H. Kang, A. Fine, M. Super, A. Meller, D. E. Ingber and S. Levenberg, *Proc. Natl. Acad. Sci. U. S. A.*, 2014, **111**, 11293–11298.
- 11 M. Kuang, L. Wang and Y. Song, *Adv. Mater.*, 2014, **26**, 6950–6958.
- 12 D. Kang, C. Pang, S. M. Kim, H. S. Cho, H. S. Um, Y. W. Choi and K. Y. Suh, *Adv. Mater.*, 2012, **24**, 1709–1715.
- 13 A. Piqué, *Appl. Phys. A: Mater. Sci. Process.*, 2011, **105**, 517–528.
- 14 H. Li, Q. Yang, G. Li, M. Li, S. Wang and Y. Song, *ACS Appl. Mater. Interfaces*, 2015, **7**, 9060–9065.
- 15 Y. Yamada, T. Ikuta, T. Nishiyama, K. Takahashi and Y. Takata, *Langmuir*, 2014, **30**, 14532–14537.
- 16 B. Dyett, H. Yu and X. Zhang, *Eur. Phys. J. E: Soft Matter Biol. Phys.*, 2017, **40**, 26.
- 17 H. Yu, S. Peng, L. Lei, J. W. Zhang, T. L. Greaves and X. Zhang, *ACS Appl. Mater. Interfaces*, 2016, **8**, 22679–22687.
- 18 D. Lohse and X. Zhang, *Rev. Mod. Phys.*, 2015, **87**, 981.
- 19 X. Zhang, Z. Lu, H. Tan, L. Bao, Y. He, C. Sun and D. Lohse, *Proc. Natl. Acad. Sci. U. S. A.*, 2015, **112**, 9253–9257.
- 20 H. Yu, S. Maheshwari, J. Zhu, D. Lohse and X. Zhang, *Lab Chip*, 2017, **17**, 1496–1504.
- 21 R. Aris, *Proc. R. Soc. London, Ser. A*, 1956, 67–77.
- 22 R. Aris, *Proc. R. Soc. London, Ser. A*, 1959, 538–550.
- 23 G. Taylor, *Proc. R. Soc. London, Ser. A*, 1953, 186–203.
- 24 C. Xu, H. Yu, S. Peng, Z. Lu, L. Lei, D. Lohse and X. Zhang, *Soft Matter*, 2017, **13**, 937–944.
- 25 D. Axelrod, *Methods Cell Biol.*, 1989, **30**, 245–270.
- 26 C. U. Chan and C. D. Ohl, *Phys. Rev. Lett.*, 2012, **109**, 1–5.
- 27 C. U. Chan, M. Arora and C.-D. Ohl, *Langmuir*, 2015, **31**, 7041–7046.
- 28 M. Lessel, O. Baumchen, M. Klos, H. Hahl, R. Fetzer, M. Paulus, R. Seemann and K. Jacobs, *Surf. Interface Anal.*, 2014, **47**, 557–564.
- 29 J. Eggers, J. R. Lister and H. A. Stone, *J. Fluid Mech.*, 1999, **401**, 293–310.
- 30 J. Hernández-Sánchez, L. Lubbers, A. Eddi and J. H. Snoeijer, *Phys. Rev. Lett.*, 2012, **109**, 184502.
- 31 A. Eddi, K. Winkels and J. H. Snoeijer, *Phys. Rev. Lett.*, 2013, **111**, 144502.
- 32 B. M. Weon and J. H. Je, *Phys. Rev. Lett.*, 2012, **108**, 224501.
- 33 Y. Kim, S. J. Lim, B. Gim and B. M. Weon, *Sci. Rep.*, 2014, **5**, 7739.
- 34 R. Chen, H. W. Yu, L. Zhu, R. M. Patil and T. Lee, *Am. Inst. Chem. Eng.*, 2017, **63**, 1441–1450.
- 35 B. Dyett, H. Hao, D. Lohse and X. Zhang, *Soft Matter*, 2018, **14**, 2628–2637.
- 36 F. Chu, X. Wu, Y. Zhu and Z. Yuan, *Int. J. Heat Mass Transfer*, 2017, **111**, 836–841.

