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Investigation on the role of interfacial water on the tribology between graphite and metals

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We investigated the role of interfacial water on the atomic-scale tribology of graphite by contact atomic force microscopy. Upon the approach of Au and Pt tips toward graphite in water, the hydration layers on the respective surfaces interact with each other. This results in a discontinuous motion of the metallic tips towards the graphite surface. Snap-in forces measured with Au and Pt tips scale with their respective water adsorption energies. Moreover, we observed significant differences for the atomic-scale friction between the Au and Pt tips and graphite in water. The atomic-scale sliding friction between an Au tip and graphite is characterized by low friction forces ($F_f < 1$ nN in the range of normal force values $F_n = 1$ –10 nN) and by a periodic stick-slip that corresponds to the honeycomb structure of graphite. With a Pt tip, the sliding friction on graphite in water is characterized by high friction forces ($F_f \approx 5$ nN in the range of normal force values $F_n = 1$ –10 nN) and by an atomic-scale stick-slip whose characteristic lengths may correspond to an ordered water adsorption layer between platinum and graphite.

A Introduction

The lubricating effect of graphite arises on the one hand from its weakly bonded basal planes that exhibit low resistance to shearing. Moreover, the lubrication of graphite has early been reported to depend on adsorbed layers that decrease the cohesion of graphite surfaces.^{1–3} In vacuum, graphite wears by dusting with a correspondingly high friction coefficient. For graphite rods or brushes sliding on copper, a friction coefficient of $\mu = 0.8$ has been measured in vacuum. For the same tribological couple exposed to water vapor, wear was found to vanish with a corresponding decrease in the friction coefficient to $\mu = 0.18$.¹ Savage discussed these results based on the condensation of water vapor on graphite. Byrant *et al.* made similar observations on the effect of water vapor on the lubrication of graphite.² In these studies, the authors discussed that in the presence of water vapor, the interlayer binding energy of graphite is significantly decreased when compared to that in the ultra-high vacuum conditions. Buckley and Brainard investigated the friction and wear of metals sliding on the prismatic and basal graphitic planes in different environments (high vacuum, HBr, O₂, H₂O vapor, and C₂H₂).⁴ For all of the tested metals (Au, Fe, and Ta), the friction was lower for the basal than the prismatic orientation of graphite. Coincidentally, the tested metals were all observed to transfer onto the prismatic surface of graphite but not on its basal surface. Material transfer was however completely inhibited by the presence of physically adsorbed oxygen, water vapor, and acetylene. These results highlight the

effect of metal/graphite adhesion on friction and how it can be inhibited by interfacial adsorbate layers.

Recently, the friction of graphite has been experimentally revisited by means of atomic force microscopy. Such experiments allow the sliding of a single nm-scale asperity to be monitored as a function of both normal force and sliding velocity. The first of these experiments were conducted by Mate *et al.* with a tungsten tip.⁵ The authors observed a non-monotonous variation in the friction forces during sliding on the basal plane of graphite. The periodicity of these variations was found to correspond to the honeycomb structure of the graphitic surface. Jinesh and Frenken investigated the effect of humidity on the friction of graphite with a tungsten tip.⁶ At low relative humidity (up to 1%), the authors observed a stick-slip of motion with a periodicity corresponding to the honeycomb structure of graphite, as well. At larger relative humidity values (from 5% to 33%), an average stick-slip distance of 0.38 nm was derived and attributed to the crystalline structure of ice water. At a low scanning velocity, the presence of a crystalline water-adsorbed film gave rise to larger friction force values than those at low relative humidity. However, in immersed conditions, Vilhena *et al.* used Si₃N₄ tips to measure the atomic stick-slip on graphitic surfaces with a periodicity of their honeycomb structure.⁷

In this study, we investigated the role of interfacial water on the tribology of graphite in water with two different metallic tips, gold- and platinum-coated AFM tips. The structure of interfacial water and its effect on the snap-in, adhesion and friction forces between the tips and a graphite surface were probed by force spectroscopy, friction force microscopy, and spectral analysis. We discussed our results based on the

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reported structure and energetics of the adsorbed water on graphitic and metallic surfaces.

B Experimental

A graphitic surface was prepared by exfoliating the top layers of a highly oriented pyrolytic graphite (HOPG) sample with adhesive tape, followed by immersion in deionized water at $T = 295$ K. The as-prepared sample surface was then analyzed by atomic force spectroscopy and friction force microscopy using a XE-100 AFM, manufactured by Park Instruments, Republic of Korea. Both types of measurements were performed with an Au-coated cantilever (type contsc-Au, manufactured by NanoSensors, Switzerland) and a Pt-coated cantilever (type contsc-Pt, manufactured by NanoSensors, Switzerland). After measurements, the AFM tips were imaged by scanning electron microscopy and compared with pristine AFM tips of the same types (see Fig. 1). The measurements were also repeated with two different AFM cantilevers of each type to ensure the reproducibility of our results. In this study, only results obtained with single AFM tips of each of the aforementioned types are presented. In Fig. 1, a circle with a radius of 25 nm is overlaid on the apex of each tip. We observed that these circles matched well with the tip

dimension, except for the unused Pt tip, which has a tip radius slightly less than 25 nm.

Before the measurements were performed in water, the sensitivity of the photodiode was calibrated by recording a force–distance curve with each cantilever on a nanocrystalline thin film sample in air. Subsequently, the thermal vibration noise of the cantilevers was recorded in air and analysed accordingly to calculate the normal stiffness C_n of the cantilevers.⁸ After immersion in the water, the sensitivity of the photodiode was recalibrated by recording a force–distance curve with each cantilever on HOPG. The cantilevers' lateral stiffnesses C_l were then calculated according to the following formula:

$$C_l = \frac{4}{3} \frac{G}{E} \left(\frac{L}{h} \right)^2 C_n \quad (1)$$

Force spectroscopy measurements were performed at various approach/retraction velocities in the range of $dZ/dt = 50\text{--}2000$ nm s^{−1} and over a Z-range of 30 nm, corresponding to a maximal normal force $F_{n,\text{max}} \approx 20$ nN. For each approach/retraction velocity, 16 force–distance $F_n(Z)$ curves were recorded. The analysis of the $F_n(Z)$ curves consisted of extracting the snap-in force and the adhesion force values as a function of the

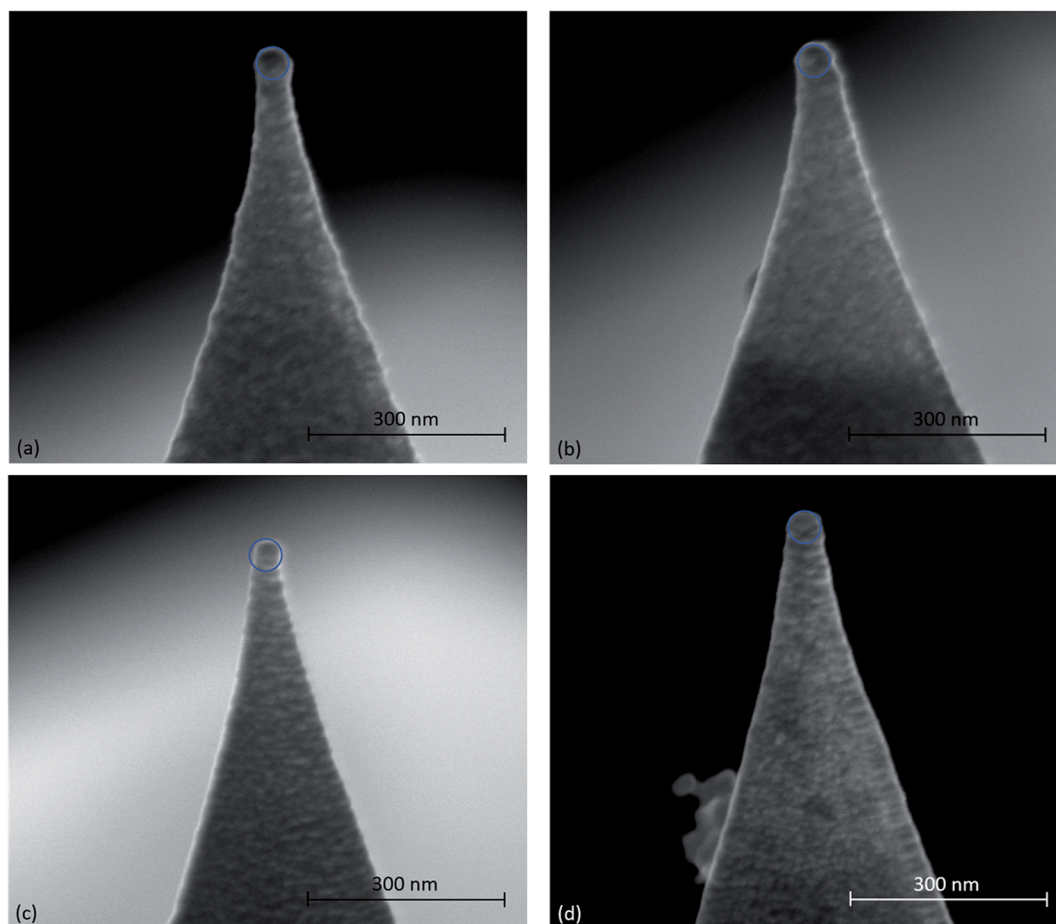


Fig. 1 SEM images of (a and c) pristine and (b and d) used tips during our tribological measurements on HOPG; (a and b) Au tips and (c and d) Pt tips. A blue-colored circle with a radius of 25 nm was overlaid on each tip apex.



approach/retraction velocity. Force-penetration $F_n(\delta)$ curves were also calculated by subtracting the cantilever deflection from the cantilever position, *i.e.*,

$$\delta = Z - \frac{F_n}{C_n} \quad (2)$$

Friction measurements were performed over a scan area of $10 \times 10 \text{ nm}^2$ with a scanning velocity of 200 nm s^{-1} over a range of normal force values $F_n = 1\text{--}10 \text{ nN}$. The friction measurements were repeated twice at each normal force value. Friction force maps were calculated according to the following formula

$$F_f = \frac{3}{2} C_1 \frac{h}{L} S \left(\frac{F_{\text{lat,forw}} - F_{\text{lat,backw}}}{2} \right) \quad (3)$$

and were averaged line by line to calculate an average friction force value F_f . Corresponding error values were calculated from the standard deviation of the calculated mean values for each line of the friction maps. Further, the power spectral density (PSD) functions of the friction force microscopy images were calculated as described by Ko *et al.*⁹

C Results and discussion

Fig. 2 compares typical $F_n(Z)$ and $F_n(\delta)$ curves recorded under water on HOPG with Au-coated and Pt-coated tips. Upon both the approach and retraction of the tip towards/from the immersed HOPG surface, we observed distinct snap-in and detachment events in the force-distance curves that correspond to the sudden jumps of magnitude $\Delta\delta_{1,2}$ toward the immersed HOPG surface. In Fig. 2, the zero position of the Z-scanner was

Table 1 Snap-in distances $\Delta\delta_i$ extracted from force spectroscopy measurements and wavenumbers k_i extracted from friction force measurements

	$\Delta\delta_1$	$\Delta\delta_2$	k_1	k_2	k_3	k_4
	[pm]		[rad nm ⁻¹]			
Au	616	359	25.76	49.01	—	—
Pt	770	433	11.62	16.96	22.62	28.9

arbitrarily set to correspond to the minimum normal force value of the approach toward the immersed HOPG surface. For both Au- and Pt-coated tips, the magnitudes of these jumps are listed in Table 1.

The magnitudes of the jumps observed with a Pt-coated tip are ~ 1.2 larger than those with an Au-coated tip. The maximum snap-in force $F_{\text{Snap-in}}$ values also significantly differed with the tip chemistry and only showed weak associations with the approaching velocity. In the case of the Au-coated tip, we found $F_{\text{Snap-in}} = -0.52 \pm 0.09 \text{ nN}$, while for the Pt-coated tip we found $F_{\text{Snap-in}} = -2.95 \pm 0.24 \text{ nN}$. The difference in the adhesion force F_{ad} values between the immersed HOPG and the Au-coated and Pt-coated tips were significantly larger. For both tips, the F_{ad} values also showed weak variations with the retraction velocity. In the case of the Au-coated tip, we found $F_{\text{ad}} = -1.23 \pm 0.11 \text{ nN}$, while for a Pt-coated tip we found $F_{\text{ad}} = -9.95 \pm 0.21 \text{ nN}$.

The geometries and energetics of the adsorbed water on Pt(111) were calculated by an *ab initio* molecular dynamics simulation.¹⁰ For a bilayer forming a $\sqrt{39} \times \sqrt{39}$ super-cell on Pt(111), a water bilayer was found to have thickness between 210

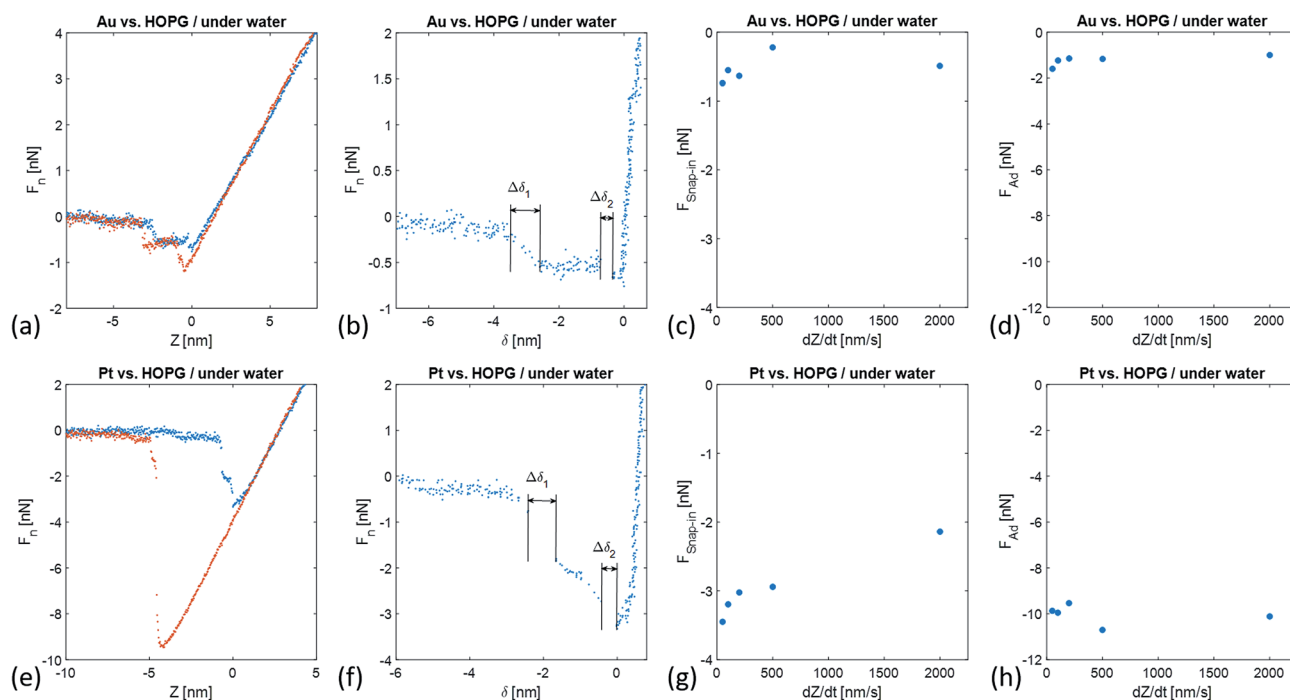


Fig. 2 (a and e) F_n - Z curves, (b and f) F_n - δ curves, and corresponding (c and g) $F_{\text{Snap-in}}$ (dZ/dt) and (d and h) F_{ad} (dZ/dt)-plots recorded under water on HOPG with (a–d) an Au-coated AFM-tip and (e–h) a Pt-coated AFM-tip. In (a and e) the blue data points correspond to the approach of the Z-scanner towards the sample surface, and the orange data points to its retraction from the sample surface.



pm and 440 pm and a corresponding adsorption energy $E_{\text{ads}} = -0.615$ eV. In the case of the Au(111) surface, the thickness of the different types of adsorbed water layers was found to vary between 361 pm and 399 pm with corresponding adsorption energies in the range of $E_{\text{ads}} = -0.15$ eV and $E_{\text{ads}} = -0.11$ eV.¹¹ In the case of graphene, the thickness of the adsorbed water layer was computed to be ~ 300 pm,¹² while the adsorption energy was measured on the carbon nanotubes to be ~ -0.25 eV.¹³ It is noteworthy that the ratio of the snap-in forces for the Pt tip and the Au tip, $\frac{F_{\text{snap-in}}^{\text{Pt}}}{F_{\text{snap-in}}^{\text{Au}}} \approx 5.58$, was close to the

ratio of the water adsorption energies on the same metals, *i.e.*, $\frac{E_{\text{ads}}^{\text{Pt}}}{E_{\text{ads}}^{\text{Au}}} \approx 4.61$.

During force spectroscopy measurements in air or ultra-high vacuum, the snap-in of the AFM tip onto a surface is a fast process. In Fig. 2, the approach of metal tips toward an immersed HOPG surface consists of two types of processes: fast and slow. At large distance of metal tips from the HOPG surface the approach velocity follows the programmed value. In the case of an Au tip approaching towards immersed HOPG, we first observed an increase in the approach velocity, 3.345 nm away from the minimal snap-in force value and within the range of δ values $\Delta\delta_1 = 616$ pm. During this first attraction process, a force decrease of $\Delta F_1 = -0.54$ nN was measured. Subsequently, the Au tip further approached towards the HOPG surface with the pre-set velocity and under the same attraction force to a distance of 715 pm away from the surface, at which point a new and fast snap-in was observed. This snap-in event was characterized by $\Delta\delta_2 = 359$ pm and $\Delta F_2 = -0.13$ nN. In the case of a Pt tip approaching an immersed HOPG surface, a similar scenario was observed. At a tip-surface distance of 2.5 nm, we observed a first snap-in event characterized by $\Delta\delta_1 = 770$ pm and $\Delta F_1 = -1.18$ nN. However, further approaching toward the immersed HOPG surface, the force sensed by the cantilever further decreased at a roughly constant rate down to -2.72 nN, corresponding to a tip-sample distance of 573 pm. At this tip-sample distance, we observed a second snap-in event characterized by $\Delta\delta_2 = 433$ pm and $\Delta F_2 = -0.51$ nN.

The observed jumps in the $F_n(\delta)$ curves were expected to immediately follow the penetration of the metallic tips through the hydration layers between the metal tips and HOPG surface. Cheng *et al.* measured the density distribution of the interfacial water oxygen atoms by X-ray reflectometry as a function of the distance z from a mica surface.¹⁴ The density distribution $\rho(z)$ plot showed a first maximum at a distance $z = 132$ pm, corresponding to the adsorbed layer of water onto mica. At larger distances of $z = 252$ pm, 373 pm, and ~ 880 pm, broader maxima were observed and attributed to the hydration layers. Ho and Striolo compared different water models to simulate the structural properties of water at the interface with graphene by molecular dynamics.¹² The calculated density distribution function for the oxygen atoms showed a first maximum at a distance from graphene of $z = 320$ pm, corresponding to the adsorbed water layer. At larger distances of $z = 625$ pm and $z = 1$ nm, broader maxima could be observed that correspond to the

hydration layers. From these results, it is apparent that the spacings between the adsorbed water and the hydration layers depended on the hydrophobicity of the wetted surface, *i.e.* these spacings increased with the hydrophobicity of the surface. Trudeau *et al.* calculated the density distribution functions of water as a function of the distance from six surfaces with different hydrophobicity using a molecular dynamics simulation.¹⁵ In this study, the hydrophobicity of the simulated surfaces was characterized by their wetting angle that varied from 84° to 156° . Moreover, all of the six simulated surfaces had a rather hydrophobic character, an increase in the wetting angle resulted in a shift in the first maximum in the density distribution function to larger distances from the water/solid interfaces and its broadening. Further maxima corresponding to the hydration layers were found to shift to larger distances and to broaden with the increase in wetting angles. In the latter case, the shifting and broadening effects were more significant than in the case of the adsorbed water layer. Limmer *et al.* also used a molecular dynamics simulation to investigate the structure and hydration of Pt-like metal–water interfaces for two different metal surface orientations: (111) and (100).¹⁶ For both of these metallic surfaces, the authors observed a first maximum in the density distribution functions at a distance of $z = 250$ pm from the metal surface. At larger distances of $z = 650$ pm and $z = 1$ nm, broader maxima corresponding to the hydration layers were observed.

In our experiments, water adsorption and hydration needed to be considered for both the metallic tips and graphite surface. Upon the approach of an AFM tip towards a graphite surface in water, we expected the hydration and adsorbed layers on both the tip and sample surface to overlap and interact with each other. We attributed the snap-in events observed with an Au or Pt tip to the successive overlaps of the hydration layers on the graphite and metallic tips.

The overlap of the water layers could be expected to give rise to repulsive forces. As we observe in Fig. 2, while approaching toward immersed HOPG surface, the Au and Pt AFM tips underwent sudden jumps that were characterized by $\Delta F_{1,2} < 0$. The jumps were however too fast to understand their mechanism by quasi-static methods, such as those applied in this study. Recently, Yang *et al.* investigated the hydration structures on mica and graphene by frequency modulation NC-AFM with a hydrophilic tip (Si/SiO_x).¹⁷ In this study, the authors recorded the frequency shift Δf of the cantilever oscillation (with a natural frequency on the order of MHz) while approaching the AFM tip towards immersed mica and graphene surfaces. The measured $\Delta f(Z)$ plots were found to exhibit oscillations for both the immersed mica and graphene, whose periods were attributed to the thickness of their hydration layers. For vibration amplitudes smaller than the tip-sample distance, a $\Delta f(Z)$ plot relates to a force–distance curve according to the following formula:

$$\Delta f = \frac{f_0}{2C_n} \frac{\partial^2 U_{\text{ts}}(Z)}{\partial Z^2} = \frac{f_0}{2C_n} \frac{\partial F_{\text{ts}}(Z)}{\partial Z} \quad (4)$$

where f_0 is the natural frequency of the cantilever, U_{ts} is the tip-sample interaction potential, and F_{ts} is the tip-sample force.¹⁸ In



$\Delta f(Z)$ plots, the penetration of the hydration layers by an AFM tip produces positive frequency shift values, corresponding to an increase in the tip-sample interaction force.

Fig. 3 shows the forward and backward FFM traces on the immersed HOPG with both types of tips. With the gold tip, the recorded signal was very weak, and the traces almost overlapped. Correspondingly, the friction force F_f values were small and showed weak variations while increasing the normal force F_n . In the case of the Pt-coated tip, the recorded FFM signals were significantly higher and corresponded to F_f values almost six times higher than those of the Au-coated tip. In the case of the Au tip, the friction force values displayed a weak dependence on the normal force values that can be fitted with the JKR model according to the following formula:^{19–21}

$$F_f = \tau A_c \quad (5)$$

with

$$A_c = \pi \left(\frac{3}{4} \frac{R}{E^*} \right)^{2/3} \left[(F_n + F_{ad}) + 2F_{ad} + \sqrt{4F_{ad}(F_n + F_{ad}) + (2F_{ad})^2} \right]^{2/3} \quad (6)$$

and

$$E^* = \left[\frac{1 - \nu_1^2}{E_1} + \frac{1 - \nu_2^2}{E_2} \right]^{-1} \quad (7)$$

where τ is the shear strength, R is the tip radius, E^* is the reduced modulus of elasticity, and $E_{1,2}$ and $\nu_{1,2}$ are the Young's moduli and Poisson's ratios of the two contacting elastic bodies,

respectively. Using $R = 25$ nm, $E_{\text{HOPG}} = 30$ GPa, $\nu_{\text{HOPG}} = 0.24$, $E_{\text{Au}} = 75$ GPa, and $\nu_{\text{Au}} = 0.44$, we obtained a shear strength between Au and HOPG of $\tau = 16.8$ MPa and $F_{ad} = 1.48$ nN. The obtained value for the shear strength between Au and HOPG was comparable with the previously reported value for an Au tip sliding on an Au(111) surface, where we found $\tau = 24.21$ MPa.⁹

The friction force $\langle F_f \rangle$ value averaged over the whole range of normal force values was found to be high for larger adhesion forces F_{ad} , i.e. $\langle F_f \rangle_{\text{Au}} = 0.62 \pm 0.07$ nN and $F_{ad,\text{Au}} = -1.23 \pm 0.11$ nN and $\langle F_f \rangle_{\text{Pt}} = 5.73 \pm 1.19$ nN and $F_{ad,\text{Pt}} = -9.57 \pm 0.21$ nN. It is interesting to note that for both tips, $\left| \frac{F_f}{F_{ad}} \right| \approx 0.5$.

In both cases, the sliding motion of the tips exhibited an atomic scale stick-slip. We determined the periodicity of the stick-slip by calculating the PSD function of the FFM image. In the case of an Au-coated tip, we observed a clear peak at $k_1 = 25.76$ rad nm⁻¹ corresponding to a characteristic wavelength $\lambda_1 = 0.244$ nm. We attributed this wavelength to the C_α - C_α inter-atomic distance $a_{\alpha\alpha} = 0.246$ nm. At higher k -values, we observed a second and wider peak at $k_2 = 49.01$ rad nm⁻¹ that corresponded to the characteristic wavelength $\lambda_2 = 0.128$ nm (see Table 2). This value somewhat agrees with the C_α - C_β inter-atomic distance $a_{\alpha\beta} = 0.142$ nm. In the case of the platinum tip, the one-dimensional PSD function of the FFM signal revealed four peaks at positions $k_1 = 11.94$ rad nm⁻¹, $k_2 = 16.96$ rad nm⁻¹, $k_3 = 22.62$ rad nm⁻¹, and $k_4 = 28.9$ rad nm⁻¹, corresponding to the characteristic wavelengths $\lambda_1 = 0.526$ nm, $\lambda_2 = 0.370$ nm, $\lambda_3 = 0.277$ nm, and $\lambda_4 = 0.217$ nm, respectively (see Table 2). It is interesting to compare these values with the structural lengths in ice water; the distance between the two O atoms in hexagonal ice was 276 pm (first coordination radius),

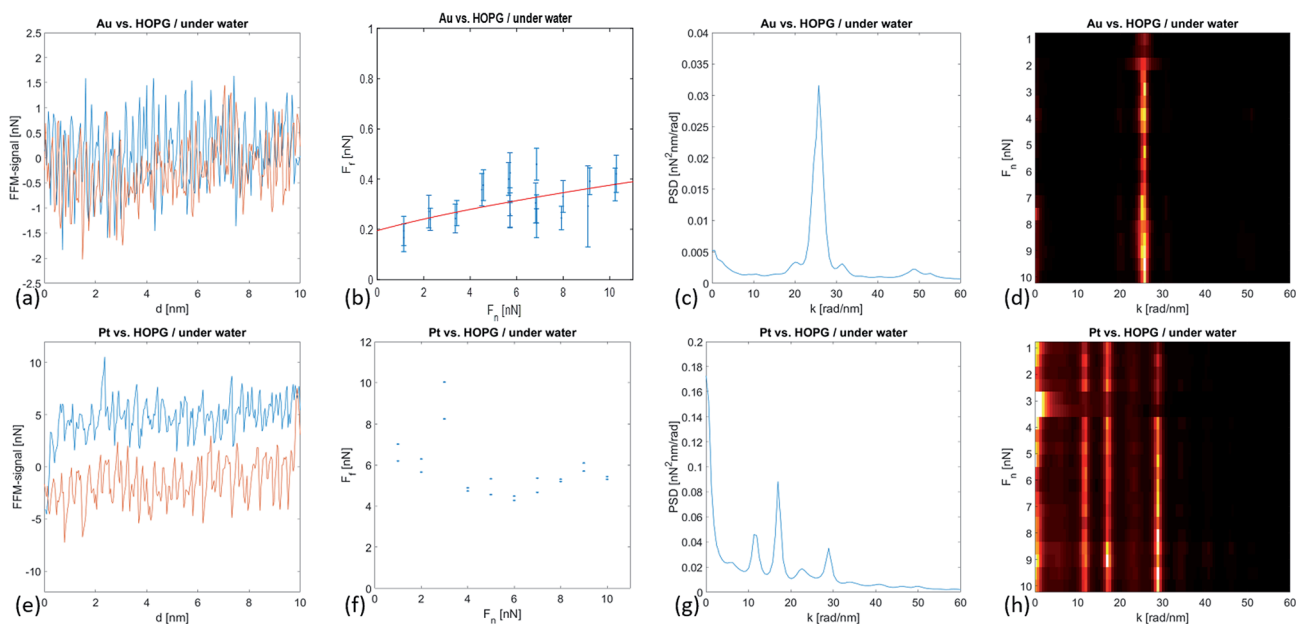


Fig. 3 (a and e) FFM-traces with $F_n = 1$ nN, (b and f) $F_f(F_n)$ -plots, (c and g) one-dimensional PSD functions of FFM-signals with $F_n = 1$ nN, and PSD functions of the FFM signals as a function of F_n recorded under water on HOPG with (a–d) an Au-coated AFM tip and (e–h) a Pt-coated AFM tip. In (a and e), the blue line corresponds to the forward sliding motion of the AFM tip on the sample surface (from left to right), and the orange line to its backward motion (from right to left). The red line in (b) corresponds to the JKR fit function of our experimental data.



Table 2 Characteristic wavelengths of atomic-scale stick-slip friction signals

	λ_1	λ_2	λ_3	λ_4
	[pm]			
Au	244	128	—	—
Pt	526	370	277	217

the interlayer spacing was 367 pm and the third coordination radius was 526 pm.²² The wavelength $\lambda_4 = 0.217$ nm might correspond to the Pt–O bond length.²³

First atomic scale friction results on HOPG were presented.⁵ There, the authors monitored the lateral deflection of a bent W wire with a tip at its end during sliding on a cleaved HOPG surface to determine the friction force. In this study, the tip radius was in the range of 150 nm to 300 nm and the normal contact force values varied from 1.5 μ N to 20 μ N. The lateral deflection signal of the wire indicated that the tip did not continuously slide over the surface but exhibited a corrugation with a typical periodicity of 0.25 nm, corresponding to the periodicity of the honeycomb structure of graphite (0.246 nm). The stick-slip motion of a sharp tip sled on HOPG was only observed at particular scanning angles of the tip with respect to the sample surface.²⁴ In line with previous observations that scanning tips can pick up a flat flake of graphite that is parallel to the basal plane of HOPG, the authors attributed the scanning angle dependence of the friction and atomic stick-slip to the commensurability of the contacting surfaces. The incommensurability of the HOPG surface and flake lattices led to ultra-low friction and continuous sliding motion commensurate with the stick-slip motion and higher friction. More recently, Vilhena *et al.* used a sharp silicon nitride tip with a radius of ~ 2 nm (according to the manufacturer's data) to resolve the lattice parameters of graphite and graphene grown onto Ni and Cu in water.⁷ In this study, the range of the applied normal force values was 5 nN to 50 nN. For the experimental results obtained by Vilhena *et al.*, the contact pressure could be computed by $p \approx \frac{F_n + F_{ad}}{A_c}$. Using $E_{\text{HOPG}} = 30$ GPa and $\nu_{\text{HOPG}} = 0.24$, and $E_{\text{Si}_3\text{N}_4} = 310$ GPa and $\nu_{\text{Si}_3\text{N}_4} = 0.27$, and $F_{ad} = 0$ nN (the adhesion force value was not reported by Vilhena *et al.*), we obtain that, in their study,⁷ the contact pressure varied between 4 GPa and 13 GPa. In our work, the AFM tip radii were measured to be ~ 25 nm (see Fig. 1), and the normal load varied between 1 nN and 10 nN. Using $E_{\text{Au}} = 75$ GPa, $\nu_{\text{Au}} = 0.44$, and $F_{ad,\text{Au}} = -1.4$ nN, and $E_{\text{Pt}} = 168$ GPa, $\nu_{\text{Pt}} = 0.38$ and $F_{ad,\text{Pt}} = -9.5$ nN, we calculated that in this study the contact pressure varied over a range of $p = 0.2$ – 0.5 GPa with an Au tip and $p = 0.3$ – 0.5 GPa with a Pt tip. These values are significantly lower than the calculated values for the experimental data presented by Vilhena *et al.*⁷ We thus suggest that the high contact pressure values in their work were sufficiently high to penetrate through the adsorbed water layer.

We believe that our force spectroscopy measurements describe the structure of the hydration layers and their

interpenetration during the approach of an AFM tip to immersed HOPG. Moreover, the friction measurements appear to be sensitive to the adsorbed water layer between an AFM tip and HOPG. Interestingly, the periodicity of the atomic-scale stick-slip with an Au tip matches the periodicity of HOPG, while the evaluated wavelengths of the stick-slip with a Pt tip indicate the presence of an ice-like water layer. As reported in the literature, water weakly got adsorbed on Au and HOPG, while the adsorption of water on Pt was significantly stronger.^{10,11,13} We thus conclude that in our friction measurements, the weakly adsorbed water between Au and HOPG was swept away, while the strongly adsorbed water between Pt and HOPG acted as a glue between the solid bodies.

D Conclusions

We found that the tribological behaviour of graphite in water strongly depends on the adsorption strength of the interfacial water layer. For water on a gold tip with a weak adsorption strength, we observed an atomic-scale stick slip with a characteristic length corresponding to the honeycomb structure of graphite. In this case, both the adhesion and friction force values were low. In contrast, the strong adsorption strength of water on a platinum tip gave rise to significantly larger adhesion and friction force values (almost ten times larger than those with a gold tip of similar size). These results provide new insights into the effect of adsorbed water layers on friction.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

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