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Quantitative determination of the spring entropy effect and its indication of the conformational change of polymer coils with varying concentration in aqueous poly(*N*-isopropylamide) solutions†

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The lower critical solution temperature (LCST) phase separation behaviors of thermosensitive poly(*N*-isopropylacrylamide) (PNIPAM) aqueous solutions were investigated by power-compensation differential scanning calorimetry (DSC). The entropic effect and hence the change of swelling state of PNIPAM polymer coils in homogeneous concentrated aqueous solutions with varied solution composition was elucidated by the isothermal enthalpy demixing recovery behaviors in distinct concentration regions.

1. Introduction

Since thermoresponsive aqueous poly(*N*-isopropylacrylamide) (PNIPAM) exhibits a type II lower critical solution temperature (LCST) phase separation behavior^{1–3} close to physiological conditions ($T_c = 32\text{ }^\circ\text{C}$), it has been utilized in a variety of applications such as drug delivery systems,^{4,5} stimuli-responsive^{6–8} and multi-stimuli responsive^{9–12} materials, separation of suspension solutions,¹³ and separation material in chromatographic procedures,¹⁴ only to name a few. Many reports in the literature indicate that the conformational change of the polymer plays a critical role in the dramatic physical property changes occurring around the LCST in PNIPAM or grafted materials.^{15–21}

As one of the fundamental problems in polymer physics, the conformational change of a linear flexible polymer chain from an expanded coil to a collapsed globule has been extensively studied in the past half century.^{22–28} However, most of these works focus on extremely dilute or semidilute solutions, investigations on the change in size of polymer coils in concentrated solution are very limited, especially for aqueous solutions, which have only been conducted in a narrow concentration region.^{29–31}

Entropic effect induced by the collapse of polymer coils is much different from that induced by the extension fashion, the latter is usually termed as elastic entropy or entropic elasticity, while the former is termed as spring entropic effect.^{32,33} It has been noted that the theoretical treatment model of spring

entropy is much different from that of elastic entropy.^{33,34} The elastic entropy in macroscopic or microscopic chain extension fashion has been investigated thoroughly,^{35–38} however, the spring entropy in the collapse mode is rarely addressed.

As discussed in a recent work,³⁹ in the demixing process of a polymer solution, the heat or enthalpy (ΔH_{total}) and free energy (ΔG_{total}) of demixing and the total demixing entropy (ΔS_{total}) can be described as:

$$\Delta G_{\text{total}} = \Delta H_{\text{total}} - T\Delta S_{\text{total}} = \Delta H_{\text{total}} - T(\Delta S_{\text{conf}}^{\text{p}} + \Delta S_{\text{solvent}} + \Delta S_{\text{r-t}} + \Delta S_{\text{other}}) \quad (1)$$

where $\Delta S_{\text{solvent}}$ is the entropy of solvent water, $\Delta S_{\text{conf}}^{\text{p}}$ is the change of the conformational entropy and $\Delta S_{\text{r-t}}$ is the rotational-translation entropy of polymer, ΔS_{other} is the contributions to entropy from other unrecognized sources.

As proposed by Budkov *et al.*,⁴⁰ in the framework of the mean-field approximation, the Gibbs free energy of polymer coils takes the form:

$$\begin{aligned} \Delta G_{\text{p}}(R_{\text{g}}) &= \Delta H_{\text{p}} - T\Delta S_{\text{p}} \\ &= K_{\text{B}}T \left(\frac{9}{4} \left(\alpha^2 + \frac{1}{\alpha^2} \right) - \frac{3}{2} \ln \alpha^2 \right) \\ &\quad - NK_{\text{B}}T \ln \left(1 - \frac{Nv_{\text{m}}}{V_{\text{g}}} \right) - \frac{a_{\text{p}}N^2}{V_{\text{g}}} \end{aligned} \quad (2)$$

where α is the chain expansion factor, $\alpha = \langle R_{\text{g}} \rangle / \langle R_{\text{g}} \rangle_0$, K_{B} is the Boltzmann constant, $v_{\text{m}} = 2\pi\sigma_{\text{m}}^3/3$ is the van der Waals volume of the monomers ($\sigma_{\text{m}} = \sigma_{\text{mm}}$ denotes the monomer's effective diameter), and $V_{\text{g}} = 4\pi R_{\text{g}}^3/3$ is the gyration volume of the polymer coils.

According to eqn (2), when a polymer solution is subjected to phase separation from two extremely conditions under the same temperature change procedure, that is, one phase

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separated from swelling coils and the other separated from collapsing globules, since the enthalpic effect due to the change of polymer–solvent interaction in the process of phase separation is almost the same, the influence of polymer coil dimensions will mainly correlated with the entropic effect.

In our recent work⁴¹ we showed that in concentrated aqueous PNIPAM solutions, phase separation from different swelling states can be achieved isothermally at a lower temperature than the LCST for different times after subjecting the first phase separation to a heating scan, and the entropic effect due to the change of swelling state was qualitatively discussed. Subsequently, similar entropic effects were also observed in another type III LCST behavior poly(vinyl methyl ether) (PVME) aqueous solutions.^{39,42} In contrast to the complicate chemical structure in PNIPAM, the structure of PVME is very simple and there is only one polar oxygen ether atom in each repeating unit and can form hydrogen bond with a maximum of two water molecules. The DSC results showed that below the critical water concentration of 38.3 wt% (*i.e.* 1 : 2 mole ratio of PVME repeating unit and water), the time independent of demixing enthalpy recovery behavior indicates that the PVME coil is in a globular state. A typical sigmoidal recovery behavior of demixing enthalpy above 38.3 wt% is ascribed as the reswelling of the collapsed polymer coils induced by the entropic effect. The increased difference between the upper and lower limits indicates the continued swelling of the PVME coils. Above 65 wt%, a dominant diluting effect can be observed, and a much longer phase separation time is needed to reach the expected lower limit.³⁹

Although the swelling state of polymer coils in extremely dilute solution and rather compact globule state of polymer chains in bulk state are clear for PNIPAM, it is still extremely challenging and difficult to confirm when and how the compact PNIPAM globules begin to swell with the continuous dilution of water solvent in concentrated solutions. Based on the above studies,^{39,41,42} in this work, the entropic effects in the demixing enthalpy recovery behavior in different concentration regions and its implications on the conformational changes of polymer coils swelling state in aqueous PNIPAM solutions are investigated.

Moreover, it should be noted that in the previous investigations the determination of entropic contributions in thermodynamic energy term is usually elucidated out from a series of molecules with similar chemical or complex characters,^{43–47} in this study and our recent work about PVME aqueous solutions³⁹ we showed that the entropic effect can be directly determined from a single polymer solution.

2. Experimental

2.1 Sample preparation

Poly(*N*-isopropylacrylamide) (PNIPAM) was obtained from Aldrich Chemical Company Inc. Its mass average molecular weight (M_w) characterized by gel permeation chromatography (GPC) is $3.59 \times 10^4 \text{ g mol}^{-1}$ and $M_w/M_n = 1.51$. The aqueous solution sample was dried in a vacuum oven at 65 °C with sufficient P_2O_5 powder as the drying agent for a few days until the weight of the sample stopped changing (error within

0.01 wt%) to obtain pure PNIPAM sample. The water used in this work was deionized and doubly distilled.

2.2 DSC experiments

A series of PNIPAM aqueous solutions with various PNIPAM content were prepared from the dried PNIPAM sample by adding appropriate amounts of deionized water in aluminum DSC crucible pans. The amount of added water is slightly higher than the anticipated composition of prepared solution, and excess water was simply removed by natural evaporation in open air for an appropriate period of time to the desired solution concentration, the pan was then hermetically sealed quickly. The prepared aqueous solution samples were left undisturbed for at least 7 days at room temperature and without any weight loss to ensure a good sealing effect before any DSC measurements.

The DSC measurements were performed on a power-compensation Perkin Elmer Diamond DSC with a Freon intra-Cooler 2P cooling accessory (the cooling agent can be cooled to as low as $-95 \text{ }^\circ\text{C}$). The power-compensation DSC was selected in this investigation because its furnace has low mass and small dimensions, ensuring a much faster heat transfer than heat-flux calorimeters. The small gap between the furnace and the cooling system, which is reduced by metallic guard ring inserts, promotes effective cooling.

All measurements were made in nitrogen atmosphere. The DSC temperature was calibrated using a two-point method with high-purity indium and mercury at a heating rate of $10 \text{ }^\circ\text{C min}^{-1}$. The heat flow was calibrated with a standard sapphire sample. The sample mass varied from 5.0 to 12.5 mg.

For the samples with water concentrations lower than 65 wt%, the aqueous PNIPAM solution samples were heated from 15 °C to 55 °C at a heating rate of $10 \text{ }^\circ\text{C min}^{-1}$ and then isothermally at 55 °C for 1 min to ensure that the samples completely undergo phase separation process. Consequently, the samples were cooled from 55 °C to 15 °C with a relatively fast cooling rate of $50 \text{ }^\circ\text{C min}^{-1}$; after being kept isothermally at 15 °C for different times varied from 0.1 min to up to 10^4 min, the samples were heated to 55 °C at $10 \text{ }^\circ\text{C min}^{-1}$ for a second time, and a series of DSC heat flow curves with different isothermal recovery times at 15 °C could be obtained. When the water concentration is equal or higher than 65 wt%, the isothermal phase separation time at 55 °C was increased as indicated for different samples. The other cooling condition and isothermal time at 15 °C are the same as those for samples with concentrations lower than 65 wt%.

3. Results and discussion

3.1 Distinctive time dependency of demixing enthalpy recovery in different concentration solutions

Fig. 1 showed the phase separation peaks in DSC curves collected from the second heating scan, which indicated different changes with isothermal recovery time at 15 °C for PNIPAM aqueous solution with 45 wt% (a) and 60 wt% (b) water content. As shown in Fig. 1(a), the heat flow curves of



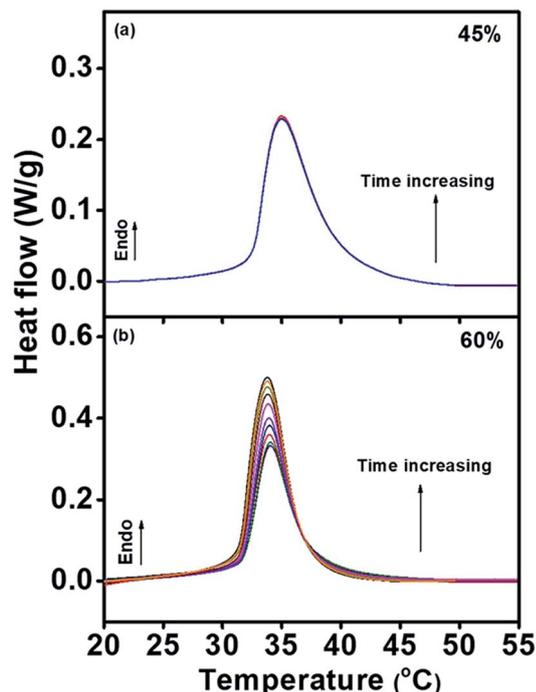


Fig. 1 The DSC curves of PNIPAM aqueous solution with (a) 45 wt% and (b) 60 wt% water content in the second heating scan after phase separation from equilibrium state as the increase of isothermal time at 15 °C.

endothermic phase separation peak demonstrate no change with the increase of isothermal time. However, in Fig. 1(b) the heat flow curves significantly increase with the raising of isothermal time. These results prove that with the rising of isothermal time, heat flow of endothermic phase separation peak is unchanged for PNIPAM aqueous solutions with low water content, and on the contrary, remarkable change of heat flow occurs with the increase of isothermal time in PNIPAM aqueous solutions with high water content.

As shown in Fig. 2, the integrated demixing enthalpy remain unchanged with the change of logarithmic isothermal time for PNIPAM aqueous solution with 45 wt% water content, while with the increasing of logarithmic isothermal time, demixing enthalpy firstly increases and then maintain constant for the sample with 60 wt% water content. When the isothermal time is less than 3 min, the demixing enthalpy retain almost constant ($\sim 8.5 \text{ J g}^{-1}$) over time. If the isothermal time situates between 3 min and 120 min, the demixing enthalpy will observably increase with the raising of isothermal time. In addition, the demixing enthalpy finally plateaus at about 13 J g^{-1} when the isothermal time is 120 min or even longer.

For the convenience of later discussions, the concept of the lower limit (isothermal recovering time at 15 °C for less than 1 min) and upper limit of demixing enthalpy (isothermal recovering time at 15 °C for longer than 120 min) is put forward.

As discussed in the recent work about PVME aqueous solutions,³⁹ the distinctive demixing enthalpy recovery behaviors in different concentration solutions may be attributed to the entropic effect due to changes in polymer chain swelling states.

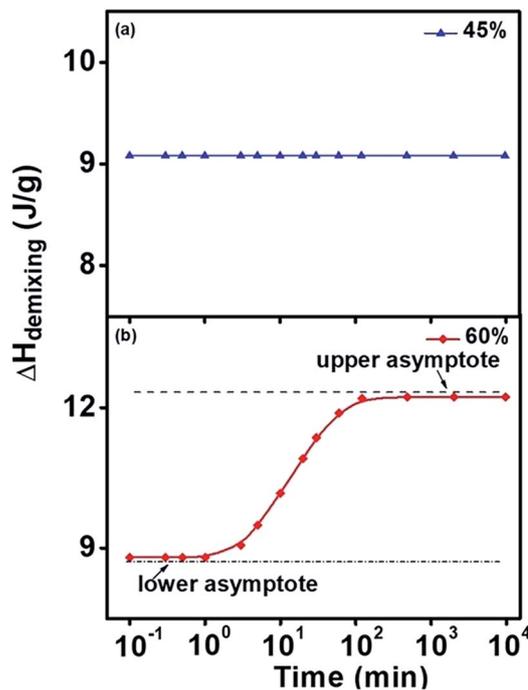


Fig. 2 The demixing enthalpy curves with various isothermal time in (a) 45 wt% and (b) 60 wt% water content of PNIPAM aqueous solution.

It is well known that the Gibbs free energy and entropy of polymer coils is correlated with the chain expansion factor.^{34,40} In a polymer solution, the polymer chain in a swelling coil state is similar to a stretched spring, while that in a relatively dense globule state is similar to a compressed spring. If the coil-to-globule transition process in the polymer solution is fast enough, the spring entropic effect caused by the change in the swelling states of the polymer chains could not be ignored and it is possible to be detected by the DSC method. That is probably the underlying reason for the distinct characteristics of demixing enthalpy recovery behaviors that observed in different concentration regions.

3.2 Concentration influence with the recovery time dependency

As reported by our previous work,⁴¹ the time dependence of demixing enthalpy recovery behavior showed distinct features in four concentration regions: (I) $0 \text{ wt}\% < W_{\text{water}} \leq 24 \text{ wt}\%$ (water concentration, similarly hereinafter), (II) $24 \text{ wt}\% < W_{\text{water}} \leq 49 \text{ wt}\%$, (III) $49 \text{ wt}\% < W_{\text{water}} < 65 \text{ wt}\%$, (IV) $W_{\text{water}} \geq 65 \text{ wt}\%$. When the water concentration is equal or lower than 24 wt%, only a glass transition behavior exists and no sign of phase separation can be observed for the mixtures⁴¹ (The DSC curves is showed in Fig. S1 in ESI†). Thus, in this work, only the other three concentration regions involved LCST phase separation behaviors will be discussed.

As shown in Fig. 3, the demixing enthalpy of three samples with different water concentrations remained almost unchanged with increasing isothermal time, indicating the time independent behavior. The result is obviously different



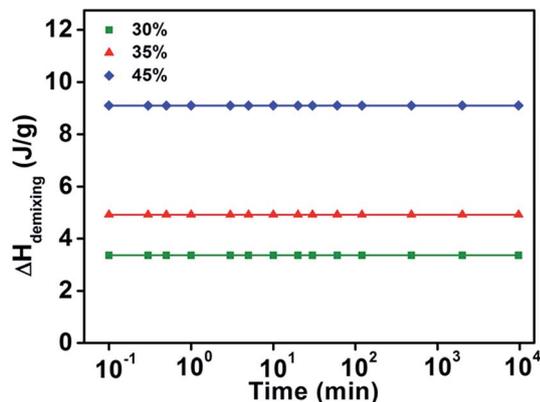


Fig. 3 The change of integrated demixing enthalpy of PNIPAM aqueous solution versus logarithmic isothermal time under 15 °C in region II (24–49 wt% water concentration).

from the demixing enthalpy recovery behavior as observed in the PNIPAM solution with 60 wt% water concentrations. In addition, the measured demixing enthalpy increases with the increasing of water content in this concentration region. The isothermal time independent of demixing enthalpy behavior illustrated in Fig. 3 indicates that the enthalpy is only contributed by the deterioration of hydrogen bond in the molecular complex formed between PNIPAM and water, according to the similar results observed in PVME aqueous solutions.³⁹

When the water concentration is between 49 wt% and 65 wt%, the typical recovery behavior of demixing enthalpy can be found. Moreover, in the case of short isothermal time, the lower limit of demixing enthalpy decreases with raising of water concentration, while the upper limit of demixing enthalpy corresponding to longer isothermal time increase with the rising of water concentration in region III. For three samples with different water concentrations, with the increasing of logarithmic isothermal time, their demixing enthalpies all firstly increase and then remain constant in a sigmoidal manner.

The typical sigmoidal shape of isothermal time dependency of the demixing enthalpy recovery behavior in Fig. 4 indicates

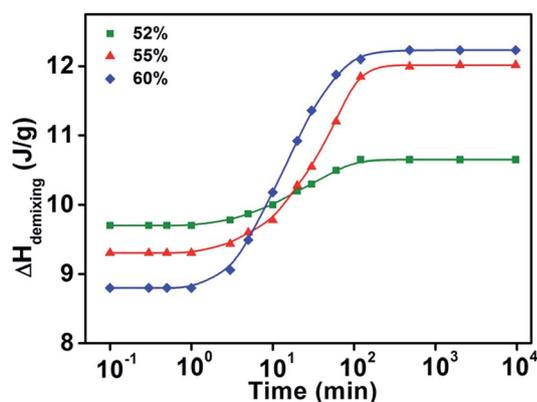


Fig. 4 The change of integrated demixing enthalpy of aqueous PVME solution versus logarithmic isothermal time under 15 °C in region III (49–65 wt% water concentration).

that the enthalpy recovery behavior of PNIPAM aqueous solution is influenced by two distinct factors. The first transition, which appeared at approximately 3 min, presumably to be dominated by the penetration of water back into the phase-separated and aggregated polymer phase when the temperature dropped to below the LCST; and the second transition at approximately 120 min may be dominated by the relaxation process of whole polymer chains from a compact collapsed globular state to a swelling coil state. Moreover, the later recovery time is in agreement with the experimentally determined relaxation time scale of a whole polymer chain.^{48,49}

When the water concentration is lower than 65 wt%, isothermal phase separation at 55 °C for 1 min is enough for PNIPAM solutions to reach a fully collapsed state, as shown in Fig. 4. However, when the water concentration exceeds 65 wt%, the required isothermal phase separation time at 55 °C significantly increases with rising water concentration. Furthermore, the detected demixing enthalpy after a short isothermal phase separation time keeps deviating to a higher value with rising water concentration, as shown by the open symbols in Fig. 5(a). In this plot, the closed symbol and the upper dashed line represent the demixing enthalpy value measured from the polymer solution in an equilibrium state, in other words, the upper limit value is measured after being isothermal at 15 °C for a sufficiently long time at each concentration indicated in Fig. 5(a).

With the increasing time of isothermal phase separation at 55 °C, the detected demixing enthalpy decreased in a sigmoidal manner versus the logarithmic time. This trend is very similar to that observed in PVME aqueous solutions.³⁹ However, as the molecular structure of PNIPAM is much more complicated, the predicted lower limit demixing enthalpy value corresponding to the fully collapsed state as in PVME solutions cannot be obtained.

Similarly, the 90 wt% water PNIPAM aqueous solution showed continuing increase of phase separation time at 55 °C, making it possible to detect the decrease in demixing enthalpy by DSC method, as illustrated in Fig. 6.

The results observed in Fig. 5(a) and 6 can be interpreted as the influence of aggregation on the retardation of the reswelling process.³⁹ As the water concentration increases, the probability that the collapsed polymer globule is in an isolated single state after phase separation also increases accordingly. The reswelling of isolated single polymer globules is much faster than that of aggregated polymer globules and cannot be detected by the DSC method. When isothermal at phase separation temperature for a longer period of time, an increasing amount of polymer globules aggregated, and the tendency for demixing enthalpy to decline became more obvious. Furthermore, the results for the 90 wt% water solution reveal that with increasing water concentration, the polymer globules are relatively stable even under the phase-separation temperature. Another plausible interpretation to the change in demixing enthalpy with concentration is that in a semidilute or dilute aqueous solution, the polymer chain will take the form of a much looser globule than in a concentrated solution. In fact, Wu and Wang⁵⁰ estimated that the single-chain globules of PNIPAM in an extremely



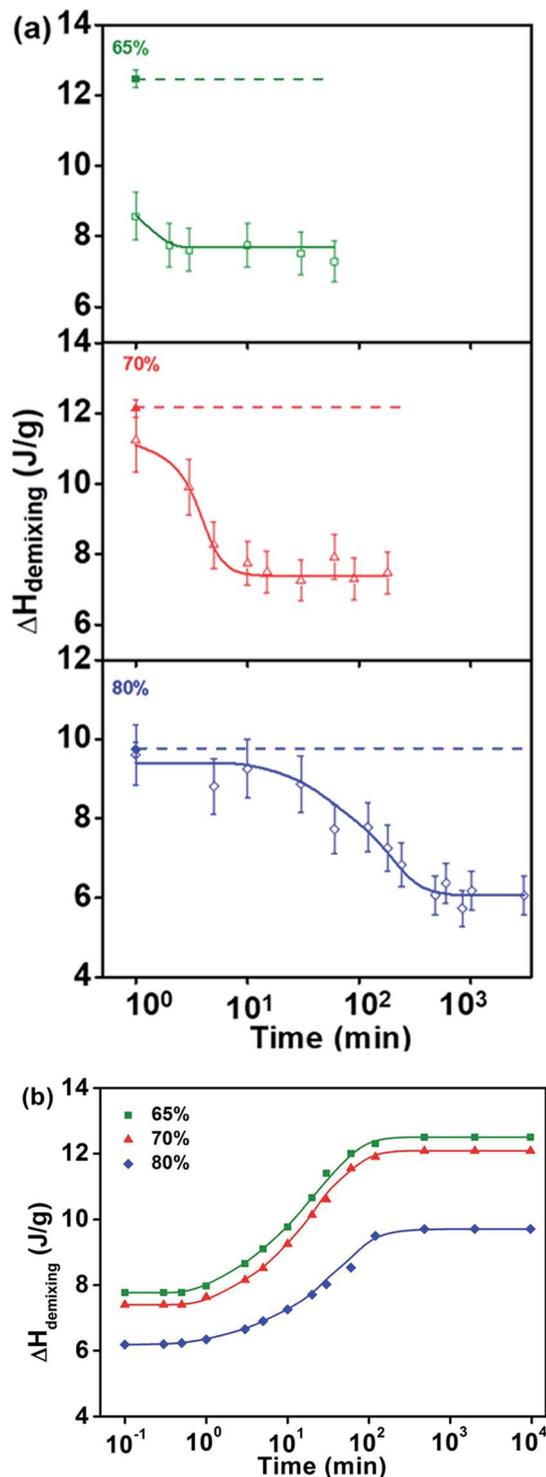


Fig. 5 (a) The change of demixing enthalpy of lower limit (isothermal recovering time of 0.1 min at 15 °C) versus logarithmic of phase separation time at 55 °C for 65 wt%, 70 wt%, and 80 wt% water PNIPAM aqueous solutions (open symbols). The closed symbols and the upper dashed lines represent the demixing enthalpy measured from well swelling solution samples, that is, the solutions remain undisturbed more than 7 days at ambient temperature. (b) The change of demixing enthalpy of PNIPAM aqueous solution versus different logarithmic isothermal times at 15 °C in concentration region IV (65 to 80 wt% water).

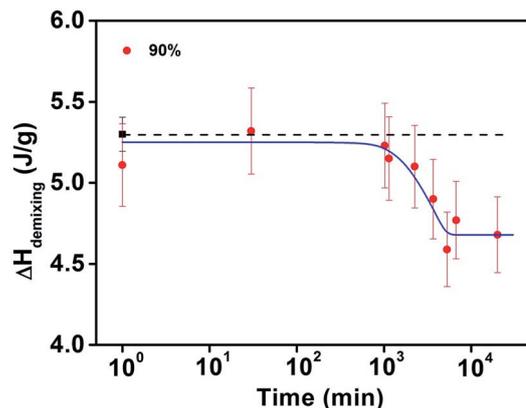


Fig. 6 The change of demixing enthalpy of lower limit (isothermal recovering time of 0.1 min at 15 °C) versus logarithmic of phase separation time at 55 °C for 90 wt% water PNIPAM aqueous solution.

dilution aqueous solution above the LCST still contain approximately 60% water inside its hydrodynamic volume, as probed by a dynamic light-scattering method.

It is worth mentioning that in the PNIPAM aqueous solutions the required isothermal phase separation time for the demixing enthalpy to reach a lower limit is much longer than that in PVME solution in the same concentration when water concentration is 65 wt% and above,³⁹ which suggests that the phase separated PNIPAM is more stable in water than PVME.

When the water concentration exceeds 65 wt%, the lower limit of demixing enthalpy corresponding to short isothermal time continues to decrease with increasing water concentration. In contrast, the upper limit of demixing enthalpy ceases to increase and declines with increasing water concentration in region IV compared to region III, but the time dependence of the recovery characteristics are almost the same, as shown in Fig. 5(b). This phenomenon demonstrates that the recovering swelling behavior of the collapsed polymer globules may be controlled by the same factors and is independent of the concentration of the aqueous solution.

Similar phenomenon is also observed in PVME aqueous solution,³⁹ and it is very surprising to find that the entanglement effect which is prevailing in polymer solutions cannot be observed in the recovering swelling process after LCST phase separation. The possible factors have been discussed in the previous work,³⁹ although the phenomenon of concentration independence of demixing enthalpy recovering behavior is not yet fully understood, these results indicate that the polymer coil collapse process is significantly different from that of shearing elongation mode as measured by viscosity method.

3.3 The quantitative measurement of the spring entropic effect in phase separation of PNIPAM aqueous solution

As shown in Fig. 7, the composition dependence of the upper limit of demixing enthalpy is nearly symmetrical and the maximum demixing enthalpy (about 12.46 J g^{-1}) appears at the 65 wt% water concentration, which is in good agreement with the results reported in literature.⁵¹ Moreover, the lower limit of



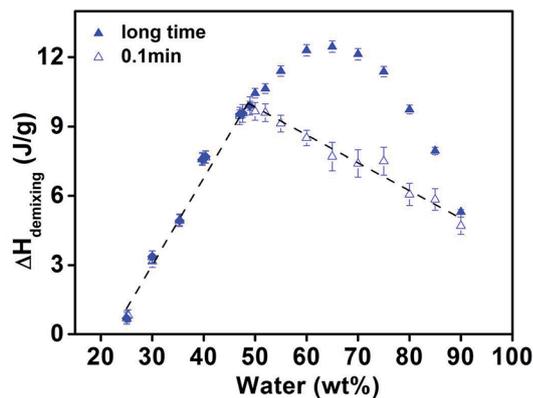


Fig. 7 The change of measured demixing enthalpy for both upper limit (close triangles) and lower limit (open triangles) versus water concentration of PNIPAM aqueous solution. The linear dashed line of the lower limit demixing enthalpy is only drawn as a guide to the eye.

demixing enthalpy observed in the study is also plotted in this figure as open symbols. As illustrated in Fig. 7, the measured lower limit of demixing enthalpy shows no discernible difference from the upper limit value in concentration region II (24–49 wt% water), and it is almost linear with the change of water content. The increasing of demixing enthalpy with rising water content indicates that the keep contribution of hydrogen bond interaction to form complex between PNIPAM and water in this concentration region.

When the concentration of water is increased to above 49 wt%, the upper limit of demixing enthalpy corresponding to longer isothermal time continues to heighten with the rising of water concentration in region III. However, the lower limit value corresponding to short isothermal time begins to decrease in proportion with the further increase of water concentration above 49 wt%. As discussed in previous study in PVME aqueous solution,³⁹ this phenomenon indicates that water molecule is in excess in the solution, the additional water will serve as free solvent and swell the PNIPAM coils. The continuous swelling of polymer coils contributed more entropic effect to the demixing enthalpy, thus the upper limit value still increases with the rising water concentration. While the lower limit value corresponding to short isothermal time that mainly contributed by the phase separation of polymer from fully collapsed state, thus only energetic enthalpic effect can be detected, the hydrogen bonds between PNIPAM and water are already saturated and the excess water mainly serve as diluents solvent, so the lower limit demixing enthalpy is found to keep decreasing with the rising water concentrations.

When the water concentration exceeds 65 wt%, the upper limit of demixing enthalpy ceases to increase and declines with increasing water concentration in region IV in contrast to region III, while the lower limit of demixing enthalpy corresponding to short isothermal time continues to decrease with increasing water concentration. This phenomenon indicates the swelling of polymer coils almost reach their maximum and further added water mainly serves as dilute solution in concentration region IV, which leads to the decline of both upper and lower

limits of demixing enthalpy with increasing water concentration.

However, as the chemical structure of PNIPAM is very complicate, the physical meaning of the critical concentrations between the different concentration regions and the influencing factors in aqueous PNIPAM solution are currently poorly understood.

As showed in Fig. 7, the lower limit of demixing enthalpy (ΔH_0) corresponding to short isothermal time is ascribed to the dissociation of hydrogen bond between PNIPAM and water in the solution, while the upper limit of demixing enthalpy (ΔH_∞) corresponding to longer isothermal time is comprehensive reflection of two kinds of effects: one is the dissociation of the hydrogen bond; the other one is entropic effect induced by the change of swelling states of polymer coils during the phase separation, which is equal to the difference between the upper and lower limits. Taking the above mentioned assumptions, normalizing the demixing enthalpies to the amount of PNIPAM as follow leads to the spring entropy effect:

$$\Delta S = (\Delta H_\infty - \Delta H_0)M_p/W_p \quad (3)$$

where M_p is the molecular weight of repeating unit of PNIPAM, W_p is the weight fraction of PNIPAM in aqueous solution.

The normalized demixing enthalpy induced by entropy spring effect is much more complex in three distinct regions: (II) 24–49 wt%, (III) 49–65 wt%, IV) above 65 wt%, as illustrated in Fig. 8. At lower water concentrations region II (24 wt% < $W_{\text{water}} \leq 49$ wt%), the entropic effect is zero, indicating that the polymer chain is in compact globule state and has almost no spring entropy effect in this region. As water concentration further increases to region III (49 wt% < $W_{\text{water}} < 65$ wt%), the normalized entropic effect obviously enhances with increasing of water content, suggesting the continuous swelling of the polymer coil as the increase of water concentration in this region. At the higher water concentrations region IV ($W_{\text{water}} \geq 65$ wt%), the spring entropy only increases slightly with increasing water content, indicating that the swelling degree of polymer coil reaches nearly its maximum when the water concentration is 65 wt%, and further increase in water

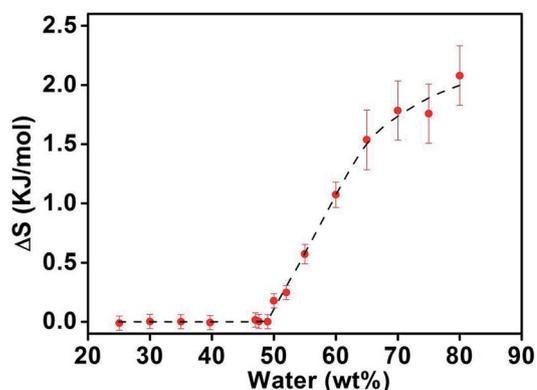


Fig. 8 The change of calculated spring entropy effect versus water concentration of PNIPAM aqueous solution.



concentration mainly induced dilution effect in the PNIPAM aqueous solution. As the concentration of water increases further to above 80 wt%, the error induced by the convention DSC apparatus will increase significantly, ultrasensitive micro-calorimetry (US-DSC) maybe more powerful in the more diluted solutions.⁵²

It should be noted that when the water concentration is increase to 80 wt% and above, as PNIPAM becomes more and more stable in aqueous solution even after phase separation, which can be found from the significantly prolonged phase separation time at 55 °C in Fig. 5(a) and 6, the lower limit demixing enthalpy which is assumed as contributed by only the hydrogen bond effect also deviate significantly, that will introduce more errors in the estimate of entropic effect in the semidilute to dilute solution regions.

4. Discussion

The critical concentration when the sigmoidal demixing enthalpy recovery behavior occurs in PNIPAM aqueous solution is 49 wt%, however, unlike the critical concentration of 38.3 wt% observed in aqueous PVME solution that corresponding to exactly 1 : 2 mole ratio between the repeating unit of PVME and water,³⁹ the physicochemical meaning of critical concentration in PNIPAM aqueous solution are poorly understood at present. These results can be compared with other experimental results in literature and help us to have a comprehensive understanding of the aqueous PNIPAM solution. For example, Ono *et al.*⁵³ found that the hydration number of NIPAM monomers aqueous solution amounts to 5, whereas that of linear PNIPAM chains in semidilute aqueous solutions is about 11–13.^{54,55} The simulation result showed that the maximum hydration number in *N*-methylacetamide/water system is 6,⁵⁶ in which *N*-methylacetamide has the same polar groups as the monomer of NIPAM. Accordingly, the concentration of water in aqueous solution with stoichiometric mole ratio of PNIPAM repeating unit and water as 1 : 5 is 44.33 wt%, and for the mole ratio as 1 : 6 is 48.87 wt%, which is very closed to the measured critical concentration of 49 wt% between region II and III in this study.

In extremely dilute good solvent–polymer solution, a polymer coil is in a swelling state, which is well investigated both theoretically⁵⁷ and experimentally.⁵⁸ While in the bulk melt state the polymer chain size is almost the same as that at the θ condition⁵⁹ within experimental uncertainties. However, in the concentrated solution region, how and when the polymer coils begin to swell with increasing solvent concentration is still not well understood.⁶⁰ So far small-angle neutron scattering (SANS) method is the most powerful experimental technique to probe polymer coil size in concentrated polymer solutions. However, since the determination of the coil size of single polymer chain requires a mixture of deuterium labeled and common hydrogen polymer sample with approximately the same molecular weight and distribution, and the solution in zero average contrast neutron scattering condition.⁶⁴ It goes without saying that these conditions are not easy to fulfill, and that is why the investigation of swelling of polymer coils in concentrated good solution

has only been reported for polystyrene (PS)^{61–64} and poly(methyl methacrylate) (PMMA)⁶⁵ in a few solvents in about fifty years since the development of SANS method. Moreover, due to the experimental uncertainty, the exact critical concentration when the polymer coil begins to swell is ambiguous and the estimated concentration value varies up to 10% or even higher;⁶⁵ in turn, the physical meaning remains an open question.⁶⁰ The DSC experiments conducted in PVME³⁹ and PNIPAM aqueous solutions in this investigation suggest that the entropic effect in the demixing enthalpy may be utilized as a promising alternative method to detect the conformational changes of polymer coils in concentrated solutions, although it can only obtain the relative changes, and at present these results can only be observed in LCST phase separation processes. However, a more precise critical concentration can be obtained from this method, which indicated that the mole ratio between the polymer repeating unit and solvent may play a critical role in the swelling of polymer coils. Based on the assumption, it is reasonable to interpret the phenomenon that polystyrene begins to swell in two different good solvents carbon disulfide⁶¹ and toluene^{62–64} which are very different in volume concentration, but very close to 1 : 1 mole ratio for both solutions. SANS experiments in PNIPAM aqueous solutions have been reported in literatures,^{66,67} unfortunately, these works only conducted in hydrated PNIPAM and deuterated water mixture, which is much different from zero average neutron contrast condition,⁶⁴ the information of the change of PVME coil size in concentrated aqueous solution could not be obtained. Our present DSC work would hopefully inspire more studies to investigate the microscopic characteristics using SANS or other techniques in concentrated aqueous PNIPAM solution in the future.

Ye *et al.* investigated the association of cyclic- and linear-PNIPAM with varying chain lengths and end groups in dilute aqueous solutions,⁶⁸ and found the aggregation behaviors varies greatly. Moreover, the end-group or initiator in polymerization also influence the demixing behavior above LCST temperature.^{69,70} The results in this investigation showed that when water concentration is lower than 65 wt%, the phase separation and demixing enthalpy recovery behavior in PNIPAM aqueous solutions were almost the same as in the previous study.⁴¹ However, when the water content is higher than 65 wt%, the change of demixing enthalpy *versus* phase separation time at 55 °C measured in this work is much different from our recent investigation.⁴¹ These results indicated that the influence of polymer chain architecture, chain lengths and end groups may affect the phase separation and aggregation in the semidilute and dilute aqueous PNIPAM solutions. Unfortunately, only the molecular weights and their distributions are known for the two samples, the polymerization procedure and end groups are not available. Moreover, due to the limitations in the heating and cooling scan rate of conventional DSC method, although a relative high cooling rate applied in this investigation, the macroscopic DSC experiment can only observe the demixing phenomenon in a long time scale. Although ultrafast DSC (the so-called flash DSC) can be utilized to investigate the influence of fast cooling and heating on the dynamic phenomena in homopolymer and polymer blends,^{71,72} but at



this stage it can only be used to test solid samples. In contrast, laser temperature-jump time-resolved technique combined with other microscopic probing method can obtain the demixing information in a millisecond scale,⁷³ which could help us in obtaining more comprehensive results on the aggregation behavior of polymer above LCST temperature.

5. Conclusions

In summary, the isothermal demixing enthalpy recovery behavior of aqueous PNIPAM solutions has been systematically investigated in this work. The variation of isothermal time exhibited distinct demixing enthalpy recovery behaviors in four concentration regions: (I) 0–24 wt%, (II) 24–49 wt%, (III) 49–65 wt%, (IV) above 65 wt%. In the case that the concentration of water is equal or lower than 24 wt%, there is only a glass transition behavior in the DSC curve and no sign of phase separation can be observed for the mixtures. In region II, the isothermal demixing enthalpy recovery behavior possesses time independence. In concentration region III and IV, the further increasing water molecule plays a role of pure solvent to swell the polymer coils, resulting in the time dependence of phase separation enthalpy recovery behavior. Based on the dependence of demixing enthalpy recovery behavior on concentrations, the spring entropic effects in the phase separation of PNIPAM aqueous solution was quantitatively analyzed. The thermal effect contributed by spring entropy showed that at lower water concentrations of region II, the spring entropy is zero and it corresponds to compact globule state of PNIPAM coil. However, in region III, the spring entropy significantly increases with the increasing of water content, corresponding to the continuous swelling of the polymer coil as the increase of water concentration. Moreover, in region IV, the tendency of increasing in entropic effect with the raising of water concentration is weakened, indicating that the swelling degree of polymer coil reaches almost its maximum when the water concentration is 65 wt%, and further increase in water concentration mainly induced dilution effect in the PNIPAM aqueous solution.

Author contributions

D. H. and S. J. conceived and designed the experiments. L. S., J. L. and P. L. planned and performed the DSC experiments. S. L., J. L. and P. L. analyzed the experimental data. L. S., J. L., P. L., J. L., S. J. and D. H. wrote the manuscript. All authors discussed the results, provided intellectual input and critical feedback and commented on the manuscript.

Conflicts of interest

There are no conflicts to declare.

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