PAPER

Kinetic investigation of the hydrolysis of uranium hexafluoride gas†

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UF_6 is commonly employed in enrichment technologies and is known to react rapidly with water vapor to form radioactive particulates and hydrofluoric acid vapor. The kinetics of the UF_6 hydrolysis reaction have been observed directly for the first time. The rate appears to be half order and second order for UF_6 and water, respectively, with a rate constant of 1.19 ± 0.22 $Torr^{-3/2}$ s^{-1}. The proposed mechanism involves formation of the $[UF_6 \cdot 2H_2O]$ adduct *via* two separate reactions.

Uranium hexafluoride (UF_6) is a key compound in the nuclear fuel cycle as the material employed in commercial enrichment, enabling production of the fuel for electricity production in nuclear power reactors. Studies evaluating the safety implications of small or large releases of UF_6 within a processing facility have been performed previously,[1–3] as it is well known that this material undergoes a hydrolysis reaction in ambient air according to the simplified reaction:

$$UF_6(g) + 2H_2O(g) \rightarrow UO_2F_2(s) + 4HF(g)$$
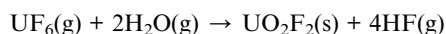
producing both uranium particulates and hydrofluoric acid vapor. Recent work[4] has explored the formation of the uranium particulate materials but the precise molecular mechanism of the initiating reaction has yet to be verified. Previous efforts to characterize this reaction have focused on spectroscopic measurements[5–7] and computational studies.[8–13] The experimental studies have focused on the spectroscopic detection of uranium species but lacked the temporal resolution to observe the reaction or identify any transient species. Unfortunately, there are major discrepancies between the experimentally observed reaction and computationally predicted mechanisms. For example, the computational studies suggest large thermodynamic energy barriers that would likely prevent the reaction of UF_6 and water vapor,[9–13] yet the hydrolysis reaction is known to occur quickly and completely under ambient conditions.[5–7] Additionally, one of the long-suspected intermediates of this reaction, UOF_4, has not been successfully identified under extreme conditions designed to optimize its production such as

reacting water with a 5000-fold excess of UF_6.[14] Relevant spectroscopy measurements need to be performed to inform computational modelling because the mechanism may not be driven by a stepwise reaction of UF_6 and water molecules.

One prior study performed an indirect measurement of the rate of the UF_6 hydrolysis by monitoring the ingrowth of hydrogen fluoride with a laser-based analyzer.[15] The reported rate constant of $4 \pm 4 \times 10^{-18}$ cm^3 s^{-1} remains questionable as limited experimental details were reported. Based on their findings, and assuming pseudo-first order kinetics under these reaction conditions in excess water vapor, the reaction half-life is calculated to be on the order of 1 ms or less. Standard infrared spectroscopy instrumentation cannot scan with sub-millisecond temporal resolution, requiring specialized instrumentation that has only recently become available.

This work focused on observing the disappearance of UF_6 under low pressure conditions by probing the most sensitive infrared (v_3 antisymmetric stretching) vibrational band,[16] located at 625 cm^{-1}, using a 5 m long-path length cell. The long path length combined with the sensitivity of the band allow the reaction rate to be investigated at sub-Torr partial pressures. The reaction is slow enough at these pressures to allow direct kinetic measurements of the hydrolysis to be made using a typical infrared spectrometer.

Experiments were performed in a 5 m long-path length gas cell fitted to an ABB MB3000 Fourier transform infrared spectrometer. The chamber was exposed to fluorine gas to passivate materials of construction and remove water from surfaces within the spectroscopy cell before each experiment. The UF_6 was then introduced into the evacuated cell at pressures between 10 and 30 mTorr and ambient temperature (22.5 ± 0.5 °C). (**Warning:** UF_6 is a radioactive gas that forms highly toxic hydrogen fluoride in the presence of water.) After initial infrared spectroscopy measurements were made, 60 or 80 mTorr of water vapor was injected into the system and allowed to react. Typical infrared spectra collected during the hydrolysis reaction occurred during 0.5–2 min for these conditions, as shown in Fig. 1A. Note, the

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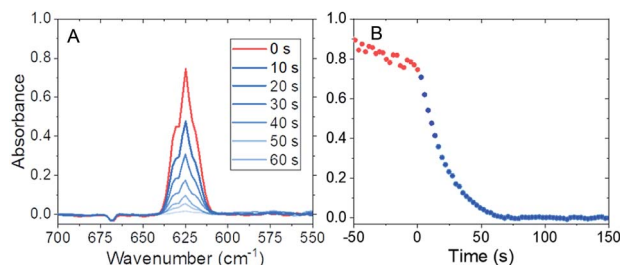
Fig. 1 (A) Select infrared spectra showing the 625 cm^{-1} band of UF$_6$ just before introducing water vapor (red) and every 10 s after (blue) for 1 min. (B) Example of absorbance change of the 625 cm^{-1} band over time during a typical hydrolysis experiment. The rate of disappearance of the UF$_6$ increased about a factor of 10 when H$_2$O was introduced.

reactions that occurred when water vapor was introduced at these partial pressures were approximately an order of magnitude faster than any reactions of UF$_6$ with materials of construction. The observed rates (Fig. 1B) were significantly slower than those expected from diffusion-limited reactivity, suggesting that mixing occurred rapidly from the injection method.

Typical changes in the absorbance due to the reaction are shown in Fig. 2 after correction for reaction with materials of construction. Each figure is the average of three experiments and the data are corrected using a linear regression of the absorbance before time zero extrapolated through the points used for initial rate determination. The initial slope of the decay was fit using a linear regression on the first five data points for each reaction condition. The data were converted from absorbance units to mTorr, and the resulting conditional reaction rates in mTorr s^{-1} are shown in Table 1.

It should be noted that the conditions under which the hydrolysis reaction rate could be measured were limited by the scan rate of the spectroscopy equipment. The concentrations had to be maintained such that the reaction rate was significantly greater than the minimized rate of UF$_6$ consumption by the materials of construction but still had to be slow enough to have multiple measurements before the reaction was completed. Due to the high dependence of the hydrolysis reaction rate on water concentration, only two of the water concentrations measured gave reaction rates that were in the appropriate time frame bounding the measurable conditions.

The conditional reaction rates were plotted against partial pressures of UF$_6$ and against the partial pressures of
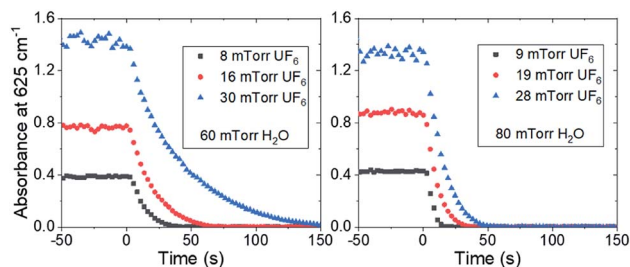
Table 1 Conditional reaction rates of the hydrolysis of gaseous UF$_6$ in the presence of H$_2$O vapor

H$_2$O (mTorr)	UF$_6$ (mTorr)	Rate (mTorr s^{-1})
60 ± 2	8.2 ± 0.5	0.387 ± 0.008
60 ± 2	16.2 ± 1.0	0.556 ± 0.071
60 ± 2	30.2 ± 1.9	0.709 ± 0.321
80 ± 3	9.1 ± 0.6	0.702 ± 0.100
80 ± 3	18.6 ± 1.5	1.018 ± 0.066
80 ± 3	28.3 ± 1.6	1.312 ± 0.112

water on a log/log plot as shown in Fig. 3. The slope of the generated linear trends is the reaction order for UF$_6$ and water, respectively. This suggests a rate equation:

$$\text{Rate} = k[\text{UF}_6]^{0.5}[\text{H}_2\text{O}]^2,$$

where k is the rate constant. Applying the data in Table 1 to the suggested rate equation gives a rate constant of 1.19 ± 0.22 Torr$^{-3/2}$ s^{-1}.

Recent work[4] explores the formation kinetics of uranyl fluoride particles from the reaction of gaseous UF$_6$ with water vapor. Some of the reactant concentrations in those studies are like those used in this work. Under humid condition (5% relative humidity and higher), the number concentration of uranyl fluoride particles produced in the hydrolysis reaction decrease during the observed time elapsed after start of the reaction (approximately 2–30 s). This is expected because the reaction is assumed to be complete in less than 2 s, and particles are undergoing various processes such as agglomeration and coagulation. Under very dry conditions (100 ppm and lower H$_2$O) the number concentration of uranyl fluoride particles increased over the same observed time (2–30 s). Applying the kinetic parameters determined in this work, after 30 s the reaction of 100 ppm (75 mTorr) UF$_6$ with 100 ppm (75 mTorr) of water is expected to only have consumed approximately 30% of the UF$_6$ and 60% of the water. The increase in number concentration of uranyl fluoride particles in very dry conditions observed
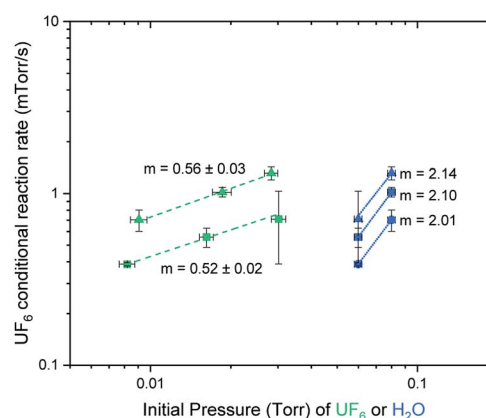

Fig. 2 The normalized absorbance of the 625 cm^{-1} band in a 5 m path length cell for various partial pressures of UF$_6$ and water vapor. Water vapor was injected at time = 0 s.

Fig. 3 Conditional reaction rates for the hydrolysis reaction as a function of the partial pressure of UF$_6$ (green, dashed) and water (blue, dotted) plotted on log−log scale. The dashed lines show the linear fit of the data for varied UF$_6$ pressures at 60 (■) and 80 (▲) mTorr H$_2$O. The dotted lines show the linear fit for varied H$_2$O pressures at 10 (●), 20 (■), and 30 (▲) mTorr UF$_6$. The slope (m) of each line is displayed.

over the first 30 s in those studies agrees well with the reaction kinetics set forth in this work.

The kinetic model developed in this work can be applied to the recent work by Hu *et al.*[13] that strongly suggests that the formation of two and three water molecule adduct species with UF_6 drastically reduced the calculated energy for the hydrolysis reaction. We propose the suggested reaction mechanism below based on the experimentally determined rate equation combined with those theoretical calculations.

Scheme 1 suggests a reaction mechanism that accounts for recent work suggesting high energy barriers for 1 : 1 UF_6 water adducts,[8–11,13] and that multiple UF_6 centres, water molecules, or a combination of both may be involved,[8,9,13] consistent with the reactant orders determined in this study. There is likely an initiation step where UF_6 reacts with water to form an adduct (eqn (1)). Note, theoretical studies suggest the formation of the single water adduct is slightly more energetically favourable than UF_6. Literature modelling suggests that further reactions toward the formation of uranyl fluoride are energetically disfavored.[9–13] The increased energy stability coupled with the inability to react further suggests that this species may be formed in significant concentrations. The formation of an adduct containing two water molecules would confirm the second order behaviour in the rate equation. This may be formed by a direct reaction with water (eqn (2)) or potentially from reactions between two of the $UF_6 \cdot H_2O$ species (eqn (3)). This may explain the fractional rate order, which is often explained by a complicated mechanism that have multiple pathways to reach the rate-limiting step. Both reactions may be viable because water and the UF_6 water adduct could be present in similar concentrations under the conditions of this work, and the formation of an anhydrous UF_6 molecule by eqn (3) would explain the fractional rate order associated with UF_6. This also suggests that the $UF_6 \cdot 2H_2O$ species is the reactant in the rate-determining step of the mechanism.

The conditions of this work were such that most of the water was consumed during the reaction and may have restricted the reaction to second order. If more water was available, Hu *et al.*[13] suggest formation of a three water adduct species is more energetically favourable. This could be accommodated by the additional reactions shown in eqn (4) and (5), providing additional reaction pathways to react with UF_6.
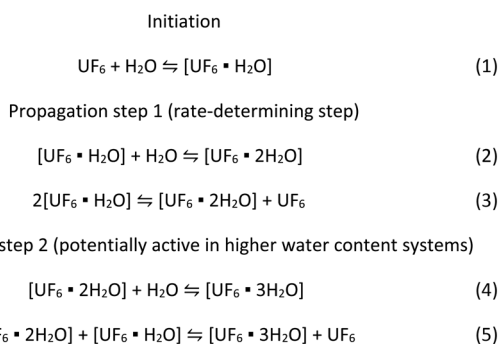
In summary, direct observation of the hydrolysis reaction kinetics of gaseous UF_6 have been accomplished under low-pressure conditions. The results show the reaction was half order and second order with respect to UF_6 and water. The rate constant was determined to be 1.19 ± 0.22 $Torr^{-3/2}$ s^{-1}. The results are consistent with recent experimental observations of the formation kinetics of uranyl fluoride particles from UF_6 hydrolysis under very dry conditions. The results also provide valuable data that support theoretical and computational studies.

Conflicts of interest

There are no conflicts to declare.

Acknowledgements

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Initiation

$$UF_6 + H_2O \rightleftharpoons [UF_6 \cdot H_2O] \qquad (1)$$

Propagation step 1 (rate-determining step)

$$[UF_6 \cdot H_2O] + H_2O \rightleftharpoons [UF_6 \cdot 2H_2O] \qquad (2)$$

$$2[UF_6 \cdot H_2O] \rightleftharpoons [UF_6 \cdot 2H_2O] + UF_6 \qquad (3)$$

Propagation step 2 (potentially active in higher water content systems)

$$[UF_6 \cdot 2H_2O] + H_2O \rightleftharpoons [UF_6 \cdot 3H_2O] \qquad (4)$$

$$[UF_6 \cdot 2H_2O] + [UF_6 \cdot H_2O] \rightleftharpoons [UF_6 \cdot 3H_2O] + UF_6 \qquad (5)$$

Scheme 1 Proposed reaction scheme for initial UF_6 hydrolysis reaction.