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Coatings of magnetic composites of iron oxide and carbon nitride for photocatalytic water purification†

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Magnetic composites of iron oxide (α -Fe₂O₃ and Fe₃O₄) and carbon nitride materials (CN) were synthesized via a microwave assisted hydrothermal method starting from iron salts and CN, which was obtained by thermal decomposition of dicyandiamide. The as-prepared composites with iron oxide loadings of 0.5 $\omega\%$ –6 $\omega\%$ were characterized by powder X-ray diffraction (PXRD), diffuse reflectance UV-vis spectroscopy, magnetization measurements, nitrogen adsorption measurements and thermogravimetric analyzes (TGA). The composites were examined for the degradation rate of an aqueous rhodamine B (RhB) solution under visible light irradiation. The magnetic composite α -Fe₂O₃(3 $\omega\%$)/CN enables 82% degradation of RhB within 90 min. Therefore, this material was selected for an immobilization approach and deposited using a spray coating technique on a magnetic polymer substrate. Coatings with loadings from 1.1 mg to 3.6 mg were compared with regard to their activity for the photocatalytic degradation of RhB under visible light irradiation. The substrate loaded with 0.4 mg cm⁻² catalyst enables a RhB degradation of 61% within 8 h. Photocatalytic degradation of triclosan and ethinyl estradiol was also successful and both compounds were degraded with up to 46% of the initial concentration within 8 h. ICP-MS measurements of the pollutant solutions after photocatalytic treatment showed that leaching does not occur.

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Introduction

The photocatalytic degradation of organic pollutants using semiconductors is an environmentally benign method for wastewater purification.^{1–3} Pollutants such as ethinyl estradiol and triclosan, which are used as biocides, increasingly enter into the ecosystems. For example, the contraceptive ethinyl estradiol was detected in wastewater in the USA, China and Australia and it is difficult to remove by conventional wastewater treatment plants. Triclosan is absorbed by the human skin and the oral mucosa and is suspected to influence the fecundity of humans and animals, affects the immune response and promotes the development of allergies, asthma and food sensitizations.^{4–6} Ethinyl estradiol may also influence the amphibian mating behavior.⁶ The admission of levels above safe thresholds of ethinyl estradiol could increase the risk of cancer and induce cardiovascular diseases in humans.^{4,5,7} Photocatalytic degradation processes using TiO₂ were

developed for the degradation of organic pollutants,^{8,9} but with a band gap of 3.2 eV TiO₂ uses only 4% of the solar spectrum for photocatalytic reactions.^{8,10} Our work focuses on alternative materials such as carbon nitride materials (CN) with a band gap of 2.7–2.8 eV. Carbon nitride materials have received much attention recently because of their excellent chemical and temperature stability and their environmental sustainability for photocatalytic applications. Various forms of CN have been extensively examined for photocatalytic hydrogen evolution and photocatalytic water splitting, gas sensors and solar cells.^{11–17} They are promising candidates for photocatalytic wastewater treatment^{12,18,19} among others.^{3,10,15,20–24} Doping and exfoliation was demonstrated to enhance the degradation efficiencies of CN materials and alternatively the combination with other semiconductors was demonstrated to be successful.^{12,25–27} Selected examples for CN composites comprise MoS₂/C₃N₄, Bi₂WO₆/C₃N₄, Ag/C₃N₄, Fe₃O₄/C₃N₄ and α -Fe₂O₃/C₃N₄.^{12,15,22,28,29} However, these investigations are based on dispersions of particles, and their use requires an additional costly process step for particle separation in any technologically relevant approach. Although, dispersions show generally significant higher activities than immobilized particles, it is essential to establish photocatalytic processes using immobilized photocatalysts.^{19,20,23,30–33} So far only a few studies focus on the immobilization of CN materials: for the photocatalytic removal of NO in air, the immobilization of carbon nitride on Al₂O₃

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foam has been reported by Dong *et al.*³⁴ The immobilization of photocatalysts such as TiO₂/C₃N₄ composites for the photocatalytic degradation of methylene blue was presented by Boonprakob *et al.* and is based on a doctor blade coating technique on glass.³⁵

Herein, we present an alternative route to obtain photocatalytically active CN-based coatings. Therefore, composites composed of CN particles and iron oxides (α -Fe₂O₃ and Fe₃O₄) were synthesized. The combination of CN particles with magnetic iron oxides as magnetically separable dispersions for photocatalytic applications has been demonstrated recently.^{15,23} A common approach for iron oxide/CN composites is the hydrothermal synthesis.^{30–32,36,37} An alternative way to obtain such composites is the microwave assisted synthetic approach. This method reveals uniform and crystalline particles in shorter reaction times at lower temperatures.^{38,39} We describe the microwave assisted synthesis for iron oxide/CN composites, which were coated on a magnetic polymer matrix by a high volume low pressure (HVLP) spray coating technique. This coating technique is easy to handle, transferable to other photocatalyst materials and has low acquisition costs. The coatings

were used to study the degradation rate of an aqueous RhB solution. Selected coated substrates were chosen to investigate the decomposition rate of the biocide triclosan and the medicinal drug ethinyl estradiol.

Results and discussion

The focus of this work is given to the formation of coatings of iron oxide/CN composites on magnetic substrates and their potential use for wastewater purification. Thus, we first discuss the synthesis and characterization of carbon nitride materials, iron oxides and the composites, thereafter the preparation of coatings and finally the catalytic activity of the coatings is described.

Preparation and characterization of the photocatalysts

The carbon nitride material was obtained after decomposition of dried dicyandiamide at 550 °C for 4 h in a crucible, covered with a simple lid. Iron oxide particles were prepared by a microwave assisted synthesis, either starting from an aqueous

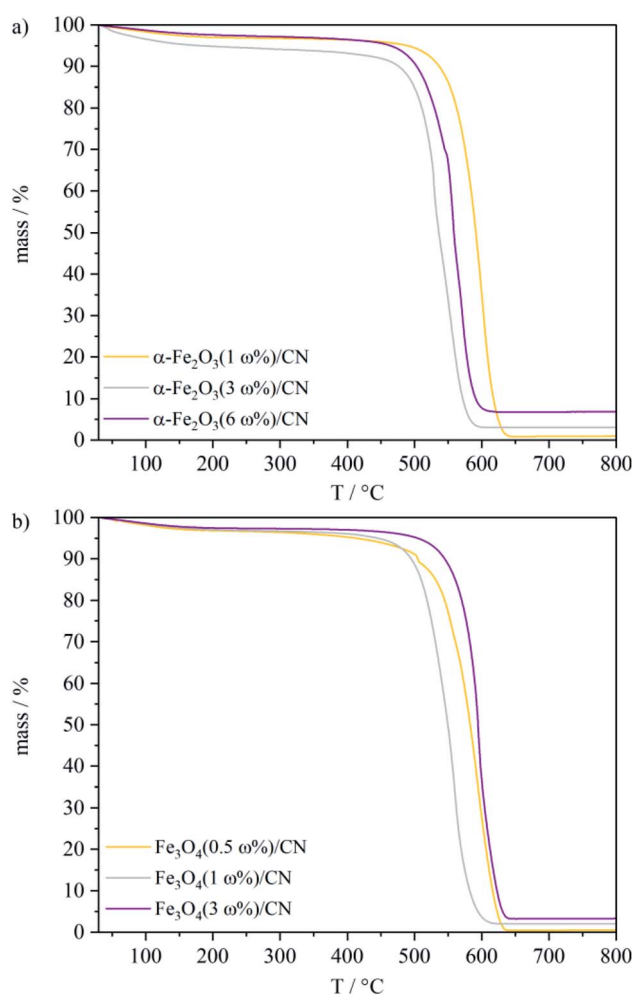


Fig. 1 TGA curves of the as-prepared (a) α -Fe₂O₃/CN composite and (b) Fe₃O₄/CN composite particles under synthetic air.

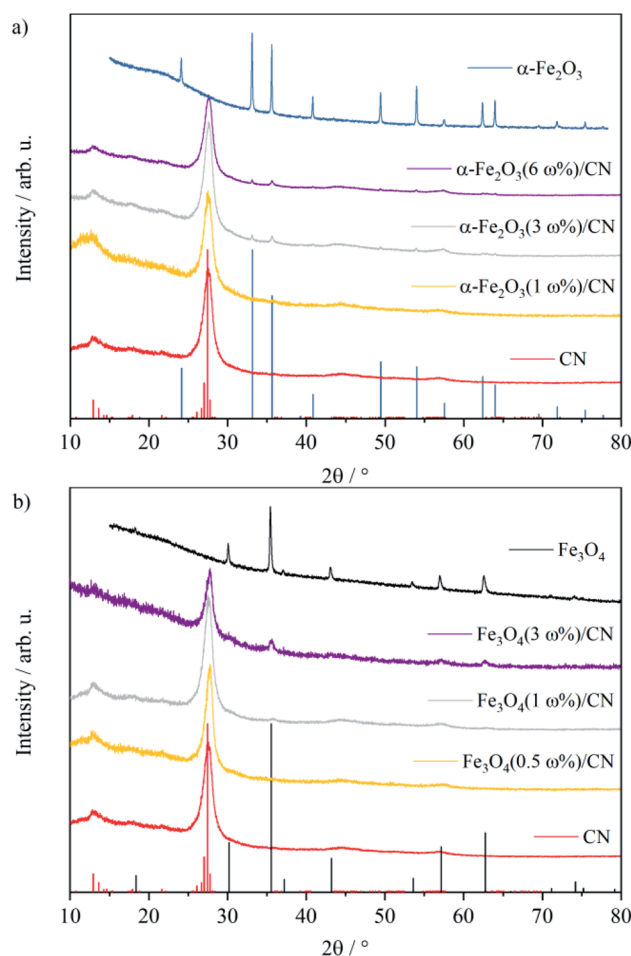


Fig. 2 PXRD patterns of the as-prepared catalysts (a) α -Fe₂O₃/CN composites, α -Fe₂O₃ and (b) Fe₃O₄/CN composites and Fe₃O₄ (references: CN ICDD 00-066-0813,⁴⁰ red bars; α -Fe₂O₃ ICDD 01-089-0597,⁴² blue bars; Fe₃O₄ ICDD 00-019-0629,⁴¹ black bars).



solution of $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ and $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ ($\alpha\text{-Fe}_2\text{O}_3$) or from $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ (Fe_3O_4). After addition of KOH the solutions were transferred to a microwave reactor and heated for 1.5 h, respectively 2 h. To obtain iron oxide/CN composites, CN particles were added to the solutions. Different iron oxide loadings on the CN material particles were obtained by variation of the ratio iron precursor:CN. To determine the iron oxide loading of the resulting iron oxide/CN composites, thermogravimetric analyzes were carried out (Fig. 1).

For the $\alpha\text{-Fe}_2\text{O}_3$ /CN composites, loadings of 1 $\omega\%$, 3 $\omega\%$ and 6 $\omega\%$ of $\alpha\text{-Fe}_2\text{O}_3$ were obtained, and Fe_3O_4 /CN composites with a Fe_3O_4 content of 0.5 $\omega\%$, 1 $\omega\%$ and 3 $\omega\%$ were isolated. The XRD patterns of the as-prepared iron oxides and the CN material are in good agreement with the literature ref. 40–42 (Fig. 2 and SI1†) and the phase purity of $\alpha\text{-Fe}_2\text{O}_3$ and Fe_3O_4 is verified. The crystallite size of $\alpha\text{-Fe}_2\text{O}_3$ and Fe_3O_4 is determined to 74 ± 18 nm and 45 ± 5 nm respectively according to the Scherrer equation. The reflexes for CN at $2\theta = 12.9^\circ$ and $2\theta = 27.6^\circ$ correspond to the (100) and (002) planes.^{40,43} For the iron oxide/CN composites ($\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN, $\alpha\text{-Fe}_2\text{O}_3$ (6 $\omega\%$)/CN, Fe_3O_4 (3 $\omega\%$)/CN) the broad main reflexes of the iron oxides at $2\theta = 33.1^\circ$ and $2\theta = 35.5^\circ$ for $\alpha\text{-Fe}_2\text{O}_3$ and at $2\theta = 35.6^\circ$ for Fe_3O_4 indicate that these particles are even of smaller crystallite size

than the as-prepared iron oxide particles. However, for samples with iron oxide loadings lower than 3 $\omega\%$ (SI1†) PXRD was not sensitive enough for characterization but TGA and magnetic behaviour support the successful composite formation.

Iron oxides, CN particles and the corresponding composites show absorption in the visible light region.^{12,15,23,37,44} The absorption edge of the CN material at 475 nm and the calculated band gap of 2.8 eV are in good agreement with reported data (Fig. 3a and SI2†).^{12,28} As expected on the basis of previous reports the black Fe_3O_4 particles absorb the whole spectrum of the irradiated light, which prevents the determination of the band gap by UV-vis.¹⁵ The calculated band gap of 2.1 eV for $\alpha\text{-Fe}_2\text{O}_3$ and the absorption edge of 651 nm are in good agreement with literature data (Fig. 3a and SI2†).³⁰ Due to the combination of the CN materials with $\alpha\text{-Fe}_2\text{O}_3$ (Fig. 3a), a bathochromic shift is observed with increasing $\alpha\text{-Fe}_2\text{O}_3$ loading. The absorption edges are in the range of 496 nm–545 nm. The baseline approach⁴⁵ to determine the direct and indirect band gaps of the iron oxide/CN composites (SI2†) gave band gaps of 2.7 eV–2.8 eV for the $\alpha\text{-Fe}_2\text{O}_3$ /CN composites. For the Fe_3O_4 /CN composites similar absorption curves are observed in the UV-vis spectra (Fig. 3b). The absorption edges for the composites with different Fe_3O_4 loading are in the range of 470 nm–480 nm and the band gaps are calculated to be 2.7 eV–2.8 eV (SI2†). The values of the composites do not change significantly as compared to the band gap of as prepared CN with 2.8 eV.

The specific surface areas are determined by nitrogen absorption measurements. A specific surface area of $20 \text{ m}^2 \text{ g}^{-1}$ was obtained for $\alpha\text{-Fe}_2\text{O}_3$ particles and $14 \text{ m}^2 \text{ g}^{-1}$ for Fe_3O_4 . The composites reveal surface areas of $22 \text{ m}^2 \text{ g}^{-1}$ for $\alpha\text{-Fe}_2\text{O}_3$ (1 $\omega\%$)/CN, $21 \text{ m}^2 \text{ g}^{-1}$ for $\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN and $23 \text{ m}^2 \text{ g}^{-1}$ for $\alpha\text{-Fe}_2\text{O}_3$ (6 $\omega\%$)/CN. The Fe_3O_4 /CN composites show surface areas of $39 \text{ m}^2 \text{ g}^{-1}$ for Fe_3O_4 (0.5 $\omega\%$)/CN, $48 \text{ m}^2 \text{ g}^{-1}$ for Fe_3O_4 (1 $\omega\%$)/CN and $22 \text{ m}^2 \text{ g}^{-1}$ for Fe_3O_4 (3 $\omega\%$)/CN. The data demonstrate that the functionalization with $\alpha\text{-Fe}_2\text{O}_3$ results in a small increase in surface area compared to the pristine CN material, whose BET surface area is around $18 \text{ m}^2 \text{ g}^{-1}$. Combination of CN with Fe_3O_4 gave larger BET surface areas than for $\alpha\text{-Fe}_2\text{O}_3$ /CN composites, which is indicative for the formation of smaller Fe_3O_4 particles as compared to $\alpha\text{-Fe}_2\text{O}_3$ on CN.

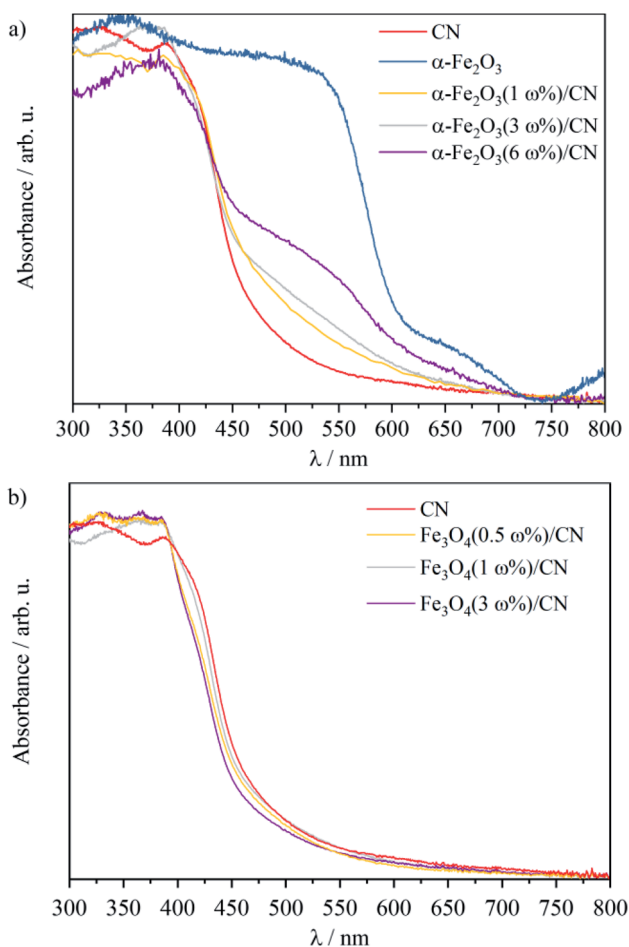


Fig. 3 Diffuse UV-vis reflectance spectra of (a) $\alpha\text{-Fe}_2\text{O}_3$ /CN and (b) Fe_3O_4 /CN composites and CN and $\alpha\text{-Fe}_2\text{O}_3$.



Fig. 4 Magnetic behavior towards a neodymium magnet of $\alpha\text{-Fe}_2\text{O}_3$, Fe_3O_4 and the corresponding iron oxide/CN composites.



To assess the potential of magnetism induced adhesion on the neodymium-containing substrate, the saturation magnetizations of the composites were determined. A value of $58.3 \text{ A m}^2 \text{ kg}^{-1}$ is obtained for the as-prepared Fe_3O_4 and for $\alpha\text{-Fe}_2\text{O}_3$ a value of $2.7 \text{ A m}^2 \text{ kg}^{-1}$ was determined. The data correspond to literature values with saturation magnetization values of $30\text{--}60 \text{ A m}^2 \text{ kg}^{-1}$ for Fe_3O_4 and $0.3\text{--}6.2 \text{ A m}^2 \text{ kg}^{-1}$ for $\alpha\text{-Fe}_2\text{O}_3$.^{46,47} For all composites, an increase in saturation magnetization with an increase of iron oxide loading is given. Values of $0.2 \text{ A m}^2 \text{ kg}^{-1}$, $0.9 \text{ A m}^2 \text{ kg}^{-1}$ and $2.0 \text{ A m}^2 \text{ kg}^{-1}$ were obtained for CN particles loaded with 1 $\omega\%$, 3 $\omega\%$ and 6 $\omega\%$ $\alpha\text{-Fe}_2\text{O}_3$, respectively. The loading with 0.5 $\omega\%$, 1 $\omega\%$ and 3 $\omega\%$ Fe_3O_4 gave compounds with magnetizations of $0.1 \text{ A m}^2 \text{ kg}^{-1}$, $0.2 \text{ A m}^2 \text{ kg}^{-1}$ and $0.5 \text{ A m}^2 \text{ kg}^{-1}$.

The increase in saturation magnetization with increase of the corresponding iron oxide loading is approximately linear, which is as expected. The low saturation magnetization of the $\text{Fe}_3\text{O}_4/\text{CN}$ materials as compared to $\alpha\text{-Fe}_2\text{O}_3/\text{CN}$ might be assigned to particle size effects (see PXRD, Fig. 2). As reported in literature, the magnetic properties of Fe_3O_4 nanoparticles are influenced by the particle and the domain size. The saturation magnetization increases with increasing particle size, regardless to domain structure and particle morphology.^{46,48,49} As expected to our assumption, the $\text{Fe}_3\text{O}_4/\text{CN}$ composites show higher specific surface areas than the $\alpha\text{-Fe}_2\text{O}_3/\text{CN}$ composites. In addition, surface oxidation of Fe_3O_4 particles is reported to result in a significant decrease of the saturation magnetization.^{46,50,51} Similar observations were reported for magnetic oxidation-sensitive $\text{La}_{0.8}\text{Sr}_{0.2}\text{MnO}_{3-\delta}$ particles.⁵²

In order to make a selection for the composites which show the highest potential for adhesion to magnetic substrates, the magnetic properties were investigated qualitatively (Fig. 4). Composites with a $\alpha\text{-Fe}_2\text{O}_3$ content of less than 3 $\omega\%$ do not show pronounced magnetic behavior. For the $\text{Fe}_3\text{O}_4/\text{CN}$ composites a loading of more than 1 $\omega\%$ Fe_3O_4 is necessary to maintain magnetic properties. In conclusion composites with a Fe_3O_4 loading of more than 1 $\omega\%$ and composites with more than 3 $\omega\%$ $\alpha\text{-Fe}_2\text{O}_3$ are suitable for the immobilization approach.

To evaluate the photocatalytic potential of the iron oxides, CN materials and the as-prepared composites, the degradation rate of an aqueous RhB ($1 \times 10^{-5} \text{ M}$) solution under visible light irradiation was studied (Fig. 5 and S13[†]). Prior to irradiation the solutions were stirred for 30 min in the dark to establish the adsorption–desorption equilibrium. The CN material decomposes 85% RhB within 25 min. The $\alpha\text{-Fe}_2\text{O}_3$ particles degrade 29% and the Fe_3O_4 particles 13% of the RhB in aqueous solution within 150 min of light irradiation. Due to the high photocatalytic degradation rates for the CN material as compared to the iron oxides, the iron content of composites of CN and $\alpha\text{-Fe}_2\text{O}_3$, respectively Fe_3O_4 , was chosen to be as low as possible, but high enough to retain magnetic behavior for the immobilization approach. $\alpha\text{-Fe}_2\text{O}_3(1 \omega\%)/\text{CN}$ shows a higher photocatalytic degradation rate for RhB than $\alpha\text{-Fe}_2\text{O}_3(3 \omega\%)/\text{CN}$, and degrades 85% RhB within 60 min (Fig. 5a), but does not show any magnetic behavior. $\alpha\text{-Fe}_2\text{O}_3(3 \omega\%)/\text{CN}$ decomposes RhB within 120 min and is better suited than $\alpha\text{-Fe}_2\text{O}_3(6 \omega\%)/\text{CN}$. The

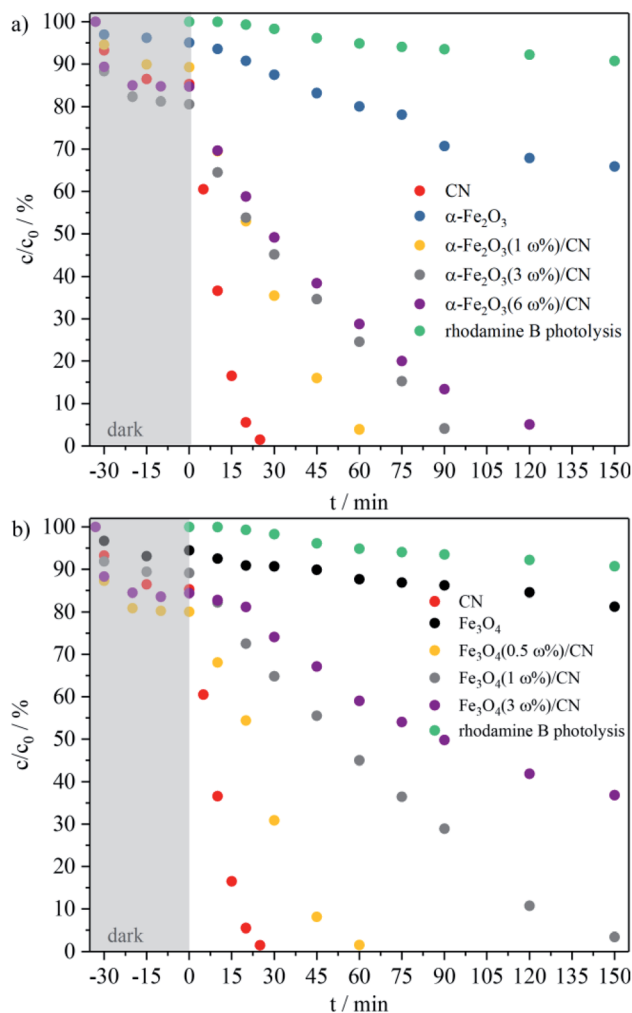
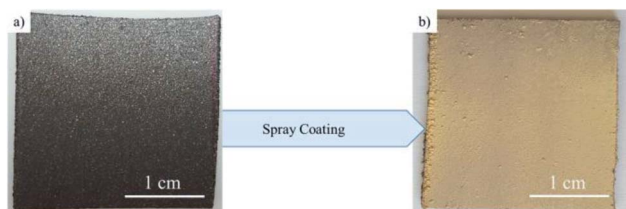


Fig. 5 Time-dependent photodegradation of an aqueous RhB solution ($1 \times 10^{-5} \text{ M}$) under visible light irradiation ($t > 0 \text{ min}$) without catalyst and in the presence of 40 mg $\alpha\text{-Fe}_2\text{O}_3$, Fe_3O_4 or CN. (a) $\alpha\text{-Fe}_2\text{O}_3/\text{CN}$ compounds and (b) $\text{Fe}_3\text{O}_4/\text{CN}$ compounds as dispersion.

same applies for the $\text{Fe}_3\text{O}_4/\text{CN}$ composites (Fig. 5b), where the composite $\text{Fe}_3\text{O}_4(0.5 \omega\%)/\text{CN}$ enables a similar degradation rate as observed for the sample $\alpha\text{-Fe}_2\text{O}_3(1 \omega\%)/\text{CN}$. A composite with a loading of 1 $\omega\%$ Fe_3O_4 degrades 85% RhB within 150 min and with $\text{Fe}_3\text{O}_4(3 \omega\%)/\text{CN}$ 48% of the initial concentration is decomposed.

The highest reaction rate constant is obtained for the CN particles with $2.7 \times 10^{-3} \text{ s}^{-1}$. The reaction rate constants of $\alpha\text{-Fe}_2\text{O}_3$ and Fe_3O_4 are significant lower with values of $0.4 \times 10^{-4} \text{ s}^{-1}$ and $0.2 \times 10^{-4} \text{ s}^{-1}$, respectively, and the reaction rate constants for the composites are found in between these values (S14[†]). All iron oxide/CN composites show lower values than CN, but higher reaction rate constants than the iron oxides themselves, which is as expected. For example, the composite $\text{Fe}_2\text{O}_3(3.5 \omega\%)/\text{CN}$ shows a methyl orange degradation of 80% in 4 h, whereas the degradation rate with pure Fe_2O_3 is only about 5%.²² Similar observations were made for $\text{Fe}_3\text{O}_4/\text{CN}$ composites. A RhB degradation rate of about 10% with Fe_3O_4 was increased to around 90% using a $\text{Fe}_3\text{O}_4(15.2 \omega\%)/\text{CN}$





Scheme 1 (a) Bare polymer substrate with embedded magnetic neodymium particles, (b) substrate coated with $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN}$ photocatalyst with an HVLP spray gun.

composite.¹⁵ However, evaluation of the literature data with the as-obtained values presented here is only possible qualitatively, since different catalyst concentrations, pollutants, pollutant concentrations and measurement setups were used.

With a deposition mass of less than 3 $\omega\%$ $\alpha\text{-Fe}_2\text{O}_3$ or less than 1 $\omega\%$ Fe_3O_4 for the iron oxide/CN particles, the corresponding composites do not show magnetic behavior. Regarding the photocatalytic activity of the magnetic composites, $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN}$ shows the highest degradation rate for an aqueous RhB solution and is therefore selected for the immobilization approach.

Spray coating of magnetic $\alpha\text{-Fe}_2\text{O}_3/\text{CN}$ composites

To immobilize the as-prepared magnetic catalyst particles, a polymer substrate with embedded magnetic neodymium particles was used. A dispersion of $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN}$ in methanol was prepared and deposited on the substrates using a HVLP spray gun at a 100 psi working pressure. The substrate is heated at 80 °C to evaporate the solvent during the deposition process (Scheme 1).

For the degradation experiments of RhB, different amounts of the photocatalyst were deposited on the substrates. Fig. 6 shows the light microscope images of the samples $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-1}$ with a deposited mass of 1.1 mg, $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-2}$

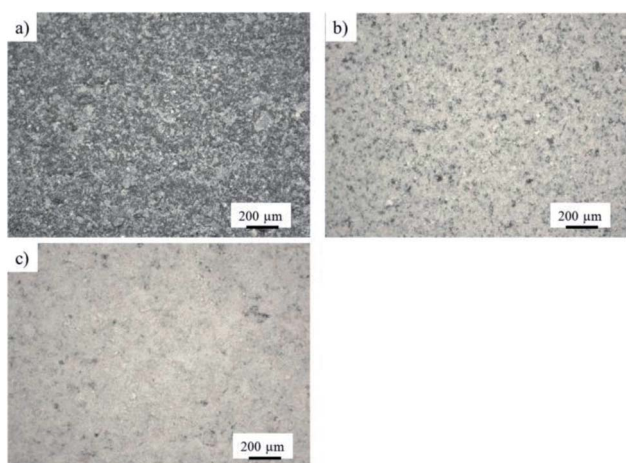


Fig. 6 Light microscope images of coatings with different deposited masses (a) $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-1}$, (b) $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-2}$ and (c) $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-3}$, 5 \times magnification.

with 2.2 mg catalyst and $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-3}$ with a mass of 3.6 mg catalyst. The deposition of a catalyst mass of 1.1 mg results in moderate coverage of the black substrate (Fig. 6a).

Deposition of 2.2 mg of the catalyst reveals better but still incomplete coverage (Fig. 6b), while deposition of 3.6 mg results in coatings with an almost full coverage (Fig. 6c). The deposition method intrinsically results in rough surfaces in any case, which is beneficial for photocatalytic activity.

Photocatalytic degradation of organic pollutants using composite coatings

To evaluate the photocatalytic degradation rates of RhB for different amounts of deposited catalyst masses, the samples were placed in a photoreactor and 35 mL of a RhB solution (1×10^{-5} M) was irradiated using visible light (Fig. 7).

The sample $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-1}$ showed the lowest degradation rate, most probably caused by the low coverage of the substrate (Fig. 6a). The sample $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-3}$ enabled a degradation of 61% RhB after 480 min irradiation time, while $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-2}$ generates a decomposition of 62% RhB. A similar RhB degradation of 56% is observed for a dispersion of $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN}$ (2.2 mg) (SI5[†]).

The reaction rate constants of all coatings follow the pseudo-first order kinetic (SI4[†]). The values of $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-2}$ and $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-3}$ are almost similar with $3.5 \times 10^{-5}\ \text{s}^{-1}$ and significantly higher than the value for $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-1}$ with $0.8 \times 10^{-5}\ \text{s}^{-1}$. As might be expected, the degree of coverage is the determining factor rather than the deposited amount.

The visible light spectra of the RhB degradation process indicate a photosensitive degradation mechanism (Fig. 8a). The slight hypsochromic shift from 554 nm to 551 nm after 480 min light irradiation is caused by the stepwise de-ethylation of the RhB molecule,^{53,54} which was observed for all three samples. The same mechanism is operating for the degradation of RhB

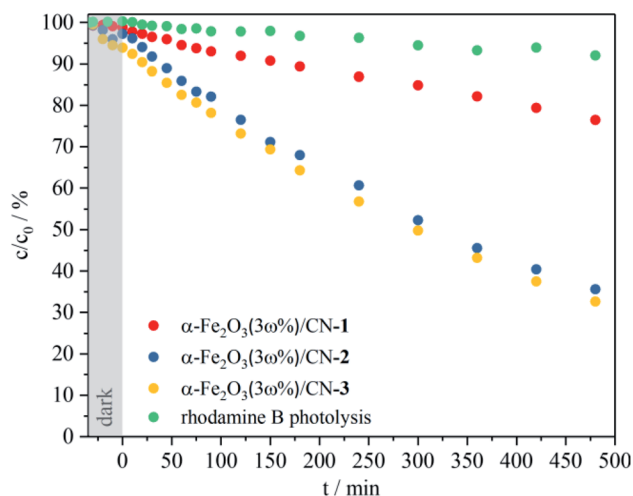


Fig. 7 Time-dependent photodegradation of an aqueous RhB solution (1×10^{-5} M) under visible light irradiation ($t > 0$ min) without catalyst and in the presence of coatings $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-1}$, $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-2}$ and $\alpha\text{-Fe}_2\text{O}_3(3\ \omega\%)/\text{CN-3}$.



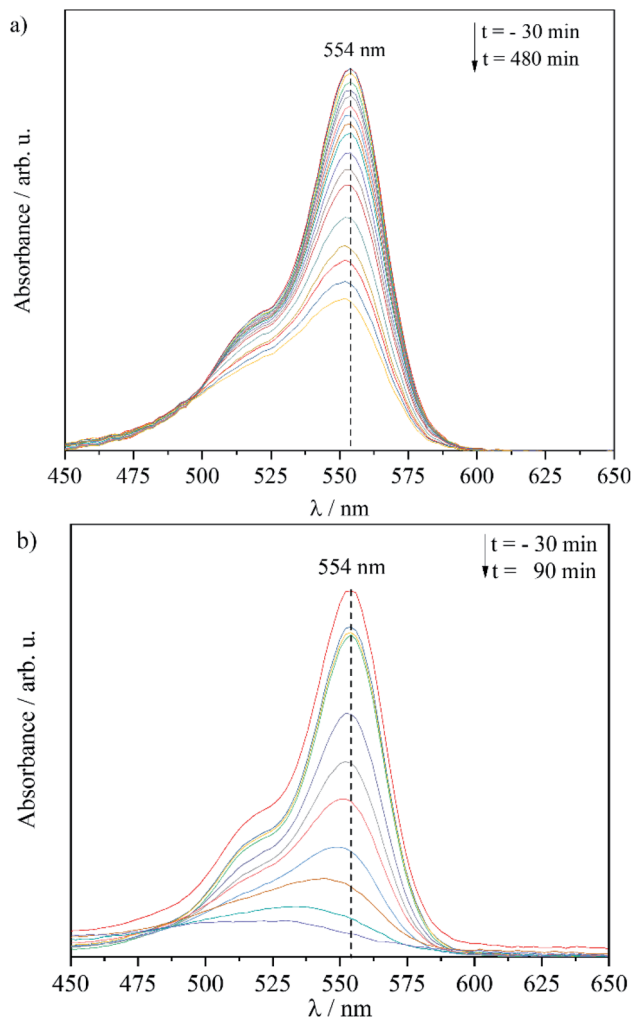


Fig. 8 Visible light spectra of RhB while photodegradation process using (a) α -Fe₂O₃(3 wt%)/CN-2 and (b) α -Fe₂O₃(3 wt%)/CN particles as photocatalyst.

with α -Fe₂O₃(3 wt%)/CN particles (Fig. 8b), where a shift of 26 nm was observed.

The RhB solutions after photocatalytic degradation with catalyst films were analyzed with ICP-MS to determine the iron content and to evaluate, if material loss occurs during the photocatalytic experiments. In addition, a solution after a photolysis measurement of a blank substrate was analyzed. For the blank sample an iron content of 0.14 mg L⁻¹ was determined. For sample α -Fe₂O₃(3 wt%)/CN-1 an iron content of 0.13 mg L⁻¹, for sample α -Fe₂O₃(3 wt%)/CN-2 a value of 0.17 mg L⁻¹ and for α -Fe₂O₃(3 wt%)/CN-3 an iron content of 0.12 mg L⁻¹ was observed. The dissolved iron in the blank sample most probably results from the neodymium particles in the polymer matrix of the substrate.

EDX measurements showed, that these magnetic particles consist of 75 wt% iron, 12 wt% neodymium and 13 wt% tungsten, and a small amount of these particles was leached out from the polymer substrate during the photocatalytic measurement. With regard to the photolysis measurement and the layers

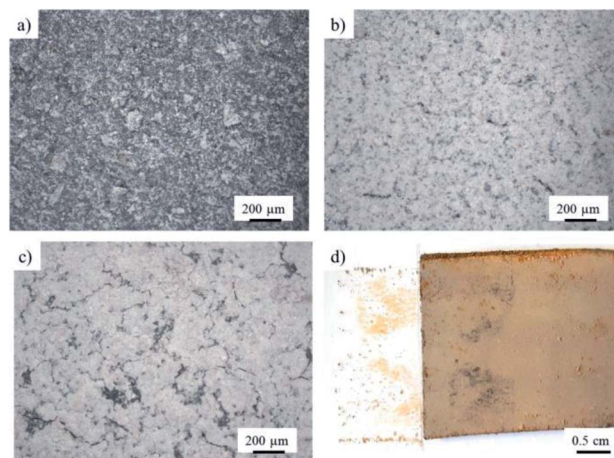


Fig. 9 Light microscope images after catalysis using coatings with different deposited masses (a) α -Fe₂O₃(3 wt%)/CN-1, (b) α -Fe₂O₃(3 wt%)/CN-2 and (c) α -Fe₂O₃(3 wt%)/CN-3, 5 \times magnification (d) scotch tape test of sample Fe₂O₃(3 wt%)/CN-2.

loaded with catalyst, the iron values do not differ significantly. Thus, it is concluded that leaching from the coatings seems to be negligible. According to the guidelines for limit values for the iron content in water by the WHO and the European Union, the iron content of drinking water should not be higher than 0.2 mg L⁻¹ while the iron content of ground water or surface water might range between 0.5–50 mg L⁻¹.⁵⁵ This limit values are not exceeded for any of the samples.

To allow a comparison of the different coatings with consideration of the different deposited masses, the activity of each sample was calculated. α -Fe₂O₃(3 wt%)/CN-2 showed the highest photocatalytic activity with 2.0 \times 10⁻¹⁰ mol mg⁻¹ min⁻¹. For sample α -Fe₂O₃(3 wt%)/CN-1 an activity of 1.5 \times 10⁻¹⁰ mol mg⁻¹ min⁻¹ and for α -Fe₂O₃(3 wt%)/CN-3 a value of

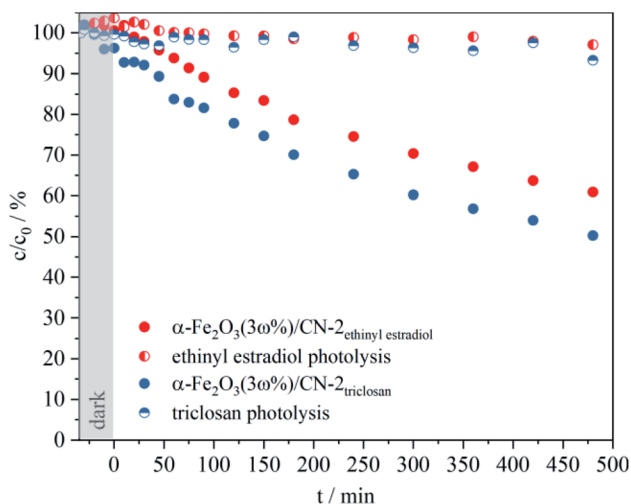


Fig. 10 Time-dependent photodegradation of aqueous ethinyl estradiol and triclosan solutions (4 \times 10⁻⁵ M) under visible-light irradiation ($t > 0$ min) without catalyst and in the presence of α -Fe₂O₃(3 wt%)/CN-2 as photocatalytic coating.



Table 1 Listed masses of starting materials to obtain the corresponding composites

Compound	FeCl ₂ ·4H ₂ O/mg	Fe(NO ₃) ₃ ·9H ₂ O/mg	KOH/mg	CN material/mg
Fe ₃ O ₄	258	—	145	—
Fe ₃ O ₄ (0.5 ω%)/CN	3	—	2	199
Fe ₃ O ₄ (1 ω%)/CN	3	—	2	99
Fe ₃ O ₄ (3 ω%)/CN	16	—	9	194
α-Fe ₂ O ₃	83	337	187	—
α-Fe ₂ O ₃ (1 ω%)/CN	8	34	48	980
α-Fe ₂ O ₃ (3 ω%)/CN	23	95	53	910
α-Fe ₂ O ₃ (6 ω%)/CN	4	17	9	95

1.2×10^{-10} mol mg⁻¹ min⁻¹ was calculated. Therefore, α-Fe₂O₃(3 ω%)/CN-2 was chosen for further experiments.

In addition, light microscope images of the coatings after catalysis were taken (Fig. 9). The layers were washed with ethanol and dried. In comparison to the images which were taken after preparation of the samples, only α-Fe₂O₃(3 ω%)/CN-3 shows significant optical changes (Fig. 9c). Cracks and holes become visible in the layer, which can be explained by leaching during the washing and drying process. Exemplarily, a scotch tape test for α-Fe₂O₃(3 ω%)/CN-2 was performed to get a qualitative idea of the adhesion strength of the catalyst to the substrate (Fig. 9d). The film is not fully resistant to external forces, but the deposited particles remain mainly adhered to the substrate.

In addition to the investigations for the degradation of RhB using the catalyst coatings, the photocatalytic degradation of other organic compounds was investigated. To evaluate the photocatalytic degradation rate for these organic pollutants, α-Fe₂O₃(3 ω%)/CN-2 coatings were selected. The photolysis of aqueous solutions of triclosan and ethinyl estradiol with a concentration of 4×10^{-5} M showed only minor degradation (Fig. 10). Using the catalyst coatings, 46% of triclosan and 40% of ethinyl estradiol were degraded after 8 h irradiation time. The determination of the reaction rate constant (SI4†) also reflects the higher degradation rate for triclosan with a value of 2.3×10^{-5} s⁻¹ compared to the value for EE2 with 1.8×10^{-5} s⁻¹.

Considering the increased concentration of the pollutant solutions (4×10^{-5} M) compared to the concentration of the RhB solution (1×10^{-5} M), a three times higher photocatalytic activity for the degradation of triclosan (6.7×10^{-10} mol mg⁻¹ min⁻¹) and ethinyl estradiol (6.3×10^{-10} mol mg⁻¹ min⁻¹) with α-Fe₂O₃(3 ω%)/CN-2 was calculated. Therefore, the as-obtained α-Fe₂O₃(3 ω%)/CN catalyst might be considered for conventional wastewater treatment plants to reduce the concentration of disinfectants and contraceptives in drinking water.

Conclusion

An easy method to obtain coatings of magnetic iron oxide/CN composite *via* a HVLP spray coating process on neodymium-containing polymeric substrates is presented. The microwave assisted synthesis gave α-Fe₂O₃/CN and Fe₃O₄/CN within less than 2 h. The as-prepared composites show band gaps of 2.7–2.8 eV and are suitable for the photocatalytic degradation of

organic pollutants. To evaluate the photocatalytic performance of CN materials, iron oxides and the corresponding composites, the materials were used to degrade RhB. The photocatalytic activity of the composites is significantly higher as compared to the iron oxides, but lower than pure CN. However, α-Fe₂O₃(3 ω%)/CN still shows a promising photocatalytic degradation rate and in addition exhibits magnetic behavior. It was therefore used for the immobilization approach on a magnetic substrate.

Starting from dispersions α-Fe₂O₃(3 ω%)/CN composites were deposited by a HVLP spray coating technique on a magnetic polymer matrix. The coating α-Fe₂O₃(3 ω%)/CN-2 (2.2 mg) decomposes 62% of an aqueous RhB solution within 8 h. A higher amount of deposited catalyst mass did not enhance the degradation rate and a lower amount of catalyst results in an incomplete coverage of the substrate and thus lower degradation efficiencies. The obtained rough surface of the coatings is beneficial for high degradation rates. The analysis of the residual dye solutions after catalysis by ICP-MS showed, that leaching of iron from the coatings can be neglected. Photocatalytic degradation of triclosan and ethinyl estradiol was successful, which demonstrates the potential of the coatings to degrade different pollutant classes such as chlorinated phenols, xanthene dyes and estrogens. Dispersions of the catalyst particles enable higher photocatalytic degradation rates of aqueous pollutant solutions as compared to the coatings, but the immobilization approach makes cost-intensive separation steps redundant. In this way, organic pollutants that were previously difficult to remove by conventional techniques, might be removed from drinking water by photocatalytically active coatings using sunlight.

Experimental section

Chemicals

Dicyandiamide (99% Co. Alfa Aesar) was dried with P₂O₅ for 5 days under vacuum before usage. FeCl₂·4H₂O (Co. Merck), Fe(NO₃)₃·9H₂O (Co. Merck) and KOH (Co. Merck) were used as received. The polymer matrix with embedded neodymium particles was received from dogeo GmbH.

Catalyst preparation

The dried dicyandiamide is decomposed in a crucible with a lid at 550 °C for 4 h using a heating rate of 5 K min⁻¹. The obtained yellow powder is grinded in a mortar and sieved to a particle size



smaller than 100 μm . To prepare $\alpha\text{-Fe}_2\text{O}_3/\text{CN}$ composites, the CN materials are placed in a microwave vessel and dispersed in 5 mL distilled water under vigorous stirring. Then $\text{Fe}(\text{NO}_3)_3 \cdot 9\text{H}_2\text{O}$ and $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ are added and dissolved. After addition of KOH, dissolved in 5 mL distilled water, the vessel is placed in a microwave reactor (Co. CEM) for 2 h at 130 $^\circ\text{C}$ and a power of 200 W is applied. The as-obtained beige magnetic powder is collected by centrifugation, washed with distilled water several times and dried at 120 $^\circ\text{C}$. For the preparation of the $\text{Fe}_3\text{O}_4/\text{CN}$ composites, CN particles are dispersed in 5 mL distilled water in a microwave vessel. Then $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ is dissolved and after addition of KOH in 5 mL distilled water, the vessel is placed in the microwave reactor for 1.5 h at 160 $^\circ\text{C}$ at 200 W. The as-obtained powder is washed and dried to give the $\text{Fe}_3\text{O}_4/\text{CN}$ composites. For the synthesis of Fe_3O_4 and $\alpha\text{-Fe}_2\text{O}_3$ particles, the parameters are chosen according to the above described method. The corresponding masses of the used starting materials are listed in Table 1.

Spray coating

The spray coating process of $\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN composite is carried out with a HVLP (high volume low pressure) airbrush spray gun. The spray gun is equipped with a 0.5 mm nozzle and operates at a working pressure of 100 psi with a working distance of approximately 20 cm. During the coating process the substrate is placed on a heat plate with a temperature of 80 $^\circ\text{C}$. The as-prepared particles are dispersed in methanol with a mass concentration of 3 g L^{-1} and sprayed on a 23 mm–25 mm polymer matrix with embedded magnetic neodymium particles. To determine the deposited masses, the samples were weighed after the spraying process. The samples were labelled according to their deposited masses, whereupon sample $\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN-1 shows a deposited mass of 1.1 mg, $\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN-2 2.2 mg catalyst and $\alpha\text{-Fe}_2\text{O}_3$ (3 $\omega\%$)/CN-3 with a mass of 3.6 mg catalyst.

Evaluation of the photocatalytic activity

The photocatalytic activity of the as-prepared composite coatings was evaluated in a water cooled glass reactor ($T = 15$ $^\circ\text{C}$) using the coated carrier material and 35 mL of an aqueous solution of 1×10^{-5} M RhB, 4×10^{-5} M triclosan and 4×10^{-5} M ethinyl estradiol (EE2). The concentrations of the pollutant solutions (triclosan, EE2) are higher compared to the RhB solution due to the different absorption coefficients. To allow reproducible and accurate traceability by UV-vis, higher concentrations have to be used for triclosan and EE2. The photoreactor is equipped with a 300 W xenon lamp (type Cermax® VQTM ME300BF, Co. Perkin Elmer, intensity of ~ 1839 W m^{-2}). A hot mirror filter ($\lambda \leq 700$ nm) is located within a distance of 12.3 cm at one side of the reactor and directly illuminates an area of 4.5 cm^2 . A cut-off filter (λ_c ($\tau_1 = 0.50$) = 420 ± 6 nm, GG420, Co. Schott) is used to remove the UV light. Before illumination, the solutions are stirred for 30 min in the dark to establish the adsorption–desorption equilibrium of the dye at the catalyst surface, which was verified by UV-vis measurements. The progress of photodegradation was studied

using *in situ* UV-vis spectroscopy. The illumination process is interrupted by stopping to stir and darkening the light beam by a cover prior to the UV-vis measurement. The interval of measurement is timed every 10 min for the first 30 min, every 15 min between 30 min to 90 min, every 30 min between 90 min and 180 min and every 60 min to the last measurement after 480 min. The concentration of the pollutant is determined by calculating the area under the UV-vis curve from 450 nm–600 nm for RhB, 200 nm–300 nm for triclosan and ethinyl estradiol. The photodegradation is plotted as a function of the irradiation time. The photocatalytic degradation using dispersions is carried out analogously, while 40 mL of 1×10^{-5} M RhB solution and 40 mg of the catalyst are used. The photocatalytic activity A is calculated according to the equation:

$$A = \frac{c_0 \times X_{\text{PC}} \times V}{m_{\text{Cat}} \times t_{\text{PC}} \times 100}$$

here, c_0 is the initial concentration of the pollutant solution, V is the volume of the solution, X_{PC} is the conversion in moles at the time t_{PC} and m_{Cat} is the catalyst mass. The determination of the photocatalytic activity for coatings is carried out by means of the conversion after 480 min irradiation time. The photocatalytic activity for dispersed particles is calculated using the determined degradation after 20 min irradiation time.

Materials characterization

Powder X-ray diffraction (XRD) was carried out with a STOE-STADI-P diffractometer equipped with a Ge(111)-monochromator. The X-ray source was $\text{CuK}_{\alpha 1}$ -radiation (40 kV, 40 mA). The crystallite size was estimated using the formula determined by the Scherrer equation

$$\tau = \frac{K\lambda}{\beta \cos \theta}$$

where τ is the volume-weighted crystallite size in nanometers, K is the Scherrer constant, here taken as 1.0, λ is the X-ray wavelength, θ is the Bragg angle and β is the full width of diffraction line at half of the maximum intensity (FWHM; background subtracted). The FWHM is corrected for instrumental broadening using a LaB₆ US National Institute of Standards and Technology (NIST). Diffuse reflectance UV-vis spectroscopy was performed using a Carry 60 UV-vis (Co. Agilent Technologies) equipped with a Barrelineo™ (Co. Harrick Scientific Products) remote diffuse reflection probe. The band gap E_g of the semiconductor was estimated according to the equation

$$(\alpha h\nu)^{1/n} = A(h\nu - E_g)$$

where α is the absorption coefficient of the material, $h\nu$ is the photon energy and A represents a proportionality constant. For a direct band gap $n = 0.5$, for determination of an indirect band gap $n = 2$.⁵⁶ In accordance to literature data direct band gaps were assumed for CN, $\alpha\text{-Fe}_2\text{O}_3$ and Fe_3O_4 (ref. 57–60) and direct as well as indirect band gaps for the composites using the baseline approach were calculated. The photocatalytic dye decomposition was analyzed by *in situ* UV-vis spectroscopy using a Carry 60 UV-vis (Co. Agilent Technologies) equipped



with fiber optics. Nitrogen physisorption isotherms were obtained at $-196\text{ }^{\circ}\text{C}$ using an Autosorb IQ2 apparatus (Co. Quantachrome). All samples were activated in vacuum at $150\text{ }^{\circ}\text{C}$ for 3 h prior to the measurements. Specific surface areas were calculated applying the single point BET equation ($p/p_0 = 0.150 \pm 0.002$). The light microscope images were carried out on an Axio Scope.A1 (Co. Zeiss), equipped with a HBO 100 illuminator and halogen lamp Hal 100 under polarized light. Thermogravimetric analyzes (Co. Mettler Toledo) were measured under synthetic air atmosphere with a flow rate of 50 mL min^{-1} and heat rate of 10 K min^{-1} in a temperature range between $30\text{ }^{\circ}\text{C}$ to $800\text{ }^{\circ}\text{C}$. EDX spectroscopy and elemental mappings were performed using a XL 30 (Co. Philips). The magnetization measurements were carried out on a MPMS Squid MS 3 (Co. Quantum Design) with a magnetic field of 3 T. The ICP-MS measurements were carried out by adding 4 mL of 63% HNO_3 to 20 mL of the degraded solution (RhB ; $1 \times 10^{-5}\text{ M}$) after an irradiation time of 480 min and usage the $\alpha\text{-Fe}_2\text{O}_3(3\text{ }\omega\%)$ /CN layers as catalysts in order to convert dissolved iron into soluble compounds. The samples were analyzed by Berghof Analytik + Umweltengineering GmbH. A sample after a photolysis measurement was also analyzed. Therefore, a blank substrate was irradiated for 480 minutes.

Conflicts of interest

There are no conflicts to declare.

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