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Performance and reaction mechanisms of tin compounds as high-capacity negative electrodes of lithium and sodium ion batteries

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We study the characteristics of tin sulfide (SnS) and tin phosphate (Sn₄P₃) as negative electrodes for rechargeable Li and Na ion batteries by first-principles calculations. The electrode reaction formulae during the discharge processes are fully revealed by the energy analyses of ternary A–Sn–B (A = Li, Na; B = S, P) phase diagrams. The phase diagrams of ternary systems with the constructed convex-hull surfaces show a possible reaction route considering intermediate products in discharge reactions. The voltage–capacity curves along the reaction paths obtained from the ternary phase diagrams are calculated. To evaluate the battery performance of tin compounds, we analyze the volume expansion ratios of the materials by incorporation of Li and Na ions. In the case of Li/SnS, Na/SnS, and Li/Sn₄P₃, it is found that the conversion reactions and subsequently the alloying reactions proceed stepwise in the electrode, contributing to their high capacities. In Na/Sn₄P₃, however, the conversion and alloying reactions proceed alternately or simultaneously, showing more complex reactions than the others.

Introduction

In the last few decades, the invention of lithium-ion batteries has dramatically changed our lives and led to various developments through the storage and efficient use of electrical energy. Nowadays, electrical energy is widely used in mobile phones, cameras, laptops, power tools, *etc.* and has become an indispensable technology deeply connected to our lives. As the use of power sources is further expanding in the market and becoming larger in size, there is a demand for a secondary battery that is good in terms of both cost and performance.

In recent years, the environmental damage caused due to industrial development has become a global concern, so the effective use of power generation systems using natural energies including solar power has been promoted. Until now, one of the reasons why renewable energy power generation has not been mainstream is the disadvantage that the amount of power supply is not constant. The amount of power supply from renewable energy sources increases or decreases due to the environmental factors on which the system depends (such as day or night and weather). To stably operate renewable energy power supplies, temporary storage of the generated energy is necessary. A large stationary power supply with a high energy density is useful for reducing the difference in electricity consumption between day and night.

The construction of large-scale energy storage facilities requires secondary batteries that excel in both cost and performance. Currently, Li-ion batteries,1-5 which are typically composed of a LiCoO₂ cathode and a C anode, use expensive rare metals (such as Li and Co) that are distributed through limited countries, and it is difficult to produce huge amounts of batteries enough to meet future requirements. It is necessary to develop battery storage systems that are good in terms of cost and performance as an alternative to the currently used Li-ion batteries. If rare metals can be replaced with relatively inexpensive and readily available elements, the mass production of rechargeable ion batteries becomes possible. In particular, Li, which plays a key role as charge carriers, is an expensive metal because of its limited production area. Materials research studies have been carried out for developing novel electrodes to replace Li with inexpensive elements such as Na,⁶⁻⁹ K and Mg.^{10–13}

In typical Li-ion batteries, Li-insertion and Li-intercalation reactions have been known as the primary atomistic mechanisms in $LiCoO_2$ cathode and C anode reactions, respectively, with high cycle performance. In Na ion batteries, however, the carrier ions have a larger ionic radius than Li, and thus suitable electrode materials are needed to promote the insertion/intercalation reactions, although superior battery performance has

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not been easily realized for large-size ionic species.^{14–16} Since the conversion or alloying reactions generate compounds or alloys with carrier ions,^{17–21} which differ from an initial electrode material, the storage capacity does not strongly depend on the ionic radius but is determined by the reaction path expected from the phase stability of the negative electrode material and the carrier ions. Even for Na with a larger ionic radius than Li, a higher storage capacity can be obtained for conversion-type electrodes. We have theoretically studied candidate anode and cathode materials with conversion-type electrochemical reactions applicable to Na batteries.^{22–27}

The idea of using alloy-based negative electrodes, especially Sn-based materials due to their nontoxicity and low cost, has attracted great interest to achieve high capacities with low voltages. In this study, we focus our attention on Sn sulfides and phosphates (SnS and Sn₄P₃ as initial electrode materials) as candidate materials for negative electrodes in both Li- and Naion rechargeable batteries. Elemental Sn itself has been expected to be one of the candidate negative electrode materials because of its high capacity, sufficient Na-reserve ability, and high safety, and the alloying reactions producing Li-Sn or Na-Sn alloys have been considered to be key reaction mechanisms in Sn electrodes.²⁸⁻³⁴ However, Sn electrodes show significant deterioration of the cycle characteristics due to the large volume expansion with Li or Na absorption.²⁸⁻³⁴ Sn oxides (such as SnO and SnO₂) and sulfides (such as SnS₂) have been experimentally studied as negative electrodes for Na-ion batteries,^{35–38} but their reversible capacities are still lower than those of Sn.

One advantage of Sn-compound electrodes is that the capacity can be expected to further increase due to the multi-step reaction processes including conversion reactions in addition to alloving reactions. Also, if the volume changes between products before and after the reactions are small, the performance degradation due to the volume expansion can be reduced. In Sn-compound negative electrodes, it is expected that two types of battery reactions including conversion reactions (possibly producing binary Li/Na-S/P or ternary Li/Na-Sn-S/P products) and alloying reactions (possibly producing Li/Na-Sn alloys) can proceed sequentially, and the former may improve the longevity of the cycle characteristics of anodes. Many experimental studies have been conducted aiming to develop negative electrode materials with Sn-containing structures, which can achieve better electrochemical performance with both good cycle performance and high capacities for Li- and Na-ion rechargeable batteries,39-45 but detailed microscopic reaction mechanisms are not clear yet.

To systematically understand the Li- and Na-ion battery performances of Sn sulfides and phosphates, we calculate the discharge reaction processes for SnS and Sn_4P_3 negative electrodes. We compare the differences in battery performance and the reaction pathways depending on various compounds (S or P) and the carrier ions (Li or Na). The first-principles electronic state calculation method is used to accurately predict the charge/discharge reaction processes and to calculate the voltage–capacity characteristics, which enables us to propose powerful battery material candidates from a theoretical point of view. From the theoretical viewpoint, extensive energy analyses on ternary phase diagrams clarified the voltage–capacity curves and the volume expansion ratios during the discharge processes in the Sn-compound electrodes. In this study, the battery performance is predicted by comparing the formation energies from first-principles calculations, and our results will be a clue to design superior materials if we can find regularity in the reaction process of each tin additive and ion carrier.

Materials and methods

To obtain the discharge reaction formulae of the SnS and Sn_4P_3 electrodes during the discharge processes in half-cell systems with Li and Na (described as Li/SnS, Na/SnS, Li/Sn₄P₃ and Na/Sn₄P₃), we theoretically search for the most stable reaction pathways on the ternary A–Sn–B (A = Li, Na; B = S, P) energetic phase diagrams by using formation energy analyses with first-principles calculations. To construct ternary energetic phase diagrams, we consider all the $A_xSn_yB_z$ materials that are listed in the crystal structure databases Crystallography Open Database⁴⁶ and AtomWork,⁴⁷ from which the experimentally known crystal structures have been collected. The formation energies (*H*) of $A_xSn_yB_z$ are calculated with reference to elemental *A*, Sn and *B* as

$$H = E[A_x Sn_y B_z] - (xE[A] + yE[Sn] + zE[B])$$
(1)

where E[X] stands for the total energy of a material *X*. As reference materials, we calculate bcc-lithium, bcc-sodium, β -tin, α -sulfur, and Hittorf's phosphorus. For each ternary system, the convex hull surfaces are constructed, showing the thermodynamically stable phases at respective elemental composition ratios.

The first-principles calculations are performed using the VASP code,^{48,49} which is based on density functional theory (DFT) within generalized gradient approximation (GGA) by Perdew, Burke, and Ernzerhof.⁵⁰ The wave functions are expressed in projector augmented wave and plane-wave basis sets.⁵¹ The lattice constants and atomic positions of all the materials are fully optimized by first-principles calculations.

The discharge reaction formulae can be obtained from the theoretical ternary phase diagrams along the SnS–A and Sn_4P_3 –A lines considering intermediate products. Based on the obtained reaction formulae, we study the electrochemical properties of Li/SnS, Na/SnS, Li/Sn₄P₃ and Na/Sn₄P₃ systems. The voltage values can be calculated by estimating the DFT total energy differences for the given reaction formulae.^{52–54} (In the first-principles calculations, the kinetics of structural reversibility is difficult to consider under an external voltage or current applied in the charging process, especially for the present conversion/alloying-type electrodes, and understanding the reversibility will require significant advances in theoretical and modelling methodologies.).

The electrochemical compound and alloy formation by lithiation or sodiation processes is advantageous for achieving

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a higher capacity, but cycle stability is typically reduced by the volume expansion induced by incorporation of larger carrier ions. We investigate the volume expansion ratio during the discharge reaction processes and clarify the reactions that cause large volume expansion.

Results and discussion

Phase diagrams of A-Sn-B (A = Li, Na; B = S, P)

To theoretically clarify the discharge reaction processes in the tin-compound negative electrodes, we calculate the formation energies of possible reaction products using the first-principles calculations. To specify the reaction products likely formed during discharge reactions in the electrodes, we construct the ternary phase diagrams with formation energies for the A–Sn–B (A = Li, Na; B = S, P) systems as shown in Fig. 1. At each composition ratio, the calculated formation energies of several $A_x Sn_y B_z$ materials (shown by colored circles in Fig. 1) show negative values, indicating that the thermodynamically stable phases (thus the reaction products) strongly depend on the composition ratios. We determine the combinations of the most stable phases by constructing the convex hull surfaces (shown by grey lines in Fig. 1) of formation energies.

On the Sn–S and Sn–P edge lines, SnS and Sn_4P_3 (and also SnS_2 and SnP_3) are found to be thermodynamically stable, supporting that they can be actually synthesizable as the initial electrode materials. On the Li–Sn and Na–Sn edge lines, several



Fig. 1 The ternary phase diagrams of (a) Li–Sn–S, (b) Na–Sn–S, (c) Li–Sn–P, and (d) Na–Sn–P. All the experimentally known materials listed in the crystal structure databases Crystallography Open Database⁴⁶ and AtomWork⁴⁷ are calculated by DFT, and their formation energies [eqn (1)] are shown by colored circles. When the electrode reaction path (red broken lines) crosses the convex-hull lines (grey lines), phase separation into materials at each vertex can occur. The conversion and alloying reactions occur in the sky blue and pink shaded regions, respectively.

Li–Sn (Li₂Sn₅, LiSn, Li₁₃Sn₅, Li₇Sn₂ and Li₁₇Sn₄) and Na–Sn (NaSn₅, NaSn₂, NaSn, Na₉Sn₄ and Na₁₅Sn₄) binary alloy phases are found to be stable, consistent with previous reports.^{28–32}

Notable differences among the four systems are found on/ near the A–B (A = Li, Na; B = S, P) edges. In Fig. 1(a and b), Li_2S and Na_2S have the lowest energies, respectively, showing that they are very stable. The ternary materials such as Na_4SnS_4 in Fig. 1(b) also show very low energies, indicating that the ternary phases are possibly involved in discharge reactions. In Fig. 1(c and d), several binary Li–P and Na–P materials are found to be stable. The ternary material (Na_5P_3Sn in the Na–Sn–P system) can be thermodynamically stable, but no stable ternary material is found in the Li–Sn–P system. The convex-hull surfaces of the phosphide systems are shallower than those of the sulfide systems, especially in the A–B sides, indicating that Sn phosphides have lower voltages than Sn sulfides.

The phase diagrams with the convex-hull curves indicate the possible reaction routes of SnS and Sn_4P_3 electrodes with respect to Li and Na. The discharge reactions can proceed along the SnS–*A* and Sn_4P_3 –A (A = Li, Na) lines (shown by red broken lines in Fig. 1) with increasing *A* concentration, assuming constant composition ratios of Sn : S = 1 : 1 and Sn : P = 4 : 3. Following the reaction paths, we can find most likely discharge reaction products. There is no single-phase product just on the reaction paths, but the mixed phases at both ends of convex hulls can be produced in the electrodes when the reaction path crosses the convex hull lines.

Discharge reaction formulae

Table 1 lists the full discharge reaction formulae of SnS and Sn₄P₃ with Li and Na including the intermediate processes, which are derived from Fig. 1. The reaction processes in both SnS and Sn₄P₃ have a common character for Li electrodes. Firstly, binary Li–B (B = S, P) materials with the elemental Sn substance are produced, called conversion reactions. In the conversion reactions, only Li2S is produced in the Li/SnS system, but the three phases of Li₃P₇, LiP, and Li₃P are produced step by step in the Li/Sn₄P₃ system as the Li concentration increases. After the conversion reactions, the separated Sn reacts with Li producing the binary Li-Sn alloys, and subsequently the Li-Sn alloys further react with Li generating more Li-rich Li-Sn alloys, called alloying reactions. In both Li/ SnS and Li/Sn₄P₃ systems, five Li-Sn phases of Li₂Sn₅, LiSn, $Li_{13}Sn_5$, Li_7Sn_2 , and $Li_{17}Sn_4$ are sequentially generated in the alloying reactions. Therefore, one conversion and five alloying reactions in Li/SnS (six-step reactions in total) and three conversion and five alloying reactions in Li/Sn₄P₃ (eight-step reactions in total) can occur step by step as the Li concentration increases in the electrodes.

In the case of Na carrier ions, however, the discharge reactions in the tin-compound electrodes show more complicated processes because the ternary compounds are involved in the reactions. In the Na/SnS system, Na_4SnS_4 is produced in the early stage of conversion reactions, and then it is converted to Na_2S with the elemental Sn substance. After the conversion reactions, the alloying reactions generating five Na–Sn phases

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Table 1 The discharge reaction equations of SnS and Sn₄P₃ with Li and Na, which are derived from Fig. 1. The calculated voltages (*V*) and volume expansion ratios of products to SnS or Sn₄P₃ (Ω/Ω_0) are listed for each reaction

	$V\left(\mathrm{V} ight)$	Ω/Ω_0
Li/SnS		
$SnS + 2Li \rightarrow Li_2S + Sn$	1.57	1.44
$5Sn + 2Li \rightarrow Li_2Sn_5$	0.69	1.54
$Li_2Sn_5 + 3Li \rightarrow 5LiSn$	0.67	1.68
$5\text{LiSn} + 8\text{Li} \rightarrow \text{Li}_{13}\text{Sn}_5$	0.50	2.11
$2Li_{13}Sn_5 + 9Li \rightarrow 5Li_7Sn_2$	0.26	2.38
$2\text{Li}_7\text{Sn}_2 + 3\text{Li} \rightarrow \text{Li}_{17}\text{Sn}_4$	0.13	2.65
Na/SnS		
4 SnS + 4 Na \rightarrow Na ₄ SnS ₄ + 3 Sn	1.30	1.60
$Na_4SnS_4 + 4Na \rightarrow Sn + 4Na_2S$	1.05	2.09
$5Sn + Na \rightarrow NaSn_5$	0.66	2.10
$2NaSn_5 + 3Na \rightarrow 5NaSn_2$	0.47	2.25
$NaSn_2 + Na \rightarrow 2NaSn$	0.43	2.53
$4NaSn + 5Na \rightarrow Na_9Sn_4$	0.14	3.14
$Na_9Sn_4 + 6Na \rightarrow Na_{15}Sn_4$	0.10	4.03
Li/Sn ₄ P ₃		
$7\mathrm{Sn}_4\mathrm{P}_3 + 9\mathrm{Li} \rightarrow 28\mathrm{Sn} + 3\mathrm{Li}_3\mathrm{P}_7$	1.05	1.37
$Li_3P_7 + 4Li \rightarrow 7LiP$	0.95	1.42
$LiP + 2Li \rightarrow Li_3P$	0.88	1.88
$5Sn + 2Li \rightarrow Li_2Sn_5$	0.69	1.82
$Li_2Sn_5 + 3Li \rightarrow 5LiSn$	0.67	1.99
$5\text{LiSn} + 8\text{Li} \rightarrow \text{Li}_{13}\text{Sn}_5$	0.50	2.50
$2\text{Li}_{13}\text{Sn}_5 + 9\text{Li} \rightarrow 5\text{Li}_7\text{Sn}_2$	0.26	2.82
$2\text{Li}_7\text{Sn}_2 + 3\text{Li} \rightarrow 5\text{Li}_{17}\text{Sn}_4$	0.13	3.17
Na/Sn ₄ P ₃		
$11\text{Sn}_4\text{P}_3 + 9\text{Na} \rightarrow 44\text{Sn} + 3\text{Na}_3\text{P}_{11}$	0.92	1.40
$Na_3P_{11} + 8Na \rightarrow 11NaP$	0.65	1.64
$3NaP + 2Na + Sn \rightarrow Na_5P_3Sn$	0.59	1.89
$2\text{Sn} + \text{Na} \rightarrow \text{NaSn}_2$	0.46	2.03
$NaSn_2 + Na \rightarrow 2NaSn$	0.43	2.29
$Na_5P_3Sn + 5Na \rightarrow NaSn + 3Na_3P$	0.22	3.06
$4NaSn + 5Na \rightarrow Na_9Sn_4$	0.14	3.82
$Na_9Sn_4 + 6Na \rightarrow Na_{15}Sn_4$	0.10	4.91

of NaSn₅, NaSn₂, NaSn, Na₉Sn₄, and Na₁₅Sn₄ proceed step by step. In the Na/Sn₄P₃ system, it is found that the conversion and alloying reactions are not well divided by the Na concentrations in the electrode. Firstly, the binary Na₃P₁₁ and NaP and then the ternary Na₅SnP₃ are produced step by step generating elemental Sn. Secondly, the alloying reactions forming NaSn₂ and NaSn proceed. Thirdly, the ternary Na₅SnP₃ reacts with Na producing Na₃P. Finally, the alloying reactions producing Na₉Sn₄ and Na₁₅Sn₄ occur. Therefore, Na/Sn₄P₃ shows a mixture of reaction mechanisms, especially in the late discharge processes.

Voltage-capacity characteristics

Based on the reaction formulae obtained from the phase diagrams, we study the electrochemical properties of the halfcell systems of SnS and $Sn_4P_3 vs$. Li and Na. To evaluate the battery performances, we calculate and compare their voltagecapacity curves. The voltage values can be estimated by calculating the DFT total energy differences for a given reaction formula.^{52–54} Fig. 2 shows the calculated voltage–capacity curves of the Li/SnS, Na/SnS, Li/Sn₄P₃, and Na/Sn₄P₃ systems. The calculated voltage values are also listed for each reaction in Table 1.



Fig. 2 The voltage–capacity curves of (a) Li/SnS, (b) Na/SnS, (c) Li/Sn₄P₃ and (d) Na/Sn₄P₃ systems as negative electrodes (blue solid lines). The experimental values of the first discharge processes (red solid lines) were taken from ref. 39 (Li/SnS), 27 (Na/SnS), 42 (Li/Sn₄P₃), and 43 (Na/Sn₄P₃).

As can be seen in both Li/SnS [Fig. 2(a)] and Na/SnS [Fig. 2(b)], the SnS electrode shows an voltage over 1 V in the early reaction processes, in which the conversion reactions occur. In Li/SnS, the voltage is about 1.6 V up to about 350 mA h g⁻¹. Even in Na/SnS, high voltages of 1.1–1.3 V are estimated at the initial stage of reactions corresponding to the conversion reactions. The voltage values show a sudden drop to less than 0.7 V at a capacity of about 400 mA h g⁻¹, where the alloying reactions start to take place. The voltages of Na/SnS are smaller than those of Li/SnS in the overall capacity range.

In Li/Sn₄P₃ [Fig. 2(c)] and Na/Sn₄P₃ [Fig. 2(d)], the voltage values are less than about 1 V in the whole capacity range (except for very beginning in Li/Sn₄P₃), and the Sn₄P₃ electrodes show lower voltages by roughly 0.5 V than the SnS electrodes in the early discharge processes. In addition, the voltage drops in the Sn₄P₃ electrodes associated with the mechanism change from the conversion to the alloying reactions are moderate compared with the cases of SnS electrodes. In the Sn₄P₃ electrodes as well, the voltages of Na/Sn₄P₃ are smaller than those of Li/Sn₄P₃ in the overall capacity range.

In both SnS and Sn_4P_3 , the voltages vs. Na are lower than those vs. Li, and the theoretical capacities for Na are comparable to those for Li. The Sn_4P_3 electrodes for both Li and Na involve a larger number of intermediate reactions compared with those in the SnS electrodes, which can contribute to smooth voltage-capacity profiles and may increase capacities in real materials.

We compare the calculated voltage–capacity curves with the reported experimental results. The experimental voltage–capacity curves of the first discharge process for Li/Sns,³⁹ Na/SnS,²⁷ Li/Sn₄P₃,⁴² and Na/Sn₄P₃⁴³ are also plotted in Fig. 2. We can observe an overall agreement between the calculated and observed curves. In the Sn₄P₃ anode for Li-ion batteries, the conversion reactions (LiP and Li₃P) and the subsequent alloying reactions (Li_xSn) have been experimentally considered, and

the formation of $Li_{13}Sn_5$ is observed by XRD.⁴² In the Sn_4P_3 anode for Na-ion batteries, the formation of $Na_{15}Sn_4$ and Na_3P has been observed experimentally.⁴³ In the SnS anode for Naion batteries, the discharge product of Na_2S has been confirmed by experiments.²⁷ These experimentally observed products are actually included in the present reaction formulae.

To be precise, the voltage values differ between calculations and experiments within 0.3 V or less in size. In particular, the calculated voltages of SnS for Li and Na overestimate the experimental values in the early reaction processes, where the conversion reactions take place. Since we calculate the voltage values at each reaction step from the energy differences before and after the reactions assuming the reaction formulae, the theoretical voltage-capacity curves show ideal step functions. In experiments, the voltage-capacity curves usually depend on actual conditions such as temperature, current rate, sample shape and additive, and multiple conversion/alloying reactions can simultaneously occur in electrodes, especially at high temperatures. In addition, the discharge reactions near surfaces or inside the electrode particles can differ, and, perhaps, the reactions near surfaces proceed before those that occur inside. Therefore, the experimental voltage-capacity profiles typically do not show ideal step-like functions and have oblique shapes. It has been experimentally reported that electrolyte materials, which are not considered in this work, significantly affect battery performances for Sn₄P₃-based electrodes.55

Volume expansion ratios during discharge

The formation of Li/Na compounds and Li/Na–Sn alloys during the discharge reactions is advantageous for increasing the capacities, but it is expected that the cycle stability decreases due to the volume increase as the amount of carrier ions increases in the electrodes. In the case of the Sn anodes, significantly large volume expansion ratios of 260% for Li and 420% for Na have been reported.^{33,34} Based on the reaction processes summarized in Table 1, we calculate the volume expansion ratios of the SnS and Sn₄P₃ electrodes with respect to the Li/Na concentration in each reaction process. The volume expansion ratio is calculated as Ω/Ω_0 , where Ω is the volume of products after lithiation or sodiation and Ω_0 is the volume of SnS or Sn₄P₃ ($\Omega_0 = \Omega_{SnS}$ or Ω_{Sn4P3}) per SnS or Sn₄P₃.

Fig. 3 shows the calculated volume expansion ratios of the SnS and Sn_4P_3 electrodes (the initial materials as the references) during the discharge processes for Li and Na carrier ions. Generally, the volume expansion ratio is related to the number of Li or Na ions incorporated into the SnS or Sn_4P_3 electrode. Sn_4P_3 shows a slightly larger volume expansion than SnS in the entire capacity range for both Li and Na carrier ions. Therefore, SnS is better than Sn_4P_3 in terms of volume changes. For the Li carrier in the small capacity range near 400 mA h g⁻¹, the volume of the Sn_4P_3 electrode largely increases due to the formation of Li_3P compared with the SnS electrode generating Li_2S. The difference of ionic radii between Li and Na ions essentially affects the volume expansion and therefore the cycle



Fig. 3 The volume expansion ratios of (a) Li/SnS, (b) Na/SnS, (c) Li/Sn₄P₃ and (d) Na/Sn₄P₃ as negative electrodes.

characteristics. Since the volumes of the Na compounds and alloys in the reactions are larger than those of Li compounds, the volume expansion in the whole capacity range is significantly large for the Na carrier ions, showing a larger slope for Na than for Li. The volumes of the Na compounds (Na₂S and Na_xP_{1-x}) are larger than those of the Li compounds for the same composition ratio.

Conversion/alloying-type electrodes usually suffer from such large volume changes, which cause electrode deterioration such as cracks and fractures of electrode materials, leading to degradation of cycle stability.^{56,57} This is the most difficult part in their practical applications, especially for Na-ion batteries due to the larger ionic radius of Na than that of Li. Therefore, nanoparticles with smaller sizes or porous structures of the electrode materials, in which stress due to volume changes can be effectively relieved, may be particularly suitable for Na-ion battery applications,^{56,57} as experimentally reported for the Sn nanoparticle anodes.³³

Conclusions

We investigate the battery characteristics of SnS and Sn_4P_3 materials as negative electrodes for both Li- and Na-ion rechargeable batteries by first-principles calculations. We clarify the detailed discharge reaction processes in the electrodes from the energy analyses based on the first-principles calculations. Considering all the possible $A_xSn_yB_z$ (A = Li, Na; B = S, P) crystals that are listed in the databases, we calculate the ternary A–Sn–B phase diagrams with formation energies and construct the energy convex-hull surfaces. From the phase diagrams, we clarify the discharge reaction paths including intermediate reactions following the convex-hull curves.

In SnS and Sn_4P_3 for Li carrier-ions, it is found that first the conversion reactions producing the binary Li–S and Li–P compounds with elemental Sn proceed and then the alloying

reactions forming the Li–Sn alloys follow stepwise. In the case of Na ions, on the other hand, it is found that ternary materials are involved in the reactions, making the reaction processes complex, and the conversion and alloying reactions can proceed alternately and simultaneously in the Na/Sn₄P₃ system. Based on the obtained reaction processes, we evaluate the voltage–capacity curves of SnS and Sn₄P₃ vs. Li and Na. In both materials, the voltages for Na are lower than those for Li, and the theoretical capacities for Na are comparable to those for Li. In the case of Na, we find a larger number of intermediate reaction processes than those for Li, which may increase the capacities of the electrodes in Na-ion batteries. In terms of voltage values, Sn₄P₃ shows lower values than SnS for both Liand Na-ion batteries, especially in the early reaction stage, being suitable for anode materials.

In the discharge reactions, Li/Na compounds and Li/Na–Sn alloys are formed in the electrodes, which is advantageous for increasing the capacity. However, it is expected that cycle performance decreases due to the volume expansion by incorporating carrier ions. We actually estimate the volume expansion ratio in each reaction process. Because the ionic radius of Na ions is larger than that of Li ions, the volumes of products with Na significantly expand in the whole capacity range. Although Sn_4P_3 and SnS have large theoretical capacities, Sn_4P_3 suffers from larger volume expansion than SnS, especially for Na-ion battery applications.

Author contributions

Hiroki Kotaka: conceptualization, data curation, formal analysis, investigation, methodology, software, visualization, and writing – original draft; Hiroyoshi Momida and Tamio Oguchi: funding acquisition, project administration, resources, supervision, and writing – review and editing.

Conflicts of interest

There are no conflicts to declare.

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