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Modeling and simulation for Cattaneo–Christov heat analysis of entropy optimized hybrid nanomaterial flow

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Here, the hydromagnetic entropy optimized flow of a hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanoliquid by a curved stretchable surface is addressed. The Darcy–Forchheimer model is utilized for porous space. Lead (Pb) and ferric oxide (Fe₂O₃) are considered the nanoparticles and ethylene glycol (C₂H₆O₂) as the base liquid. Thermal expression consists of dissipation and ohmic heating. Entropy generation is under consideration. The Cattaneo–Christov heat flux impact is discussed. Non-dimensional partial expressions by adequate transformations have been reduced to ordinary differential systems. The ND-solve technique is implemented for numerical solutions of dimensionless systems. Graphical illustrations of velocity, thermal field and entropy against influential variables for both nanoliquid (Pb/C₂H₆O₂) and hybrid nanoliquid (Pb + Fe₂O₃/C₂H₆O₂) are presented. Graphical illustrations of velocity, thermal field and entropy against sundry variables for both nanoliquid (Pb/C₂H₆O₂) and hybrid nanoliquid (Pb + Fe₂O₃/C₂H₆O₂) are presented. Influences of sundry variables on the Nusselt number and drag force for both nanoliquid (Pb/C₂H₆O₂) and hybrid nanoliquid (Pb + Fe₂O₃/C₂H₆O₂) are examined. A higher thermal relaxation time tends to intensify the heat transport rate and temperature. An increment in the magnetic variable leads to an enhancement of the entropy and thermal field. An improvement in liquid flow is seen for volume fraction variables. Velocity against the porosity variable and Forchheimer number is reduced. The Brinkman number leads to maximization of entropy generation.

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1. Introduction

During the past few decades, hybrid nano-fluids have become popular among researchers, scientists and engineers due to their superior heat transport properties. Hybrid nano-fluids are suspensions of two or more nano-particles in the base fluid. The heat conductive performance of convectional materials (like blood, water, engine oil, ethylene glycol, *etc.*) can be enhanced by inserting nano-particles (like silica, carbon nanotubes, silver alumina, gold, lead, ferric oxide, *etc.*). Hybrid nano-fluids possess higher thermal conductivity for heat transfer phenomena such as those relevant to engines, vehicle radiators, machining, biomedicine, warming procedure on buildings, hybrid powered engines, pharmaceutical industries, paper production and many others. The concept of heat transport enhancement of the base liquid through addition of nano-particles was initially given by Choi and Eastman *et al.*^{1,2} Hassan *et al.*³ examined the partial slip effect for the flow of hybrid ferro-liquids. Radiation and porous space effects were addressed. Chabani *et al.*⁴ examined the electrically conducting

hybrid (Ag–Al₂O₃/H₂O) nanomaterial flow inside a modified trapezoidal permeable enclosure. Thermal transport analysis for hybrid nanoliquids with suction/injection in a rotating system was reported by Abdollahi *et al.*⁵ Cattaneo–Christov analysis in the magnetohydrodynamic flow of ternary nanomaterials with nonlinear radiation was studied by Alqawasmi *et al.*⁶ Few latest developments related to hybrid nano-fluid flow under different geometric configurations are given in ref. 7–15.

Heat transfer is induced in view of temperature differences and subsequent temperature changes and distribution in different bodies. Heat transfer plays a significant role in industries, and biomedical and engineering processes such as those relevant to heat exchangers, air conditioning, refrigeration, equipment power collectors, fuel cells, drug targeting, microelectronics, heat conduction in tissues, *etc.* The mechanism of heat transfer was initially given by Fourier.¹⁶ Fourier's law through parabolic expression predicts the infinite speed of heat waves. It is not acceptable physically. Therefore the thermal relaxation time was taken into account by Cattaneo.¹⁷ For material invariant formulation to the Cattaneo's frame work Christov¹⁸ introduced Oldroyd's upper convected derivative. Razaq *et al.*¹⁹ explored the convective flow of the Reiner–Rivlin fluid subject to Cattaneo–Christov fluxes and MHD. Radiation impact for the magnetized flow of Prandtl nanoliquid with Cattaneo–Christov fluxes theory was given by Salmi *et al.*²⁰

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Haneef *et al.*²¹ analyzed heat transport for Oldroyd-B material flow with Cattaneo–Christov fluxes. Random motion and thermophoresis effects in magnetohydrodynamic Oldroyd-B nanoliquid flow were studied by Hayat *et al.*²² Latest articles for Cattaneo–Christov heat and mass fluxes are mentioned in ref. 23–28.

Entropy minimization (EM) optimizes thermal system performance by exploring associated irreversibility through heat and mass transfer, Joule heating and liquid friction. Entropy is a measure of uncertainty and disorderliness of a system and its surroundings. All natural processes are thermodynamically irreversible. Entropy is inversely proportional to the temperature of a system. Entropy has a direct proportion to the reversible change in heat. Entropy generation is the loss of energy in thermodynamical systems due to diffusion processes, temperature difference, electric resistance, fluid mixing, chemical reaction, radiation and resistive forces. Applications of entropy generation are found in electronic cooling systems, geothermal reservoirs, thermal and nuclear reactors and heat exchanger pumps. Entropy optimization in thermally convection flow was studied in Bejan.^{29–31} Iftikhar *et al.*³² analyzed entropy generation for non-Newtonian biviscosity fluid in a square cavity. Hayat *et al.*³³ addressed the magnetized entropy optimized flow of the Reiner–Rivlin material. Maiti *et al.*³⁴ reported entropy generation analysis for time-dependent hybrid nanoliquid flow by shrinking a disk. Latest investigations for entropy analysis are highlighted in studies.^{35–42}

This communication discusses the magnetohydrodynamic Darcy–Forchheimer flow of a hybrid nanomaterial. The Cattaneo–Christov heat relation is under consideration. Ferric oxide (Fe₂O₃) and lead (Pb) are used as nanoparticles. Ethylene glycol (C₂H₆O₂) is used as a conventional liquid. Joule heating and dissipation are considered in thermal relation. Entropy generation analysis is carried out. Governing nonlinear expressions are made dimensionless by implementation of suitable transformations. ND-solve is utilized for numerical solutions. Liquid

flow, entropy and temperature for both nanoliquid (Pb/C₂H₆O₂) and hybrid nanoliquid (Fe₂O₃ + Pb/C₂H₆O₂) are explored. Surface drag force and heat transport rate against emerging variables for nanoliquid (Pb/C₂H₆O₂) and hybrid nanoliquid (Fe₂O₃ + Pb/C₂H₆O₂) are numerically discussed.

2. Modeling

Two-dimensional magnetized flow of the hybrid (Fe₂O₃ + Pb/C₂H₆O₂) nanoliquid by the curved stretching surface is addressed. Darcy–Forchheimer model analysis is carried out. Lead (Pb) and ferric oxide (Fe₂O₃) are used as nanoparticles and ethylene glycol (C₂H₆O₂) as the base liquid. Cattaneo–Christov heat flux with ohmic heating and dissipation is under consideration. Entropy analysis is carried out. The surface has stretching velocity ($u_w = u_0 e^{s/L}$) with u_0 reference velocity. The magnetic field of constant strength (B_0) is applied. Fig. 1 comprises a physical model.⁴³

The governing equations satisfy:^{44–49}

$$\frac{\partial}{\partial r}((r+R)v) + R \frac{\partial u}{\partial s} = 0, \quad (1)$$

$$\frac{1}{(r+R)} u^2 = \frac{1}{\rho_{\text{hnf}}} \frac{\partial p}{\partial r}, \quad (2)$$

$$\begin{aligned} v \frac{\partial u}{\partial r} + \frac{uR}{(r+R)} \frac{\partial u}{\partial s} + \frac{u}{(r+R)} v = \\ - \frac{1}{\rho_{\text{hnf}}} \frac{R}{(r+R)} \frac{\mu_{\text{hnf}}}{\rho_{\text{hnf}}} \left(\frac{\partial^2 u}{\partial r^2} + \frac{1}{(r+R)} \frac{\partial u}{\partial r} - \frac{u}{(r+R)^2} \right) \\ - \left. \frac{\sigma_{\text{hnf}} B_0^2 u}{\rho_{\text{hnf}}} - \frac{\mu_{\text{hnf}}}{\rho_{\text{hnf}}} \frac{1}{k_p} u - F u^2 \right\}, \quad (3) \end{aligned}$$

$$\left. \begin{aligned} v \frac{\partial T}{\partial r} + \frac{uR}{(r+R)} \frac{\partial T}{\partial s} - \frac{\mu_{\text{hnf}}}{(\rho c_p)_{\text{hnf}}} \left(\frac{\partial u}{\partial r} + \frac{u}{(r+R)} \right)^2 - \frac{\sigma_{\text{hnf}}}{(\rho c_p)_{\text{hnf}}} B_0^2 u^2 - 2\delta_E \frac{\sigma_{\text{hnf}}}{(\rho c_p)_{\text{hnf}}} B_0^2 \left(uv \frac{\partial u}{\partial r} + u^2 \frac{R}{(r+R)} \frac{\partial u}{\partial s} \right) \\ + \delta_E \left(v \frac{\partial v}{\partial r} \frac{\partial T}{\partial r} + v^2 \frac{\partial^2 T}{\partial r^2} + \frac{vR}{(r+R)} \frac{\partial u}{\partial r} \frac{\partial T}{\partial s} + 2uv \frac{R}{(r+R)} \frac{\partial^2 T}{\partial r \partial s} - uv \frac{R}{(r+R)^2} \frac{\partial T}{\partial s} \right. \\ \left. + \frac{uR}{(r+R)} \frac{\partial T}{\partial r} \frac{\partial v}{\partial s} + u \left(\frac{R}{(r+R)} \right)^2 \frac{\partial u}{\partial s} \frac{\partial T}{\partial s} + \left(\frac{uR}{(r+R)} \right)^2 \frac{\partial^2 T}{\partial s^2} \right) \\ - 2\delta_E \frac{\mu_{\text{hnf}}}{(\rho c_p)_{\text{hnf}}} \left(v \frac{\partial u}{\partial r} \frac{\partial^2 u}{\partial r^2} + \frac{v}{(r+R)} \left(\frac{\partial u}{\partial r} \right)^2 + \frac{uv}{(r+R)} \frac{\partial^2 u}{\partial r^2} - \frac{u^2 v}{(r+R)^3} + \frac{uR}{(r+R)} \frac{\partial u}{\partial r} \frac{\partial^2 u}{\partial r \partial s} \right. \\ \left. + \frac{u^2 R}{(r+R)^2} \frac{\partial^2 u}{\partial r \partial s} + \frac{uR}{(r+R)^2} \frac{\partial u}{\partial r} \frac{\partial u}{\partial s} + \frac{uR}{(r+R)^3} \frac{\partial u}{\partial s} \right) \\ = \frac{k_{\text{hnf}}}{(\rho c_p)_{\text{hnf}}} \left(\frac{\partial^2 T}{\partial r^2} + \frac{1}{r+R} \frac{\partial T}{\partial r} \right) \end{aligned} \right\}, \quad (4)$$



with^{50–52}

$$\left. \begin{aligned} u = u_w(s), v = 0, T = T_w = T_\infty + T_0 e^{\frac{As}{2L}}, \quad \text{at } r = 0 \\ u \rightarrow 0, T \rightarrow T_\infty, \quad \text{as } r \rightarrow \infty \end{aligned} \right\} \quad (5)$$

In the above expressions (u, v) depict velocity components, μ_{hnf} the dynamic viscosity, ρ_{hnf} the density, (r, s) signify the Cartesian coordinates, σ_{hnf} the electrical conductivity, $F \left(= \frac{C_b}{\sqrt{k_p}} \right)$ the inertia coefficient, k_p the porous medium permeability coefficient, R the radius of curvature, $(\rho c_p)_{\text{hnf}}$ the heat capacitance, C_b the drag force coefficient, L the reference length, T the temperature, k_{hnf} the thermal conductivity, c_p the specific heat, T_∞ the ambient temperature, δ_E the heat relaxation time, B_0 the magnetic field strength, T_w the wall temperature and p the pressure.

2.1. Thermophysical characteristics

Mathematical expressions for nanofluid and hybrid nanomaterials and numerical values of conventional fluid and nanoparticles have been given through Tables 1 and 2.^{53,54}

Letting

$$\left. \begin{aligned} u = u_0 e^{s/L} \frac{\partial f(\xi, \eta)}{\partial \eta}, v = -\frac{R}{r+R} \sqrt{\frac{\nu_f u_0 e^{s/L}}{2L}} \left(f(\xi, \eta) + 2\xi \frac{\partial f(\xi, \eta)}{\partial \xi} + \eta \frac{\partial f(\xi, \eta)}{\partial \eta} \right) \\ T = T_\infty + T_0 e^{\frac{As}{2L}} \theta(\xi, \eta), \eta = \sqrt{\frac{u_0 e^{s/L}}{2L\nu_f}} r, \xi = e^{s/L}, p = \rho_f u_0^2 e^{\frac{2s}{L}} P(\xi, \eta) \end{aligned} \right\} \quad (6)$$

one obtains

$$\frac{\partial P}{\partial \eta} = \frac{A_2}{(\eta + \sqrt{\xi} K_1)} \left(\frac{\partial f}{\partial \eta} \right)^2, \quad (7)$$

$$\left. \begin{aligned} \left(\frac{\partial^3 f}{\partial \eta^3} + \frac{1}{(\eta + \sqrt{\xi} K_1)} \left(\frac{\partial f}{\partial \eta} \right)^2 - \frac{1}{(\eta + \sqrt{\xi} K_1)^2} \frac{\partial f}{\partial \eta} \right) - A_1 \left(\frac{4\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} P(\xi, \eta) + \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \xi \frac{\partial P}{\partial \xi} + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \eta \frac{\partial P}{\partial \eta} \right) \\ + A_1 A_2 \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} f \frac{\partial^2 f}{\partial \eta^2} + \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \xi \frac{\partial f}{\partial \xi} \frac{\partial^2 f}{\partial \eta^2} - \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(\frac{\partial f}{\partial \eta} \right)^2 - \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \xi \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \xi \partial \eta} \right) \\ + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} f \frac{\partial f}{\partial \eta} + \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} \xi \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \\ - A_1 \frac{2}{\xi} \frac{\sigma_{\text{hnf}}}{\sigma_f} M \frac{\partial f}{\partial \eta} - \frac{2}{\xi} \lambda \frac{\partial f}{\partial \eta} - A_1 A_2 \text{Fr} \left(\frac{\partial f}{\partial \eta} \right)^2 = 0 \end{aligned} \right\} \quad (8)$$

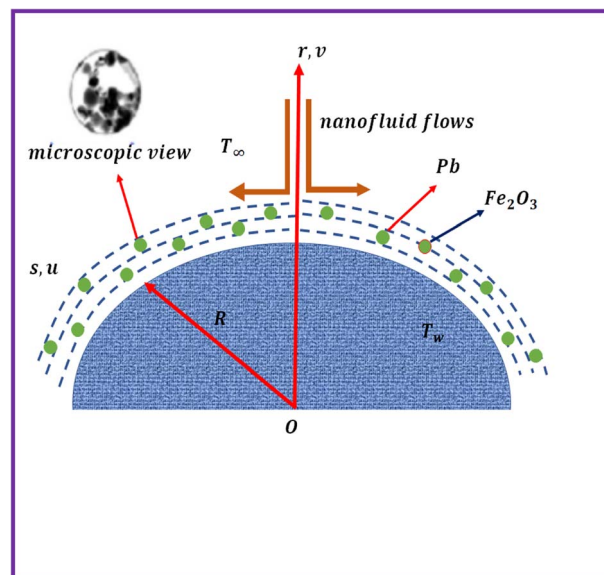


Fig. 1 Flow sketch.



Table 1 Mathematical expressions for thermophysical characteristics^{53,54}

Properties	Nanoliquid
Viscosity	$\mu_{nf} = \frac{\mu_f}{(1 - \phi_1)^{5/2}}$
Density	$\rho_{nf} = (1 - \phi_1)\rho_f + \phi_1\rho_{s1}$
Heat capacity	$(\rho c_p)_{nf} = (1 - \phi_1)(\rho c_p)_f + \phi_1(\rho c_p)_{s1}$
Electrical conductivity	$\frac{\sigma_{nf}}{\sigma_f} = \frac{\sigma_{s1}(1 + 2\phi_1) + 2\sigma_f(1 - \phi_1)}{\sigma_{s1}(1 - \phi_1) + \sigma_f(2 + \phi_1)}$
Thermal conductivity	$\frac{k_{nf}}{k_f} = \frac{k_{s1} + 2k_f - 2\phi_1(k_f - k_{s1})}{k_{s1} + 2k_f + \phi_1(k_f - k_{s1})}$
Properties	Hybrid nanoliquid
Viscosity	$\mu_{hnf} = \frac{\mu_f}{(1 - \phi_1)^{5/2}(1 - \phi_2)^{5/2}}$
Density	$\rho_{hnf} = (1 - \phi_2)\{(1 - \phi_1)\rho_f + \phi_1\rho_{s1}\} + \phi_2\rho_{s2}$
Heat capacity	$(\rho c_p)_{hnf} = (1 - \phi_2)\{(1 - \phi_1)(\rho c_p)_f + \phi_1(\rho c_p)_{s1}\} + \phi_2(\rho c_p)_{s2}$
Electrical conductivity	$\frac{\sigma_{hnf}}{\sigma_{nf}} = \frac{\sigma_{s2}(1 + 2\phi_2) + 2\sigma_{nf}(1 - \phi_2)}{\sigma_{s2}(1 - \phi_2) + \sigma_{nf}(2 + \phi_2)}$
Thermal conductivity	$\frac{k_{hnf}}{k_{nf}} = \frac{k_{s2} + 2k_{nf} - 2\phi_2(k_{nf} - k_{s2})}{k_{s2} + 2k_{nf} + \phi_2(k_{nf} - k_{s2})}$

Table 2 Thermophysical characteristics of ethylene glycol (C₂H₆O₂), lead (Pb) and ferric oxide (Fe₂O₃)^{53,54}

Properties	ρ (kg m ⁻³)	k (W m ⁻¹ K ⁻¹)	c_p (J k ⁻¹ g ⁻¹ K ⁻¹)	σ (Ω^{-1} m ⁻¹)
Ethylene glycol	1116.6	0.249	2382	1.07×10^{-7}
Lead (Pb)	11 343	35	130	4.55×10^6
Ferric oxide (Fe ₂ O ₃)	5200	80.2	670	0.74×10^6

$$\left. \begin{aligned}
 & \frac{k_{hnf}}{k_f} \left(\frac{\partial^2 \theta}{\partial \eta^2} + \frac{1}{(\eta + \sqrt{\xi} K_1)} \frac{\partial \theta}{\partial \eta} \right) + \frac{Ec}{A_1} \text{Pr} \xi^{2-\frac{4}{2}} \left(\frac{\partial^2 f}{\partial \eta^2} + \frac{1}{(\eta + \sqrt{\xi} K_1)} \frac{\partial f}{\partial \eta} \right)^2 + \frac{\sigma_{hnf}}{\sigma_f} \text{MEcPr} \xi^{1-\frac{4}{2}} \left(\frac{\partial f}{\partial \eta} \right)^2 \\
 & + A_3 \text{Pr} \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(f \frac{\partial \theta}{\partial \eta} + 2\xi \frac{\partial f}{\partial \xi} \frac{\partial \theta}{\partial \eta} - A\theta \frac{\partial f}{\partial \eta} - 2 \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \xi} \right) + A_3 \text{Pr} \beta \left(A_{11} - \xi \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \right)^2 (A_{22} - A_{33}) \right) \\
 & - \beta \frac{Ec}{A_1} \text{Pr} \xi^{3-\frac{4}{2}} A_{44} - 2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \beta \frac{\sigma_{hnf}}{\sigma_f} \text{MEcPr} \xi^{2-\frac{4}{2}} \left(\begin{aligned}
 & f \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} + 2\xi \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} + \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 f}{\partial \eta^2} \\
 & - 2 \left(\frac{\partial f}{\partial \eta} \right)^3 - \eta \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} - 2\xi \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \xi \partial \eta}
 \end{aligned} \right) = 0
 \end{aligned} \right\} \quad (9)$$

$$\left. \begin{aligned}
 & \frac{\partial f}{\partial \eta}(\xi, 0) = 1, f(\xi, 0) = -\xi \frac{\partial f}{\partial \xi}(\xi, 0), \theta(\xi, 0) = 1, \\
 & \frac{\partial f}{\partial \eta}(\xi, \infty) = 0, \theta(\xi, \infty) = 0,
 \end{aligned} \right\} \quad (10)$$

Here $K_1 \left(= \sqrt{\frac{u_0}{2\nu_f L}} R \right)$ shows the material parameter, $Ec \left(= \frac{u_0^2}{c_p T_0} \right)$ the Eckert number, $Fr \left(= \frac{C_b}{\sqrt{k_p}} L \right)$ the Forchheimer number, $\beta \left(= \frac{\delta_E u_0}{L} \right)$ the thermal relaxation time, $M \left(= \frac{2\sigma_f B_0^2 L}{u_0 \rho_f} \right)$ the magnetic variable, $Pr \left(= \frac{\nu_f}{\alpha_f} \right)$ the Prandtl

number and $\lambda \left(= \frac{\nu_f L}{u_0 k_p} \right)$ the porosity parameter. Here $A_1, A_2, A_3, A_{11}, A_{22}, A_{33}$ and A_{44} are expressed as

$$\left. \begin{aligned}
 & A_1 = (1 - \phi_1)^{5/2} (1 - \phi_2)^{5/2} \\
 & A_2 = (1 - \phi_2) \left((1 - \phi_1) + \frac{\phi_1 \rho_{s1}}{\rho_f} \right) + \frac{\phi_2 \rho_{s2}}{\rho_f} \\
 & A_3 = (1 - \phi_2) \left((1 - \phi_1) + \frac{\phi_1 (\rho c_p)_{s1}}{(\rho c_p)_f} \right) + \frac{\phi_2 (\rho c_p)_{s2}}{(\rho c_p)_f}
 \end{aligned} \right\} \quad (11)$$



$$A_{11} = \left[\frac{1}{2} \xi^2 \frac{K_1^2}{(\eta + \sqrt{\xi} K_1)^3} \left(\begin{aligned} & f^2 \frac{\partial \theta}{\partial \eta} + 3\xi f \frac{\partial f}{\partial \xi} \frac{\partial \theta}{\partial \eta} + 2\eta f \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + 2\xi \left(\frac{\partial f}{\partial \xi} \right)^2 \frac{\partial \theta}{\partial \eta} \\ & + \eta \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + 2\xi \eta \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + \eta^2 \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial \theta}{\partial \eta} - \xi f \theta \frac{\partial f}{\partial \eta} \\ & - 2\xi^2 A \theta \frac{\partial f}{\partial \eta} \frac{\partial f}{\partial \xi} - \xi \eta A \theta \left(\frac{\partial f}{\partial \eta} \right)^2 - 2\xi^2 f \frac{\partial \theta}{\partial \xi} \frac{\partial f}{\partial \eta} \\ & - 4\xi^2 \frac{\partial \theta}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial f}{\partial \xi} - 2\xi^2 \eta \frac{\partial \theta}{\partial \xi} \left(\frac{\partial f}{\partial \eta} \right)^2 - \xi \eta f \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} \end{aligned} \right) \right] \quad (12)$$

$$A_{22} = \left[\begin{aligned} & \frac{1}{2} f \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + \xi f \frac{\partial \theta}{\partial \eta} \frac{\partial^2 f}{\partial \xi \partial \eta} + 2\eta f \frac{\partial^2 f}{\partial \eta^2} \frac{\partial \theta}{\partial \eta} + \xi \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + 2\xi^2 \frac{\partial f}{\partial \xi} \frac{\partial^2 f}{\partial \xi \partial \eta} \frac{\partial \theta}{\partial \eta} + \xi \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta \partial \xi} \\ & + \xi \eta \frac{\partial f}{\partial \xi} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial \theta}{\partial \eta} + \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial \theta}{\partial \eta} + \xi \eta \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} + \frac{1}{2} \eta^2 \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial \theta}{\partial \eta} + \frac{1}{2} f^2 \frac{\partial^2 \theta}{\partial \eta^2} + 2\xi^2 \eta \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \xi} \frac{\partial^2 f}{\partial \eta \partial \xi} \\ & + 4\xi^2 \left(\frac{\partial f}{\partial \xi} \right)^2 \frac{\partial^2 \theta}{\partial \eta^2} + \eta^2 \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta^2} + 4f\xi \frac{\partial f}{\partial \xi} \frac{\partial^2 \theta}{\partial \eta^2} + 4\xi \eta \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \eta^2} + 2\eta f \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \eta^2} + \frac{1}{2} A^2 \theta \left(\frac{\partial f}{\partial \eta} \right)^2 \\ & + 4\xi A \frac{\partial \theta}{\partial \xi} \left(\frac{\partial f}{\partial \eta} \right)^2 + 2\xi^2 \frac{\partial^2 \theta}{\partial \xi^2} \left(\frac{\partial f}{\partial \eta} \right)^2 + \xi \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta \partial \xi} + \frac{1}{2} \eta^2 \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta^2} + \frac{1}{2} \eta^2 \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta^2} \\ & + \xi A^2 \theta \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta \partial \xi} + 2 \frac{\partial \theta}{\partial \xi} \left(\frac{\partial f}{\partial \eta} \right)^2 + \frac{1}{2} \eta A \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial \theta}{\partial \eta} \end{aligned} \right] \quad (13)$$

$$A_{33} = \left[\left(\begin{aligned} & -\frac{1}{2} A f \theta \frac{\partial^2 f}{\partial \eta^2} - \xi f \frac{\partial \theta}{\partial \xi} \frac{\partial^2 f}{\partial \eta^2} - \frac{1}{2} \eta f \frac{\partial \theta}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} - A \xi \theta \frac{\partial^2 f}{\partial \eta^2} \frac{\partial f}{\partial \xi} - 2\xi^2 \frac{\partial^2 f}{\partial \eta^2} \frac{\partial f}{\partial \xi} \frac{\partial \theta}{\partial \xi} \\ & - \xi \eta \frac{\partial^2 f}{\partial \eta^2} \frac{\partial f}{\partial \xi} \frac{\partial \theta}{\partial \eta} - \frac{1}{2} \eta^2 \frac{\partial \theta}{\partial \eta} \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} - 2f \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \xi \partial \eta} - A f \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} - f \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} \\ & - 2A \xi \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} \frac{\partial f}{\partial \xi} - 5\xi \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} \frac{\partial f}{\partial \xi} - 4\xi \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \eta \partial \xi} \frac{\partial f}{\partial \xi} - 2\xi \eta \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \eta^2} \frac{\partial f}{\partial \xi} \\ & - \frac{5}{2} \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial \theta}{\partial \eta} - 2\eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \xi \partial \eta} - \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 \theta}{\partial \eta^2} - 2\xi^2 \frac{\partial f}{\partial \eta} \frac{\partial \theta}{\partial \eta} \frac{\partial^2 f}{\partial \xi^2} \\ & - \eta f \frac{\partial f}{\partial \eta} \frac{\partial^2 \theta}{\partial \eta^2} - \xi \eta \frac{\partial \theta}{\partial \eta} \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta \partial \xi} + A \theta \left(\frac{\partial f}{\partial \eta} \right)^2 \end{aligned} \right) \right] \quad (14)$$

$$A_{44} = \left[\begin{aligned} & 2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(\begin{aligned} & \frac{1}{2} f \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^3 f}{\partial \eta^3} + \xi \frac{\partial f}{\partial \xi} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^3 f}{\partial \eta^3} + \frac{1}{2} \eta \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^3 f}{\partial \eta^3} - \frac{3}{2} \frac{\partial f}{\partial \eta} \left(\frac{\partial^2 f}{\partial \eta^2} \right)^2 \\ & - \frac{1}{2} \xi \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^3 f}{\partial \xi \partial \eta^2} - \frac{1}{2} \eta \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^3 f}{\partial \eta^3} \end{aligned} \right) - \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^3} \left(\frac{\partial f}{\partial \eta} \right)^3 \\ & + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} \left(\begin{aligned} & f + 2\xi \frac{\partial f}{\partial \xi} + \eta \frac{\partial f}{\partial \eta} + f \frac{\partial f}{\partial \eta} \frac{\partial^3 f}{\partial \eta^3} + 2\xi \frac{\partial f}{\partial \eta} \frac{\partial f}{\partial \xi} \frac{\partial^3 f}{\partial \eta^3} + \eta \frac{\partial^3 f}{\partial \eta^3} \left(\frac{\partial f}{\partial \eta} \right)^2 \\ & - 5 \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 f}{\partial \eta^2} - \xi \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^3 f}{\partial \xi \partial \eta^2} - \eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^3 f}{\partial \eta^3} - \eta \frac{\partial f}{\partial \eta} \left(\frac{\partial^2 f}{\partial \eta^2} \right)^2 - 2 \frac{\partial f}{\partial \eta} \frac{\partial^2 f}{\partial \eta^2} \frac{\partial^2 f}{\partial \xi \partial \eta} \end{aligned} \right) \\ & + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^4} \left(f \left(\frac{\partial f}{\partial \eta} \right)^2 + 2\xi \frac{\partial f}{\partial \xi} \frac{\partial f}{\partial \xi} + \eta \left(\frac{\partial f}{\partial \eta} \right)^3 \right) - \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^3} \left(\eta \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 f}{\partial \eta^2} + 2\xi \left(\frac{\partial f}{\partial \eta} \right)^2 \frac{\partial^2 f}{\partial \xi \partial \eta} \right) \end{aligned} \right] \quad (15)$$



3. Interesting quantities

3.1. Surface drag force

One may write

$$C_{f,s} = \frac{\tau_{rs}|_{r=0}}{\rho_f u_w^2}. \quad (16)$$

Here τ_{rs} wall shear stress is

$$\tau_{rs} = \mu_{hnf} \left(\frac{\partial u}{\partial r} - \frac{1}{(r+R)} u \right), \quad (17) \text{ or}$$

Dimensionless version is

$$C_{f,s} \text{Re}_s^{1/2} = \frac{1}{A_1} \left(f''(0) + \frac{1}{K_1} f'(0) \right). \quad (18)$$

3.2. Nusselt number

Considering

$$\text{Nu}_s = \frac{sq_w}{k_f(T_w - T_\infty)}, \quad (19)$$

and heat flux q_w

$$q_w = -k_{hnf} \left(\frac{\partial T}{\partial r} \right) \Big|_{r=0}, \quad (20)$$

we can express that

$$\sqrt{\frac{2L}{s}} \text{Nu}_s \text{Re}_s^{-1/2} = -\frac{k_{hnf}}{k_f} \theta'(0), \quad (21)$$

in which $\text{Re}_s = \frac{u_w s}{\nu_f}$ indicates the local Reynolds number.

$$\left. \begin{aligned} & \left(f''' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f'^2 - \frac{1}{(\eta + \sqrt{\xi} K_1)^2} f' \right) - A_1 \left(\frac{4\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} P + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \eta P' \right) \\ & + A_1 A_2 \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} f f'' - \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} f'^2 + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} f f' + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} \eta f'^2 \right) \\ & - A_1 \frac{2}{\xi} \frac{\sigma_{hnf}}{\sigma_f} M f' - \frac{2}{\xi} \lambda f' - A_1 A_2 \text{Fr} f'^2 = 0 \end{aligned} \right\}, \quad (25)$$

$$\left. \begin{aligned} & \frac{k_{hnf}}{k_f} \left(\theta'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} \theta' \right) + \frac{\text{Ec}}{A_1} \text{Pr} \xi^{2-\frac{4}{2}} \left(f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f' \right)^2 + \frac{\sigma_{hnf}}{\sigma_f} M \text{Ec} \text{Pr} \xi^{1-\frac{4}{2}} f'^2 \\ & + A_3 \text{Pr} \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} (f \theta' - A \theta f') + A_3 \text{Pr} \beta A_{55} - \beta \frac{\text{Ec}}{A_1} \text{Pr} \xi^{3-\frac{4}{2}} A_{66} \\ & - 2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \frac{\sigma_{hnf}}{\sigma_f} \beta M \text{Ec} \text{Pr} \xi^{2-\frac{4}{2}} (f f' f'' + \eta f'^2 f'' - 2f'^3 - \eta f' f'') = 0 \end{aligned} \right\}, \quad (26)$$

4. Entropy formulation

Mathematical expression is given by

$$E_G(\xi, \eta) = \frac{1}{T_\infty^2} k_{hnf} \left(\frac{\partial T}{\partial r} \right)^2 + \frac{\mu_{hnf}}{T_\infty} \left(\frac{\partial u}{\partial r} + \frac{u}{r+R} \right)^2 + \frac{\mu_{hnf}}{T_\infty} \frac{1}{k_p} u^2 + \frac{\sigma_{hnf}}{T_\infty} B_0^2 u^2, \quad (22)$$

$$S_G(\xi, \eta) = \alpha_1 \frac{k_{hnf}}{k_f} \xi^{(1+A)} \left(\frac{\partial \theta}{\partial \eta} \right)^2 + \frac{1}{A_1} \text{Br} \xi^3 \left(\frac{\partial^2 f}{\partial \eta^2} + \frac{1}{(\eta + \sqrt{\xi} K_1)} \frac{\partial f}{\partial \eta} \right)^2 + \frac{1}{A_1} \lambda \text{Br} \xi^2 \left(\frac{\partial f}{\partial \eta} \right)^2 + \frac{\sigma_{hnf}}{\sigma_f} M \text{Br} \xi^2 \left(\frac{\partial f}{\partial \eta} \right)^2 \quad (23)$$

Here $\alpha_1 \left(= \frac{T_0}{T_\infty} \right)$ represents the heat ratio parameter,

$\text{Br} \left(= \frac{\mu_f u_0^2}{T_0 k_f} \right)$ the Brinkman number and $S_G \left(= \frac{2E_G L T_\infty \nu_f}{k_f u_0 T_0} \right)$ the

entropy rate.

5. Solutions methodology

Considering the derivatives with respect to ξ (i.e. $\frac{\partial(\cdot)}{\partial \xi} = 0$) in

eqn (7)–(10) we arrive at

$$P' = \frac{A_2}{(\eta + \sqrt{\xi} K_1)} f'^2, \quad (24)$$



$$\left. \begin{aligned} f'(\xi, 0) = 1, f(\xi, 0) = 0, \theta(\xi, 0) = 1, \\ f'(\xi, \infty) = 0, \theta(\xi, \infty) = 0 \end{aligned} \right\} \quad (27)$$

with A_{55} and A_{66} as

$$A_{55} = \left[\begin{aligned} & \frac{1}{2} \xi^2 \frac{K_1^2}{(\eta + \sqrt{\xi} K_1)^3} \left(f^2 \theta' + 2\eta f' \theta' + \eta^2 f'^2 \theta' - \xi f \theta f' - \xi \eta A \theta f'^2 - \xi \eta f f' \theta' \right) \\ & - \xi \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \right)^2 \left(\begin{aligned} & \frac{1}{2} f f' \theta' + 2\eta f f'' \theta' - \frac{3}{2} \eta f'^2 \theta' + \xi \eta f' \theta'' + \frac{1}{2} f^2 \theta'' \\ & + \eta^2 f'^2 \theta'' + 2\eta f f' \theta'' - \frac{1}{2} A f \theta f'' - \frac{1}{2} \eta f \theta' f'' - A f f' \theta'' - f f' \theta'' \\ & - \eta f f' \theta'' + \frac{1}{2} \eta A f'^2 \theta' - \eta f'^2 \theta'' + \frac{1}{2} A^2 \theta f'^2 + \frac{1}{2} \eta^2 f'^2 \theta'' + A \theta f'^2 \end{aligned} \right) \end{aligned} \right] \quad (28)$$

$$A_{66} = \left[\begin{aligned} & \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} \left(f + \eta f' + f f' f'' + \eta f'' f'^2 - 5 f'^2 f'' - \eta f'^2 f'' - \eta f' f''^2 \right) \\ & + 2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(\frac{1}{2} f f'' f''' - \frac{3}{2} f' f''^2 \right) + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^4} \left(f f'^2 + \eta f'^3 \right) - \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^3} \left(2 f'^3 + \eta f'^2 f'' \right) \end{aligned} \right] \quad (29)$$

Elimination of pressure from eqn (22) and (23) yields

$$\left. \begin{aligned} & \frac{1}{A_1} \left(f^{(iv)} + \frac{2}{(\eta + \sqrt{\xi} K_1)} f''' - \frac{1}{(\eta + \sqrt{\xi} K_1)^2} f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)^3} f' - 2 \frac{\lambda}{\xi} \left(f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f' \right) \right) \\ & + A_2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(\begin{aligned} & f f''' - \frac{1}{(\eta + \sqrt{\xi} K_1)^2} f f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f f'' - \frac{2 \sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} f'^2 - 3 f' f'' \\ & + \frac{2}{(\eta + \sqrt{\xi} K_1)} (\eta - 1) f' f'' - \frac{1}{(\eta + \sqrt{\xi} K_1)} (1 + 2\eta) f'^2 \end{aligned} \right) \\ & - \frac{2}{\xi} \frac{\sigma_{\text{hnf}}}{\sigma_f} M \left(f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f' \right) - 2 A_2 \text{Fr} \left(2 f' f'' + \frac{1}{(\eta + \sqrt{\xi} K_1)} f'^2 \right) = 0 \end{aligned} \right\} \quad (30)$$

5.1. Numerical approach

Governing problems are solved by the ND-solve algorithm. The Mathematica software is utilized to develop the computational results. For this we converted the boundary value problem to the initial value situation as follows:

$$\left. \begin{aligned} f = y_1, f' = y_2, f'' = y_3, f''' = y_4, f^{iv} = y_4' \\ \theta = y_5, \theta' = y_6, \theta'' = y_6' \end{aligned} \right\}, \quad (31)$$



$$y'_4 = \left\{ \begin{array}{l} \frac{1}{(\eta + \sqrt{\xi} K_1)^2} y_3^3 - \frac{2}{(\eta + \sqrt{\xi} K_1)} y_4 - \frac{1}{(\eta + \sqrt{\xi} K_1)^3} y_2 + \frac{2\lambda}{\xi} \left(y_3 + \frac{1}{(\eta + \sqrt{\xi} K_1)} y_2 \right) \\ -A_1 A_2 \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \left(\begin{array}{l} y_1 y_4 - \frac{1}{(\eta + \sqrt{\xi} K_1)} y_1 y_2 + \frac{1}{(\eta + \sqrt{\xi} K_1)} y_1 y_3 - \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} y_2^2 \\ -3y_2 y_3 + \frac{2}{(\eta + \sqrt{\xi} K_1)} (\eta - 1) y_1 y_3 - \frac{1}{(\eta + \sqrt{\xi} K_1)} (1 + 2\eta) y_2^2 \end{array} \right) \\ + \frac{2}{\xi} A_1 \frac{\sigma_{\text{hnf}}}{\sigma_f} M \left(y_3 - \frac{1}{(\eta + \sqrt{\xi} K_1)} y_2 \right) - 2A_1 A_2 \text{Fr} \left(2y_1 y_3 + \frac{1}{(\eta + \sqrt{\xi} K_1)} y_2^2 \right) \end{array} \right\} \quad (32)$$

$$y'_6 = \left\{ \begin{array}{l} -\frac{1}{(\eta + \sqrt{\xi} K_1)} - \frac{k_f}{k_{\text{hnf}}} \left(\frac{\text{PrEc}}{A_1} \xi^{2-\frac{4}{2}} \left(y_3 + \frac{1}{(\eta + \sqrt{\xi} K_1)} y_2 \right)^2 + \frac{\sigma_{\text{hnf}}}{\sigma_f} M \text{PrEc} \xi^{1-\frac{4}{2}} y_2^2 \right) \\ -\frac{k_f}{k_{\text{hnf}}} A_3 \text{Pr} \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} (y_1 y_6 - A y_2 y_5) - \frac{k_f}{k_{\text{hnf}}} \left(A_3 \text{Pr} \beta A_{77} - \frac{\beta \text{PrEc}}{A_1} \xi^{3-\frac{4}{2}} A_{88} \right) \\ + \frac{2\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \frac{k_f}{k_{\text{hnf}}} \frac{\sigma_{\text{hnf}}}{\sigma_f} M \text{PrEc} \xi^{2-\frac{4}{2}} (y_1 y_2 y_3 - \eta y_2^2 y_3 - 2y_2^3 - \eta y_2 y_3) \end{array} \right\} \quad (33)$$

$$\left. \begin{array}{l} y_1(0) = 0, y_2(0) = 1, y_5(0) = 0 \\ y_2(\infty) = 0, y_5(\infty) = 0 \end{array} \right\} \quad (34)$$

with A_{77} and A_{88} given below:

$$A_{77} = \left\{ \begin{array}{l} \frac{\xi^2 K_1^2}{2(\eta + \sqrt{\xi} K_1)} (y_1^2 y_6 + 2\eta y_2 y_6 + \eta^2 y_2^2 y_6 - \xi y_1 y_2 y_5 - \xi \eta y_2^2 y_5 - \xi \eta y_1 y_2 y_6) \\ -\xi \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \right)^2 \left(\frac{1}{2} y_1 y_2 y_5 + 2\eta y_1 y_3 y_5 - \frac{3}{2} \eta y_2^2 y_5 + \xi \eta y_2 y_5 + \frac{1}{2} \eta y_1^2 y'_6 + \eta^2 y_2^2 y'_6 \right) \\ -\xi \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \right)^2 \left(-\frac{1}{2} A y_1 y_3 y_5 - \frac{1}{2} \eta y_1 y_3 y_6 - A y_1 y_2 y_5 - y_1 y_2 y_6 - \eta y_1 y_2 y'_6 + \frac{1}{2} A y_2^2 y_6 \right) \\ -\xi \left(\frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} \right)^2 \left(\eta y_2^2 y_6 + \frac{1}{2} A^2 y_2^2 y_5 + \frac{1}{2} \eta^2 y_2^2 y'_6 + A y_2^2 y_5 \right) \end{array} \right\} \quad (35)$$

$$A_{88} = \left\{ \begin{array}{l} \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)^2} (y_1 + \eta y_2 + y_1 y_2 y_4 + \eta y_2^2 y_4 - 5y_2^2 y_3 - \eta y_1^2 y_4 - \eta y_2 y_3^2) \\ + \frac{\sqrt{\xi} K_1}{(\eta + \sqrt{\xi} K_1)} (y_1 y_3 y_4 - 3y_2 y_3^2 + y_1 y_2^2 + \eta y_2^3 - 2y_2^3 - \eta y_2^2 y_3) \end{array} \right\} \quad (36)$$



6. Discussion

The influence of emerging variables on liquid flow, entropy rate and temperature for both nanoliquid ($\text{Pb}/\text{C}_2\text{H}_6\text{O}_2$) and hybrid nanoliquid ($\text{Fe}_2\text{O}_3 + \text{Pb}/\text{C}_2\text{H}_6\text{O}_2$) is discussed. Here dotted lines show nanoliquid ($\text{Pb}/\text{C}_2\text{H}_6\text{O}_2$) behaviors and solid lines characterize the hybrid ($\text{Pb} + \text{Fe}_2\text{O}_3/\text{C}_2\text{H}_6\text{O}_2$) nanoliquid characteristics. Engineering quantities like the skin friction coefficient and heat transport rate are discussed through tabulated forms. Comparison of recent analysis with previous results in the literature is constructed in Table 3. Here we discussed the

Table 3 Coefficient of skin friction comparison with Okechi *et al.*⁵⁵

K_1	Okechi <i>et al.</i> ⁵⁵	Present results
5	1.4196	1.41963
10	1.3467	1.34675
20	1.3135	1.31354
30	1.3028	1.30281

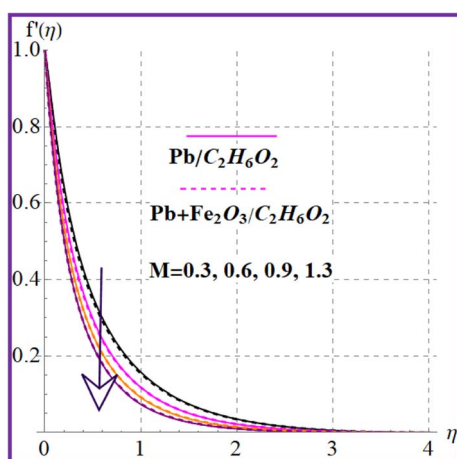


Fig. 2 $f'(\eta)$ variation versus M .

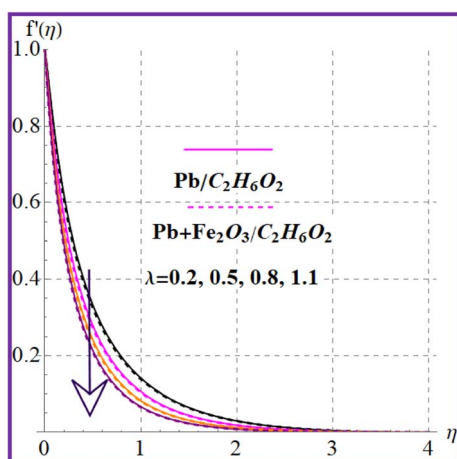


Fig. 3 $f'(\eta)$ variation versus λ .

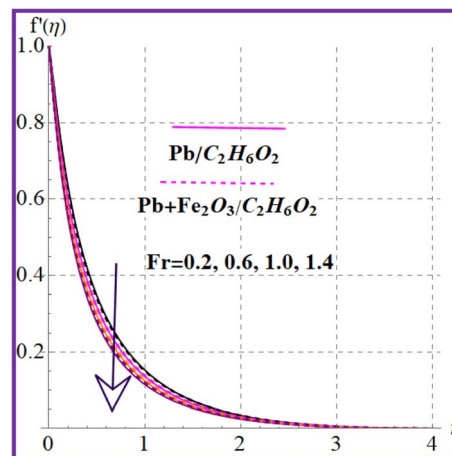


Fig. 4 $f'(\eta)$ variation versus Fr .

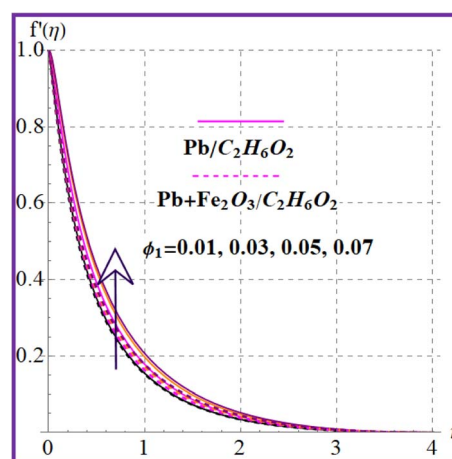


Fig. 5 $f'(\eta)$ variation versus ϕ_1 .

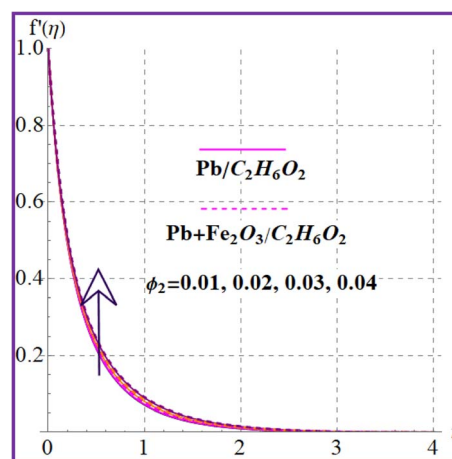
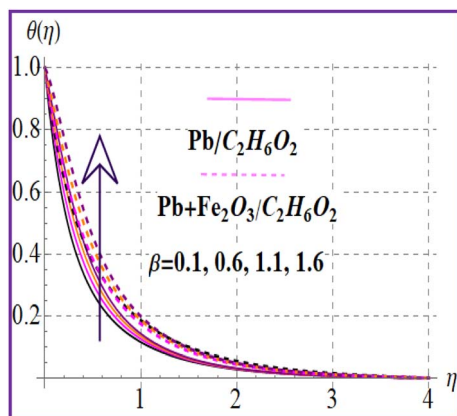
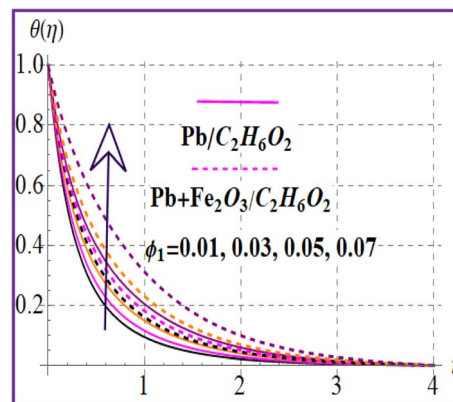
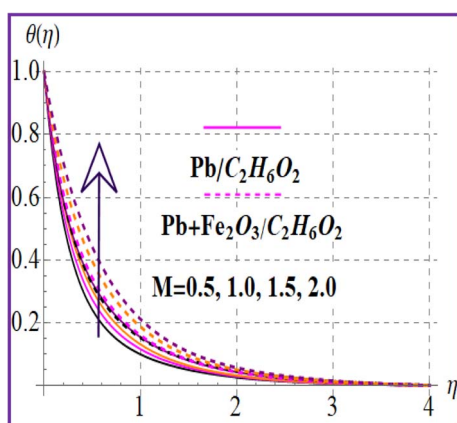
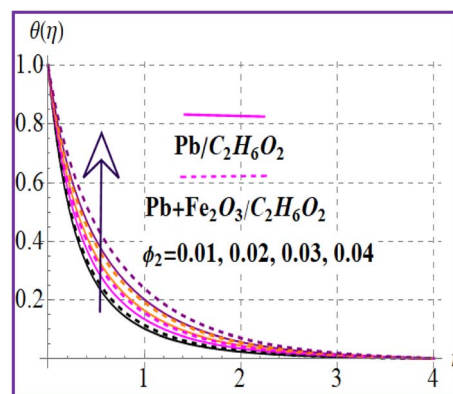


Fig. 6 $f'(\eta)$ variation versus ϕ_2 .



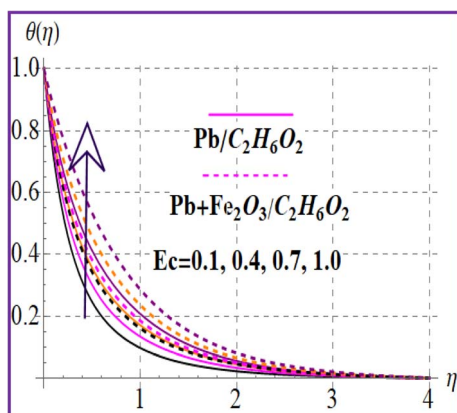
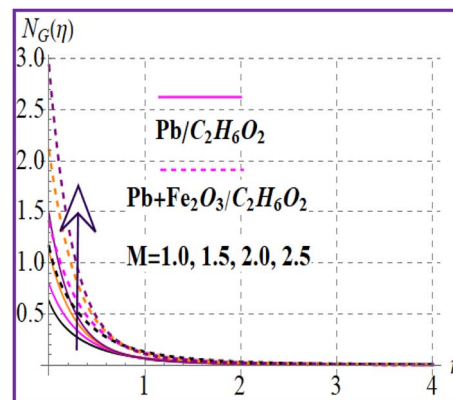
Fig. 7 $\theta(\eta)$ versus β .Fig. 10 $\theta(\eta)$ versus ϕ_1 .Fig. 8 $\theta(\eta)$ versus M .Fig. 11 $\theta(\eta)$ versus ϕ_2 .

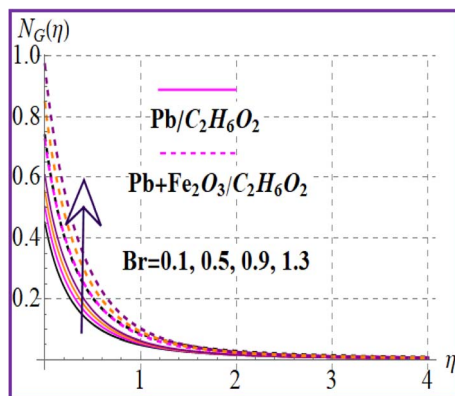
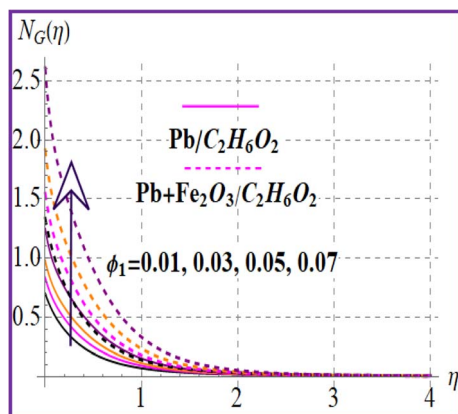
comparison of the coefficient of skin friction *versus* a higher approximation of the curvature variable with Okechi *et al.*⁵⁵ for a limiting case (viscous fluid flow). Clearly a good consensus is noticed.

6.1. Velocity

Fig. 2 illustrates the flow behavior against the magnetic variable (M). An increment in the magnetic variable leads to

intensification of the Lorentz force which declines the liquid flow. The influence of (λ) on ($f'(\eta)$) is portrayed in Fig. 3. Higher porosity corresponds to diminished velocity in both nanoliquid ($\text{Pb}/\text{C}_2\text{H}_6\text{O}_2$) and hybrid ($\text{Pb} + \text{Fe}_2\text{O}_3/\text{C}_2\text{H}_6\text{O}_2$) nanoliquid cases. Fig. 4 shows the velocity impact against the Forchheimer number (Fr). A reduction in liquid flow ($f'(\eta)$) is noticed *versus* the Forchheimer number for both nanoliquid ($\text{Pb}/\text{C}_2\text{H}_6\text{O}_2$) and hybrid ($\text{Pb} + \text{Fe}_2\text{O}_3/\text{C}_2\text{H}_6\text{O}_2$) nanomaterials. Fig. 5 and 6

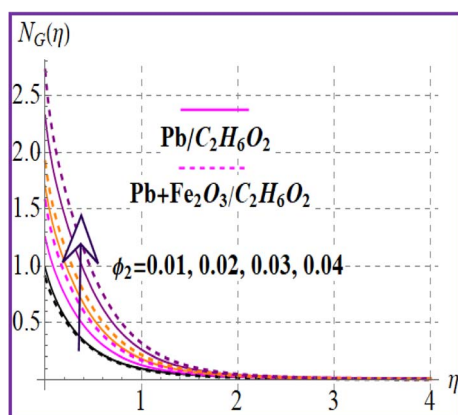
Fig. 9 $\theta(\eta)$ versus Ec .Fig. 12 $N_G(\eta)$ versus M .

Fig. 13 $N_G(\eta)$ versus Br .Fig. 14 $N_G(\eta)$ versus ϕ_1 .

elucidate the impact for flow *versus* nanoparticle volume fractions (ϕ_1 and ϕ_2). It is noticed that there is an enhancement in liquid flow *versus* higher nanoparticle volume fractions (ϕ_1 and ϕ_2).

6.2. Thermal field

Fig. 7 presents the trend of temperature against the thermal relaxation time variable (β). A higher estimation of thermal

Fig. 15 $N_G(\eta)$ versus ϕ_2 .Table 4 Numerical results of the skin friction ($Re_s^{-1/2}C_{fs}$) coefficient

M	K_1	λ	Fr	$Re_s^{-1/2}C_{fs}$		
				Pb/C ₂ H ₆ O ₂	Pb + Fe ₂ O ₃ /C ₂ H ₆ O ₂	
0.4	0.1	0.1	0.2	8.4631	19.9922	
0.8				7.35445	17.5033	
0.12				6.57457	15.7212	
0.3	0.45	0.1	0.2	0.475582	1.04693	
				0.34613	0.754253	
				0.231708	0.496568	
0.3	0.45	0.2	0.2	0.344601	0.738767	
				0.223838	0.453805	
		0.3	0.4	0.1	0.11172	0.188597
					0.564833	1.20704
				0.313042	0.748393	
				0.0991132	0.343877	

Table 5 Computational values for $Re_s^{-1/2}Nu_s$

β	M	Pr	Ec	$Re_s^{-1/2}Nu_s$		
				Pb/C ₂ H ₆ O ₂	Pb + Fe ₂ O ₃ /C ₂ H ₆ O ₂	
0.01	0.1	5.0	0.4	2.94351	3.10761	
0.03				2.81501	2.44288	
0.05				2.68726	2.09427	
0.01	0.4	5.0	0.4	2.59787	2.34593	
				0.5	2.48648	1.82663
				0.6	2.37692	1.59412
0.01	0.1	3.5	0.4	2.45597	2.38122	
				4.0	2.62835	2.52681
				4.5	2.79038	2.6638
0.01	0.1	5.0	0.2	3.23399	3.85736	
				0.7	2.50778	1.71628
				0.11	1.92682	0.280292

relaxation time corresponds to an increase of the thermal field. Fig. 8 indicates the importance for (M) on $\theta(\eta)$. A larger approximation of the magnetic variable intensifies the Lorentz force which raises the resistance to flow. Therefore, the temperature is increased. The influence of the Eckert number on ($\theta(\eta)$) is depicted in Fig. 9. The outcome for the Eckert number (Ec) leads to creation of an additional kinetic energy and consequently the thermal field is improved. Characteristics of nanoparticle volume fractions (ϕ_1 and ϕ_2) on the thermal field are disclosed in Fig. 10 and 11. Clearly, higher nanoparticle volume fractions (ϕ_1 and ϕ_2) enhance the thermal field for both nanoliquid (Pb/C₂H₆O₂) and hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanomaterials.

6.3. Entropy rate

Fig. 12 reveals the impact of the magnetic variable on $N_G(\eta)$. Increasing values of the magnetic variable enhance the resistive force in the flow region which produces an additional energy in the system and therefore entropy is maximized. Fig. 13 depicts the importance of entropy for the Brinkman number. The



entropy rate rises *versus* a higher Brinkman number due to the viscous force. Fig. 14 and 15 show entropy characteristics against nanoparticle volume fractions (ϕ_1 and ϕ_2). A higher estimation of volume fractions (ϕ_1 and ϕ_2) leads to augmentation of the entropy rate for both nanoliquid (Pb/C₂H₆O₂) and hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanomaterials.

6.4. Physical quantities

Engineering quantities like the skin friction coefficient ($Re_s^{-1/2}C_{fs}$) and heat transport rate ($Re_s^{-1/2}Nu_s$) for nanoliquid (Pb/C₂H₆O₂) and hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanomaterials are discussed through tabulated forms.

6.4.1. Skin friction. Table 4 highlights the characteristics of the skin friction ($Re_s^{-1/2}C_{fs}$) coefficient against sundry parameters for both nanoliquid (Pb/C₂H₆O₂) and hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanomaterials. It is found that larger Forchheimer number (Fr), porosity (λ), material (K_1) and magnetic (M) parameters result in skin friction reduction.

6.4.2. Heat transport rate. Table 5 shows the heat transport rate ($Re_s^{-1/2}Nu_s$) variation *versus* influential variables for both nanoliquid (Pb/C₂H₆O₂) and hybrid (Pb + Fe₂O₃/C₂H₆O₂) nanomaterials. Decay in the thermal transport rate is witnessed for larger Eckert number (Ec), thermal relaxation time (β) and magnetic (M) variables. An increment in the temperature gradient is detected for the Prandtl number.

7. Closing remarks

Main findings are listed below.

- A higher magnetic parameter decays fluid flow whereas temperature enhances.
- Velocity for the Forchheimer number and porosity parameter is the same.
- A larger thermal relaxation time variable raises temperature.
- A larger estimation of nanoparticle volume fractions corresponds to an amplified fluid flow and thermal field.
- Entropy shows increasing behavior due to the Brinkman number.
- A Higher magnetic parameter leads to entropy rate enhancement.
- Surface drag force shows decreasing behavior for Forchheimer, porosity, material and magnetic parameters.
- The Prandtl number leads to Nusselt number enhancement.
- Nusselt number improvement against thermal relaxation time and magnetic parameters is ensured.

Conflicts of interest

There are no conflicts to declare.

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