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# DFT insights into Nb-based 211 MAX phase carbides: Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd)†

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In this study, we performed the first-principles calculations to study the 211 MAX phase carbides: Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al). The structural characteristics are in good agreement with those of the prior studies. The mechanical behavior has been explored by calculating the stiffness constants, elastic moduli, and Vickers hardness. The stiffness constants and phonon dispersion curves were used to check the structural stability of the selected compounds. 2D and 3D plotting of elastic moduli and calculated anisotropy indices disclosed the anisotropy of the elastic properties. We utilized the Mulliken atomic and bond overlap population to explain the mixture of ionic and covalent bonding among these carbides. The metallic behavior has been confirmed by calculating the band structure and density of states (DOS). Partial DOS was also used to discuss the bonding nature and strength among the different states. The optical properties of these phases have also been computed and analyzed to reveal possible relevance in diverse fields. The Debye temperature ( $\Theta_D$ ), Grüneisen parameter ( $\gamma$ ), melting temperature ( $T_m$ ), and minimum thermal conductivity ( $K_{min}$ ) were studied to bring out their possible relevance in high-temperature technology. The outcomes of this research indicate that the titled carbides are suitable for use as solar radiation-protecting coating and thermal barrier coating (TBC) materials.

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## 1 Introduction

Many ternary compounds such as carbides, nitrides, and borides have been included in the MAX phase materials family and can be expressed as M<sub>n+1</sub>AX<sub>n</sub>, where M belongs to the early transition metal group, A is the element that exists within the groups 12–16, and X can only be C, N, and B, and n is a positive integer with a value of 1–3.<sup>1–4</sup> The MAX phase was first revealed in the 1960s by Nowotny *et al.*<sup>1–4</sup> In the 1990s, Barsoum *et al.*<sup>5,6</sup> renewed the interest by revealing their remarkable characteristics. They have remarkable mechanical strength, machinability, electronic conductivity, and thermal conductivity. They are also machinable, similar to metals, have better mechanical properties at high temperatures, and have superior corrosion and oxidation resistance including ceramics.<sup>7</sup> The MAX phase family has become a significant materials group from both research and application points of view. Owing to the magnificent fusing of metallic and ceramic properties, the number of published articles is increasing day by day.<sup>8</sup>

Use of C and N as X elements was confined for a long time<sup>9–11</sup> and has been extended recently, where B has been used as an X element. The extension has opened a new platform for the MAX phase materials, owing to the interesting properties and

potential applications of B and B-containing compounds.<sup>12,13</sup> To date, only a few of the MAX phase borides have been synthesized so far in spite of a large number of predicted phases.<sup>14</sup> On the contrary, a significant number of MAX phase carbides have already been synthesized and characterized, revealing their prospective applications. In parallel to the experimental study, a large number of computational approaches<sup>15,16</sup> have also already been performed throughout the last decades. Cover *et al.*<sup>17</sup> performed the first-principles calculation of the elastic properties of 240 elemental combinations, revealing the role of A elements and their interaction with M elements. Keast *et al.*<sup>18</sup> computed the total energies of competing phases to check the stability of five different schemes (Cr<sub>n+1</sub>-Al-C<sub>n</sub>, Ti<sub>n+1</sub>-Al-C<sub>n</sub>, Ti<sub>n+1</sub>-Si-N<sub>n</sub>, Ti<sub>n+1</sub>-Al-N<sub>n</sub>, and Ti<sub>n+1</sub>-Si-C<sub>n</sub>, where n is a positive integer with a value of 1 ~ 4). Aryal *et al.*<sup>19</sup> studied 792 MAX phases, and 665 phases were found to be thermodynamically and elastically stable. 10 314 solid solutions and 216 possible M<sub>2</sub>AX phases were revealed by Ashton *et al.*<sup>20</sup> Khaledialidusti *et al.*<sup>21</sup> explored a large group of MAX phases, where M is taken as Sc, Ti, Y, Zr, V, Cr, Nb, Hf, Ta, Mo, and W and A is taken as P, S, Al, Si, Zn, Cu, Ga, As, Ge, Sn, Cd, In, Bi, Ir, Tl, Au, and Pb, and revealed their possibility of exfoliation to produce 2D systems. More than 80 MAX phases have been synthesized, most of which are 211 phases (58 prominent members).<sup>22</sup> These studies have inspired us to think about Nb-based 211 MAX phases.

Nb-based 211 MAX phases have also attracted attention in recent years. For example, Nb<sub>2</sub>AC (A = Al, Ge, Ga, Sn, In, As, P, S, and Cu) MAX phases were studied by Hadi *et al.*<sup>23</sup> to explore the

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elastic behavior and radiation tolerant behavior. Superconducting nature has been found in the Nb<sub>2</sub>SnC, Nb<sub>2</sub>InC, Nb<sub>2</sub>AsC, and Nb<sub>2</sub>SC phases<sup>23</sup> with the lowest superconducting temperature for Nb<sub>2</sub>AsC.<sup>22</sup> Bouhemadou *et al.*<sup>24,25</sup> performed first-principles calculations to study the structural and elastic properties of Nb<sub>2</sub>InC and Nb<sub>2</sub>GeC. The Nb<sub>2</sub>InC phase was first synthesized by Jeitschko *et al.*<sup>26</sup> Nb<sub>2</sub>AlC has attracted much attention as a viable material because of its better mechanical and thermal properties.<sup>27,28</sup> When compared with several MAX phases, it has been seen that Nb<sub>2</sub>PC has higher elastic constants.<sup>17</sup> The exfoliation possibility of Nb<sub>2</sub>GaC and Nb<sub>2</sub>InC into 2D MXene systems has been reported.<sup>29</sup> The electrochemical properties of Nb<sub>2</sub>SnC have been investigated for use in a Li-ion electrolyte.<sup>30</sup> The noble transition metal Cu has also been selected as an A element in Nb<sub>2</sub>CuC.<sup>31</sup> Shein *et al.*<sup>32</sup> explored the structural, electrical, and elastic properties of M<sub>2</sub>GaC (M = Mo, V, and Nb). Cover *et al.*<sup>17</sup> studied only the elastic and structural properties of Nb<sub>2</sub>SiC, whereas some fundamental properties need to be investigated. Bouhemadou *et al.*<sup>33</sup> carried out a theoretical study to calculate the structural, elastic, electronic, and thermal properties of Nb<sub>2</sub>SiC.

Moreover, so far, we know only the electronic and mechanical characteristics of Nb<sub>2</sub>AC (A = Ga, Ge, P, and In) phases have been investigated, whereas Nb<sub>2</sub>AC (A = Tl, Zn, and Cd) phases have been predicted to be stable *via* the calculation of formation energy,<sup>21</sup> and the physical properties are not disclosed yet. Exploration of the physical properties of new materials carries the same significance as prediction of new materials: it is impossible to take any advantage of new materials unless their physical properties are brought out. Several essential physical aspects, important optical properties, mechanical anisotropy, Vickers hardness including Mulliken populations, and thermal properties of Nb<sub>2</sub>AC (A = Ga, Ge, P, and In) are still unexplored. Mechanical anisotropy is critical for structural materials since it is linked to important mechanisms such as crack formation (and propagation), plastic deformation, and elastic instability, all of which limit their utility. The Vickers hardness describes the total strength properties of a solid's particular bonds. Mulliken population analysis is important to prove the existence of the combination of the ceramic and metallic nature. Understanding the thermal properties is important to forecast their appropriateness for use in extreme conditions. The optical characteristics of standard MAX phase compounds are necessary to predict their possible applications, for instance, as coating materials for protection from solar heating. These are the motivations behind this study, which demonstrates the significance of in-depth research on MAX phase carbides Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd).

Therefore, we aimed to provide a theoretical insight into the MAX phase carbides Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd), in which we will consider the first-time investigation of Nb<sub>2</sub>AC (A = Tl, Zn, and Cd) and some important unexplored properties of Nb<sub>2</sub>AC (A = Ga, Ge, P, and In) phases. Last of all, the calculated parameters of the titled phases are compared with those of the most known Nb-based phase, Nb<sub>2</sub>AlC, to make this research a systematic one.

## 2 Computational methodology

The Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd) carbides' physical properties have been calculated using the pseudopotential-based DFT, implemented in CASTEP (Cambridge Serial Total Energy Package).<sup>34,35</sup> For the term of exchange-correlation, the GGA (generalized gradient approximation) of the PBE (Perdew–Burke–Ernzerhof)<sup>36</sup> and PBEsol (Perdew–Burke–Ernzerhof for solids)<sup>37</sup> were used. The PBE has been widely used for DFT calculations, whereas PBEsol gives a more accurate lattice constant for solids.<sup>38</sup> Recently, the effect of different functionals on the calculated values of the parameters has been reported, in which it is seen that the PBEsol gives more accurate results of the lattice parameters compared with other functionals for solids. The more accurate values of the lattice parameters give more accurate results, especially the mechanical behavior characterizing parameters. Thus, we have selected PBEsol in association with the mostly used GGA-PBE functional for this study.<sup>39,40</sup> The electronic structure was optimized by density mixing, and the atomic configuration was relaxed using BFGS (Broyden Fletcher Goldfarb Shanno).<sup>41</sup> The electronic orbitals of Nb- 4d<sup>4</sup> 5s<sup>1</sup>, C- 2s<sup>2</sup> 2p<sup>2</sup>, Ga- 4s<sup>2</sup> 4p<sup>1</sup>, Ge- 3d<sup>10</sup> 4s<sup>2</sup> 4p<sup>2</sup>, Tl- 5d<sup>10</sup> 6s<sup>2</sup> 6p<sup>1</sup>, Zn- 3d<sup>10</sup> 4s<sup>2</sup>, P- 3s<sup>2</sup> 3p<sup>3</sup>, In- 4d<sup>10</sup> 5s<sup>2</sup> 5p<sup>1</sup> and Cd- 4d<sup>10</sup> 5s<sup>2</sup> were accomplished for pseudo-atomic calculations. The cutoff energy was set to 500 eV, and the convergence was assured using a *k*-point mesh of 9 × 9 × 2.<sup>42</sup> The total energy self-consistent convergence was carried out using 5 × 10<sup>-6</sup> eV per atom, with 0.01 eV Å as the maximum force on the atom. Again, 5 × 10<sup>-4</sup> Å is used for an ionic displacement, which is the maximum range, with a maximum stress of 0.02 GPa. The phonon dispersion curves were calculated using the Density Functional Perturbation Theory (DFPT) linear-response method.<sup>43</sup> Most of our data have been compared to those of ref. 23 (and 25), where the calculations were performed using the following inputs: exchange-correlation – GGA-PBE (LDA-CA), cut-off energy- 550 (350) eV, *k*-points-10 × 10 × 2 (9 × 9 × 2).

## 3 Results and discussion

### 3.1 Structural properties and phase stability

**3.1.1 Structural properties.** As shown in Fig. 1, the unit cell of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) compounds belongs to the hexagonal system wherein the space group is *P6<sub>3</sub>/mmc* (No. 194).<sup>6</sup> Two formula units are there in the unit cell. Each formula unit cell has four atoms. The atomic positions in the unit cell are as follows: Nb atoms at (1/3, 2/3, *z<sub>M</sub>*), A atoms at (2/3, 1/3, 1/4) and the C atoms at (0, 0, 0). Additionally, *z<sub>M</sub>* is an internal parameter; its value is listed in Table 1.

Table 1 shows the lattice constants (*a*, *c*) for an optimized cell, internal parameters, and the hexagonal ratio (*c/a*) ratio of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al). The fundamental polyhedrons of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) are studied using Hug's distortion indexes (DIS).<sup>44,45</sup> Two parameters- the distortion of octahedral (*O<sub>d</sub>*) and trigonal prism (*P<sub>d</sub>*) of the M<sub>6</sub>X octahedrons and M<sub>6</sub>A trigonal prisms, respectively, are used to describe the distortions in the structure of the 211 MAX phases using the following equations:<sup>46</sup>



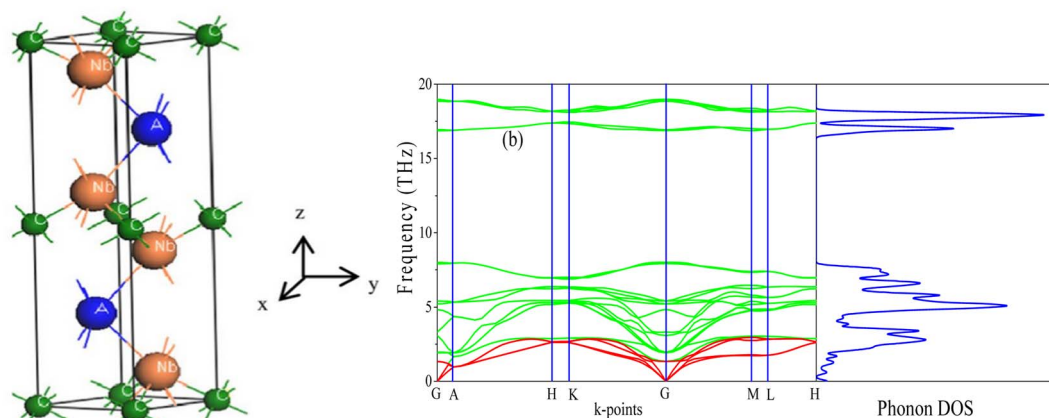


Fig. 1 (a) The unit cell of  $\text{Nb}_2\text{AC}$  ( $A = \text{Ga, Ge, Tl, Zn, P, In, Cd, and Al}$ ); (b) phonon dispersion curve and DOS of  $\text{Nb}_2\text{GaC}$  calculated using GGA PBEsol.

Table 1 Calculated lattice parameters ( $a$  and  $c$ ),  $c/a$  ratio, internal parameter ( $Z_m$ ), density ( $\rho$ ), volume ( $\text{\AA}^3$ ), and distortion parameters of octahedral ( $O_d$ ) and trigonal prisms ( $P_d$ ) of  $\text{Nb}_2\text{AC}$  ( $A = \text{Ga, Ge, Tl, Zn, P, In, Cd, and Al}$ ) MAX phases

Phases	$a$ ( $\text{\AA}$ )	$c$ ( $\text{\AA}$ )	$Z_m$	$c/a$	Density ( $\rho$ )	Volume ( $\text{\AA}^3$ )	$O_d$	$P_d$	Ref.
$\text{Nb}_2\text{GaC}$	3.145	13.73	0.0896	4.366	7.59	<sup>a</sup> 116.97	1.039	0.689	<sup>a</sup> This
	3.115	13.51		4.337		<sup>b</sup> 113.53	1.044	0.834	<sup>b</sup> This
	3.143	13.64		4.340		116.66	*1.044	*0.834	23
	3.13	13.56		4.332		115.05	*1.046	*0.836	6
$\text{Nb}_2\text{GeC}$	3.244	12.69	0.095	3.914	7.76	115.75	1.086	0.904	<sup>a</sup> This
	3.194	12.77		3.998		112.83	1.066	0.890	<sup>b</sup> This
	3.255	12.59		3.868			*1.097	*0.912	32
	3.237	12.35		3.815			*1.109	*0.959	25
	3.228	12.76		3.953		115.10	*1.076	*0.898	23
$\text{Nb}_2\text{TlC}$	3.229	12.74	0.0795	3.944	10.18	131.11	1.254	0.891	<sup>a</sup> This
	3.199	14.27		4.461		126.46	1.131	0.781	<sup>b</sup> This
$\text{Nb}_2\text{ZnC}$	3.145	13.73	0.0875	4.366	7.43	117.58	1.060	0.829	<sup>a</sup> This
	3.117	13.53		4.341		113.83	1.066	0.833	<sup>b</sup> This
$\text{Nb}_2\text{PC}$	3.299	11.59	0.0999	3.515	8.28	109.33	1.149	0.978	<sup>a</sup> This
	3.267	11.52		3.526		106.48	1.146	0.976	<sup>b</sup> This
	3.292	11.578		3.517		108.68	*1.139	*0.978	23
	3.28	11.5		3.506		107.15	*1.152	*0.979	6
$\text{Nb}_2\text{InC}$	3.185	14.54	0.0821	4.563	11.49	127.69	1.103	0.799	<sup>a</sup> This
	3.152	14.37		4.559		123.67	1.079	0.799	<sup>b</sup> This
	3.186	14.528		4.560		127.72	*1.079	*0.799	23
	3.172	14.37		4.530		125.21	*1.085	*0.804	47
$\text{Nb}_2\text{CdC}$	3.172	14.68	0.0830	4.628	8.06	127.87	1.055	0.790	<sup>a</sup> This
	3.140	14.45		4.602		123.37	1.060	0.794	<sup>b</sup> This
$\text{Nb}_2\text{AlC}$	3.245	12.69	0.0897	3.911	6.34	115.74	1.142	0.902	<sup>a</sup> This
	3.102	13.79		4.446		114.99	1.021	0.819	<sup>b</sup> This
	3.12	13.93		4.463		117.41	*1.017	*0.817	23

<sup>a</sup> Calculated values using GGA PBE.<sup>36</sup> <sup>b</sup> Calculated values using GGAPBEsol<sup>37</sup> and \*calculated values using reported data.

$$O_d = \sqrt{3/2} \{4z_M^2 (ca)^2 + 1/12\}^{1/2}$$

$$P_d = 1/\{1/3 + (1/4 - z_M)^2 (ca)^2\}^{1/2}$$

The polyhedron would be ideal when both the octahedron and the trigonal parameters are equal to 1.<sup>46</sup> The distortion of the polyhedron is measured by the deviation from 1, where a low distortion value indicates a more stable structure.<sup>46</sup>

Table 1 shows the value of the  $O_d$  and  $P_d$  of  $\text{Nb}_2\text{AC}$  ( $A = \text{Ga, Ge, Tl, Zn, P, In, Cd, and Al}$ ). Table 1 also contains the  $O_d$  and  $P_d$  of  $\text{Nb}_2\text{AC}$  ( $A = \text{Ga, Ge, P, In, and Al}$ ) as calculated from the reported lattice parameters. A very good consistency is observed for the previously studied phases, indicating the reliability of our present calculations. The comparison is not possible for  $\text{Nb}_2\text{AC}$  ( $A = \text{Tl, Zn, and Cd}$ ) phases because of their first-time calculation. The accuracy of the present calculations is also revealed by the close agreement of the values of  $a$  and  $c$



[Table 1] of Nb<sub>2</sub>AC (A = Ga, Ge, P, In, and Al) phases with previously reported values.<sup>23,25,32</sup>

**3.1.2 The dynamical stability.** To check the dynamical stability of the titled phases, we have computed the phonon dispersion curves (PDC) and phonon density of states (PHDOS) of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd), displayed in Fig. 1(b) for Nb<sub>2</sub>GaC and Fig. S1(a–f) [in the ESI file†] for the rest of the six compounds. The phonon frequency across the entire BZ is used to determine whether a compound is stable or not: positive frequencies indicate stability, whereas any negative frequencies indicate the instability of the compounds. As evident from Fig. 1(b) and S1(a–f),† the studied phases are dynamically stable owing to the non-existence of the negative frequency. In addition, one can obtain some more information from the PDCs. The PDCs have 24 vibrational modes that are caused by the eight atoms in the unit cell. There are only three acoustic modes, whereas the rest 21 are called optical modes. The dispersion curve for the lower three modes is of the form  $\omega = \nu k$  at small  $k$  values, and it illustrates the sound wave's  $\omega(k)$  relations. These modes are the part of the acoustic branch. The upper vibrational modes create the optical branch. The optical phonons are produced due to the atom's out-of-phase oscillations caused by photon-induced excitation. Acoustic modes have zero frequency just at the  $G$  point. No phononic band gap is found due to the overlap of the optical branches and acoustic modes. Furthermore, the PHDOS is presented alongside the PDCs, wherein the PDC's flat modes lead the sharp peaks. Peaks are diminished when the dispersion changes, either upward or downward. We have presented only the results for GGA PBEsol; GGA PBE results are not shown because of similarity in nature (Fig. 2).

## 3.2 Mechanical properties

**3.2.1 Stiffness constants and elastic moduli.** We have calculated the elastic stiffness constants and the polycrystalline elastic moduli using the strain–stress method<sup>48</sup> to bring out the mechanical behavior of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al). Checking mechanical stability is a must for solids before studying the mechanical properties. The Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) phases belong to the hexagonal system,

which need to satisfy the following requirements:  $C_{11} > 0$ ,  $C_{33} > 0$ ,  $C_{44} > 0$ ,  $C_{11} - C_{12} > 0$ ,  $(C_{11} + C_{12})C_{33} - 2(C_{13})^2 > 0$ .<sup>49,50</sup> We have calculated the elastic constants and presented them in Table 2, revealing that the requirements mentioned earlier have been satisfied by the selected carbides. Thus, Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) phases are considered to be mechanically stable. We may use the calculated stiffness constants to get some additional information. For instance,  $C_{11}$  and  $C_{33}$  measure the stiffness of the solid along the  $a$ -axis and  $c$ -axis when pressure is applied along [100] and [001] directions, respectively. Here,  $C_{11} > C_{33}$  for Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) compounds, revealing the requirement of more pressure along the  $a$ -axis for deformation compared to the  $c$ -axis, whereas for Nb<sub>2</sub>PC  $C_{33} > C_{11}$ . Moreover, the inequality of  $C_{11}$  and  $C_{33}$  also indicates the anisotropic bonding strength. The hexagonal structure contains different atomic arrangements along the  $a$ - and  $c$ -axis, which is assumed to be responsible for the difference in the bonding strength along the  $a$ - and  $c$ -axis. One of the stiffness constants,  $C_{44}$ , is considered to be a better hardness predictor<sup>51</sup> in comparison with other elastic constants. Thus, Nb<sub>2</sub>PC is expected to be the hardest one with the highest  $C_{44}$  (194 GPa), while Nb<sub>2</sub>TlC is the softest one with the lowest  $C_{44}$  (71 GPa). The  $C_{11}$ ,  $C_{33}$ , and  $C_{44}$  of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, In, and Cd) are lower than those of the most known Nb-based Nb<sub>2</sub>AlC phase, but the values are greater for Nb<sub>2</sub>PC. Better visualization of the differences among the values of the stiffness constants is done by presenting them in Fig. 2(a) for the GGA-PBEsol functional. Fig. S2(a)† shows the values calculated using GGA-PBE.

Furthermore, the stiffness constants are used to predict the ductile/brittle behavior of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, P, Zn, In, Cd, and Al) phases by computing the Cauchy pressure (CP). The difference between  $C_{11}$  and  $C_{44}$  is defined as the CP;<sup>52</sup> a negative and positive value represents the brittle and ductile nature, respectively. Negative and positive values also indicate the directional covalent and ionic bonds, respectively. As evident from Table 2, Nb<sub>2</sub>GaC, Nb<sub>2</sub>GeC, Nb<sub>2</sub>PC, Nb<sub>2</sub>InC, and Nb<sub>2</sub>AlC have directional covalent bonds and behave as brittle solids. On the contrary, Nb<sub>2</sub>TlC, Nb<sub>2</sub>ZnC, and Nb<sub>2</sub>CdC phases behave as ductile solids with a positive CP. Though most MAX phases are brittle, a few of them, such as Zr<sub>3</sub>CdB<sub>4</sub>, Ti<sub>2</sub>CdC,

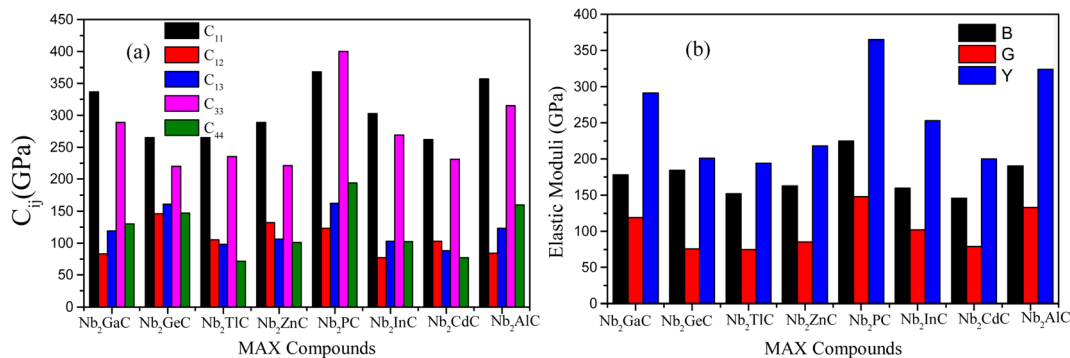


Fig. 2 Comparison of (a) stiffness constants and (b) elastic moduli of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) MAX phases calculated using GGA PBEsol.



**Table 2** Calculated stiffness constant ( $C_{ij}$ ), bulk modulus ( $B$ ), shear modulus ( $G$ ), Young's modulus ( $Y$ ), machinability index ( $B/C_{44}$ ), Cauchy pressure (CP), Poisson's ratio ( $\nu$ ), and Pugh ratio ( $G/B$ )

Parameters	Nb <sub>2</sub> GaC	Nb <sub>2</sub> GeC	Nb <sub>2</sub> TiC	Nb <sub>2</sub> ZnC	Nb <sub>2</sub> PC	Nb <sub>2</sub> InC	Nb <sub>2</sub> CdC	Nb <sub>2</sub> AlC	Ref.
$C_{11}$ (GPa)	337	265	265	289	368	303	262	357	<sup>a</sup> This
	363	306	283	294	394	331	282	368	<sup>b</sup> This
	323	284			373	280		333	23
$C_{33}$ (GPa)		308							25
	289	220	235	221	400	269	231	315	<sup>a</sup> This
	313	295	258	225	423	295	258	314	<sup>b</sup> This
	281	275			407	266		284	23
$C_{44}$ (GPa)		306							25
	130	147	71	101	194	102	77	160	<sup>a</sup> This
	141	151	86	113	212	112	89	164	<sup>b</sup> This
	126	152			193	104		138	23
$C_{12}$ (GPa)		177							25
	83	146	105	132	123	77	103	98	<sup>a</sup> This
	92	137	106	137	132	85	123	84	<sup>b</sup> This
	77	136			114	80		84	23
$C_{13}$ (GPa)		133							25
	119	161	98	106	162	103	88	123	<sup>a</sup> This
	131	161	118	122	179	112	102	119	<sup>b</sup> This
	130	161			172	113		117	23
CP (GPa)		168							25
	-47	-1	34	31	-71	-25	26	-62	<sup>a</sup> This
	-49	-14	20	24	-80	-27	34	-80	<sup>b</sup> This
	*-49	*-16			*-79	*-24		*-54	23
$B$ (GPa)		*-44							25
	178	184	152	163	225	160	146	190	<sup>a</sup> This
	194	203	168	173	242	175	163	188	<sup>b</sup> This
	178	195			230	160		176	23
$G$ (GPa)		206							25
	119	76	75	85	148	102	79	133	<sup>a</sup> This
	128	101	84	88	153	112	85	140	<sup>b</sup> This
	114	101			150	96		122	23
$Y$ (GPa)		109							25
	291	201	194	218	365	253	200	324	<sup>a</sup> This
	314	261	215	225	379	277	216	337	<sup>b</sup> This
	282	258			369	240		298	23
$\nu$		279							25
	0.23	0.32	0.29	0.28	0.23	0.24	0.27	0.22	<sup>a</sup> This
	0.23	0.29	0.29	0.28	0.24	0.23	0.28	0.20	<sup>b</sup> This
	*0.24	*0.28			*0.23	*0.25		*0.22	23
$G/B$		*0.28							25
	0.67	0.41	0.49	0.52	0.65	0.63	0.54	0.70	<sup>a</sup> This
	0.66	0.49	0.50	0.51	0.63	0.64	0.52	0.74	<sup>b</sup> This
	*0.64	*0.52			*0.65	*0.60		*0.69	23
$B/C_{44}$		*0.53							25
	1.36	1.25	2.14	1.61	1.15	1.56	1.89	1.18	<sup>a</sup> This
	1.38	1.34	1.95	1.53	1.14	1.56	1.83	1.15	<sup>b</sup> This
	*1.41	*1.28			*1.19	*1.54		*1.28	23
	*1.16							25	

<sup>a</sup> Calculated values using GGA PBE.<sup>36</sup> <sup>b</sup> Calculated values using GGA PBEsol<sup>37</sup> and \*calculated values using reported data.

and Ti<sub>2</sub>ZnX (X = C and N), have already been reported to be ductile.<sup>53–55</sup>

Finally, the stiffness constants were used to calculate the polycrystalline elastic moduli. Hill's approximation<sup>56</sup> was used to compute the bulk modulus ( $B$ ) and shear modulus ( $G$ ), which is the average of the Voigt<sup>57</sup> and the Reuss<sup>58</sup> models as follows:  $[B = (B_V + B_R)/2]$ ; here,  $B_V = [2(C_{11} + C_{12}) + C_{33} + 4C_{13}]/9$  and  $B_R = C^2/M$ , where  $C^2 = C_{11} + C_{12}C_{33} - 2C_{13}^2$ ;  $M = C_{11} + C_{12} + 2C_{33} - 4C_{13}$ .  $B_V$  and  $B_R$  are expressed as the upper (Voigt) and lower

limit (Reuss) of  $B$ , respectively. Again,  $[G = (G_V + G_R)/2]$ ; here,  $G_V = [12C_{44} + 12C_{66}]/30$  and  $G_R = (5/2) [C^2C_{44}C_{66}]/[3B_VC_{44}C_{66} + C^2(C_{44} + C_{66})]$ , where  $C_{66} = (C_{11} - C_{12})/2$ . Here, like  $B$ ,  $G_V$  and  $G_R$  are also expressed as the upper (Voigt) and lower limit (Reuss) of  $G$ , respectively. The Poisson's ratio ( $\nu$ ) and Young's modulus ( $Y$ ) are also computed from  $B$  and  $G$  by using these relations:  $Y = 9BG/(3B + G)$  and  $\nu = (3B - Y)/(6B)$ .<sup>59,60</sup>

As known, the pure deformations (volume and shape) are studied by the bulk modulus (mostly known for the study of



elastic response against pressure) and the shear modulus (mostly known for the study of rigidity of solids against pressure). It is seen from Table 2 that Nb<sub>2</sub>PC (Nb<sub>2</sub>CdC) has the highest (lowest) resistance against hydrostatic pressure, whereas the lowest resistance to plastic deformation is noted for Nb<sub>2</sub>TlC among the studied compounds. However, the compounds can be ranked based on the values of *B* (calculated using GGA-PBESol) as follows: Nb<sub>2</sub>PC > Nb<sub>2</sub>GeC > Nb<sub>2</sub>GaC > Nb<sub>2</sub>AlC > Nb<sub>2</sub>InC > Nb<sub>2</sub>ZnC > Nb<sub>2</sub>TlC > Nb<sub>2</sub>CdC, whereas the ranking for *G* will be as follows: Nb<sub>2</sub>PC > Nb<sub>2</sub>AlC > Nb<sub>2</sub>GaC > Nb<sub>2</sub>InC > Nb<sub>2</sub>GeC > Nb<sub>2</sub>ZnC > Nb<sub>2</sub>CdC > Nb<sub>2</sub>TlC. For Young's modulus, *Y* is the measure of the stiffness of solids that relates the stiffness with the thermal shock resistance (inverse relationship) of solids. Therefore, a solid with a high *Y* value indicates high stiffness and low thermal shock resistance (TSR).<sup>61</sup> The *Y*-based ranking of the phases also follows the *G*-based ranking. Table 2 implies that Nb<sub>2</sub>TlC exhibits high TSR, while Nb<sub>2</sub>PC has the lowest TSR, followed by the *Y*-based reverse ranking among the herein-studied phases. Although these moduli do not indicate hardness, they are usually higher for harder materials.<sup>62</sup> Compared to *Y*, *B* and *G* have a close relationship with the material's hardness. In some cases, these parameters are used to predict the hardness of solids using the following formulae:  $H_{\text{Chen}} = 2 \left[ \left( \frac{G}{B} \right)^2 G \right]^{0.585} - 3$ ,<sup>63</sup> and  $H_{\text{miao}} = \frac{(1-2\nu)E}{6(1+\nu)}$ ,<sup>64</sup> Table 2 also includes the previously reported values.<sup>23</sup> As evident from Table 2, the obtained values are in good accord with reported values, ensuring the accuracy of the present calculation that helps other researchers to consider our calculated values as a reference for both application and research purposes. A comparison of the elastic moduli for the studied compounds is shown in Fig. 2(b).

**3.2.2 The brittleness of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al).** The remarkable combination of metal and ceramic characteristics is the most excellent feature of MAX phases.<sup>65</sup> They are machinable, just like metals, as stated in the preceding section, and brittle, just like ceramic materials. But, some of them are also ductile,<sup>53,55,66</sup> making them more machinable and, consequently, more useful owing to easy shaping. By using the Pugh ratio (*G/B*)<sup>67</sup> and Poisson's ratio (*ν*),<sup>68</sup> the ductile/brittle characteristics of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) have been evaluated and are presented in Table 2. Pugh proposed a critical value of *G/B* ratio (0.571) for ductile (less than 0.571) and brittle (greater than 0.571) classification, whereas *ν* is used to separate the brittle (less than 0.26) and ductile (greater than 0.26) solids with a critical value of 0.26. As evident, Nb<sub>2</sub>GaC, Nb<sub>2</sub>PC, Nb<sub>2</sub>InC, and Nb<sub>2</sub>AlC are brittle, while Nb<sub>2</sub>GeC, Nb<sub>2</sub>TlC, Nb<sub>2</sub>ZnC, and Nb<sub>2</sub>CdC are ductile; the results are in good agreement with the CP results presented above and the previously reported results.<sup>23,25</sup>

The Machinability Index (MI) is commonly used in the tribological sector to forecast a solid's performance and is defined as the *B/C*<sub>44</sub> ratio. The MI index is presented in Table 2. As evident, the MI of Nb<sub>2</sub>TlC, Nb<sub>2</sub>ZnC, and Nb<sub>2</sub>CdC is higher than that of other studied phases owing to their ductile nature. Though Nb<sub>2</sub>GeC is ductile, its *C*<sub>44</sub> is comparatively higher,

which results in a lower MI value. Based on the values [Table 2], the titled phases are expected to be more machinable than the widely known Nb<sub>2</sub>AlC phase except for Nb<sub>2</sub>PC. The lowest MI is found for Nb<sub>2</sub>PC, as expected, due to its highest *C*<sub>44</sub>. In addition, a good relationship between machinability and ductility is observed as expected. The MI values are also different for PBE and PBESol functions because of the different values of *B* and *C*<sub>44</sub>. However, the obtained values of MI are comparable with those of some other 211 MAX phases, like Ti<sub>2</sub>AlC, whose machinability index is 1.23.<sup>69</sup> Though some 211 phases exhibit a very high value of MI, such as W<sub>2</sub>SnC (MI = 33.3) and Mo<sub>2</sub>PbC (MI = 15.8),<sup>17,70</sup> it should be noted that their *C*<sub>44</sub> values are much lower (W<sub>2</sub>SnC, 6 GPa, and Mo<sub>2</sub>PbC, 10 GPa).<sup>17</sup>

**3.2.3 Theoretical values of Vickers hardness.** The Vickers hardness, due to the atomic bonds present within the solids, is the solid's ability to resist deformation under extreme conditions. Different factors, such as the strength of the atomic bonds, atomic arrangement, the structure of the solids, crystal defects, *etc.*, determine the hardness of solids. The Vickers hardness of the Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) MAX phases is calculated using Mulliken bond population based on Gou *et al.*,<sup>71,72</sup> which is mostly suitable for partial metallic systems like MAX phases. The relevant hardness formula is  $H_v^{\mu} = 740(P^{\mu} - P^{\mu'}) (v_b^{\mu})^{-5/3}$ , here,  $P^{\mu}$  indicates the  $\mu$  type bond's Mulliken overlap population and  $P^{\mu'} = n_{\text{free}}/v$ ;  $n_{\text{free}} = \int_{E_p}^{E_F} N(E)dE$ ,  $E_p$  indicates the energy of the pseudogap and  $E_F$  indicates the energy of the Fermi level. The volume of the  $\mu$ -type bond is denoted by  $v_b^{\mu}$ , which is calculated in the following way:  $v_b^{\mu} = (d\mu)^3 / \sum v[(d\mu)^3 N_b^{\nu}]$ . At last, the equation for Vickers hardness is as follows:  $H_v = [\prod \pi(H_v^{\mu}) n^{\mu}]^{1/3} / \sum n^{\mu}$ ;  $n^{\mu} = \mu$ -type bond number. Table 3 shows the computed Vickers hardness of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al). As shown in Table 3, Nb<sub>2</sub>PC has higher Vickers hardness than other studied compounds, wherein Nb<sub>2</sub>TlC possesses the lowest value of  $H_v$ , in agreement with mechanical parameters such as *C*<sub>44</sub> and *G*, which are assumed to be more related to the hardness of solids. The  $H_v$  values of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, In, Cd, and Al) are comparable with the exception of Nb<sub>2</sub>PC, which has a much higher value of  $H_v$ . This can be explained on the basis of the bond overlap population ( $P^{\mu}$ ). As seen in Table 3, the  $P^{\mu}$  of Nb<sub>2</sub>PC is 1.01 and 0.98 for C–Nb and P–Nb bonds, respectively, which indicates that strong covalent bonding is found between both Nb–C and Nb–P atoms, whereas for Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, In, Cd, and Al),  $P^{\mu}$  is found only for Nb–C atoms, and no other significant covalent bond is noticed for these phases. Thus, both significant covalent bonding among Nb–C and Nb–P atoms is assumed to be responsible for such higher hardness. However, the variation in  $H_v$  of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, In, Cd, and Al) phases is due to the combined effect of the variation in both bond population  $P^{\mu}$  and bond length  $d^{\mu}$ .

### 3.3 Electronic properties, and Mulliken atomic and bond population analysis

**3.3.1 Electronic properties.** The electronic conductivity, contribution from different states, and nature of atomic



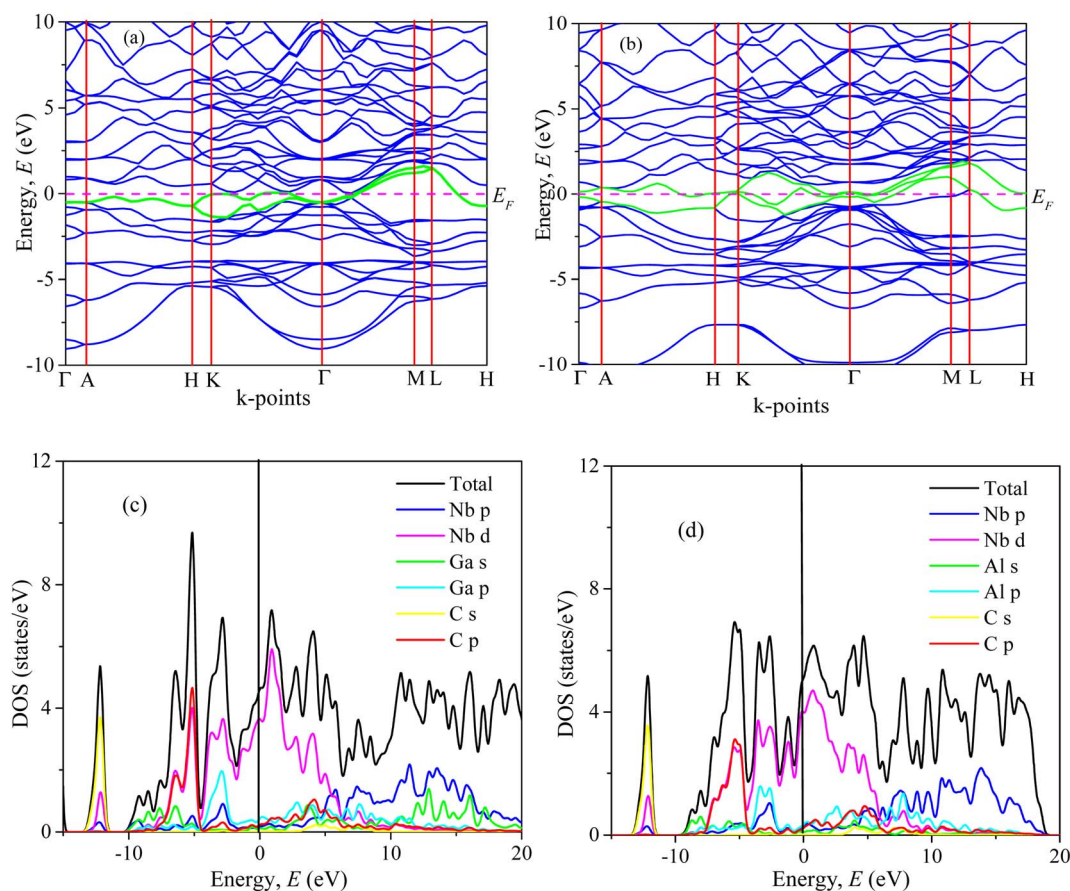
**Table 3** Calculated Mulliken bond number  $n^\mu$ , bond length  $d^\mu$ , bond overlap population  $P^\mu$ , metallic population  $P^{\mu'}$ , bond volume  $v_b^\mu$ , bond hardness  $H_v^\mu$  of the  $\mu$ -type bond and Vickers hardness  $H_v$

Compounds	Bond	$n^\mu$	$d^\mu$ (Å)	$P^\mu$	$P^{\mu'}$	$v_b^\mu$ (Å <sup>3</sup> )	$H_v^\mu$ (GPa)	$H_v$ (GPa)	Ref.
Nb <sub>2</sub> GaC	C–Nb	4	2.177	0.93	0.0223	0.0036	2.418	2.418	<sup>a</sup> This
			2.167	0.93	0.0209	0.0037	2.55	2.55	<sup>b</sup> This
Nb <sub>2</sub> GeC	C–Nb	4	2.208	0.99	0.0443	0.0037	1.498	1.498	<sup>a</sup> This
			2.183	1.02	0.0100	0.0038	2.86	2.86	<sup>b</sup> This
Nb <sub>2</sub> TlC	C–Nb	4	2.194	0.94	0.0358	0.0029	1.994	1.994	<sup>a</sup> This
			2.176	0.96	0.0207	0.0031	2.19	2.19	<sup>b</sup> This
Nb <sub>2</sub> ZnC	C–Nb	4	2.177	0.92	0.0504	0.0036	2.297	2.297	<sup>a</sup> This
			2.160	0.91	0.0741	0.0037	2.33	2.33	<sup>b</sup> This
Nb <sub>2</sub> PC	C–Nb	4	2.229	1.01	0.0195	0.0187	13.706	9.312	<sup>a</sup> This
			2.580	0.98	0.0089	0.0089	6.326		<sup>a</sup> This
	P–Nb	4	2.211	1.00	0.0166	0.0200	14.56	10.02	<sup>b</sup> This
			2.557	0.98	0.0096	0.0096	6.89		<sup>b</sup> This
Nb <sub>2</sub> InC	C–Nb	4	2.193	0.96	0.0184	0.0031	2.160	2.160	<sup>a</sup> This
			2.174	0.95	0.0105	0.0032	2.82	2.82	<sup>b</sup> This
Nb <sub>2</sub> CdC	C–Nb	4	2.177	0.99	0.0206	0.0031	2.224	2.224	<sup>a</sup> This
			2.160	0.93	0.0648	0.0032	2.11	2.11	<sup>b</sup> This
Nb <sub>2</sub> AlC	C–Nb	4	2.165	0.98	0.0179	0.0037	2.63	2.63	<sup>a</sup> This
			2.166	1.00	0.0112	0.0037	2.71	2.71	<sup>b</sup> This

<sup>a</sup> Calculated values using GGA PBE.<sup>36</sup> <sup>b</sup> Calculated values using GGA PBEsol.<sup>37</sup>

bonding can be revealed by studying the electronic band structure, total and partial density of states (DOS), and Mulliken's population analysis. We have calculated the electronic

band structure to predict the metallic nature of the titled MAX compounds. Fig. 3(a), (b) and S3† [calculated using PBEsol] show the calculated electronic band structure of Nb<sub>2</sub>AC (A = Ga,



**Fig. 3** Band structure, and total and partial DOS of (a, c) Nb<sub>2</sub>GaC and (b, d) Nb<sub>2</sub>AlC calculated using GGA PBEsol.



Ge, Tl, Zn, P, In, Cd, and Al), in which the Fermi level ( $E_F$ ) is represented by a horizontal dashed line. The green curves indicate the Fermi level crossing bands and blue curves denote the bands in the valence and conduction bands. As seen from Fig. 3(a), (b) and S3(a)–(f)† due to the overlapping of the conduction and valence bands, there is no band gap at the Fermi level; thus, the Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) phases are considered to be metallic solids. The pathways  $\Gamma$ -A, H-K, and M-L show the energy dispersion for the  $c$ -direction. On the other hand, the pathways A-H, K- $\Gamma$ ,  $\Gamma$ -M, and L-H show energy dispersion in the basal planes. It has been seen from Fig. 3(a), (b) and S3(a)–(f)† that the energy dispersion is smaller in the  $c$ -direction than that of the basal plane ( $ab$ -plane); thus, the electronic conductivity in the basal plane is higher than that of the  $c$ -direction.<sup>73</sup> The effective mass tensor is assumed to be higher in the  $c$ -direction than that of the basal plane, which is responsible for smaller dispersion in the  $c$ -direction.<sup>74</sup> Consequently, the anisotropic nature of electronic conductivity is observed in the herein-studied phases, a common feature of the MAX phases, including Nb<sub>2</sub>AlC.<sup>25,72</sup>

We have also computed the total and partial density of states (DOS) of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al), which are also shown in Fig. 3(c), (d) and S4(a)–(f)† [calculated using PBEsol]. Here,  $E_F$  is the Fermi level, where the DOS values are 3.2, 3.3, 4.0, 3.5, 3.0, 3.1, 2.8, and 3.0 for Nb<sub>2</sub>GaC, Nb<sub>2</sub>GeC, Nb<sub>2</sub>TlC, Nb<sub>2</sub>ZnC, Nb<sub>2</sub>PC, Nb<sub>2</sub>InC, Nb<sub>2</sub>CdC, and Nb<sub>2</sub>AlC, respectively. The computed compound's DOSs of the studied phases are found to be similar to those of reported MAX phases<sup>25,72</sup> and Nb<sub>2</sub>AlC, which is presented here for comparison.

We have also computed the partial density of states (PDOS) to understand better the chemical bonding of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al). Fig. 3(c), (d), and S4(a)–(f)† [calculated using PBEsol] show the PDOS for Nb<sub>2</sub>AC. As seen, C-2s is not involved in the DOS at  $E_F$ . As a result, the conduction properties are not attributed to carbon. On the other hand, at the Fermi level, Nb-d electrons contribute significantly to the DOS; therefore, the conduction properties ought to be involved in Nb. The A-p (A = Ga, Ge, Tl, Zn, P, In, and Cd) electrons are also involved in the conduction mechanism, with a much lower level of contribution. C-p states also slightly contribute to the conduction properties. This outcome is in line with an earlier MAX phase reported.<sup>68</sup> The degenerate states concerning both lattice sites and angular momentum indicate that a covalent interaction exists between the atoms of the compounds. Hybridized states include C-p and Nb-d and A (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) p and Nb d states. Moreover, some ionic characteristics can be anticipated because of the disparity in electro-negativity between the constituent atoms. There is a covalent-ionic combination in the bonding character, which has been explained in Section 3.3.2. When compared to Nb-d and A-p states, the hybridization peak of Nb-d and C-p lies in the lower energy side, as seen in the PDOS; consequently, covalent bonding due to hybridization between Nb-d and C-p states is stronger than that of Nb-d and A p states (A = Ga, Ge, Tl, Zn, P, In, and Cd). The peak position of hybridization between Nb-X and Nb and A states is also responsible for the variation in the hardness of the

studied phases. For example, the hybridization among Nb-d, P-p and C-p states is observed in the lowest energy side (below  $-5$  eV), which results in strong hybridization among them, and a higher bond overlap population is found, which results in the hardest phase of Nb<sub>2</sub>PC among the considered phases. The same hybridization peak for other phases is found to appear at an energy scale of above  $-5$  eV. Similar results are also reported for the MAX phases.<sup>25,72</sup> Additionally, we demonstrated the PDOS of Nb<sub>2</sub>AlC, which is similar to those of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al).

**3.3.2 Mulliken's atomic and bond population analysis.** The charge transfer mechanism can be understood by analyzing the atomic population. Mulliken's atomic populations are presented in Table 4 [calculated using GGA PBEsol] and Table S1† [calculated using GGA PBE]. As seen, C possesses a negative charge for each phase, whereas Nb and A (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) have positive charges, which indicates that the charges are transferred from A (A = Ga, Ge, Tl, and Zn) and Nb to the C atoms. The charge transfer mechanism in these phases indicates the existence of ionic bonding within them. The BOP (bond overlap population) study quantitatively provides bonding and anti-bonding strength.<sup>75</sup> A positive BOP stands for covalent bonds, and a negative BOP value certifies ionic bonds. As evident from Table 4, a strong covalent bond is formed between Nb and C atoms for each of the titled phases. For Nb<sub>2</sub>PC, a strong covalent bond is also expected to be formed in association with the Nb–C bonds, which is responsible for a much higher hardness value compared to other phases presented here. Thus, electronic charge transfer ensured the presence of ionic bonding. In contrast, the high positive value of BOP revealed the existence of covalent bonding, a common characteristic of the MAX phase materials.

### 3.4 The elastic anisotropy

The study of the elastic anisotropy of the MAX phases is essential because of their potential use in practical applications. Some important physical processes, such as plastic deformation, unusual phonon modes, dislocation dynamics, crack behavior, *etc.*, are caused by mechanical anisotropy in solids.<sup>76,77</sup> Since the values of  $C_{11}$  and  $C_{33}$  are unequal [Table 2], other elastic moduli are calculated using these elastic constants. Thus anisotropic nature of the elastic properties is expected for these compounds. These facts encourage us to study the mechanical anisotropy of the titled carbides in the 211 MAX phases. It is possible to demonstrate the level of anisotropy by plotting the elastic moduli in different directions. In this manner, we used the ELATE code<sup>78</sup> to compute the values of Young's modulus, compressibility, shear modulus, and Poisson's ratio, which are presented in Fig. 4(a–d) for Nb<sub>2</sub>GaC, 5(a–d) for Nb<sub>2</sub>AlC, S5(a–d) for Nb<sub>2</sub>GeC, S6(a–d) for Nb<sub>2</sub>TlC, S7(a–d) for Nb<sub>2</sub>ZnC, S8(a–d) for Nb<sub>2</sub>PC, S9(a–d) for Nb<sub>2</sub>InC and S10(a–d)† for Nb<sub>2</sub>CdC. The 3D and 2D plots will help to explain the anisotropic nature. The isotropic nature of solids is represented by the sphere in 3D plots and the circle in 2D plots. In contrast, the anisotropy is indicated by a departure from a perfect circle or sphere, and the degree depends on the





Table 4 Mulliken atomic and bond overlap population (BOP) calculated using GGA PBEsol

Phases	Atoms	s	p	d	Total	Charge (e)	Bond	Bond number $n^{\mu}$	Bond overlap population $P^{\mu}$
Nb <sub>2</sub> GaC	C	1.43	3.22	0.00	4.65	-0.65	C-Nb	4	0.93
	Ga	0.88	1.84	9.99	12.71	0.29			
	Nb	2.27	6.62	3.94	12.82	0.18			
Nb <sub>2</sub> GeC	C	1.45	3.23	0.00	4.67	-0.67	C-Nb	4	1.02
	Ge	0.99	2.53	0.00	3.52	0.48			
	Nb	2.35	6.56	3.99	12.90	0.10			
Nb <sub>2</sub> TlC	C	1.43	3.22	0.00	4.65	-0.65	C-Nb	4	0.96
	Tl	3.11	7.84	9.92	20.87	0.13			
	Nb	2.25	6.58	3.92	12.74	0.26			
Nb <sub>2</sub> ZnC	C	1.43	3.23	0.00	4.66	-0.66	C-Nb	4	0.91
	Zn	0.53	1.32	9.93	11.78	0.22			
	Nb	2.28	6.63	3.87	12.78	0.22			
Nb <sub>2</sub> PC	C	1.44	3.20	0.00	4.63	-0.63	C-Nb	4	1.00
	P	1.57	3.45	0.00	5.02	0.04			
	Nb	2.24	6.45	3.98	12.67	0.33			
Nb <sub>2</sub> InC	C	1.43	3.22	0.00	4.65	-0.65	C-Nb	4	0.95
	In	0.99	1.81	9.97	12.77	0.23			
	Nb	2.22	6.63	3.94	12.79	0.21			
Nb <sub>2</sub> CdC	C	1.43	3.23	0.00	4.66	-0.66	C-Nb	4	0.93
	Cd	0.55	1.28	9.91	11.73	0.27			
	Nb	2.29	6.65	3.87	12.81	0.19			
Nb <sub>2</sub> AlC	C	1.45	3.22	0.00	4.67	-0.67	C-Nb	4	1.00
	Al	0.97	1.83	0.00	2.80	0.20			
	Nb	2.22	6.57	3.98	12.76	0.24			

departure level. Young's modulus ( $Y$ ) is anisotropic in the  $xz$  and  $yz$  planes but isotropic in the  $xy$  planes, as seen in Fig. 4(a), 5(a), S5(a), S6(a), S7(a), S8(a), S9(a), and S10(a).<sup>†</sup>  $Y$  has minimum values at the vertical axis of the  $xz$  and  $yz$  planes and a maximum value at an intermediate angle of  $45^\circ$  of those axes. Fig. 4(b), 5(b), S5(b), S6(b), S7(b), S8(b), S9(b), and S10(b)<sup>†</sup> depict the compressibility ( $K$ ), which exhibits a similar anisotropic character to  $Y$ . The compressibility ( $K$ ) is isotropic in the  $xy$  plane but anisotropic in the  $xz$  and  $yz$  planes, where  $K$  has maximum values on the axes of the  $xz$  and  $yz$  planes and a minimum value at an angle of  $45^\circ$  to those axes. For the considered compounds presented in Fig. 4(c), 5(c), S5(c), S6(c), S7(c), S8(c), S9(c), and S10(c),<sup>†</sup> the shear modulus ( $G$ ) displays two surfaces for both 2D and 3D representations. The green line shows the minimum values for a  $45^\circ$  angle, while the blue line shows the maximum values for the same angle. In the  $xy$  and  $yz$  planes,  $G$  is maximum along both axes, with the minimum value found at an angle of  $45^\circ$  between the axes. In the  $xy$  plane, it is seen to be isotropic. In Fig. 4(d), 5(d), S5(d), S6(d), S7(d), S8(d), S9(d), and S10(d),<sup>†</sup> a different anisotropic characteristic is seen for Poisson's ratio. Like  $G$ , there are two surfaces for both 2D and 3D representations, except Nb<sub>2</sub>GeC. The blue line indicates maximum values at a  $45^\circ$  angle, whereas the green line indicates minimum values at the same angle for all compounds except Nb<sub>2</sub>GeC. For Nb<sub>2</sub>GeC, the green line indicates positive values, where the values are maximum at an angle of  $45^\circ$ , and the red line indicates maximum negative values for the same angle. Poisson's ratio is also shown to be anisotropic, with the minimum values found within the vertical axes in the  $xz$  and  $yz$  planes. In contrast, the maximum values are found within the horizontal axes for both

compounds. In the  $xy$  plane, Poisson's ratio is found to be isotropic.

Other important anisotropic indices have also been calculated. Using the following relationships, the three shear anisotropic factors  $A_i$  ( $i = 1, 2,$  and  $3$ ) are computed:

$$A_1 = \frac{1}{6} \frac{(C_{11} + C_{12} + 2C_{33} - 4C_{13})}{C_{44}}, A_2 = \frac{2C_{44}}{C_{11} - C_{12}}, \text{ and } A_3 = A_1.$$

$$A_2 = \frac{1}{3} \frac{(C_{11} + C_{12} + 2C_{33} - 4C_{13})}{C_{11} - C_{12}},^{79} \text{ for the } \{100\}, \{011\}, \text{ and}$$

$\{001\}$ , respectively. Using the following relations, the elastic anisotropy for the bulk modulus ( $B_a$  and  $B_c$ ) across both the

$a$  and  $c$ -axes is computed:<sup>80</sup>  $B_a = a \frac{dp}{da} = \frac{A}{2 + \alpha}$  and

$B_c = c \frac{dp}{dc} = \frac{B_a}{\alpha}$ , where  $A = 2(C_{11} + C_{12}) + 4C_{13\alpha} + C_{33}\alpha^2$ , where

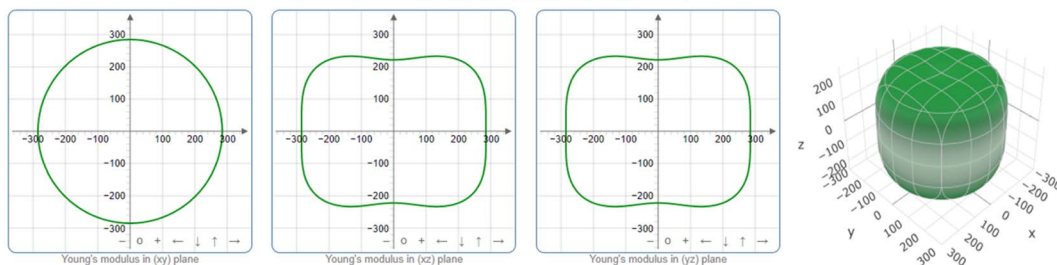
$$\alpha = \frac{(C_{11} + C_{12}) - 2C_{11}}{C_{33} + C_{13}}. \text{ Additionally, the elastic anisotropy for}$$

the ratio of the linear compressibility coefficients ( $k_c/k_a$ ) [ $k_a$  for  $a$  and  $k_c$  for  $c$ -directions] is computed using the following relation:<sup>81</sup>  $\frac{k_c}{k_a} = C_{11} + C_{12} - 2C_{13}/(C_{33} - C_{13})$ . Table 5 and S2<sup>†</sup> show

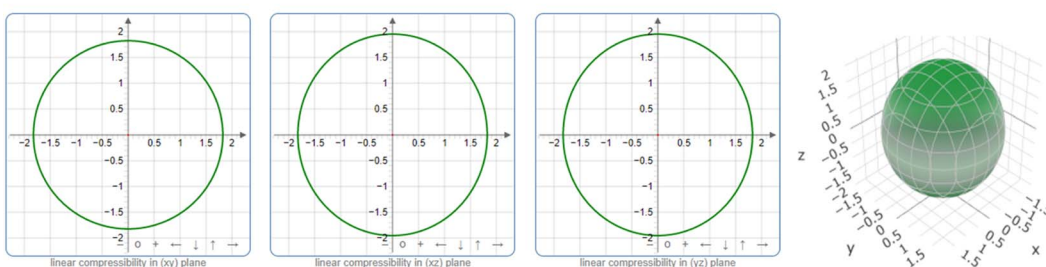
the value of the obtained anisotropy factors. The value of  $A_i = 1$  implies isotropy, otherwise anisotropic nature; thus, the Nb<sub>2</sub>AC ( $A = \text{Ga, Ge, Tl, Zn, P, In, Cd, and Al}$ ) compounds are anisotropic owing to their non-unit (1) value. The equality of  $k_c$  and  $k_a$ , and  $B_a$  and  $B_c$  also implies the isotropic nature. As evident, these parameters also suggest the anisotropic nature of the studied compounds. Furthermore, the percentage anisotropies of compressibility and shear modulus were computed as follows:<sup>82</sup>



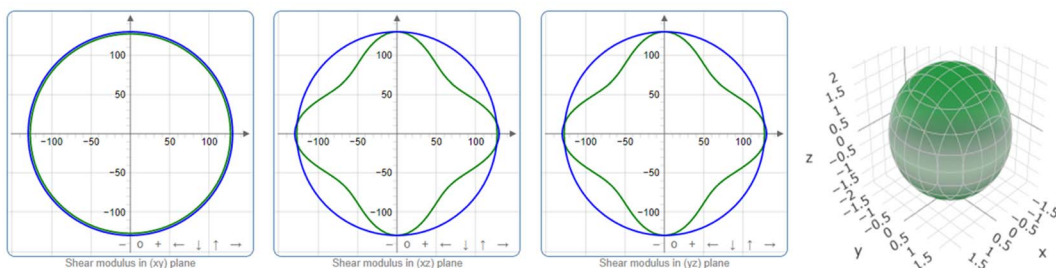
## (a) Young's modulus



## (b) Compressibility



## (c) Shear modulus



## (d) Poisson's ratio

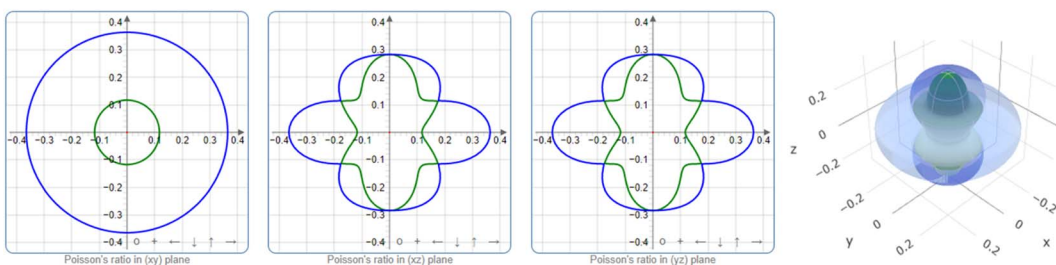


Fig. 4 The 2D and 3D plots of (a)  $Y$ , (b)  $K$ , (c)  $G$  and (d)  $\nu$  of  $\text{Nb}_2\text{GaC}$  for GGA PBEsol.

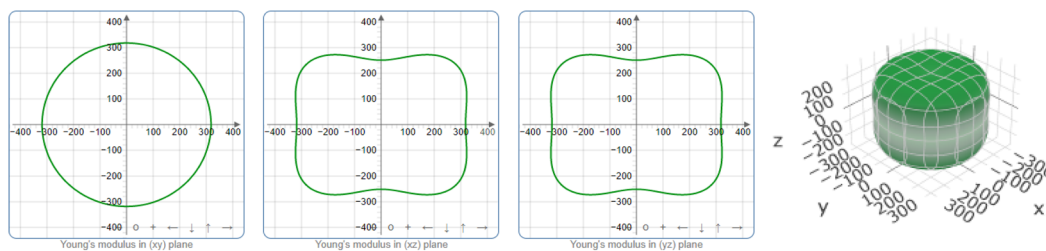
$A_B = \frac{B_V - B_R}{B_V + B_R} \times 100\%$  and  $A_G = \frac{G_V - G_R}{G_V + G_R} \times 100\%$ , also certifying the anisotropic nature.

Finally, we have calculated the universal anisotropy index  $A^U$  based on the Voigt,  $V$  (upper limit), and Reuss,  $R$  (lower limit), models using the following relation:<sup>83</sup>  $A^U = 5 \frac{G_V}{G_R} + \frac{B_V}{B_R} - 6 \geq 0$ .

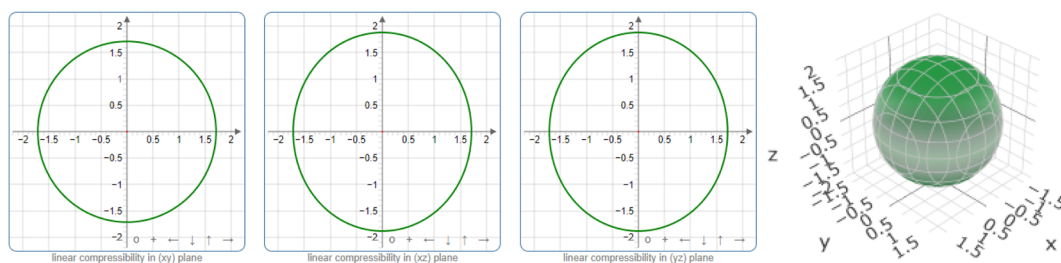
If the value of  $A^U$  is zero, it implies isotropic behavior, whereas a non-zero value reveals anisotropic behavior; the non-zero values of  $A^U$  reveal the anisotropic behavior of the studied compounds. In summary, we have found the anisotropic nature of  $\text{Nb}_2\text{AC}$  ( $A = \text{Ga, Ge, Tl, Zn, P, In, Cd, and Al}$ ) compounds.



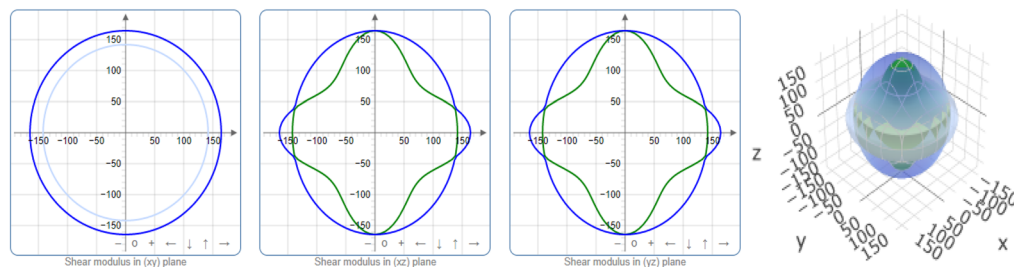
## (a) Young's modulus



## (b) Compressibility



## (c) Shear modulus



## (d) Poisson's ratio

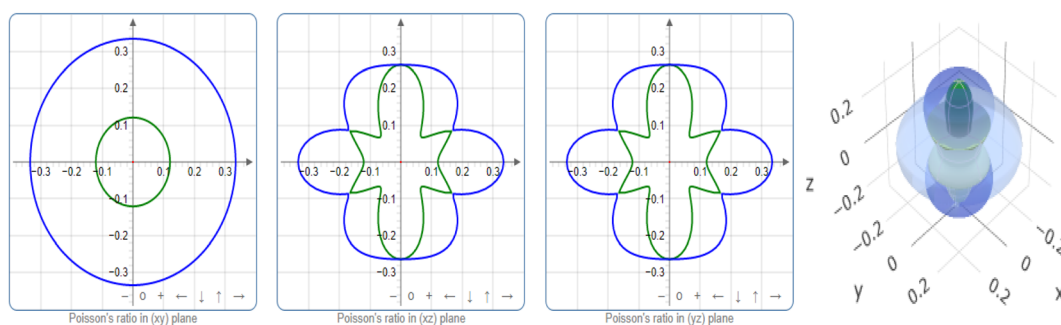


Fig. 5 The 2D and 3D plots of (a)  $Y$ , (b)  $K$ , (c)  $G$  and (d)  $\nu$  of  $\text{Nb}_2\text{AlC}$  for GGA PBEsol.

### 3.5 Optical properties

The MAX phase materials have already been identified as prospective candidates for use as a coating layer to lessen

solar heating.<sup>84</sup> They have also been used in other sectors, such as optical systems.<sup>84</sup> Therefore, it is also hoped that the studied carbides will also be appropriate for the above mentioned ones. We have computed a variety of optical



**Table 5** Anisotropy factors  $A_1$ ,  $A_2$ ,  $A_3$ ,  $k_c/k_a$ ,  $B_a$ , and  $B_c$ , percentage anisotropy factors  $A_G$  and  $A_B$  and universal anisotropic index  $A^u$ , calculated values using GGA PBESOL<sup>37 a</sup>

Phase	$A_1$	$A_2$	$A_3$	$B_a$	$B_c$	$K_c/k_a$	$A_B$	$A_G$	$A^u$	Ref.
Nb <sub>2</sub> GaC	0.658	1.041	0.685	491.61	1130.96	1.06	0.001	0.013	0.130	This
	*0.585	*1.024	*0.599	*505.19	*1483.25	0.93	*0.001	*0.022	*0.224	23
Nb <sub>2</sub> GeC	0.429	1.787	0.767	475.71	1792.77	0.90	0.003	0.057	0.607	This
	*0.358	*2.054	*0.734	*448.88	*1317.91	0.86	*0.004	*0.085	*0.932	23
	*0.359	*2.023	*0.723	*470.79	*2125.46	*0.76	*0.001	*0.084	*0.922	*25
Nb <sub>2</sub> TlC	0.839	0.972	0.816	420.78	1034.08	1.09	0.002	0.003	0.031	This
Nb <sub>2</sub> ZnC	0.579	1.439	0.833	468.84	869.98	1.82	0.012	0.027	0.296	This
Nb <sub>2</sub> PC	0.515	1.618	0.833	563.72	2019.99	0.69	0.004	0.038	0.407	This
	*0.529	*1.490	*0.789	*520.15	*2105.85	0.61	*0.007	*0.033	*0.358	*23
Nb <sub>2</sub> InC	0.830	0.911	0.756	448.67	951.08	1.05	0.006	0.005	0.051	This
	*0.705	*1.037	*0.731	*387.65	*1095.07	0.88	*0.005	*0.008	*0.095	25
Nb <sub>2</sub> CdC	0.960	1.119	1.074	437.09	782.85	1.29	0.003	0.002	0.023	This
Nb <sub>2</sub> AlC	0.614	1.155	0.709	487.51	986.40	1.09	0.003	0.016	0.165	This
	0.656	1.074	0.704	*438.87	*1042.45	0.95	0.006	0.012	0.129	23

<sup>a</sup> \*Calculated values using reported data.

constants in an approach to reveal the optical response of these carbides when electromagnetic radiation is incident upon them.

To estimate the optical properties, it is essential to use the equation  $\varepsilon(\omega) = \varepsilon_1(\omega) + i\varepsilon_2(\omega)$ . Based on the electronic states of each momentum matrix element's occupied and unoccupied states, it is possible to state that  $\varepsilon_2(\omega)$  is the imaginary portion of the related dielectric function and fully calculated by CASTEP using the formula below:

$$\varepsilon_2(\omega) = \frac{2e^2\pi}{\Omega\varepsilon_0} \sum_{k,v,c} |\psi_k^c| \langle u \cdot r | \psi_k^v \rangle|^2 \delta(E_k^c - E_k^v - E)$$

where the vector  $u$  designates how the incident electric field is polarized,  $\omega$  represents the frequency of light,  $e$  stands for the electronic charge,  $\psi_k^c$  represents the conduction band wave function and  $\psi_k^v$  indicates the valence band wave function. By using the Kramers-Kronig transform, the real part ( $\varepsilon_1$ ) is obtained from the imaginary part  $\varepsilon_2(\omega)$ . The refractive index ( $n$ ), extinction coefficient ( $k$ ), absorption coefficient ( $\alpha$ ), reflectivity ( $R$ ), photoconductivity ( $\sigma$ ) and loss function (LF) were calculated by the following equations:<sup>85-87</sup>

$$n(\omega) = \frac{1}{\sqrt{2}} \left[ \sqrt{\{\varepsilon_1(\omega)\}^2 + \{\varepsilon_2(\omega)\}^2} + \varepsilon_1(\omega) \right]^{1/2}$$

$$k(\omega) = \frac{1}{\sqrt{2}} \left[ \sqrt{\{\varepsilon_1(\omega)\}^2 + \{\varepsilon_2(\omega)\}^2} - \varepsilon_1(\omega) \right]^{1/2}$$

$$R(\omega) = \frac{(n-1)^2 + k^2}{(n+1)^2 + k^2}$$

$$\alpha(\omega) = \frac{2k\omega}{c}$$

$$L(\omega) = \text{Im} \left( \frac{-1}{\varepsilon(\omega)} \right) = \varepsilon_2(\omega) / [\{\varepsilon_1(\omega)\}^2 + \{\varepsilon_2(\omega)\}^2]$$

$$\sigma(\omega) = \sigma_1(\omega) + i\sigma_2(\omega) = -i \frac{\omega}{4\pi} [\varepsilon(\omega) - 1]$$

A Drude correction must be made for the study of the dielectric function of metallic materials, which is usually done by adding the plasma frequency and a broadening factor during first-principles calculations.<sup>88,89</sup> Because of the metallic nature of the studied carbides, a damping of 0.05 eV and plasma frequency of 3 eV were used to enhance the computed spectra lower energy side. Moreover, a Gaussian smearing value of 0.5 eV was also used to smear out the  $k$ -points around the Fermi level. The calculated optical constants of the titled phases are presented in Fig. 6, along with those of Nb<sub>2</sub>AlC for comparison. The real part  $\varepsilon_2(\omega)$  of the dielectric function, where the low energy peaks are attributed to electron intra-band transitions,<sup>90</sup> is shown in Fig. 6(a). Because of the electron intra-band transitions, the assigned value for each peak is less than 1 eV. The materials exhibit Drude-like behavior, as indicated by the massive negative values of  $\varepsilon_1(\omega)$ , whereas inter-band transitions occur at higher energies. Fig. 6(b) shows the imaginary part of the dielectric function  $\varepsilon_2(\omega)$ . At around 16 eV, it has been seen that the values of  $\varepsilon_2(\omega)$  pass through zero from above. This is another example of the compound's metallic nature. A similar nature of the real and imaginary parts of the dielectric function was reported for the most studied MAX phase Ti<sub>3</sub>SiC<sub>2</sub> (ref. 84) and widely used 211 MAX phase Ti<sub>2</sub>AlC.<sup>91</sup> The refractive index,  $n(\omega)$ , of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) is depicted in Fig. 6(c). This significant optical constant contributes to the design of optical systems like photonic crystals and wave guides. As shown in Fig. 6(c), the static value of  $n(0)$  for Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) is 7.0, 8.9, 9.4, 11, 8.3, 10.9, 9.5 and 8.9, respectively. Fig. 6(d) shows the extinction coefficient,  $k(\omega)$ , for the Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al)



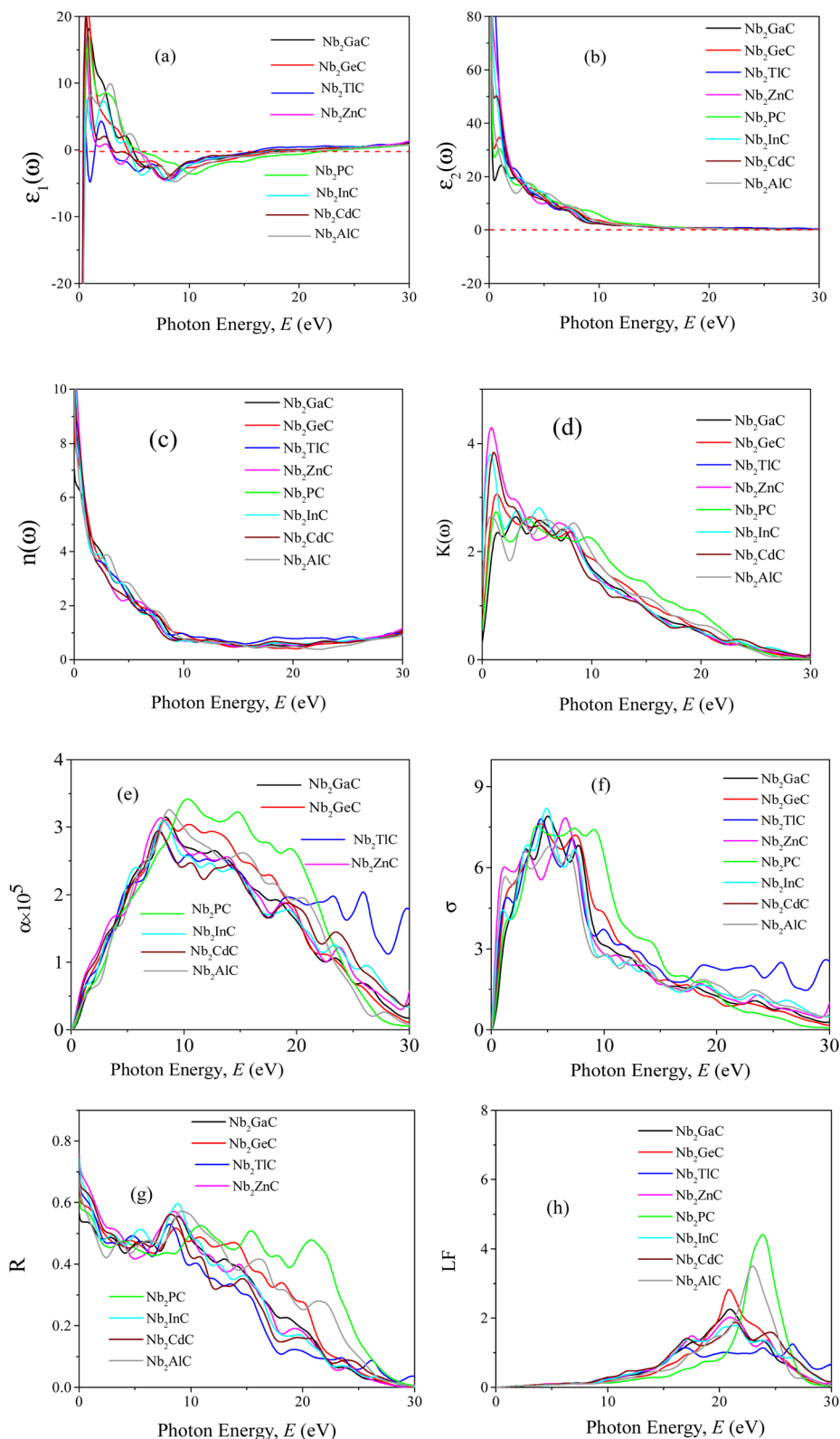


Fig. 6 (a) Real part ( $\epsilon_1$ ) and (b) imaginary part ( $\epsilon_2$ ) of dielectric function ( $\epsilon$ ), (c) refractive index ( $n$ ), (d) extinction coefficient ( $k$ ), (e) absorption coefficient ( $\alpha$ ), (f) photoconductivity ( $\sigma$ ), (g) reflectivity ( $R$ ), and (h) loss function (LF) of Nb<sub>2</sub>AC (A = Ga, Ge, Ti, Zn, P, In, Cd, and Al) MAX phases as a function of photon energy calculated using GGA PBEsol.



MAX phases. The extinction coefficient,  $k(\omega)$ , is used for measuring the loss of electromagnetic radiation due to absorption and is found to vary similarly to  $\varepsilon_2(\omega)$ , like other MAX phases.<sup>89,90</sup> In Fig. 6(e), the absorption coefficient of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) MAX phases is illustrated, where the spectra are shown to increase from zero photon energy due to the metallic behavior of the researched compounds. The spectra are seen to increase as incident energy increases. It showed the strongest absorption region in the spectral range of 7–10 eV; it decreases with a further increase in photon energy. Because of the high absorption coefficients in the high energy range (7–10 eV), Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) MAX phases can be considered potential absorbing materials in this energy range. The photoconductivity of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) is shown in Fig. 6(f), which is also found to start at the beginning from zero photon energy because of the metallic behavior of the selected phases. The band structure and electronic DOS results are well consistent with the absorption coefficient and photoconductivity results.

MAX phases are used as coating materials to reduce solar heating, which is one of their most significant applications. The reflectivity of the target materials has been investigated to disclose this possibility, shown in Fig. 6(g). It was reported by Li *et al.*<sup>84,92</sup> that if a MAX compound has a reflectivity of 44% in the visible range, it will be able to reduce solar heating. The reflectivity spectrum for Nb<sub>2</sub>GaC begins with a value of 0.569 (56.9%), the minimum value among the studied phases. Nb<sub>2</sub>TiC has the highest value, which is 0.982 (98.2%). For Ti<sub>3</sub>SiC<sub>2</sub>, the spectrum has an initial value of  $\sim 0.75$  (75%), going down at around 1 eV, and then remaining almost constant up to 6 eV, whereas for Nb<sub>2</sub>AlC, it starts with an initial value of 0.68 (68%), which is down to below 44% at around 2.1 eV. Though Nb<sub>2</sub>AC (A = Ga, Ge, and P) has a lower initial value of  $R$  than Nb<sub>2</sub>AlC, neither of their spectra are down to less than 44% up to the visible light range. However, each spectrum of the titled compounds exhibits average higher values (also higher than 44% up to the visible light range) than that of Nb<sub>2</sub>AlC. Thus, in comparison with Ti<sub>3</sub>SiC<sub>2</sub> and Nb<sub>2</sub>AlC, it can be concluded that Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd) compounds are candidates for use as cover materials to lessen solar heating. In the energy range of 5.5 to 11 eV, there are a few sharp peaks in the reflectivity spectra, and around 30 eV, reflectivity finally approaches zero.

When electrons move through materials, they lose their energy. An optical constant called the loss function is used to evaluate this type of energy loss. Fig. 6(h) displays the calculated loss functions for the aforementioned MAX phase compounds. The loss function's peak frequency is referred to as the plasma frequency ( $\omega_p$ ), which is observed at 20.89, 20.92, 16.38, 17.50, 23.91, 20.54, 17.21 and 23.11 for Nb<sub>2</sub>GaC, Nb<sub>2</sub>GeC, Nb<sub>2</sub>TiC, Nb<sub>2</sub>ZnC, Nb<sub>2</sub>PC, Nb<sub>2</sub>InC, Nb<sub>2</sub>CdC, and Nb<sub>2</sub>AlC, respectively. In a loss function, this energy is determined by its characteristic frequency when  $\varepsilon_1(\omega)$  and  $\varepsilon_2(\omega)$  both pass through zero from below and above, respectively. Reflectivity also identifies the falling edges. This is the critical value that is established by the plasma frequency when the materials are transformed into transparent dielectrics from the metallic system. We have also

calculated the optical constant using GGA PBE, but not been shown due to their similar nature.

### 3.6 Thermal properties

MAX phases are excellent candidates for applications at high-temperature because of their excellent mechanical properties at high temperatures. Therefore, the study of the basic parameters required to predict their application carries significant interest. The Debye temperature ( $\Theta_D$ ), minimum thermal conductivity ( $K_{\min}$ ), Grüneisen parameter ( $\gamma$ ), melting temperature ( $T_m$ ), *etc.* of the researched compounds have been calculated for predicting their high temperature applications.

The Debye temperature ( $\Theta_D$ ), one of the key characteristic parameters of solids, is closely related to the material's bonding strength, melting temperature, thermal expansion, thermal conductivity, *etc.* The  $\Theta_D$  of studied phases has been calculated using sound velocity following Anderson's method.<sup>93</sup> The relevant formulae are as follows:

$$\Theta_D = \frac{h}{k_B} \left[ \left( \frac{3n}{4\pi} \right) N_A \rho / M \right]^{1/3} v_m;$$

where  $M$  is the molar mass;  $n$  is the number of atoms in the molecules;  $\rho$  is the mass density;  $h$  is Planck's constant;  $k_B$  is the Boltzmann constant;  $N_A$  is Avogadro's number; and  $v_m$  is the average sound velocity. In an isotropic material, the  $v_m$  can be computed from the longitudinal sound velocities ( $v_l$ ) and transverse sound velocities ( $v_t$ ) using the given relationship:

$$v_m = \left[ \frac{1}{3} \left( \frac{1}{v_l^3} + \frac{1}{v_t^3} \right) \right]^{-1/3}; v_l \text{ and } v_t \text{ can be obtained from their relationships with the polycrystalline bulk modulus } (B) \text{ and shear modulus } (G): v_l = [(3B + 4G)/3\rho]^{1/2} \text{ and } v_t = [G/\rho]^{1/2}. \text{ The calculated } \Theta_D \text{ of Nb}_2\text{AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) is presented in Table 6 for GGA PBEsol and Table S3† for GGA PBE.}$$

As shown in Table 6,  $\Theta_D$  is highest for Nb<sub>2</sub>PC and lowest for Nb<sub>2</sub>TiC. The ranking of the compounds roughly followed the hardness-based ranking, which fairly agrees with the hardness and Debye temperature relationship.<sup>95</sup> The  $\Theta_D$  of the titled compounds is lower than that of Nb<sub>2</sub>AlC, except Nb<sub>2</sub>PC. Recently, Hadi *et al.*<sup>96</sup> reported a MAX (V<sub>2</sub>SnC) phase as a TBC material with a  $\Theta_D$  value of 472 K. Among the studied compounds, a much lower  $\Theta_D$  is found for only Nb<sub>2</sub>TiC (372 K) and Nb<sub>2</sub>CdC (424 K); others have  $\Theta_D$  either comparable to or higher than that of V<sub>2</sub>SnC. In addition, the  $\Theta_D$  of Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub>, a well-known TBC material, is 564 K.<sup>97</sup> Thus,  $\Theta_D$  values of Nb<sub>2</sub>AC (A = P, Al, Ga, and Ge) phases [Table 6] are comparable with that of Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub>.<sup>97</sup>

The minimum thermal conductivity ( $K_{\min}$ ) is defined as the constant value of thermal conductivity at high temperature. As its name suggests, this conductivity is minimum owing to the breaking of the pairing of phonons at high temperature. Calculation of minimum thermal conductivity is essential for predicting the use of solids at high temperature. It has already been established that the MAX phases are suitable for use in high temperature technology as a coating layer (TBC). Thus, calculation of  $K_{\min}$  is also required for the titled phases. We



**Table 6** Calculated density ( $\rho$ ), longitudinal, transverse and average sound velocities ( $v_l$ ,  $v_t$ , and  $v_m$ , respectively), Debye temperature ( $\Theta_D$ ), minimum thermal conductivity ( $K_{\min}$ ) and Grüneisen parameter ( $\gamma$ ) of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al)<sup>a</sup>

Phases	$\rho$ (g cm <sup>-3</sup> )	$v_l$ (m s <sup>-1</sup> )	$v_t$ (m s <sup>-1</sup> )	$v_m$ (m s <sup>-1</sup> )	$\Theta_D$ (K)	$K_{\min}$ (W mK <sup>-1</sup> )	$\Gamma$	$T_m$ (K)	Ref.
Nb <sub>2</sub> GaC	7.59	6931	4106	4547	548	1.05	1.41	1913	This
Nb <sub>2</sub> GeC	7.76	6596	3607	4022	485	0.93	1.71	1715	This
		6632	3695	4114	508	*0.95	*1.66	*1737	25
Nb <sub>2</sub> TlC	10.18	5244	2872	3202	372	0.68	1.71	1590	This
Nb <sub>2</sub> ZnC	7.43	6248	3440	3834	461	0.88	1.66	1574	This
Nb <sub>2</sub> PC	8.28	7337	4297	4764	640	1.29	1.45	2171	This
Nb <sub>2</sub> InC	11.49	5311	3121	3459	483	0.95	1.41	1790	This
Nb <sub>2</sub> CdC	8.06	5855	3247	3616	424	0.79	1.65	1587	This
Nb <sub>2</sub> AlC	6.34	7315	4405	4871	592	1.46	*1.37	1800	94

<sup>a</sup> Calculated values using GGA PBESOL<sup>37</sup> and \*calculated values using reported data.

have calculated the  $K_{\min}$  of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) compounds using the following equation:<sup>98</sup>

$$K_{\min} = k_B v_m \left( \frac{M}{n \rho N_A} \right)^{-2/3}, \text{ where } k_B \text{ is the Boltzmann constant,}$$

$v_m$  is the average phonon velocity,  $N_A$  is Avogadro's number, and  $\rho$  is the crystal's density, respectively, as listed in Table 6. The order of the  $K_{\min}$  value is expected to be as follows: Nb<sub>2</sub>AlC > Nb<sub>2</sub>PC > Nb<sub>2</sub>GaC > Nb<sub>2</sub>InC > Nb<sub>2</sub>GeC > Nb<sub>2</sub>ZnC > Nb<sub>2</sub>CdC > Nb<sub>2</sub>TlC; that is, the  $K_{\min}$  values of the studied compounds are lower than that of Nb<sub>2</sub>AlC, indicating more suitability of the phases as the smaller the  $K_{\min}$  is, the more suitable as TBC materials. It should be noted that the  $K_{\min}$  of V<sub>2</sub>SnC is 1.20 Wm<sup>-1</sup> K<sup>-1</sup> and Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub> is 1.13 Wm<sup>-1</sup> K<sup>-1</sup>.<sup>96,98</sup> Thus, it is expected that the  $K_{\min}$  value suggests the studied compounds as suitable TBC materials.

An essential thermal parameter that helps to explain the anharmonic effects of lattice dynamics is the Grüneisen parameter ( $\gamma$ ); lower anharmonic effects are expected for the solids used at high temperature. Therefore, we have calculated  $\gamma$  of Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, Cd, and Al) compounds using the following equation:<sup>99</sup>  $\gamma = \frac{3(1+\nu)}{2(2-3\nu)}$ . According to

Table 6, the obtained values of  $\gamma$  are lying in between 0.85 and 3.53, which is in line with what is predicted for the polycrystalline materials with  $\nu$  values in the range of 0.05–0.46.<sup>100</sup> Besides, the low values of  $\gamma$  confirm the lower anharmonic effects in the selected compounds, like other MAX phase materials.<sup>99</sup>

Finally, we have calculated the melting temperature ( $T_m$ ) of the studied compounds using the following equation:

$$T_m = 354 + \frac{4.5(C_{11} + C_{33})}{3},^{101} \text{ and listed it in Table 6. The}$$

melting temperature of the solids mainly depends on atomic bonding strength; the stronger the atomic bonding, the higher the  $T_m$ . Thus, a close relationship between  $T_m$  and  $Y$  is expected,<sup>94,97</sup> and the order of  $T_m$  for the titled phases is found to be following the  $Y$ -based ranking of the phases. It is seen from Table 6 that  $T_m$  of Nb<sub>2</sub>AC (A = Ge, Tl, Zn, In, and Cd) is lower than that of the Nb<sub>2</sub>AlC, but still higher than that of the V<sub>2</sub>SnC (1533 K) MAX phase, a known TBC material.<sup>96</sup> In addition, the  $T_m$  of Nb<sub>2</sub>AC (A = Ga and P) is not only higher

than that of Nb<sub>2</sub>AlC<sup>94</sup> but also comparable to that of Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub> (2000 K).  $T_m$  values of Nb<sub>2</sub>AC (A = Ge, Tl, Zn, In, and Cd) are lower than that of Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub> (2000 K) but still reasonably high. Thus, based on the values of  $\Theta_D$ ,  $k_{\min}$ , and  $T_m$  of the studied phases, in comparison with those of Y<sub>4</sub>Al<sub>2</sub>O<sub>9</sub> and some other MAX phases that have already been reported as TBC materials, we conclude that the titled phases can be considered as potential TBC materials.

## 4 Conclusion

A DFT investigation of 211 Nb<sub>2</sub>AC (A = Ga, Ge, Tl, Zn, P, In, and Cd) carbides has been carried out in this research. The studied phases are dynamically and mechanically stable. Among the studied phases, Nb<sub>2</sub>PC exhibits the best combination of mechanical properties, while Nb<sub>2</sub>TlC exhibits the lowest. The Nb<sub>2</sub>GaC, Nb<sub>2</sub>PC, and Nb<sub>2</sub>InC are brittle, whereas Nb<sub>2</sub>GeC, Nb<sub>2</sub>TlC, Nb<sub>2</sub>ZnC, and Nb<sub>2</sub>CdC are ductile. The Vickers hardness of Nb<sub>2</sub>PC is also higher than that of others considered here, while the lowest Vickers hardness is found for Nb<sub>2</sub>TlC, in good agreement with elastic moduli. The calculated direction-dependent (2D and 3D) elastic moduli and anisotropic indices confirm the anisotropic character of the studied phases. The electronic band structure and DOS confirm the metallic nature with a dominating contribution from Nb-3d states. Partial DOS discloses strong hybridization between Nb-d and C-2p states. Mulliken's population analysis reveals the existence of both ionic bonds and covalent bonds within the studied compounds. The optical constants, such as real and imaginary parts of the dielectric function, absorption coefficient, and photoconductivity spectra, are in good accord with band structure results. The reflectivity spectra reveal the possibility of their use as coating materials to diminish solar heating. The obtained values of the Grüneisen parameter ( $\gamma$ ) show a lower anharmonic effect within the title carbides. The low value of  $K_{\min}$  and comparatively higher melting temperature with reasonable Debye temperature suggest the studied compounds as TBC materials. The results found in this study are encouraging and hoped to attract attention from the scientific community for further investigation of new MAX phase materials.



## Conflicts of interest

There are no conflicts to declare.

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