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Two-step leaching of spent lithium-ion batteries and effective regeneration of critical metals and graphitic carbon employing hexuronic acid†

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Recovering precious metal ions like Co, Li, Mn, and Ni from discarded lithium-ion batteries (LIBs) has significant environmental and economic benefits. Also, graphite will be in high demand in the coming years due to the development of LIBs for use in electric vehicles (EVs) and the need for it for electrodes in a variety of energy storage devices. However, it has been overlooked during the recycling of used LIBs, which resulted in resource waste and environmental pollution. In this work, a comprehensive and environmentally friendly approach for recycling critical metals as well as graphitic carbon from discarded LIBs was proposed. To optimize the leaching process, various leaching parameters were investigated by employing hexuronic acid or ascorbic acid. The feed sample was analyzed using XRD, SEM-EDS, and a Laser Scattering Particle Size Distribution Analyzer to determine the phases, morphology, and particle size. 100% of Li and 99.5% of Co were leached at the optimum conditions of 0.8 mol L⁻¹ of ascorbic acid, a particle size of ~25 μm, 70 °C, 60 min of leaching time, and 50 g L⁻¹ of S/L ratio. A detailed study of the leaching kinetics was carried out. The leaching process was found to be well-fitted with the surface chemical reaction model based on the findings of temperature, acid concentration, and particle size variations. To obtain pure graphitic carbon after the initial leaching, the leached residue was subjected to further leaching with various acids (HCl, H₂SO₄, and HNO₃). The Raman spectra, XRD, TGA, and SEM-EDS analysis of the leached residues following the two-step leaching process were examined to exemplify the quality of the graphitic carbon.

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1 Introduction

Lithium-ion batteries (LIBs), which have the distinctive qualities of higher specific energy density, higher charging capacity, and exceptional cycle longevity, are extensively used in electric vehicles, computers, laptops, smartphones, video cameras, solar energy storage devices, and many electronic gadgets.¹ The need for LIBs has significantly increased, particularly with the meteoric rise of electric and hybrid vehicles.² Sales of lithium-ion batteries for electric vehicles are expected to rise from 7 million in 2020 to 180 million in 2045.³ Although LIBs have many useful advantages, one drawback is that they generally have a lifespan of fewer than 1000 cycles.⁴ As LIBs have a limited lifespan, the dramatic increase in LIB consumption may suggest that there will be a huge amount of waste in the form of spent LIBs in the coming decades.⁵ The total number of spent

LIBs worldwide is predicted to exceed 11 million tonnes by 2030.⁶ Concerns about the environment, human health, and safety have been raised by the disposal of used LIBs and the little efforts made to recycle them. In addition, non-recycled LIB parts provide pollution issues owing to the possibility of toxic leaks that must damage soils and eventually water systems.⁷ So, the advancement of efficient and affordable methods to recycle and transform LIB components are essential for reducing harmful emissions to the environment and the excess use of precious natural resources.

Due to the high recycling values, there is currently a strong emphasis on collecting scarce and precious energy materials from spent LIBs.^{8,9} The recovery of such valuable metals (Li, Co, Mn, Ni, *etc.*) from discarded LIBs has been summarized in numerous publications.^{10–13} Graphitic carbon recycling, on the other hand, has received little attention in the past due to its abundance and lower economic value.¹⁴ Graphitic carbon is typically obtained during the recycling of spent LIBs as a residual scrap and by-product, both of which are not effectively recycled. Graphite is indeed present in LIBs in amounts ranging from 12 to 21 wt%.^{15,16} Without a doubt, the rise in spent LIBs results in the generation of a significant amount of spent graphite. Additionally, the cost of battery graphite, which makes up about 8% to 13% of the overall cost of the battery, is

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between \$8000 and \$13 000 per ton.¹⁷ Due to an unanticipated surge in EV sales over the past few years, the worldwide graphite sector has seen constantly rising demand and limited supply. The market for graphite was estimated to be worth USD 14.3 billion in 2019 and is expected to grow to USD 21.6 billion by 2027, based on a recent analysis by Allied Market Research.¹⁸ If used graphite is not properly recycled, resources will be wasted and environmental pollution will be increased. Therefore, for the preservation of resources and the protection of the environment, effective recycling of spent graphite is crucial.¹⁹

Various techniques have been utilized to develop LIB recycling, however, hydrometallurgy is frequently employed in industrial sectors as a cost-effective and environmentally sustainable method to extract valuable metals from spent LIBs due to its higher efficiency and lower harmful gas emissions.^{20–22} Several investigations have been conducted on the leaching of critical metals using both inorganic acids (such as HCl,²³ HNO₃,²⁴ H₂SO₄,^{25,26} and H₃PO₄²⁷) and organic acids (such as citric acid,^{28,29} malic acid,^{30,31} lactic acid,³² ascorbic acid,³³ oxalic acid,³⁴ and succinic acid³⁵). Compared to inorganic acids, organic acids are almost natural and sustainable. Employing organic acids as efficient leaching agents that are also safe for the environment, allowing for the selective leaching of certain metals whilst delaying equipment corrosion and preventing secondary emissions.³⁶ Furthermore, organic acids are biodegradable, don't often emit toxic gases, and the leaching-related trash would be easy to treat.³⁷ Musariri *et al.* reported that employing 1.5 mol L⁻¹ citric acid with 2% H₂O₂ as reductant at 95 °C, 97% of Li and 95% of Co were leached.³⁸ Succinic acid was utilized as a leaching agent and H₂O₂ as a reductant by Li *et al.* to leach metal values from waste calcined LiCoO₂ battery samples. The results showed that with 1.5 mol L⁻¹ succinic acid and 4% H₂O₂, nearly 96% of Li and 100% of Co were leached.³⁵ Another report used citric acid and H₂O₂ to dissolve the NCM-type battery sample, and the results showed that Li, Co, Ni, and Mn leached out at rates of 96%, 87%, 93%, and 90.5%, respectively.³⁹ A detailed survey of the literature revealed that H₂O₂ is the most efficient reductant for the leaching of Li and Co,^{40–42} whereas the leaching of both Li and Co is ineffective without the presence of a reducing agent.⁴³ To avoid the increasing cost of the leaching process by the addition of H₂O₂, it is essential to select a lixiviant that has dual capacity *i.e.*, leachant and reductant. Ascorbic acid can be a candidate for this purpose because of its capacity to reduce metal ions from higher oxidation states to lower oxidation states. Li *et al.*⁴⁴ reported the recycling of Co and Li from the cathode materials using ultrasonic washing followed by calcination and then leaching with ascorbic acid. Using 1.25 mol L⁻¹ ascorbic acid at 70 °C temperature, pulp density of 25 g L⁻¹, 98.5% Li and 94.8% Co were leached. In another study, a closed vessel microwave leaching was reported using ascorbic acid for the recovery of Co, Mn, and Li from spent LIB cathode powder.⁴⁵ The reduction property of ascorbic acid was studied using XPS studies. Oxalates of Co and Mn were precipitated using oxalic acid. Although the optimal leaching efficiency was achieved at a higher temperature (125 °C), it was not a favorable condition from an environmental perspective. For the recovery of

graphitic carbon majority of investigations were carried out after removing the cathode and anode from the spent LIBs. Da *et al.*⁴⁶ demonstrated a feasible method for recycling spent graphite (SG) anode. In order to obtain pure SG, residual insoluble impurities including Al and Fe-based compounds were successfully removed through alkali roasting at a higher temperature. Yuwen *et al.*⁴⁷ reported that the separation of graphite and Cu foil under microwave irradiation is about 100% due to the LIBs anode's strong microwave absorption capability. The recovery of Li is then accomplished through water leaching and subsequent heating. Markey *et al.*⁴⁸ showed the effectiveness of an upcycling technique that directly regenerates spent graphite anodes while also incorporating healing and doping. In particular, employing a boric acid pretreatment and a brief annealing step, their regeneration technique not only corrected the compositional and structural defects of degraded graphite but also functionally doped the surface of the graphite particles, resulting in high electrochemical activity and outstanding cycling stability. But, there haven't been any studies on simultaneously separating graphitic carbon and precious metal values from the used LIB sample using a leaching-based method. Using ascorbic acid as the lixiviant, limited research studies have been reported for spent LiCoO₂ batteries. However, the detailed leaching kinetics of the leaching process and the recycling of both critical metals and graphitic carbon from spent LiCoO₂ in a single approach were not explored. Because of the higher acid content and lower S/L ratio of the previous studies, the findings need to be reconsidered to enhance the leaching efficiency with minimum acid consumption with a higher S/L ratio. In this work, the most effective ascorbic acid was chosen from different organic acid leaching studies for further investigations followed by two-step leaching to recover graphitic carbon along with Co and Li. All leaching parameters, variations in acid concentration, leaching time, temperature, and solid to liquid ratio (S/L) were studied. The rate of reaction and the mechanism behind the leaching process were both determined by analyzing the leaching kinetics. Following the initial leaching process, the leached residue was subjected to further acid leaching to obtain pure graphitic carbon. The effect of various acids on the regeneration of pure graphitic carbon was also investigated.

2 Experimental methods

2.1 Reagents and materials

The spent LIB sample was collected from an authorized supplier of waste materials. Ascorbic acid (C₆H₈O₆) was purchased from Merck life science Pvt. with a purity of ≥ 99%. Similarly, HCl (36% purity), H₂SO₄ (98% purity), HNO₃ (69% purity), and all other reagents were purchased from Merck of analytical grade. All solutions were prepared with Millipore water.

2.2 Analytical method

The total metal content of the spent LIB sample was analyzed using ICP-OES (inductively coupled plasma optical emission spectrometry) of PerkinElmer make after treatment with a 3 : 1



Table 1 Different metal contents in the cathode

Metals	Li	Co	Cu	Al
Concentration, g L ⁻¹	0.39	3.412	0.031	0.027

solution of hydrochloric and nitric acid (aqua regia) (Table 1). In the digestion process, 1 g sample was mixed with 40 mL of aqua regia, heated to boiling, and then stirred for one hour. The cooled sample was filtered into a 100 mL volumetric flask and the final volume was made up to 100 mL. Before and after leaching, the solid samples were investigated using X-ray diffraction (XRD, Rigaku Ultima IV), scanning electron microscopy, and energy-dispersive X-ray spectroscopy (SEM-EDS, EVO-18, Carl Zeiss). Raman spectra of the leached residues were analyzed using Renishaw's inVia Raman Microscope. The thermogravimetric analysis (TGA) and differential thermal analysis (DTA) were carried out using a Hitachi thermogravimetric analyzer (Hitachi STA 7200) at a heating rate of 25 °C min⁻¹ with a temperature range of 30 °C to 900 °C.

2.3 Leaching process

A 500 mL three-necked flat-bottomed flask with a magnetic stirrer, a temperature sensor, and a vapor condenser was used to leach the waste LIB sample. A certain amount of LIB sample was exactly weighed, and ascorbic acid solutions of varying concentrations were made as leaching reagents. Solid-liquid separation was carried out through filtration. The metal ions present in the leach liquor were examined using ICP-OES. The leaching efficiency for different metals was evaluated using eqn (1). The experimental conditions for different leaching parameters using ascorbic acid were addressed in Table 2. The second step leaching was carried out with the leached residues of ascorbic acid.

$$\text{Leaching efficiency (\% L)} = \frac{\text{Metal concentration in the leach liquor}}{\text{Total metal content in aqua regia}} \times 100 \quad (1)$$

3 Results and discussion

3.1 Characterization of the LIB sample

The waste LIB sample was characterized using XRD analysis with a Cu K α radiation source ($\lambda = 1.5406 \text{ \AA}$). The LIB sample

was scanned at 25 °C in the 2θ range from 10° to 80°. The diffraction patterns were compared to the reference data (LiCoO₂ = 01-070-2685 and C = 00-008-0415) in the JCPDS database. The presence of Li and Co in the form of LiCoO₂ was confirmed by XRD analysis (Fig. 1a). Additionally, the same feed sample was analyzed using SEM and EDS analysis at various magnifications, and the SEM images showed the presence of LiCoO₂ particles with irregular shape and a wider particle size distribution (Fig. 1b). The presence of cobalt, carbon, and oxygen was also confirmed by elemental analysis. But lithium was not detected by EDS elemental analysis due to its light-weight, and light elements emit an auger electron rather than a proton most of the time, which is another reason. Because of the low weight% (<0.4%), the presence of Al and Cu can be neglected. The particle size distribution of the spent LIB sample has been analyzed with Laser Scattering Particle Size Distribution Analyzer LA-960, HORIBA (Fig. 1c). With $D_{10} = 10.5 \text{ }\mu\text{m}$ and $D_{50} = 18.3 \text{ }\mu\text{m}$, the average particle size was found to be 16.2 μm .

3.2 Leaching of waste LIB sample

3.2.1 Effect of different organic acids. Different organic acids *i.e.*, lactic acid, tartaric acid, ascorbic acid, formic acid, and citric acid were used to study the leaching efficiencies of Li and Co from the waste LIB sample. The structures and possible dissociations of all acids are presented in Table 3.^{49–52} The acids with more dissociation forms, such as citric acid, tartaric acid, and ascorbic acid, should be more efficient at enhancing the leaching efficiency of metals. But, it was revealed after a thorough review of the literature that citric acid and tartaric acid are ineffective for the leaching of metal ions from spent LIB samples without the addition of any reducing agent.^{38,39,41,53–55} But, ascorbic acid deprotonates on one of the hydroxyls to create the ascorbate anion, which is a vinylogous carboxylic acid. The ascorbic acid's hydroxyl groups are much more acidic

than those of other hydroxyl compounds (pK_a values = 4.1 and 11.6) due to the two main resonance structures that stabilize the ascorbate anion. Ascorbic acid undergoes oxidation with the loss of two electrons, resulting in the production of dehydroascorbic acid (C₆H₆O₆), which acts as a reducing agent that

Table 2 Experimental conditions for different leaching parameters

Figures	Ascorbic acid concentration (mol L ⁻¹)	Leaching time (min)	Temperature (°C)	Particle size (μm)	Solid to liquid ratio (g L ⁻¹)
Fig. 4	0.05, 0.1, 0.3, 0.5, 0.8, 1.0	60	30	–25	10
Fig. 5	0.8	5, 15, 30, 45, 60, 90	30	–25	10
Fig. 6	0.8	60	30, 40, 50, 60, 70	–25	10
Fig. 7	0.8	60	70	–25, 25, 45, 75, 100	10
Fig. 8	0.8	60	70	–25	10, 20, 30, 40, 50, 60, 70



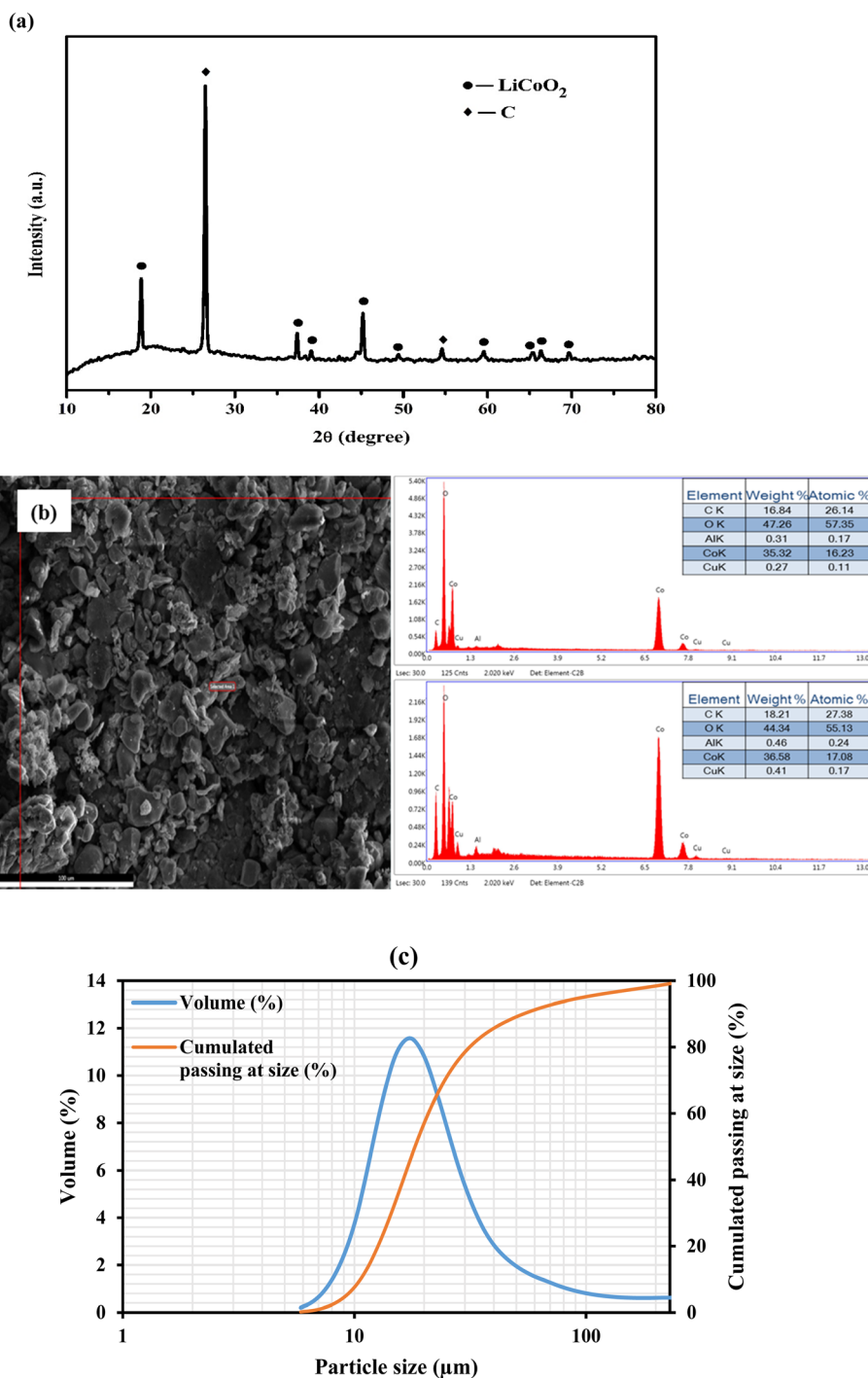


Fig. 1 (a) XRD patterns of the spent LIB sample, (b) SEM-EDS analysis of the spent LIB sample, and (c) particle size distribution of the spent LIB sample.

helps in the reduction of Co(III) to soluble Co(II).^{56,57} From the findings, it was also revealed that ascorbic acid, as opposed to other acids, significantly increased the leaching efficiency of Co and Li (Fig. 2). With 0.5 mol L⁻¹ ascorbic acid, about 81.8% of Li and 75.5% of Co were leached at room temperature (30 °C). The primary cause of this was the dual function of ascorbic acid acting as both an acid and a reducing agent, which made it

easier for Co and Li to be leached from the spent LIB sample.^{45,58} The two most likely and thermodynamically stable products are C₆H₆O₆Li₂ and C₆H₆O₆Co (Fig. 3).⁴⁴ The leaching reaction of LiCoO₂ with ascorbic acid may be expressed as

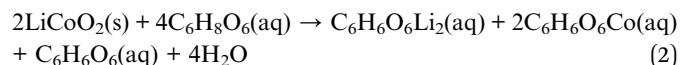
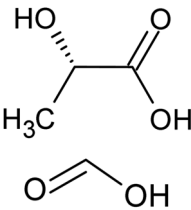
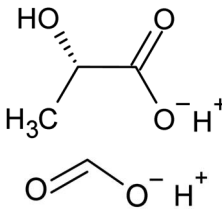
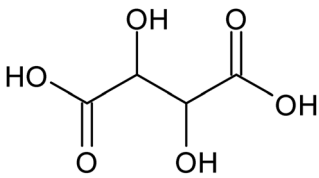
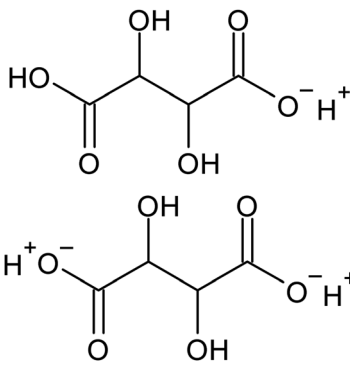
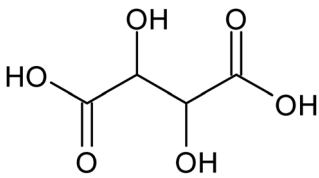
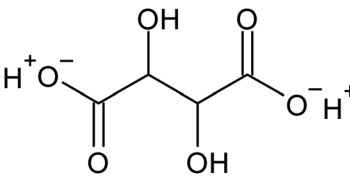
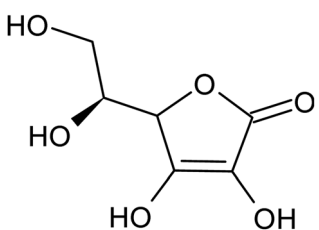
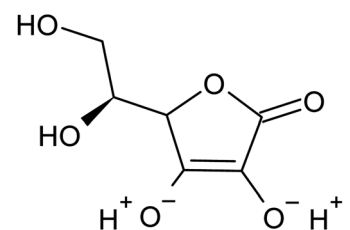
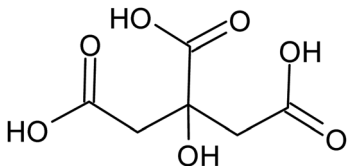
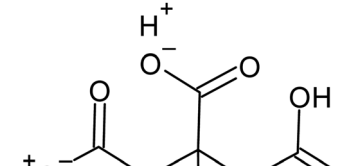


Table 3 Chemical formula, structures, and possible dissociations of organic acids

Organic acids	Chemical formula	Structure	Possible dissociation
Lactic acid	$C_3H_6O_3$		
Formic acid	CH_2O_2		
Tartaric acid	$C_4H_6O_6$		
Ascorbic acid	$C_6H_8O_6$		
Citric acid	$C_6H_8O_7$		



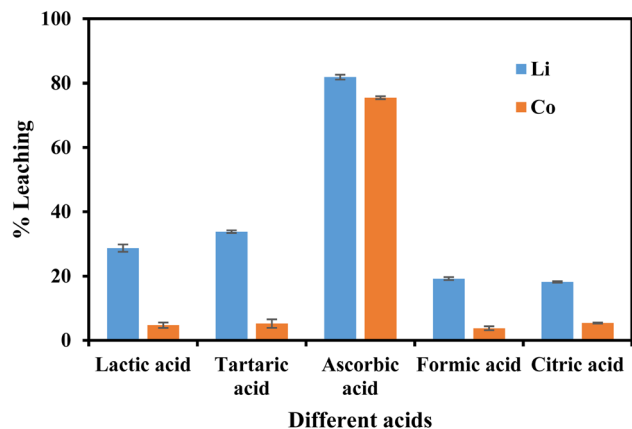


Fig. 2 Effect of different organic acids on the leaching efficiency of Li and Co (acid conc. = 0.5 mol L^{-1} , S/L = 10 g L^{-1} , temperature = $30 \text{ }^\circ\text{C}$, leaching time = 60 min, particle size = $-25 \mu\text{m}$).

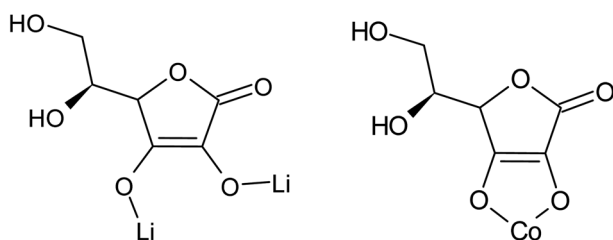


Fig. 3 Possible products formed by ascorbic acid.

3.2.2 Effect of ascorbic acid concentration. Ascorbic acid was found to be a good lixiviant for the leaching of the spent LIB. Hence a concentration variation study of ascorbic acid (0.05 to 1.0 mol L^{-1}) was carried out to figure out the maximum leaching of both the metal ions. The leaching efficiencies of Li and Co increased from 29.2% to 84.1% and 22.3% to 79.5%, respectively, when the ascorbic acid concentration was increased from 0.05 mol L^{-1} to 0.8 mol L^{-1} . The leaching efficiency of both metals was not considerably improved by further increasing the ascorbic acid content (Fig. 4). In the ascorbic acid

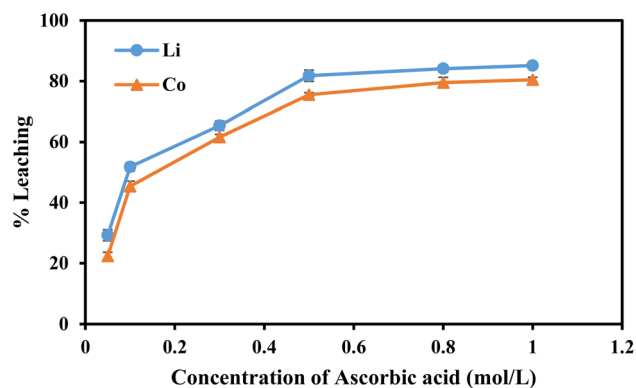


Fig. 4 Effect of ascorbic acid concentration on the leaching efficiency of Li and Co.

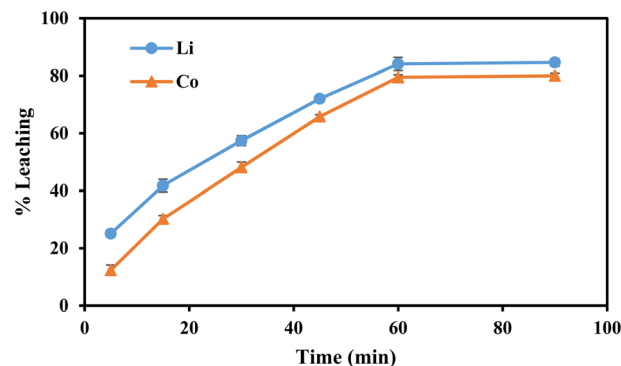


Fig. 5 Effect of leaching time on the leaching efficiency of Li and Co.

concentration range investigations, it was found that Cu and Al were not leached with ascorbic acid. As a result, the concentration of ascorbic acid was fixed at 0.8 mol L^{-1} for further experiments.

3.2.3 Effect of leaching time. Fig. 5 depicts the effect of leaching duration on the leaching efficiencies of Li and Co. The leaching duration was varied from 5 to 90 min, with 0.8 mol L^{-1} ascorbic acid, S/L 10 g L^{-1} , and a temperature of $30 \text{ }^\circ\text{C}$. Only 25.1% of Li and 12.3% of Co were leached at a leaching duration of 5 min. When the leaching time was increased to 60 min, the leaching efficiencies of Li and Co increased to 84.1% and 79.5%, respectively. However, this steadily increasing trend was maintained for up to 60 min, after which the leaching rate remained steady. As a result, the leaching time of 60 min was maintained throughout the studies.

3.2.4 Effect of temperature. The effect of temperature on Li and Co leaching was studied by varying the temperature from 30 to $70 \text{ }^\circ\text{C}$. As shown in Fig. 6, only 84.1% of Li and 79.5% of Co were leached at room temperature ($30 \text{ }^\circ\text{C}$) with 0.8 mol L^{-1} ascorbic acid, indicating that ascorbic acid is an effective leaching agent for the leaching of valuable metals from spent LIBs. As solute diffusivity increased with temperature, the rate of leaching increased as well. The main reason for this is that the probability of successful collisions is directly proportional to temperature and inversely proportional to the activation energy. The increase in kinetic energy with an increase in temperature speeds up the reaction which leads to lower

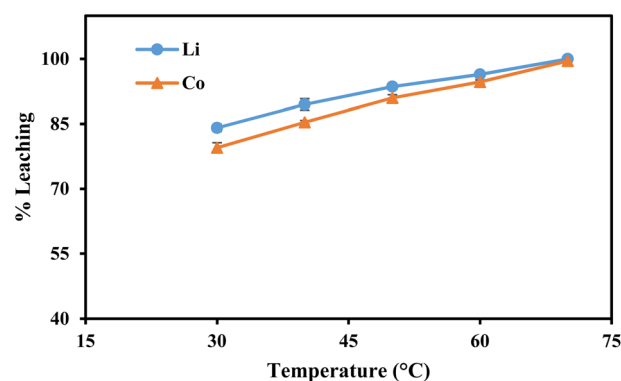


Fig. 6 Effect of temperature on the leaching efficiency of Li and Co.



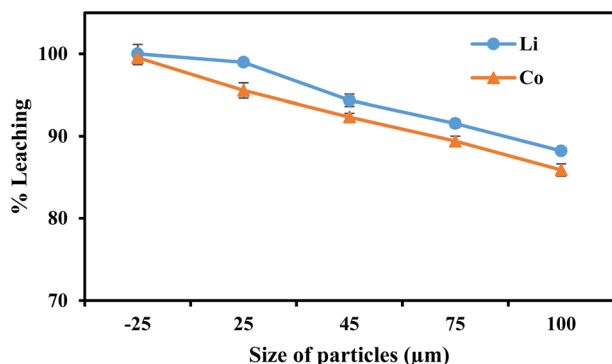


Fig. 7 Effect of particle size on the leaching efficiency of Li and Co.

activation energy and supports the enhancement of leaching efficiency. At the temperature of 70 °C, the maximum leaching of Li (0.39 g L⁻¹) and Co (3.396 g L⁻¹) was noticed.

3.2.5 Effect of particle size. The impact of particle size on the leaching of both metals was investigated using 5 different sized fractions of -25, +25-45, +45-75, +75-100, and +100 µm. Fig. 7 illustrates how a reduction in particle size increased the leaching efficiency of both Li and Co. The highest leaching efficiency of Li (100%) and Co (99.5%) was achieved after 60 minutes using the smaller particle size of -25 µm, whereas the particle size ranging from 25-100 µm showed lower leaching efficiency of both metals than that of -25 µm. This is often explained by the fact that finer particles have more surface area. These outcomes are also in line with the findings reported for metal leaching values.⁵⁹

3.2.6 Effect of solid to liquid ratio. By varying the solid to liquid ratio (S/L) from 10 g L⁻¹ to 70 g L⁻¹, the impact of S/L on Li and Co leaching efficiency was investigated. The leaching rates of both metals remained steady when the S/L ratio was increased from 10 to 50 g L⁻¹, but they decreased as the S/L ratio was increased further, as shown in Fig. 8. The maximal leaching rates of Li (100%) and Co (99.5%) were achieved at a S/L ratio of 50 g L⁻¹. The maximum concentrations of Li (2.14 g L⁻¹) and Co (17.02 g L⁻¹) in the leach liquor were obtained at a S/L ratio of 60 g L⁻¹, and the concentrations of both metals remained constant after increasing the S/L ratio further. S/L ratio of 60 g

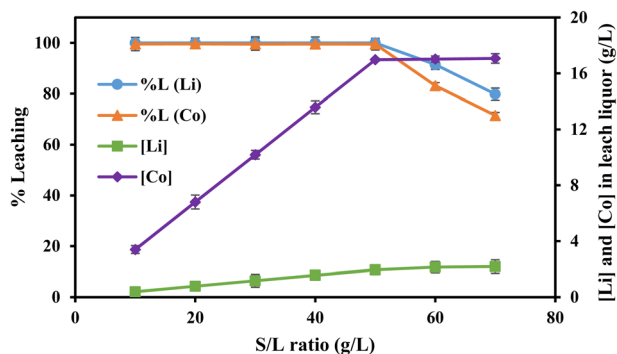


Fig. 8 Effect of solid to liquid ratio on the leaching efficiency of Li and Co.

L⁻¹ should be chosen for maximum Li and Co leaching. But, the residue still contained a sizable quantity of Li and Co, so, the S/L ratio was set at 50 g L⁻¹. Hence, the optimum conditions for leaching of spent LIB were of 0.8 mol L⁻¹ ascorbic acid, 70 °C, 60 min of leaching time, and S/L ratio of 50 g L⁻¹, corresponding recovery of 100% of Li and 99.5% of Co.

3.2.7 Leaching kinetics. To determine the rate of reaction and the mechanism underlying the leaching process, kinetic studies are frequently used. The spent LIB sample leaching is a solid-liquid heterogeneous chemical reaction that occurs on the exterior surfaces of the unreacted particles. To describe the kinetics of metal leaching from spent LIBs, several models have been developed.⁵⁹⁻⁶³ The shrinking core model is one of them, and it is often used to predict various rate-determining steps for the leaching of different metal ions. The shrinking core model includes two different equations (eqn (3) and (4)). Traditionally, the shrinking-core model is regarded as the leaching kinetics' cornerstone, and the surface chemical reaction control and diffusion control model were two possible control steps.

(a) Surface chemical reaction control

$$1 - (1 - X)^{\frac{1}{3}} = \left(\frac{2bk_i c}{\rho d_0} \right) t = k_c t \quad (3)$$

(b) Diffusion control through the product layer

$$1 - \frac{2}{3}X - (1 - X)^{\frac{2}{3}} = \left(\frac{8bDc}{(1 - \varepsilon)\rho d_0^2} \right) t = k_d t \quad (4)$$

Another kinetic model that is employed to describe the multi-metal leaching for some solid-liquid heterogeneous processes is the Avrami equation, which is a mixed control model that involves both diffusion and chemical reaction control.

(c) Avrami equation

$$-\ln(1 - X) = k_r t \quad (5)$$

By taking the natural logarithm on both sides, eqn (5) will be expressed as,

$$\ln(-\ln(1 - X)) = \ln k_r + \ln t \quad (6)$$

where, X is the leaching efficiency of the metals at leaching time t (min), k_c is the chemical reaction rate constant (min⁻¹), b is the stoichiometric factor, c is the concentration of reactant (mol m⁻³), ρ is the molar concentration (mol m⁻³) of the dissolving metal in the particle, d_0 (m) is the initial particle diameter, k_i is the intrinsic rate constant of the surface reaction (m min⁻¹), k_d is the diffusion rate constant (min⁻¹), D is the diffusivity (m² min⁻¹) of the species through a product layer, ε is the particle porosity (for eqn (3)-(6)), and k_r is the reaction rate constant for the Avrami equation model. The kinetics of leaching were studied at different times (5-60 min) and temperatures (30-70 °C). The lower R^2 values clearly indicated that the Avrami equation model was not fitted at higher temperatures, despite the fact that it was fitted at lower



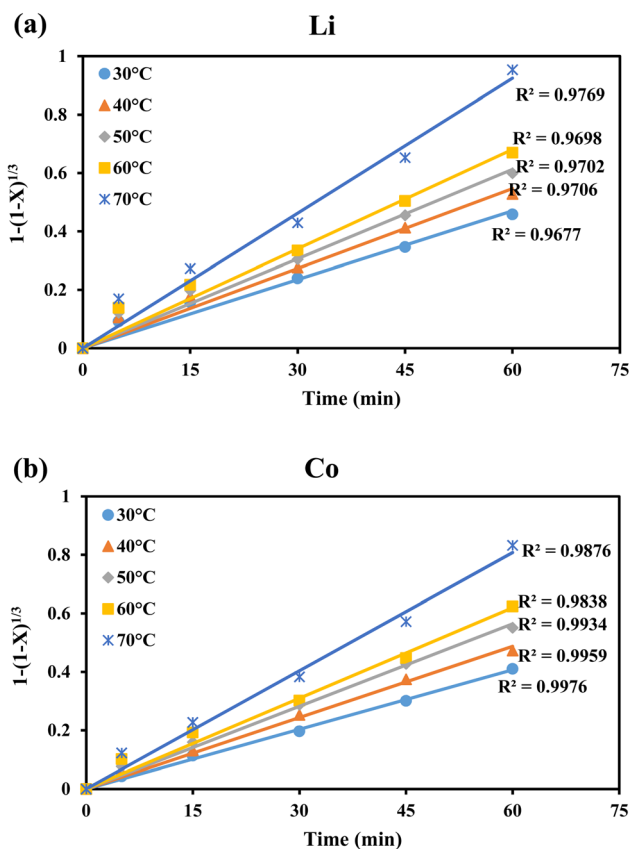


Fig. 9 Dissolution of Li and Co vs. time at different temperatures, fitted by surface chemical reaction control model for leaching of (a) Li and (b) Co.

temperatures (Fig. S1†). Although the R^2 values for the diffusion control model (Fig. S2†) and the surface chemical reaction model (Fig. 9) were comparable, the surface chemical reaction model's R^2 values were greater than 0.98, implying that the surface chemical reaction model was accountable for controlling the ascorbic acid leaching process.

The specific rate constants (k) for Li and Co were determined using the surface chemical reaction model (Fig. 9a and b). The specific rate constant (k), pre-exponential factor (A), apparent activation energy (E_a), and absolute temperature (T) are related by the Arrhenius equation (eqn (7)).

$$\ln k = \ln A - \frac{E_a}{RT} \quad (7)$$

It was observed that the reaction rate constants increased with increasing temperature, indicating that increasing the temperature is beneficial for enhancing the leaching efficiencies of Li and Co. Fig. 10 showed the plot of $\ln k$ vs. $1000/T$ and higher correlation coefficient values ($R^2 > 0.96$) suggested a better fit of the surface chemical reaction model for the leaching of Li and Co. From Fig. 10, the apparent activation energies of Li and Co were found to be 13.5 kJ mol^{-1} and 13.7 kJ mol^{-1} , respectively.

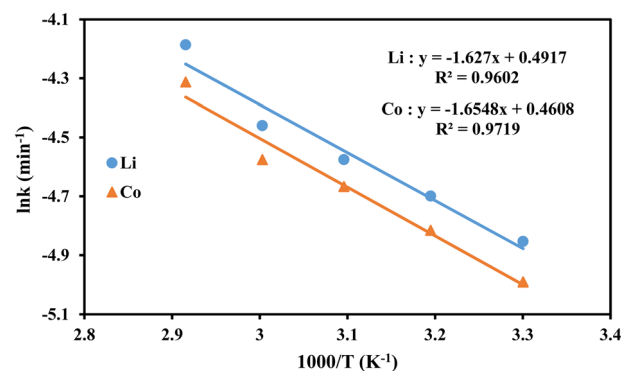


Fig. 10 Arrhenius plot for the leaching of Li and Co.

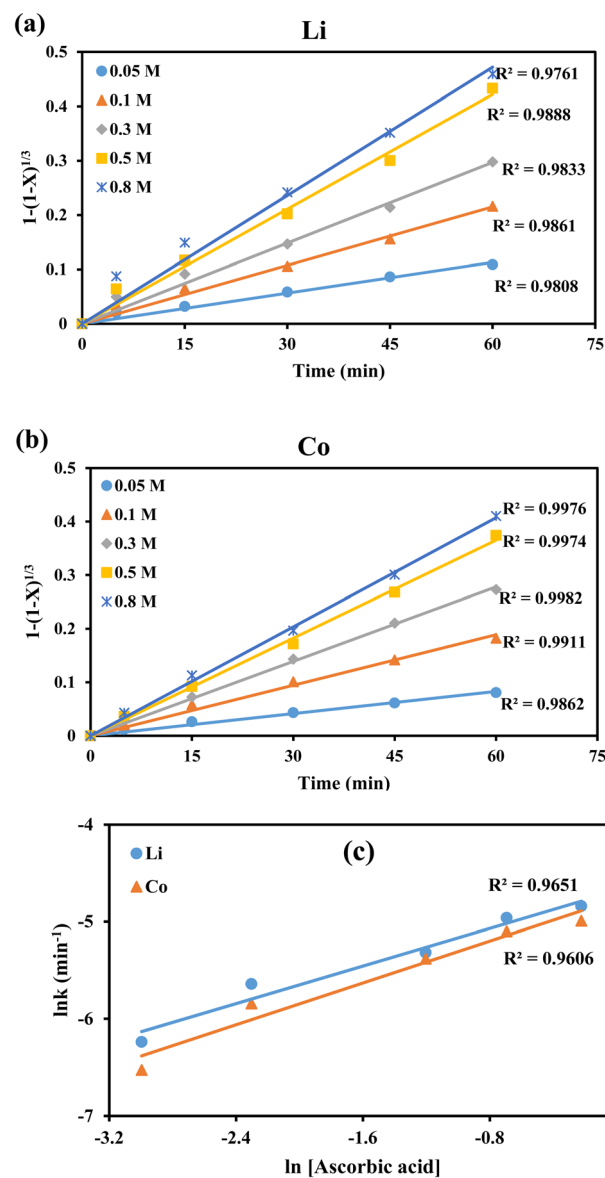


Fig. 11 Applicability of surface chemical reaction control model for leaching of (a) Li and (b) Co with different ascorbic acid concentrations and (c) plot of $\ln k$ vs. $\ln[\text{ascorbic acid}]$.



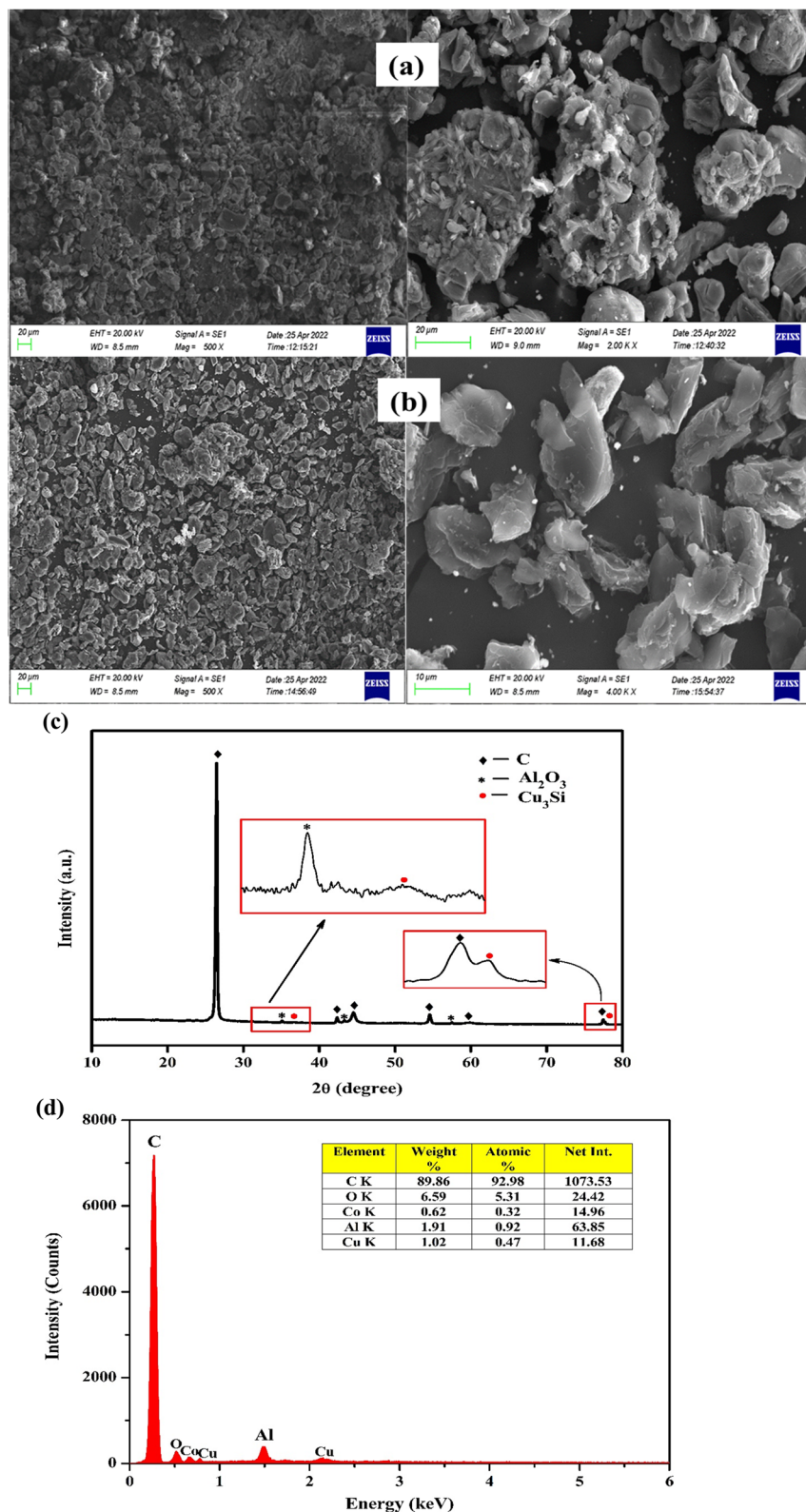


Fig. 12 SEM images of spent LIB sample (a) before leaching and (b) after leaching (c) XRD and (d) EDS analysis of spent LIB sample after first step leaching.

To support the surface chemical reaction model, the data of variation in ascorbic acid concentration (Fig. 4) was analyzed. The higher R^2 values (>0.98) for Li and Co (Fig. 11a and b), and

the plot of $\ln k$ vs. $\ln[\text{ascorbic acid}]$ (Fig. 11c) justified the fitting of the surface chemical reaction model for the leaching of both metals.



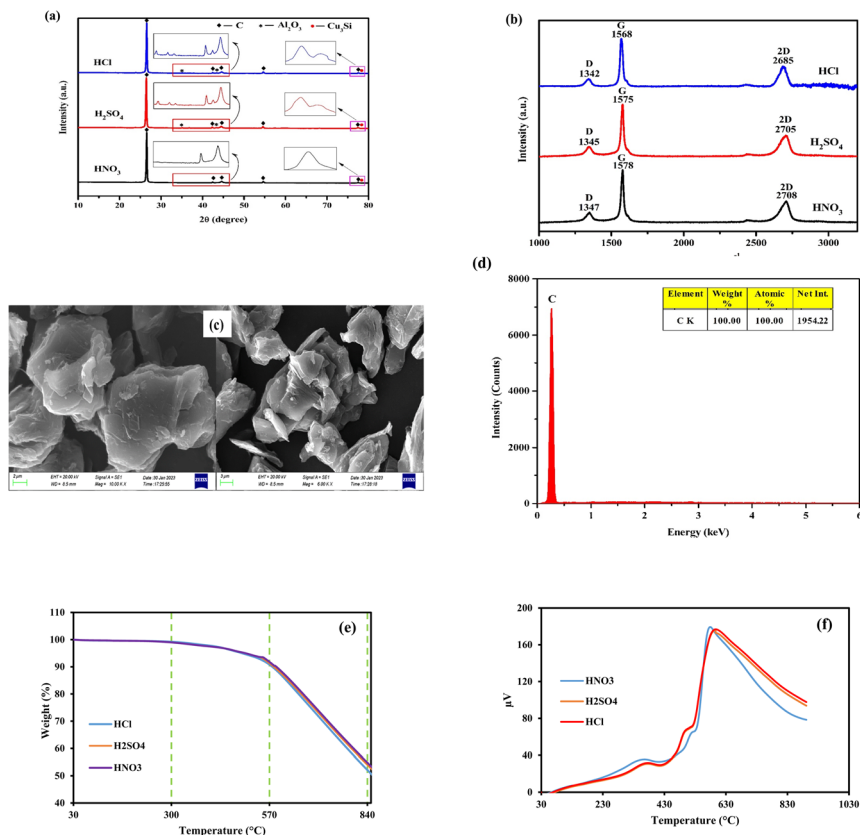


Fig. 13 (a) XRD patterns (b) Raman spectra (c) SEM images (d) EDS patterns (e) TGA and (f) DTA plots of spent LIB samples after the two-step leaching process.

Further justification of the kinetic model was checked with the effect of particle size (data from Fig. 7) using the surface chemical reaction control eqn (3). Higher correlation coefficient values were obtained for Li and Co (Fig. S3a and b[†]), ensuring a better match of the surface chemical reaction model.

The SEM images of the spent LIB samples, taken at various magnifications before and after leaching, were shown in Fig. 12a and b. According to Fig. 12a, the materials had an asymmetrical and agglomerated shape before leaching. However, the particles with agglomerated shape vanished after leaching with ascorbic acid (Fig. 12b). To determine whether complete Li and Co leaching was achieved or not, the XRD patterns of LIB samples were examined after leaching. According to Fig. 12c, Li and Co were completely leached leaving carbon, aluminum oxide, and copper silicon in the residue (JCPDS data: C = 01-089-7213, Al₂O₃ = 01-075-1865 and Cu₃Si = 00-051-0916). Additionally, some impurities have been reflected in the XRD plot as irregular patterns, but with less intensity. Also, it was confirmed through the EDS analysis of the leached residue (Fig. 12d).

3.2.8 Two-step leaching: The residual aluminum oxide and other impurities must be leached out to obtain pure graphitic carbon as shown in Fig. 12c. Therefore, a two-step leaching process was adopted to regenerate pure graphitic carbon. After ascorbic acid leaching, the residue was taken for further

treatment with different acids (HCl, H₂SO₄, and HNO₃). The acid concentration was set at 1.0 mol L⁻¹, and the other parameters were 10 g L⁻¹ of S/L, 60 min of leaching time, and a temperature of 70 °C. The findings showed that HCl and H₂SO₄ were unable to leach alumina but HNO₃ was the most effective leaching agent for alumina. Nnanwube *et al.* proposed alumina leaching with HNO₃ and the findings revealed that nitric acid showed a better efficiency for alumina leaching.⁶⁴⁻⁶⁶ The result was supported by XRD analysis (Fig. 13a) and the concentration of alumina was checked by ICP-OES. From the XRD patterns, it was revealed that after leaching with HCl and H₂SO₄ less amount of alumina and impurities still remained in the residue. In contrast to which no alumina peaks and impurities appeared in the XRD patterns of residue after leaching with HNO₃. To exemplify the quality of the graphitic carbon, the Raman spectra of the leached residues after the two-step leaching process were analyzed and shown in Fig. 13b. Raman spectra of graphite is generally dominated by a G band at nearly 1580 cm⁻¹ which appears due to the sp² bond of carbon.⁶⁷ Additionally, two prominent bands must be seen in the Raman spectra of graphite at around 1350 cm⁻¹ (D band) and 2700 cm⁻¹ (2D band).^{68,69} From Fig. 13b it was observed that all the Raman signals (D = 1347 cm⁻¹, G = 1578 cm⁻¹ and 2D = 2700 cm⁻¹) that appeared for the leached residue after leaching with HNO₃ were more reliable than that of the other two acids.



The appearance of the 2D band is clearly indicated that the leached residue is thought to be fully graphitized, or called graphitic carbon.⁷⁰ Generally, the D/G band intensity ratio (I_D/I_G) in Raman spectra, which represents the graphitization degree and defect concentration, can be used to quantify the structural properties of graphite.⁷¹ Due to the existence of edge defects, the I_D/I_G ratio tends to rise with decreasing graphite size.^{67,72} Among all the three Raman patterns, minimal defects ($I_D/I_G = 0.23$) appeared for the leached residue after HNO₃ leaching. Also for more justification of high-purity graphite and to confirm the metal residual in the leached residue SEM-EDS, thermogravimetric analysis (TGA) and differential thermal analysis (DTA) have been analyzed and are shown in Fig. 13c–f. Fig. 13c clearly indicates the presence of only graphitic carbon without any impurities. Additionally, EDS elemental analysis confirmed that the residue contained 100% carbon only (Fig. 13d). The thermal behavior of the leached residues following the two-step leaching process is depicted in Fig. 13e. There are 3 major weight-loss regions at 30–300, 300–570, and 570–840 °C, respectively. Between 30 and 300 °C, the first weight-loss region, results from the removal of bound water molecules (approx. 1.5–2.0 wt%).^{48,62} Between 300 and 570 °C, the second weight-loss region corresponds to the breakdown of binding components (approx. 6.0–6.5 wt%), and the gradual drop in wt% after 570 °C reveals the porous nature of carbon. The highest peak was similarly found at 570–590 °C as indicated by the DTA curve (Fig. 13f). Therefore, 570–590 °C is the appropriate calcination temperature.⁷³ From both graphs it was observed that for the regeneration of pure graphitic carbon, the leached residue after HNO₃ leaching was more credible than the other two acids.

4 Conclusion

This work proposed an efficient and environmentally acceptable approach for recycling essential metals as well as graphitic carbon from discarded LIBs. At room temperature (30 °C), about 84.1% of Li and 79.5% of Co were leached with 0.8 mol L⁻¹ ascorbic acid, which was increased to 100% and 99.5%, respectively, at 70 °C. Also, it was revealed from the variation in particle size that the maximal leaching of both metals was accomplished with the smaller particle size (–25 μm). It was caused by ascorbic acid's dual action as both an acid and a reducing agent. From the possible dissociations of ascorbic acid, it was concluded that the two most likely and thermodynamically stable products are C₆H₆O₆Li₂ and C₆H₆O₆Co. The detailed leaching kinetics was studied and the higher correlation coefficient values suggested a better match of the surface chemical reaction model with apparent activation energies (E_a) of Li (13.5 kJ mol⁻¹) and Co (13.7 kJ mol⁻¹). Further leaching of the leached residue was carried out in order to get pure graphitic carbon and to leach the leftover aluminum oxide and other impurities. From the Raman spectra, XRD, TGA, and SEM-EDS analysis of the final residues, it was confirmed that HNO₃ was the effective lixiviant to regenerate the graphitic carbon. The 2D band's appearance clearly

illustrates that the leached residue is considered to be completely graphitized, or referred to as graphitic carbon.

Author contribution

Sibananda Sahu (first author): writing – original draft, visualization, data curation, formal analysis, investigation, software. Niharbala Devi (corresponding author): conceptualization, methodology, supervision, Writing – review and editing, validation.

Conflicts of interest

The authors declare that there is no conflict of interest.

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