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# Gallium-based liquid metal hybridizing MoS<sub>2</sub> nanosheets with reversible rheological characteristics and enhanced lubrication properties

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Gallium-based liquid metal (GLM) is a promising lubricant candidate due to its high load capacity and high thermal stability. However, the lubrication performance of GLM is restricted by its metallic characteristics. Herein, this work proposes a facile method to obtain a GLM@MoS<sub>2</sub> composite by integrating GLM with MoS<sub>2</sub> nanosheets. The incorporation of MoS<sub>2</sub> imparts GLM with different rheological properties. Since GLM is able to be separated from the GLM@MoS<sub>2</sub> composite and agglomerates into bulk liquid metal again in alkaline solution, the bonding between GLM and MoS<sub>2</sub> nanosheets is reversible. Moreover, our frictional tests demonstrate that the GLM@MoS<sub>2</sub> composite exhibits enhanced tribological performance including reduction of friction coefficient and wear rate by 46% and 89%, respectively, in contrast to the pure GLM.

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## 1. Introduction

Gallium-based liquid metal (GLM), such as eutectic Ga–In alloy or galinstan, has attracted significant attention for applications in composites<sup>1–4</sup> and also for their potential as novel lubricants.<sup>5–8</sup> GLM holds metallic advantages including low melting point, low vapor pressure, low toxicity, good fluidity, high thermal stability, high thermal conductivity, and high extreme-pressure properties, which meet the requirements for extremely high temperature and pressure lubricants. However, the lubrication abilities of GLM are restricted by their metallic properties.<sup>9</sup> On account of high surface tension and chemically inertness, the anti-friction and anti-wear abilities of GLM is poor under low loads and speeds. The effective friction reaction films must be formed under extremely high friction work conditions. As a result, this metallicity–lubricity trade-off of GLM is limiting for emerging lubricant application.

In order to overcome this constraint, some efforts have been made to enhance the lubricity of GLM including optimizing the environmental atmospheres,<sup>10</sup> treating the surface texture of the frictional pairs<sup>11</sup> and modifying liquid metal with

particles.<sup>12,13</sup> Among these efforts, modification liquid metal with specific micro and nano-particles is an effective and convenient method, which is suitable for most actual working conditions. There are mainly two methods to mingle functional particles into liquid metal alloy.<sup>14–19</sup> For metal particles, inter-metallic wetting between liquid metal and particles can be induced by electrochemical reaction or acid solution. For non-metal particles, liquid metals' sticky oxides can be utilized to blend the particles by grinding or mechanical stirring. Guo *et al.* have reported that doping traces of aluminum element to GLM could enhance the lubricity of GLM.<sup>12</sup> However, metal particles hold a limited ability to improve the lubricity of liquid metal. And to date, the research about hybridizing non-metal particles into GLM for enhancing lubricity of GLM is relatively absent.

Some non-metal particles exhibit excellent lubrication ability such as MoS<sub>2</sub>. MoS<sub>2</sub> is an inorganic compound with layered structure and the molecular force between layers is so weak that it is easy to slip between layers, resulting in low shear strength.<sup>20,21</sup> These characteristics impart good anti-friction effect to MoS<sub>2</sub>, making it a widely used dry lubricant.<sup>22,23</sup> Furthermore, microscale or nanoscale MoS<sub>2</sub> have been proved to be a promising lubrication additive for both liquid and solid based lubricants with remarkable friction reduction and wear resistance performance.<sup>24–27</sup> For instance, Chacko *et al.* have reported that with appropriate concentrations of MoS<sub>2</sub> nanosheets, the lubrication behaviours of both coconut oil and paraffin oil could be enhanced.<sup>28</sup> Chen *et al.* have found that the addition of MoS<sub>2</sub> nanosheets was capable of improving the anti-friction and anti-wear properties of the bismaleimide resin.<sup>29</sup>

Herein, in present work, GLM@MoS<sub>2</sub> composite with desirable lubrication properties is designed by hybridizing MoS<sub>2</sub> nanosheets into GLM. GLM@MoS<sub>2</sub> composite is prepared by

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mechanical stirring and grinding, utilizing the sticky oxides of GLM. The bonding between GLM and MoS<sub>2</sub> nanosheets is reversible, which bestows reversible rheological characteristics on GLM@MoS<sub>2</sub> composite. In addition, the tribological tests prove that the prepared GLM@MoS<sub>2</sub> composite hold excellent lubrication properties.

## 2. Experiments

### 2.1 Materials

The GLM used in present work is Ga<sub>76</sub>In<sub>24</sub> with a melting point at 16 °C and the preparation procedures of Ga<sub>76</sub>In<sub>24</sub> are as the followings. First, Ga and In with mass ratio at 76 : 24 were mixed together in a graphite crucible. And then the mixtures were heated to the temperature of 180 °C under the vacuum condition for 30 minutes. After the heating treatment, a eutectic liquid metal alloy of Ga and In was produced. Finally, the eutectic liquid metal was ultrasonicated in a water bath for 15 minutes to promote the complete fusion of GLM. The densities of pure Ga and eutectic liquid metal, which are 6.1 g cm<sup>-3</sup> and 6.8 g cm<sup>-3</sup> respectively, which are in accordance with the previous studies.<sup>30</sup> MoS<sub>2</sub> nanosheets adopted in this work were purchased from Beijing Dk Nano technology Co., Ltd, China.

### 2.2 Preparation of GLM@MoS<sub>2</sub>

GLM@MoS<sub>2</sub> was prepared by mechanical mixing and grinding methods and the detailed operational procedures were shown in Fig. 1. First of all, the GLM was added in a ceramic crucible. Once the GLM was exposed to air environment, the outer sphere of the GLM would oxide quickly and produce a nanoscale Ga<sub>2</sub>O<sub>3</sub> film surrounding the GLM.<sup>31</sup> Then, MoS<sub>2</sub> nanosheets were placed in the crucible. As shown in Fig. 1a, MoS<sub>2</sub> nanosheets and GLM were separated by Ga<sub>2</sub>O<sub>3</sub> layer. After that, pestle was utilized to grind the MoS<sub>2</sub> nanosheets into GLM for hours. The grinding process could break the Ga<sub>2</sub>O<sub>3</sub> layers and the adhesion property of Ga<sub>2</sub>O<sub>3</sub> could facilitate the dispersion of MoS<sub>2</sub> nanosheets in GLM.

### 2.3 Tribological experiments

The tribological tests were conducted utilizing a ball-on-disk tribometer (UMT-2, CETR Corporation Ltd, USA) in reciprocation friction mode. Experiments were performed at room temperature (25 °C) and ambient humidity (30 ± 2%). And the experimental time of each individual test was 30 min. The disk specimens are AISI52100 bearing steel disk with surface

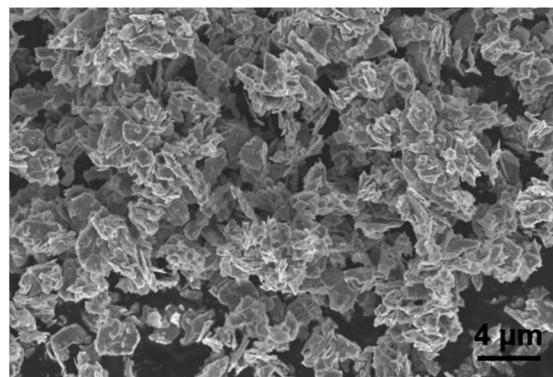


Fig. 2 SEM image of MoS<sub>2</sub> nanosheets adopted in this work.

roughness of Ra 0.021 μm and the ball specimens are Φ9.5 mm AISI52100 steel with surface roughness of Ra 0.008 μm. The applied loads were set as 2, 5, 10, 15, 20, and 25 N and kept constant for each test. The sliding frequency was 2 Hz and the sliding stroke was 6 mm. GLM and GLM@MoS<sub>2</sub> were adopted as the lubricant. In order to ensure the repeatability of the results obtained, all tests were repeated three times. Before and after every individual test, the specimen was cleaned with ethanol in an ultrasonic bath for 15 minutes.

Moreover, in order to specify the wear rate ( $k$ ) for each experiment, we have calculated the wear volume ( $V$ ) based on the corresponding wear scar radius of the ball through the following equations.

$$h = R - \sqrt{R^2 - r^2} \quad (1)$$

$$V = \pi \cdot h^2 \left( R - \frac{h}{3} \right) \quad (2)$$

$$k = \frac{V}{F \cdot S} \quad (3)$$

where  $h$  is the height of spherical cap,  $R$  is the original radius of the ball,  $F$  is the normal load in the experiment and  $S$  is the total sliding distance. For all experiments, we took three radii of each wear scar and calculated their average value.

### 2.4 Characterizations

Scanning electron microscopy (Gemini SEM 500, ZEISS, Germany) equipped with Energy dispersive spectrometer (EDS) was utilized to observe the morphology of GLM@MoS<sub>2</sub> composite



Fig. 1 Schematic presentation of preparation process of GLM@MoS<sub>2</sub>. Initially, the GLM is surrounded by Ga<sub>2</sub>O<sub>3</sub> oxides and separated from MoS<sub>2</sub> nanosheets. Then the grinding process make MoS<sub>2</sub> nanosheets disperse into GLM by the adhesion property of Ga<sub>2</sub>O<sub>3</sub>. And finally the GLM@MoS<sub>2</sub> composite is obtained.



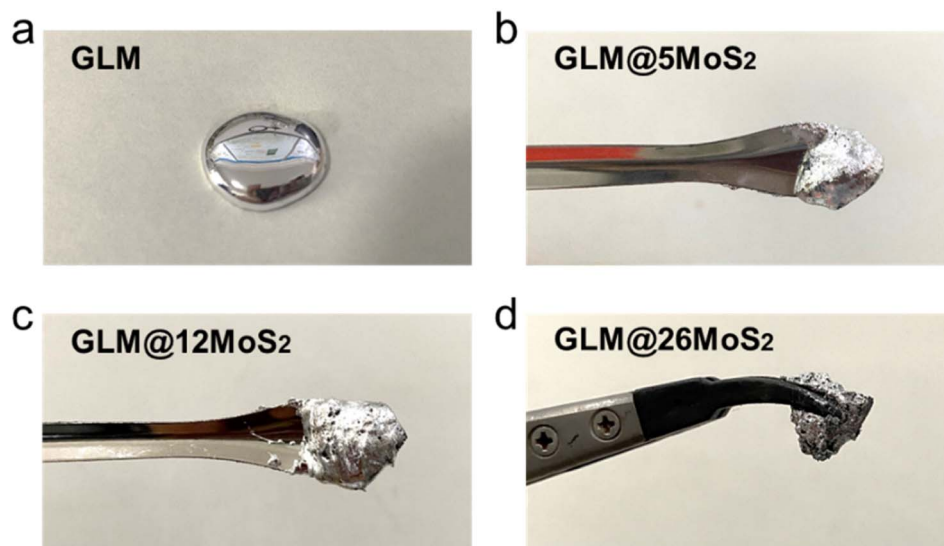


Fig. 3 (a) Image of pure GLM, (b) GLM with 5wt% MoS<sub>2</sub> nanosheets, (c) GLM with 12 wt% MoS<sub>2</sub> nanosheets, (d) GLM with 26 wt% MoS<sub>2</sub> nanosheets.

and MoS<sub>2</sub> nanosheets. Thermo gravimetric analyser (TGA) tests were conducted to evaluate the thermal properties of GLM@MoS<sub>2</sub> composite under an oxygen atmosphere from 30 to 800 °C (STA449C, NETZSCH, Germany). Optical microscope (OM) and SEM were used to observe the worn surfaces. EDS and X-ray photoelectron spectroscopy (XPS) were adopted to detect the chemical states of the worn tracks.

### 3. Results and discussion

#### 3.1 The physical properties of GLM@MoS<sub>2</sub>

The morphology of MoS<sub>2</sub> nanoparticles used in this work was characterized by SEM as shown in Fig. 2. The MoS<sub>2</sub> holds

lamellar structure with the thickness less than 50 nm and the laminae size ranging from 1 μm to 3 μm. The appearance of pure GLM is a silver colour sheeny liquid as demonstrated in Fig. 3a. Different amounts of MoS<sub>2</sub> nanosheets were hybridized into GLM and the mass fractions of MoS<sub>2</sub> nanosheets in GLM were calculated by weighing the GLM with and without the MoS<sub>2</sub> nanosheets. The GLM with 5 wt%, 12 wt% and 26 wt% MoS<sub>2</sub> nanosheets are denoted as GLM@5MoS<sub>2</sub>, GLM@12MoS<sub>2</sub> and GLM@26MoS<sub>2</sub>. It can be seen from Fig. 3 that with the increase of MoS<sub>2</sub> nanosheets, the metallic luster of GLM@MoS<sub>2</sub> composite becomes darkened and the fluidity of GLM@MoS<sub>2</sub> composite becomes poor.

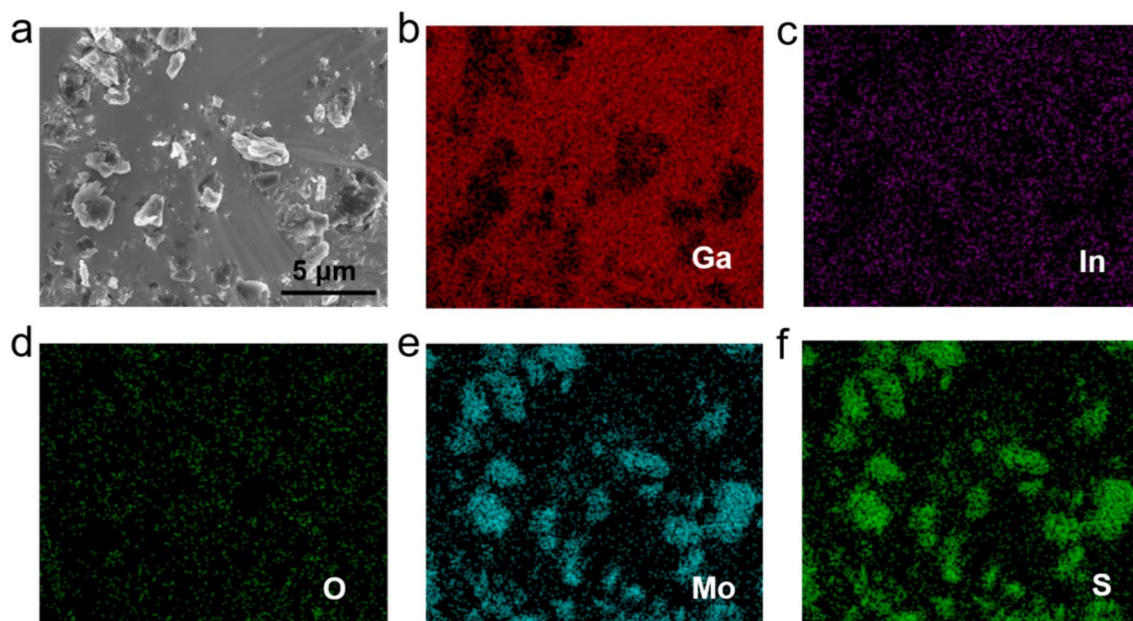


Fig. 4 (a) SEM image and (b)–(f) EDS elemental mappings of GLM@5MoS<sub>2</sub>.





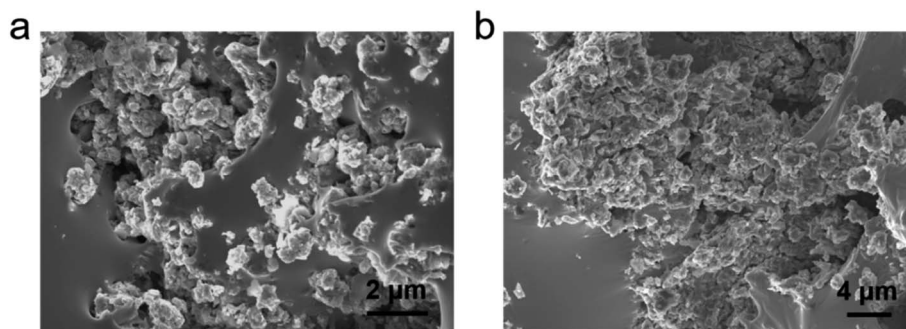


Fig. 5 SEM image of (a) GLM@12MoS<sub>2</sub> composite, (b) GLM@26MoS<sub>2</sub> composite.

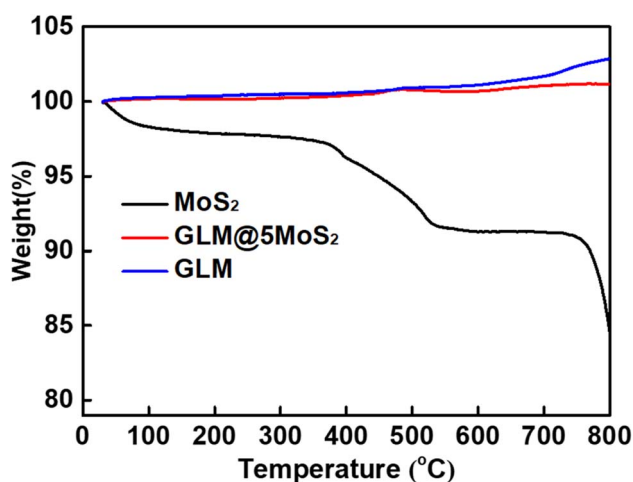


Fig. 6 The TGA curves of original MoS<sub>2</sub> nanosheets, pure GLM and prepared GLM@5MoS<sub>2</sub> composite.

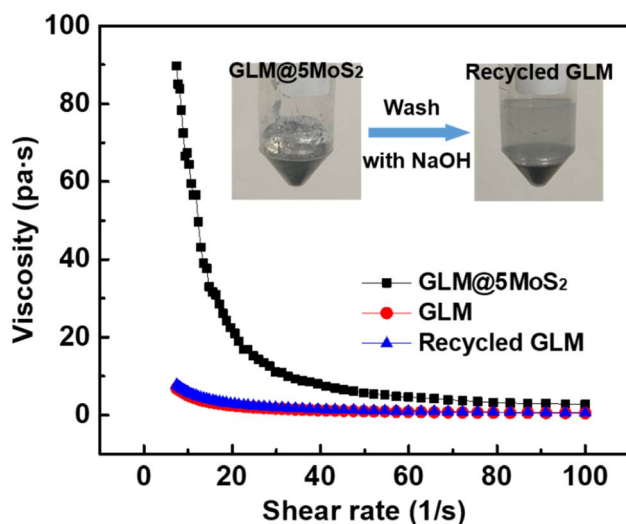


Fig. 7 The rheological characteristics of GLM@5MoS<sub>2</sub> composite, pure GLM and recycled GLM. The inset is the recycling process of GLM.

The morphology and chemical elements of GLM@5MoS<sub>2</sub> composite were characterized by SEM and EDS as shown in Fig. 4. It could be clearly seen from the results that MoS<sub>2</sub>

nanosheets are embedded and well-dispersed in GLM matrix. The morphologies of GLM@12MoS<sub>2</sub> and GLM@26MoS<sub>2</sub> composites are demonstrated in Fig. 5. In comparison with GLM@5MoS<sub>2</sub> composite in Fig. 4, when the mass fraction of MoS<sub>2</sub> nanosheets reaches 12 wt% or 26 wt%, MoS<sub>2</sub> nanosheets in liquid metal are unable to be thoroughly dispersed and MoS<sub>2</sub> nanosheets progressively agglomerate into large particles.

The thermal property of prepared GLM@5MoS<sub>2</sub> composite was tested by thermo gravimetric analyser. TGA experimental results in Fig. 6 further confirm the integration between MoS<sub>2</sub> nanosheets and GLM. For MoS<sub>2</sub> nanosheets, the slight mass loss at the range of 100–780 °C is attributed to the removal of adsorptive hydrated H<sub>2</sub>O and it shows an 8% weight loss before 780 °C. When the temperature is close to 800 °C, the MoS<sub>2</sub> nanosheets have a sudden weight loss due to the sublimation of MoS<sub>2</sub>. For pure GLM, the curve generally demonstrates an upward trend, which is due to the oxidation of GLM and a slight increase in mass. In comparison, the GLM@5MoS<sub>2</sub> composite exhibits a less increase of weight because of the hybrid of MoS<sub>2</sub> nanosheets.

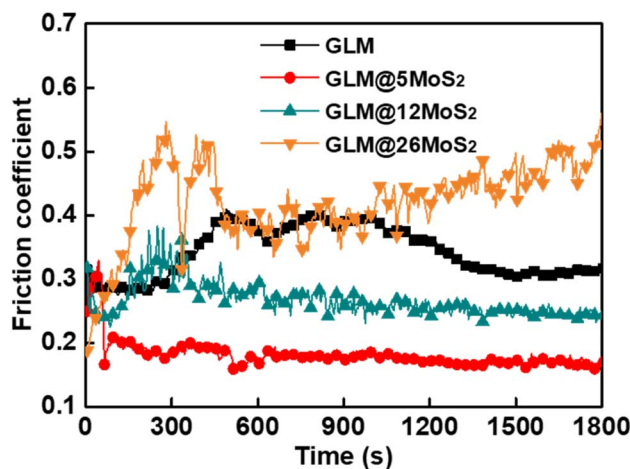


Fig. 8 Real-time friction coefficients lubricated by pure GLM, GLM@5MoS<sub>2</sub>, GLM@12MoS<sub>2</sub>, and GLM@26MoS<sub>2</sub> composite under the applied load of 25 N.



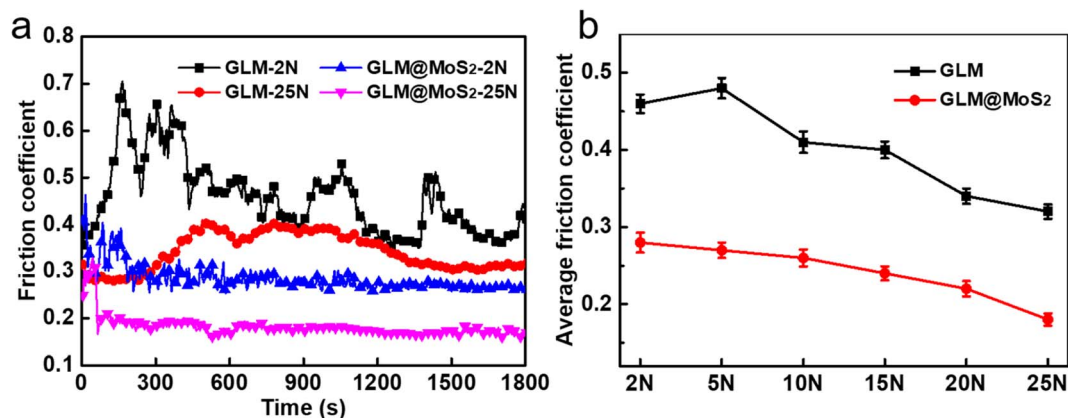


Fig. 9 (a) Comparison of real-time friction coefficient curves between pure GLM and GLM@5MoS<sub>2</sub> composite (b) average friction coefficients of pure GLM and GLM@5MoS<sub>2</sub> composite under different applied loads.

### 3.2 The reversible rheological property of GLM@MoS<sub>2</sub>

There are two kinds of fillers in GLM: metallic and nonmetallic particles. In previous works, GLM based composite is commonly made by hybridizing metal particles into liquid metal, and the binding force between liquid metal and metal particles is derived from stable intermetallic chemical bonds.<sup>32,33</sup> Therefore, it is hard to recycle liquid metal from GLM based composite with metallic particles and the rheological property of this kind of composite is irreversible.

As for nonmetallic particles such as MoS<sub>2</sub> nanosheets in this study, they are hybridized into GLM by utilizing sticky layers of liquid metals' oxides. So, it is feasible to recycle GLM by dissolving liquid metals' oxides in alkali solution and the fabrication process

of the composite is reversible. As demonstrated in Fig. 7, the obtained GLM@5MoS<sub>2</sub> composite holds reversible rheological property. The viscosity of GLM@5MoS<sub>2</sub> is decreased with the shear rate. GLM@5MoS<sub>2</sub> composite demonstrates the characteristic of non-Newtonian fluid, which could be ascribed to the addition of MoS<sub>2</sub> nanosheets. Whereas the original GLM and the recovered GLM exhibit the similar Newtonian property and the viscosities of them are almost consistent.

### 3.3 The tribological properties of GLM@MoS<sub>2</sub>

Fig. 8 demonstrates the real-time friction coefficient curves lubricated by pure GLM and GLM@MoS<sub>2</sub> composites with different contents of MoS<sub>2</sub> nanosheets under the applied load of

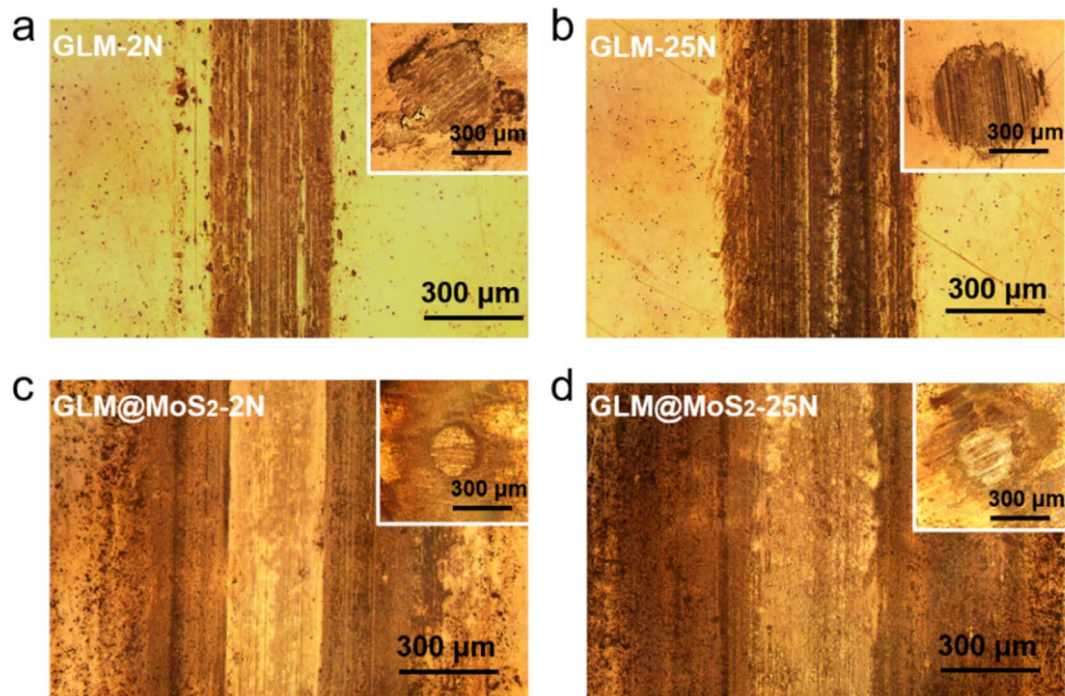


Fig. 10 OM images of wear tracks on the disks lubricated by (a) GLM under 2 N, (b) GLM under 25 N, (c) GLM@5MoS<sub>2</sub> composite under 2 N, (d) GLM@5MoS<sub>2</sub> composite under 25 N. The insets are corresponding wear scars on balls.



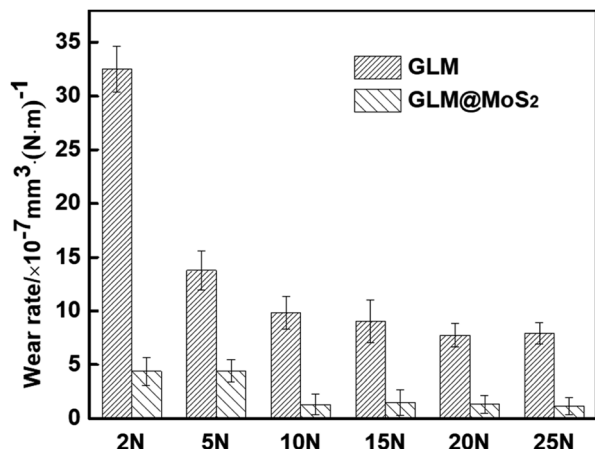


Fig. 11 Wear rates of GLM and GLM@5MoS<sub>2</sub> composite under different applied load conditions.

25 N. It could be concluded from the results in Fig. 8 that GLM@5MoS<sub>2</sub> holds the best anti-friction ability among all samples. The average friction coefficient of GLM@5MoS<sub>2</sub> is 0.18, which is 46% smaller than the friction coefficient of pure GLM. Since the pure MoS<sub>2</sub> is under solid state, the average friction coefficient of pure MoS<sub>2</sub> is as high as 0.72. With the increase of MoS<sub>2</sub> nanosheets in the GLM@MoS<sub>2</sub> composites, the anti-friction ability deteriorates. For GLM@26MoS<sub>2</sub> composite, the friction coefficient is even higher than pure GLM, which indicates the poor lubrication ability of GLM@26MoS<sub>2</sub> composite. We further

investigated the lubrication ability of GLM@5MoS<sub>2</sub> composite under different applied loads and the results are shown in Fig. 9. The GLM@5MoS<sub>2</sub> composite holds better anti-friction ability than pure GLM under all experimental conditions and the GLM@5MoS<sub>2</sub> composite can exhibit better lubrication behaviour under high applied loads.

The worn conditions of disks and balls lubricated by pure GLM and GLM@5MoS<sub>2</sub> composite under applied loads of 2 N and 25 N are shown in Fig. 10. The average wear scar widths of different samples are marked in Fig. 10. It demonstrates that when GLM@5MoS<sub>2</sub> is utilized as lubricant, the wear scar tracks on disks and balls can be effectively reduced. And it is noticeable that the wear scar widths of GLM@5MoS<sub>2</sub> under loads of 2 N and 25 N are 247  $\mu\text{m}$  and 330  $\mu\text{m}$  respectively, which are smaller than that of pure GLM. Moreover, the wear rates on the steel balls are calculated based on eqn (1)–(3) and the results are shown in Fig. 11. The increase of applied load can reduce the wear rates of both pure GLM and GLM@5MoS<sub>2</sub> composite. Whereas GLM@5MoS<sub>2</sub> composite always holds lower wear rate value than that of pure GLM under all applied loads and the wear rate can be maximally reduced by 89% under the applied load of 2 N. Therefore, combined with friction coefficient curves, it can be concluded that GLM@5MoS<sub>2</sub> composite is conducive to improving anti-friction and anti-wear abilities of GLM matrix.

### 3.4 The lubrication mechanisms

For the sake of exploring the lubrication mechanisms of GLM@5MoS<sub>2</sub>, SEM images and EDS analyses of worn surfaces

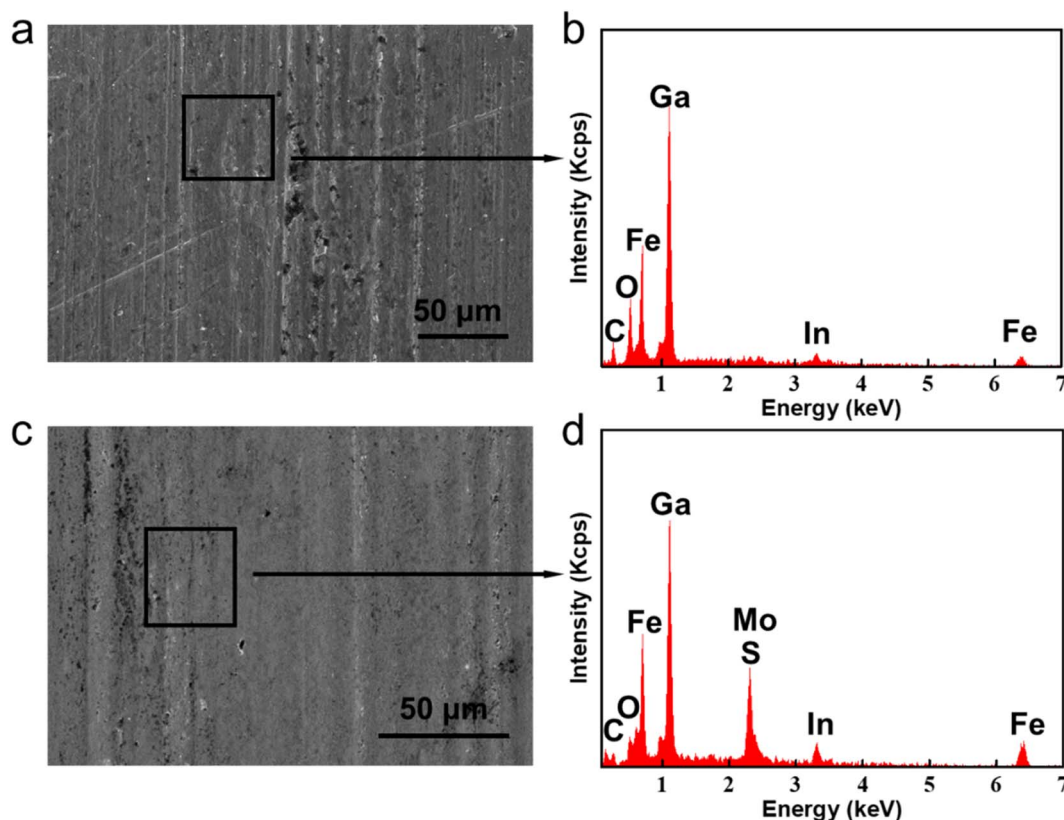


Fig. 12 SEM wear scar images and EDS analyses lubricated by (a) and (b) pure GLM, (c) and (d) GLM@5MoS<sub>2</sub> under 25 N.





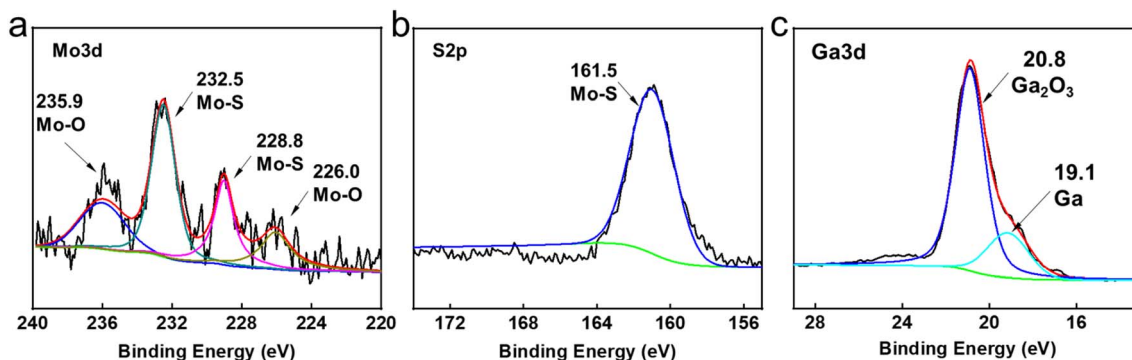


Fig. 13 High resolution XPS analyses of wear tracks lubricated by GLM@5MoS<sub>2</sub> under 25 N. (a) Mo3d, (b) S2p and (c) Ga3d.

are shown in Fig. 12. In comparison with the surface lubricated with pure GLM, less furrows are found on the surface lubricated by GLM@5MoS<sub>2</sub> composite. Combined with the EDS results, it could be concluded that there are some deposited tribo-films on the substrate, which are beneficial for improving lubrication abilities and mainly contain elements of Ga, Mo, S, O and In. To verify the chemical compositions of the tribo-films, XPS experiments are further carried out and the results are given in Fig. 13. The High resolution XPS analyses of Mo3d and Ga3d indicate the MoS<sub>2</sub> nanosheets and liquid gallium are oxidized slightly during the frictional process. Therefore, dominant compositions of tribo-films are Ga, MoS<sub>2</sub>, and oxides of Ga and Mo.

## 4. Conclusions

In summary, this study proposed a facile grinding process to integrate MoS<sub>2</sub> into GLM, thus forming GLM@MoS<sub>2</sub> composite with reversible rheological properties and desirable lubrication abilities. Because the hybridization mechanisms of GLM@MoS<sub>2</sub> composite are attributed to sticky layers of liquid metals' oxides, it is feasible to recover GLM by dissolving liquid metals' oxides. And the recovered GLM exhibits the similar Newtonian property with the original GLM. The addition concentration of MoS<sub>2</sub> nanosheets shows prominent effect on the dispersion and lubrication abilities of GLM@MoS<sub>2</sub> composite. GLM@5MoS<sub>2</sub> and GLM@12MoS<sub>2</sub> composites are able to reduce the friction coefficient and wear rate of pure GLM, while the excessive addition of MoS<sub>2</sub> nanosheets deteriorates the lubrication condition due to agglomeration problem. Furthermore, the enhanced lubricity of GLM@MoS<sub>2</sub> composite could be ascribed to the deposited tribofilms between frictional pairs, which are composed of Ga, MoS<sub>2</sub>, oxides of Ga and Mo. This study provided a feasible strategy to obtain GLM@MoS<sub>2</sub> composite with recoverable characteristic and enhanced lubrication ability, which could be expected to facilitate the application of GLM in lubrication and composite fields.

## Conflicts of interest

The authors declare no conflict of interest.

## Acknowledgements

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