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# Numerical analysis and device modelling of a lead-free $\text{Sr}_3\text{PbI}_3/\text{Sr}_3\text{SbI}_3$ double absorber solar cell for enhanced efficiency

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Halide perovskites are the most promising options for extremely efficient solar absorbers in the field of photovoltaic (PV) technology because of their remarkable optical qualities, increased efficiency, lightweight design, and affordability. This work examines the analysis of a dual-absorber solar device that uses  $\text{Sr}_3\text{SbI}_3$  as the bottom absorber layer and  $\text{Sr}_3\text{PbI}_3$  as the top absorber layer of an inorganic perovskite through the SCAPS-1D platform. The device architecture includes ZnSe as the electron transport layer (ETL), while the active layer consists of  $\text{Sr}_3\text{PbI}_3$  and  $\text{Sr}_3\text{SbI}_3$  with precise bandgap values. The bandgap value of  $\text{Sr}_3\text{SbI}_3$  is 1.307 eV and  $\text{Sr}_3\text{PbI}_3$  is 1.258 eV. By employing double-graded materials of  $\text{Sr}_3\text{PbI}_3/\text{Sr}_3\text{SbI}_3$ , the study achieves an optimized efficiency of up to 34.13% with a  $V_{\text{OC}}$  of 1.09 V, FF of 87.29%, and  $J_{\text{SC}}$  of 35.61  $\text{mA cm}^{-2}$ . The simulation explores the influence of absorber layer thickness, doping level, and defect density on electrical properties like efficiency, short-circuit current, open-circuit voltage, and fill factor. It also examines variations in temperature and assesses series and shunt resistances in addition to electrical factors. The simulation's output offers valuable insights and suggestions for designing and developing double-absorber solar cells.

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## 1. Introduction

The use of renewable energy sources, most notably solar power, is becoming more widely acknowledged as a viable way to meet the world's energy needs while also potentially reducing the adverse ecological consequences of conventional coal-based electricity industries. The imperative for high-performance, cost-effective solar panel technology has intensified in the context of addressing climate change driven by fossil fuel consumption.<sup>1</sup> Recently, inorganic perovskites have also been studied since they could be very helpful as materials for solar cell absorbers.<sup>2–8</sup> However, the inherent bandgap of absorber

materials poses a limitation on light absorption, constraining single-junction solar cells from reaching their theoretical efficiency limit, known as the Shockley–Queisser limit. The decrease in performance of single-junction solar cells is primarily attributed to the lack of absorption of photons with energies beneath the bandgap. Additionally, the conversion of photon energy into carriers, rather than generating unfettered electron–hole duos, leads to heating defeats, further diminishing device productivity without enhancing results. To circumvent the Shockley–Queisser limit, researchers are concentrating on double-absorber solar panels, aiming to strengthen device efficiency. While one-layer perovskite solar cells may demonstrate higher effectiveness in certain scenarios, double-absorber configurations offer avenues for efficiency improvement. Typically, the integration of two absorber layers aims to broaden the absorbance range of perovskite solar cells (PSCs) to establish a hybridization.

During this context, Zhang *et al.* introduced a dual-absorber solar cell constructed on  $\text{CsPbI}_x\text{Br}_{3-x}/\text{FAPbI}_y\text{Br}_{3-y}$ , achieving a power conversion efficiency (PCE) of 17.48%.<sup>9</sup> AlZoubi *et al.* conducted successful research on dual-absorber solar panels, achieving an increased 19.40% efficiency.<sup>10</sup> Using  $\text{CdTe}/\text{FeSi}_2$ , Rahman *et al.* created a numerical design for a double absorber solar cell that produced a noteworthy 27.35% power conversion efficiency.<sup>11</sup> Abedini-Ahangarkola *et al.* utilized SCAPS-1D to investigate the superior effectiveness of perovskite/perovskite

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dual-absorbing solar cells, achieving a total effectiveness of 30.29%.<sup>12</sup> Organometallic lead halide perovskite solar cells (PSCs) have garnered recent interest as a silicon-free solar power generating alternative to supplement conventional silicon photovoltaics.<sup>13,14</sup> Lead-based perovskites are safer than other materials; however, there are stability issues with them. Still, a lead-free alternative for PSCs that shows promise is tin-halide perovskites,<sup>15</sup> offering potentially higher theoretical power conversion efficiency, enhanced carrier mobilities, and improved light absorption compared to their lead-based counterparts.<sup>16</sup> Notably, perovskites based on  $\text{NaZnBr}_3$ , such as  $\text{NaZn}_{0.7}\text{Cu}_{0.3}\text{Br}_3$ , have been developed to address stability and efficiency issues.<sup>17</sup>  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  perovskites were deeply analyzed by the researchers in previous works and they showed that these materials will be very much effective for solar cell applications.<sup>18,19</sup> Reza *et al.* introduced that above 28% PCE was achieved by using  $\text{Sr}_3\text{SbI}_3$  perovskite as absorber in their work.<sup>20</sup> Therefore, researchers have gotten above 27% PCE by using  $\text{Sr}_3\text{PI}_3$  perovskite as absorber in their published work.<sup>21</sup>  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  have various benefits when used as absorbers in solar cells that are based on perovskites. To begin with, these materials have good visible-spectrum optical absorption, which is essential for effective solar energy harvesting. Additionally, because of their great chemical stability, the devices are less likely to break down over time and are more resilient.  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  are non-toxic, addressing health and environmental issues, in contrast to lead-based perovskites. Their easy production and integration into current solar cell topologies are facilitated by their straightforward cubic crystal structures. These materials can also be optimized to maximize solar performance because of their tunable bandgaps. Last but not least, their energy and manufacturing costs are decreased by their compatibility with low-temperature processing methods. So, we have tried to expand the performance of  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  perovskites based solar cells by arranging double absorber structure.

The ETL layer (n-type) is essential to the devices'  $J_{\text{SC}}$  and  $V_{\text{OC}}$ . The  $V_{\text{OC}}$  is greatly impacted by the band orientation at the absorber/buffer interface. The conduction band offset (CBO) allows us to classify the sort of band orientation at the moment of interaction as either cliff, plane, or spike. Interface recombination is inhibited by an interface spike; however, interface recombination is increased and  $V_{\text{OC}}$  levels are decreased by cliff-type band stretching.<sup>22</sup> In order to prevent blocking the electrons' passage from the absorber layer into the ETL layer, which would reduce the fill factor and current density, the spike's amplitude must be sufficiently minimal.<sup>23</sup> ZnSe (zinc selenide) is chosen as the charge carrier transport layer in this photovoltaic cell due to its favorable electronic properties, such as a suitable bandgap ( $\sim 2.7$  eV), which allows it to act as an efficient ETL. ZnSe exhibits reduced absorption losses due to its strong electron mobility and good transparency in the visible range. Furthermore, efficient electron extraction is facilitated while back-transfer of holes is prevented due to its conduction band alignment with absorber materials such as  $\text{Sr}_3\text{SbI}_3$ . Additionally, ZnSe creates stable interfaces between the absorber layer and the FTO substrate, promoting strong

adhesion and lowering interface recombination losses. Its appropriateness for these kinds of solar applications is further enhanced by its chemical stability and simplicity of manufacture. After depositing ZnSe using pulsed laser deposition (PLD) and analyzing the exceptionally preserved ZnSe layers optically and electrically, the bandgap, carrier concentration, and electron affinity in the ZnSe layers were determined.

Typically, the integration of two absorber layers aims to broaden the absorbance range of perovskite solar cells (PSCs) to establish hybridization. To our knowledge, the novel PSC prototype featuring the  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  heterojunction, which we intend to explore in this study, has not been previously investigated. Employing the SCAPS-1D software, we aim to model the behavior of this PSC setup with a heterojunction. Using the SCAPS-1D modelling instrument, a new dual-absorber solar cell was created and replicated, featuring a dual absorber layer composed of  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  as the superior and inferior absorbers, respectively. Assumptions within SCAPS-1D include visually and electrically lossless tunnelling connections between the superior and inferior absorbers. The performance of this prototype during simulation is primarily influenced by the thicknesses of the absorber layers, doping concentrations, and defect densities. These variables are meticulously examined to assess their impacts on the electrical characteristics of the model. Additionally, we analyze the effects of temperature variations, shunt resistance, series resistance, and rear contact electrode on the electrical accomplishment of the novel PSC prototype based on  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$ . In the simulation, ZnSe is selected as the layer responsible for electron transport.

## 2. Device construction and simulation techniques

### 2.1 Structure of the device

FTO glass was used as the substrate for the hole transport layer (HTL)-free perovskite solar cells (PSCs), whereas ZnSe was used for the electron transport layer (ETL). and either  $\text{Sr}_3\text{PI}_3$ ,  $\text{Sr}_3\text{SbI}_3$ , or a bilayer heterojunction of  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  as the light absorbance layer, with gold (Au) acting as the electrode. Fig. 1(a–c) illustrate the structures of these three types of PSCs. The layers of the suggested double absorber solar cell are as follows: Al/FTO/ZnSe/ $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3/\text{Au}$ , as depicted in Fig. 1(c). The proposed perovskites were named Device-I (Al/FTO/ZnSe/ $\text{Sr}_3\text{SbI}_3/\text{Au}$ ), Device-II (Al/FTO/ZnSe/ $\text{Sr}_3\text{PI}_3/\text{Au}$ ), and Device-III (Al/FTO/ZnSe/double absorber ( $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$ )/Au). If we alternate the absorber positions (Al/FTO/ZnSe/double absorber ( $\text{Sr}_3\text{SbI}_3/\text{Sr}_3\text{PI}_3$ )/Au) in Device-III, the device performances are decreased (PCE = 31.98%,  $V_{\text{OC}} = 1.04$  V, FF = 85.55%, and  $J_{\text{SC}} = 35.56$  mA cm<sup>-2</sup>). All simulations were conducted under standard conditions: temperature of 300 K, frequency of  $1.0 \times 10^6$  Hz, and standard illumination of AM 1.5 G 1 sun. While data from literary sources was used to optimize other layer properties, simulation was used to determine the optimal thickness of the absorber layer. This arrangement creates a perfect tunnel with no optical loss or electrical resistance between the two absorbers. To mitigate shifting and protect the superior layers



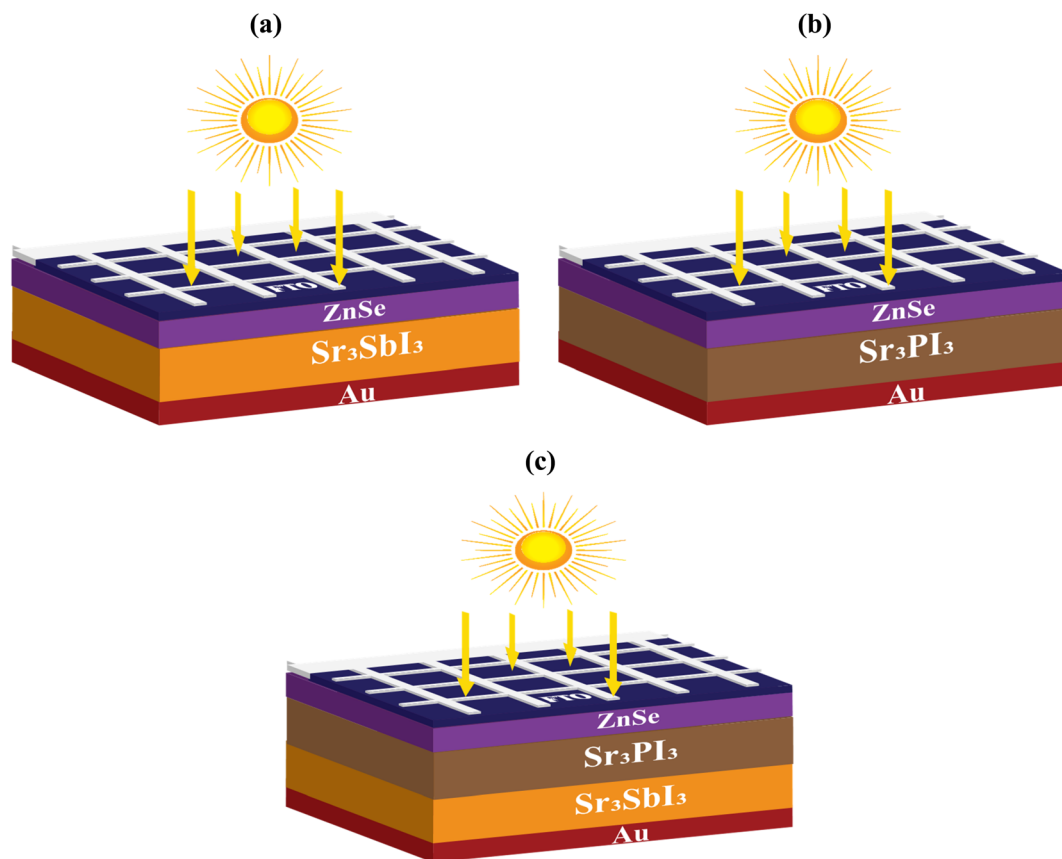


Fig. 1 Diagrammatic design configurations of (a) Device I, (b) Device II, and (c) Device III PV cells.

from solvent exposure and damage that sputters, dual-absorber solar cells include a conformal recombination layer amid absorber layers.

Table 1 lists the electrical parameters utilized in the simulations, with references to relevant computational and experimental studies found in the literature. Parameters such as layer thickness ( $t$ ), relative dielectric constant ( $\epsilon_r$ ), electron affinity ( $\chi$ ), electron and hole mobility ( $\mu_n$  &  $\mu_p$ ), bandgap ( $E_g$ ), thermal velocity ( $v_{te}$ ,  $v_{tp}$ ), donor and acceptor densities ( $N_D$  &  $N_A$ ), valence band and conduction band effective state densities ( $N_V$  &  $N_C$ ), and total defect concentration ( $N_t$ ) are included. Additionally,

Table 2 presents the interface qualities of the ZnSe/Sr<sub>3</sub>SbI<sub>3</sub>, ZnSe/Sr<sub>3</sub>PI<sub>3</sub>, and Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub> systems, allowing for the investigation of the impact of defect concentration while preserving a constant total defect density at the contact.

## 2.2 Simulation techniques

SCAPS-1D (version 3.3.0.7) is a sophisticated instrument for simulating solar cells, specifically crafted to examine the properties of individual layers in solar cells.<sup>26</sup> Established by Mark Burgelman of the University of Gent, Belgium's Department of Electronics and Information Systems, this software is

Table 1 SCAPS-1D simulation parameters for absorber, ETLs, and FTO

Parameters	Sr <sub>3</sub> SbI <sub>3</sub> (ref. 20)	Sr <sub>3</sub> PI <sub>3</sub> (ref. 21)	ZnSe <sup>24</sup>	FTO <sup>25</sup>
Layer thickness, $t$ ( $\mu\text{m}$ )	0.5	0.5	0.05	0.05
Band gap, $E_g$ (eV)	1.307	1.258	2.70	3.6
Electron affinity, $\chi$ (eV)	4.0	3.850	4.09	4.5
Dielectric permittivity (relative), $\epsilon_r$	5.40	5.90	10.0	10
Hole mobility, $\mu_h$ ( $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$ )	50	25	20	20
Electron mobility, $\mu_n$ ( $\text{cm}^2 \text{V}^{-1} \text{s}^{-1}$ )	50	20	50	100
VB effective density of states, $N_V$ ( $\text{cm}^{-3}$ )	$2.4 \times 10^{19}$	$1.7 \times 10^{19}$	$1.5 \times 10^{18}$	$1.8 \times 10^{19}$
CB effective density of states, $N_C$ ( $\text{cm}^{-3}$ )	$1.2 \times 10^{19}$	$1.03 \times 10^{19}$	$1.8 \times 10^{19}$	$2 \times 10^{18}$
Defect density, $N_t$ ( $\text{cm}^{-3}$ )	$1 \times 10^{12}$	$1 \times 10^{12}$	$1 \times 10^{14}$	$1 \times 10^{14}$
Shallow uniform acceptor density, $N_A$ ( $\text{cm}^{-3}$ )	$1 \times 10^{18}$	$1 \times 10^{18}$	0	0
Shallow uniform donor density, $N_D$ ( $\text{cm}^{-3}$ )	0	0	$1 \times 10^{17}$	$1 \times 10^{18}$



Table 2 Characteristics of interface used in heterojunction solar cells comprising Al/FTO/ZnSe/absorber (Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub>)/Au structure

Interface	Defect type	Capture cross section: electrons/holes (cm <sup>2</sup> )	Defect position above the highest EV (eV)	Reference for defect energy level	Energetic distribution	Total defect density (cm <sup>-2</sup> )
Sr <sub>3</sub> SbI <sub>3</sub> /ZnSe (Device-I)	Neutral	1 × 10 <sup>-19</sup>	0.06	Above the highest E <sub>v</sub>	Single	1.0 × 10 <sup>10</sup>
Sr <sub>3</sub> PI <sub>3</sub> /ZnSe (Device-II)	Neutral	1 × 10 <sup>-19</sup>	0.06	Above the highest E <sub>v</sub>	Single	1.0 × 10 <sup>10</sup>
Sr <sub>3</sub> SbI <sub>3</sub> /Sr <sub>3</sub> PI <sub>3</sub> (Device-III)	Neutral	1 × 10 <sup>-19</sup>	0.06	Above the highest E <sub>v</sub>	Single	1.0 × 10 <sup>10</sup>
Sr <sub>3</sub> PI <sub>3</sub> /ZnSe (Device-III)	Neutral	1 × 10 <sup>-19</sup>	0.06	Above the highest E <sub>v</sub>	Single	1.0 × 10 <sup>10</sup>

extensively utilized for analyzing different types of solar cells.<sup>27,28</sup> It provides the PV community with detailed insights into parameters such as PCE, V<sub>OC</sub>, FF, and J<sub>SC</sub> (short-circuit current density) for each layer. Those functionalities are achieved through fixing three essential equations integrated into the SCAPS-1D software: the Poisson eqn (1), continuity eqn (2) and (3), and charge transport eqn (4) and (5), which govern the behavior of charge carriers. These equations are as follows:<sup>29,30</sup>

$$\frac{\partial^2 \phi}{\partial x^2} = \frac{q}{\epsilon} (n(x) - p(x) + N_A(x) - N_D(x) - p_t(x) - N_t(x)) \quad (1)$$

In these equations, (*q*) represents the elementary charge,  $\epsilon$  denotes the dielectric constant, (*p*) signifies the hole concentration, (*n*) represents the electron concentration, (*N<sub>D</sub>*) stands for the doping concentration of donor-type, and (*N<sub>A</sub>*) represents the doping concentration acceptor-type.

$$\frac{\partial n}{\partial t} = \frac{1}{q} \frac{\partial J_n}{\partial x} + (G_n - R_n) \quad (2)$$

$$\frac{\partial p}{\partial t} = -\frac{1}{q} \frac{\partial J_p}{\partial x} + (G_p - R_p) \quad (3)$$

here, (*G<sub>n</sub>*) indicates the generation rate for electrons, (*G<sub>p</sub>*) denotes the generation rate for holes, (*R<sub>n</sub>*) represents the recombination rate for electrons, (*R<sub>p</sub>*) signifies the recombination rate for holes, (*J<sub>p</sub>*) represents the hole current density, and (*J<sub>n</sub>*) is the electron current density.

$$J_n = qD_n \frac{\partial n}{\partial x} - q\mu_n n \frac{\partial \phi}{\partial x} \quad (4)$$

$$J_p = qD_p \frac{\partial p}{\partial x} - q\mu_p p \frac{\partial \phi}{\partial x} \quad (5)$$

(*D<sub>n</sub>*) denotes the electron diffusion coefficient, (*D<sub>p</sub>*) signifies the hole diffusion coefficient, ( $\mu_n$ ) represents the electron mobility, and ( $\mu_p$ ) denotes the hole mobility. Eqn (6) and (7) illustrate the connection between important PV characteristics, as demonstrated below.<sup>31</sup>

$$FF = \frac{P_{\max}}{P_{\text{in}}} = \frac{I_{\max} \times V_{\max}}{V_{\text{oc}} \times I_{\text{sc}}} \quad (6)$$

$$PCE = \frac{I_{\text{sc}} \times V_{\max} \times FF}{P_{\text{in}}} \quad (7)$$

In these equations, (*P<sub>in</sub>*) represents the input solar energy, and (*P<sub>max</sub>*) denotes the maximum power output.

## 3. Result and discussion

### 3.1 Left contact work function's effect on solar cell performance

The productivity and general functioning of the solar panel are affected *via* the left contact, which has a substantial influence on the cellular performance.<sup>32</sup> To maximize efficiency, the left contact, which is usually a component of the electrical contacts that extract current, needs to have low resistive losses. Inadequate contact may result in higher series resistance, which lowers power output and current flow. To preserve stability and endurance, it must also guarantee strong adhesion and little chemical contact with the semiconductor. Inadequately engineered connections may result in shading effects, obstructing light, and decreasing the active area. Improved charge carrier collection and reduced recombination losses are two benefits of optimal left contact design that directly impact the effectiveness and dependability of the solar panel. The best metal for the left contact is chosen by comparing its work function, which ranges from 4.85 eV to 5.47 eV. Fig. 2(a–c) display the PV parameters that were obtained for Devices I, II, and III with various left contacts. It has been observed that with gold (Au) as the left contact, we have gotten maximum performances from Devices I, II, and III. Once Au and Al were chosen as the left and right contacts, respectively, we observed maximum PCE values of 30.56, 31.13, and 34.14%, FF values of 88.63, 83.93, and 87.29%, J<sub>SC</sub> values of 32.402, 33.936, and 35.615 mA cm<sup>-2</sup>, and V<sub>OC</sub> values of 1.064, 1.074, and 1.098 V for Devices-I, II, and III. Table 3 shows the properties for front and back contacts.

### 3.2 Band diagram

Fig. 3(a–c) depict three different kinds of HTL-free PSCs' band topologies, featuring different materials that absorb light (Sr<sub>3</sub>SbI<sub>3</sub>, Sr<sub>3</sub>PI<sub>3</sub>, Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub>) bilayer combination of the perovskite solar cells (PSCs), offering a comprehensive insight into their characteristics. Within this context, the symbols E<sub>C</sub> (eV), E<sub>n</sub> (eV), E<sub>v</sub> (eV), and E<sub>F</sub> (eV) denote various energy levels within the band structure, namely denoting the valence band's maximum energy level, or the Fermi level for holes, the Fermi





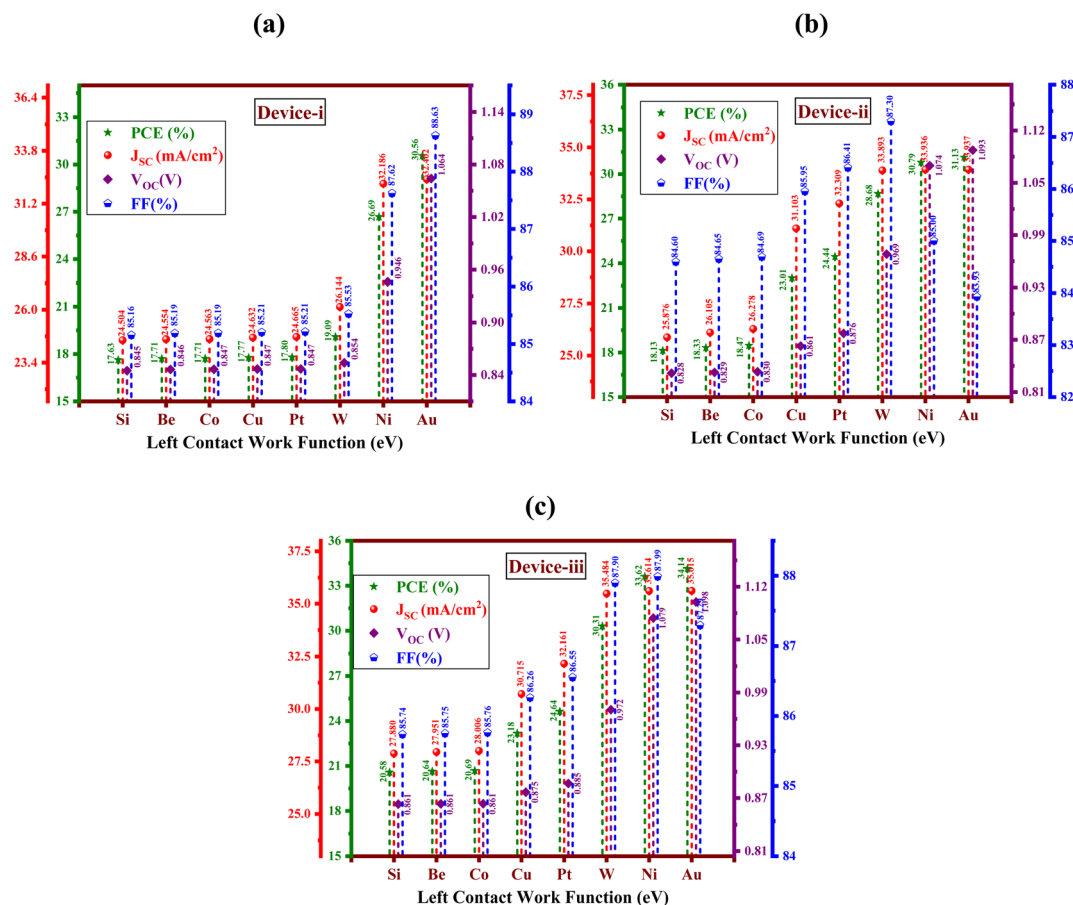


Fig. 2 Variation of left contact metal for (a) Device-I, (b) Device-II, and (c) Device-III.

level for electrons, and the conduction band's minimum energy level, respectively. The discrepancy in energy levels between the lowest point of the conduction band (CB) electrons in the perovskite layer and the electron transport layer (ETL) is referred to as the conduction band offset (CBO), whereas the difference between the highest point of the valence band (VB) holes in the perovskite layer and the hole transport layer (HTL) is termed the valence band offset (VBO). In this study, the bandgaps of  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  perovskite materials are determined to be 1.258 eV and 1.307 eV, correspondingly. The fluorine-doped tin oxide (FTO) window layer's energy gap is measured to be 3.6 eV, while the n-type zinc selenide (ZnSe) ETL layer exhibits energy gaps ( $E_g$ ) of 2.70 eV.

### 3.3 Absorption coefficient of all layers

An essential indicator of a material's capacity to absorb light energy is its optical absorption coefficient, which has a significant impact on a solar panel's power conversion efficiency (PCE).<sup>33,34</sup> The initial absorption peak is especially important for solar cells since it shows the exact light wavelengths that a material can absorb.<sup>35–37</sup> Materials such as  $\text{Sr}_3\text{PI}_3$ ,  $\text{Sr}_3\text{SbI}_3$ , ZnSe, and FTO are related to the FTO/ZnSe/absorber ( $\text{Sr}_3\text{SbI}_3/\text{Sr}_3\text{SbI}_3$ ) SC structure. Fig. 4 displays the variations in the absorption coefficient at different wavelengths for the materials  $\text{Sr}_3\text{PI}_3$ ,  $\text{Sr}_3\text{SbI}_3$ , ZnSe, and FTO. The absorption coefficient for  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  materials surprisingly exhibits high peaks at 200 nm wavelength, but the FTO material exhibits a peak at

Table 3 Back and front contact parameters used in simulation

Parameters	Left contact (back)	Right contact (front)
Surface recombination velocity of electrons ( $\text{cm s}^{-1}$ )	$1 \times 10^5$	$1 \times 10^7$
Surface recombination velocity of holes ( $\text{cm s}^{-1}$ )	$1 \times 10^7$	$1 \times 10^5$
Majority carrier barrier height (eV) relative to EF	-0.1630	-0.2400
Majority carrier barrier height (eV) relative to EV	-0.2453	-0.2580
Work function (eV)	Au (5.47)	Al (4.26)
Temperature (K)	275–475	



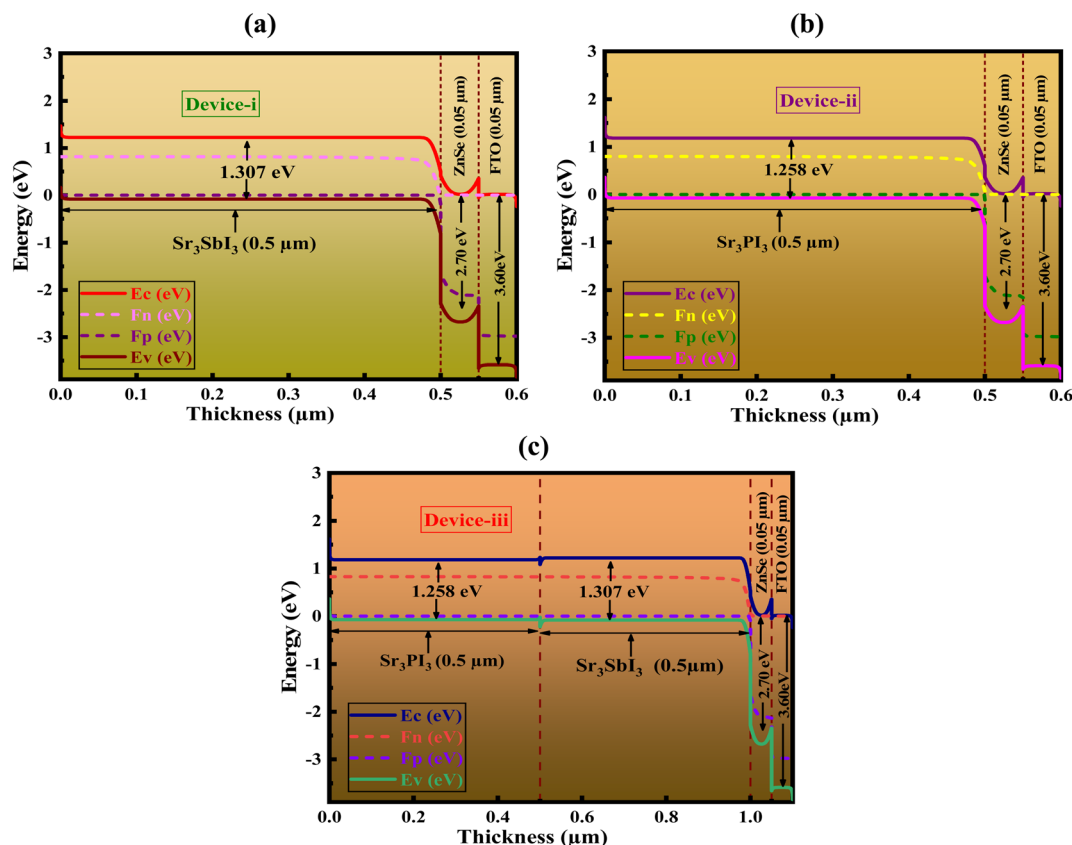


Fig. 3 Band arrangement of three types of HTL-free PSCs, featuring different light absorber materials: (a)  $\text{Sr}_3\text{SbI}_3$ , (b)  $\text{Sr}_3\text{PI}_3$ , (c)  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  bilayer combination.

174 nm wavelength. On the other hand, the absorption coefficient for ZnSe material surprisingly exhibits high peaks at the 210 nm wavelength. Each substance's optical absorption spectrum displays the maximum absorption sites in the visible and ultraviolet light spectrums. According to Fig. 4(a–d), the absorption peaks for  $\text{Sr}_3\text{PI}_3$ ,  $\text{Sr}_3\text{SbI}_3$ , ZnSe, and FTO materials are  $198\,956.35\text{ cm}^{-1}$ ,  $193\,593.72\text{ cm}^{-1}$ ,  $113\,827.57\text{ cm}^{-1}$ , and  $100\,000\text{ cm}^{-1}$ , respectively. The following tactics should be taken into consideration to make sure that target materials with bandgaps of 1.258 and 1.307 eV exhibit enough light absorption in the visible range for high-performance solar cells.

**3.3.1 Doping and alloying.** To move the absorption edge closer to the visible spectrum, modify the bandgap by doping or alloying with additional elements.

**3.3.2 Layer thickness optimization.** Optimize the thickness of the material layers to improve absorption of light while avoiding appreciable increases in recombination losses.

**3.3.3 Antireflective coatings.** To improve light absorption and decrease reflection losses, apply antireflective coatings to the surface of solar cells.

**3.3.4 Light trapping structures.** To improve absorption, include light-trapping structures in your material, such as photonic crystals or textured surfaces, which extend the light's travel length within it.

In order to optimize the material's performance for solar cell applications, these techniques can aid in adjusting its optical characteristics.

#### 3.4 Influence of the thickness, defect, and doping density of the single absorber layer

Fig. 5(a) illustrates the result of changing the absorber's thickness between three hundred and three thousand nanometers in order to figure out how to get the best results from our two simulated single absorber-based systems. An essential factor in increasing the efficiency of narrow-film photovoltaic cells is the thickness of the absorber layer.<sup>38</sup> As soon as Device-II's absorber thickness increased during optimization, the reverse saturation current rose, but the  $V_{\text{OC}}$  decreased even with a slight extension. However, with regard to device I, the variation in thickness barely affects the  $V_{\text{OC}}$ . With thickness increasing, the spectral reaction grew at extended wavelengths, causing the  $J_{\text{SC}}$  to rise and ultimately achieve an oversaturated value for all suggested gadgets. The thicker absorber in Device-II caused the structures to exhibit a noticeable FF rise, but in Device-I, it was constant. For devices I and II, efficiency was increased by using the proper thickness of absorber on both sides of 1000 nm. As the absorber layer thickens, more photons are absorbed, and the rate of recombination rises.<sup>21</sup> Therefore, the optimal thickness for the



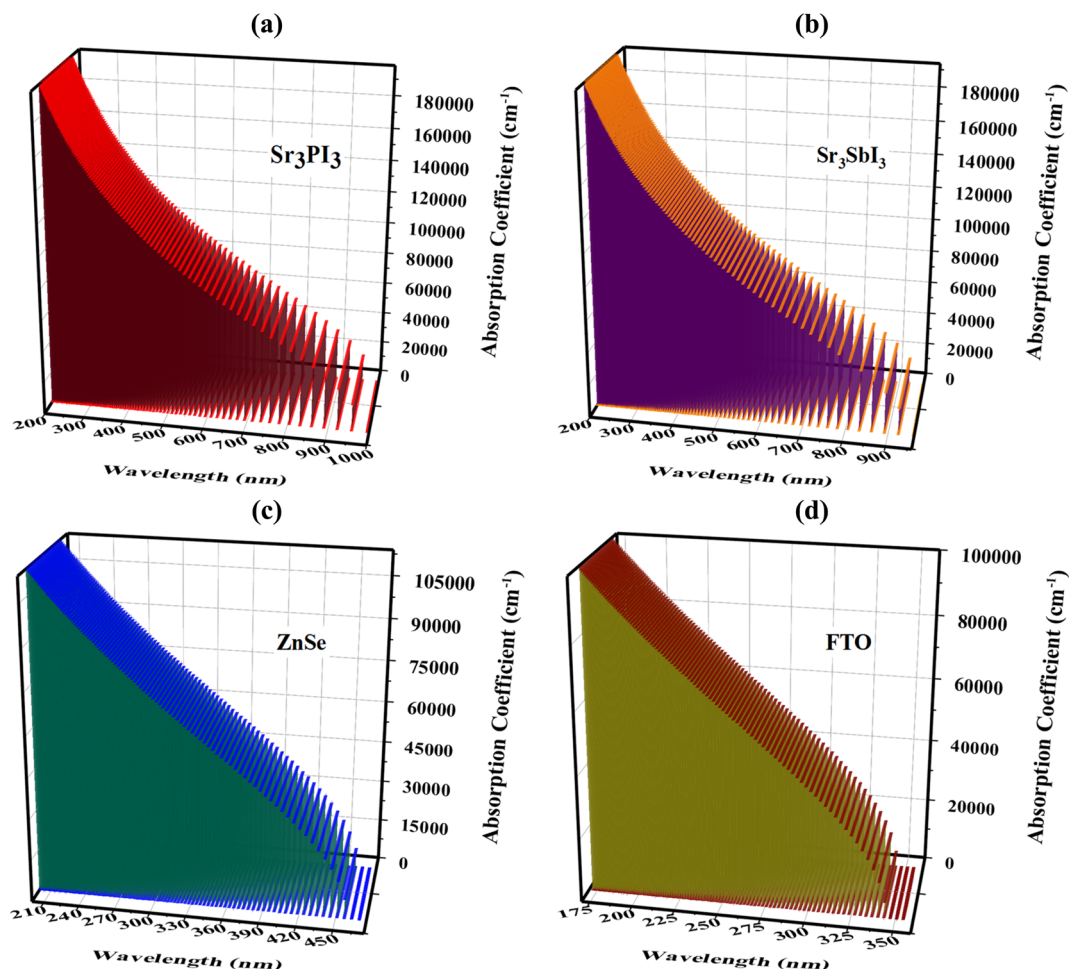


Fig. 4 Absorption coefficient of Al/FTO/ZnSe/absorber ( $\text{Sr}_3\text{SbI}_3/\text{Sr}_3\text{PI}_3$ )/Au ideal solar cell construction for the following materials: (a)  $\text{Sr}_3\text{PI}_3$ , (b)  $\text{Sr}_3\text{SbI}_3$ , (c) ZnSe, and (d) FTO.

absorber in the investigation was found to be 1000 nm in order to improve execution for Device-I and II incongruous structures. The optimal thickness values for Device-I were determined to be 30.5559% for PCE, 88.63% for FF, 32.40222  $\text{mA cm}^{-2}$  for  $J_{\text{SC}}$ , and 1.063996 V for  $V_{\text{OC}}$ . PCE of 31.1272%, FF of 83.9314%,  $J_{\text{SC}}$  of 33.93652  $\text{mA cm}^{-2}$ , and  $V_{\text{OC}}$  of 1.092819 V were measured for device II.

Recombination may be triggered by changes to the absorber layer's defect density ( $N_t$ ) in photovoltaic systems, impede the charge carriers' progress, and compromise the durability of the device; inconsistent defect allocation all over the absorber layer can affect optical properties that affect photon absorption and can also result in spatial differences in device performance; the only ways to maximize PV efficiency and reliability are to minimize fault density and ensure homogeneity in the absorber layer. The impact of the absorber layer's  $N_t$  on the PV characteristics at a thickness of 1000 nm is illustrated in Fig. 5(b). The consequences of  $N_t$  between  $10^{10}$  and  $10^{18} \text{ cm}^{-3}$  on Devices I and II were also examined. In Devices I and II, PCE, FF,  $J_{\text{SC}}$ , and  $V_{\text{OC}}$  significantly reduced from 30.60 to 8.46% and 31.31 to 8.36%, 88.66 to 72.04% and 87.18 to 72.16%, 32.402 to 17.151  $\text{mA cm}^{-2}$  and 33.936 to 15.546  $\text{mA cm}^{-2}$ , 1.065 to 0.684 and

1.126 to 0.745 V, respectively, even though  $N_t$  increased from  $10^{17} \text{ cm}^{-3}$ . For the purposes of additional computations,  $10^{12} \text{ cm}^{-3}$  is chosen as the ideal  $N_t$  worth for the absorbers.

The absorber layer's acceptor density ( $N_A$ ) was adjusted from  $10^{12}$  to  $10^{20} \text{ cm}^{-3}$  to evaluate the effect of the absorber's  $N_A$  on the PV characteristics. Fig. 5(c) shows how  $J_{\text{SC}}$ ,  $V_{\text{OC}}$ , PCE, and FF fluctuate according to the choice of  $N_A$ . The PSC's  $J_{\text{SC}}$  stayed consistent at an approximately set amount as the  $N_A$  was raised during optimization. The hole's Fermi energy level collapses as the absorber layer's  $N_A$  grows, increasing the  $V_{\text{OC}}$  in Device-II but remaining constant in Device-I. The built-in potential grows as the absorber layer's  $N_A$  expands, and the boost in charge separation is an additional consideration contributing to the development of  $V_{\text{OC}}$ . However, when the absorber layer's  $N_A$  value surpassed  $10^{16} \text{ cm}^{-3}$ , the PCE and FF rose. Regarding the variant of  $N_A$  from  $10^{12}$  to  $10^{20} \text{ cm}^{-3}$ , the maximum ideals obtained for the  $V_{\text{OC}}$ ,  $J_{\text{SC}}$ , FF, and PCE were 1.066 V, 32.402  $\text{mA cm}^{-2}$ , 88.73%, and 30.61% for Device-I, and 1.147 V, 33.941  $\text{mA cm}^{-2}$ , 87.65%, and 34.14% for Device-II. As mentioned in the paper, this could be the outcome of a higher number of defect states due to an increase in the  $N_A$  of the absorber stratum.



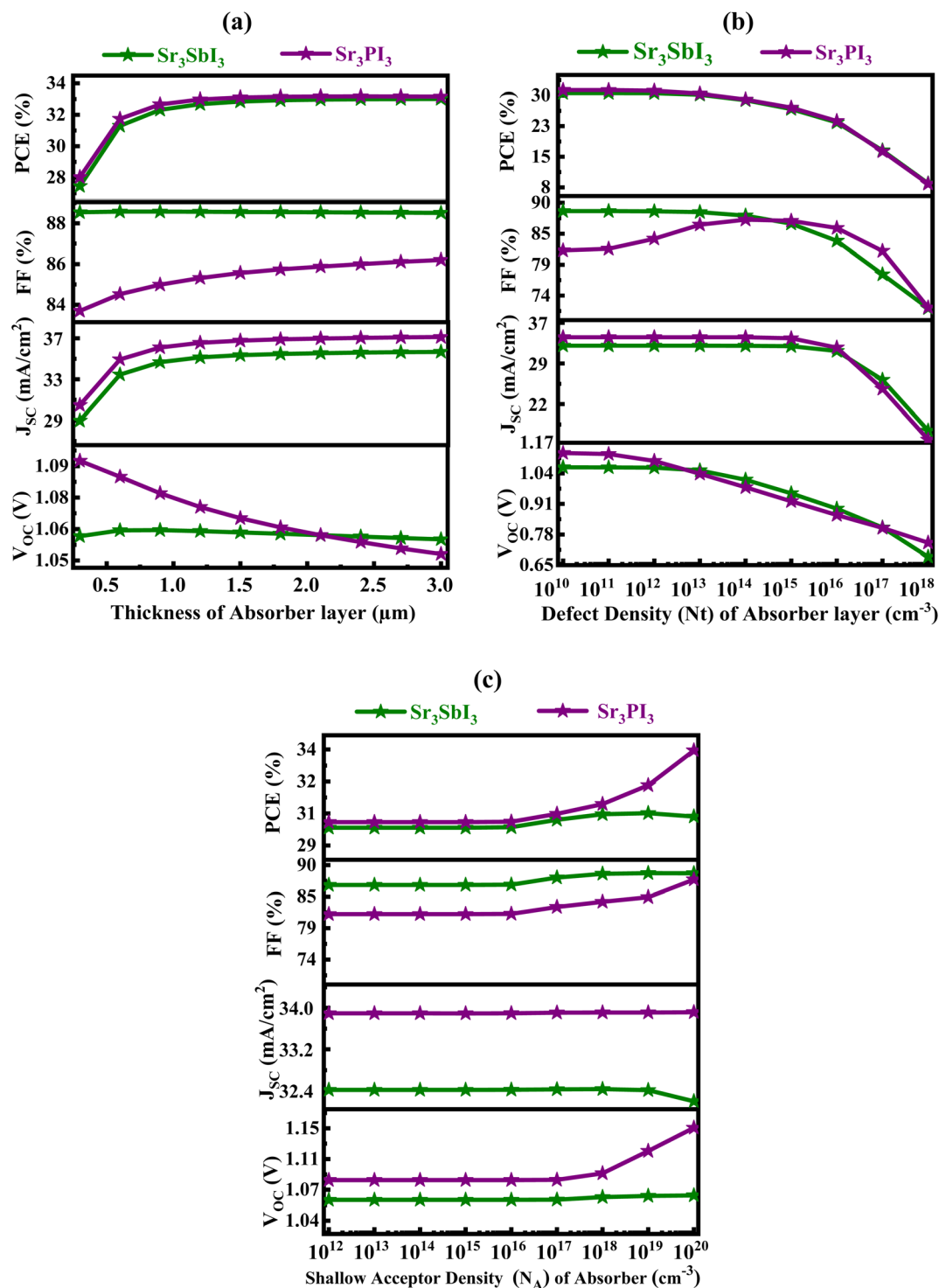


Fig. 5 Impact of (a) thickness, (b) defect density, and (c) doping concentration of absorber layer on the solar cell's performance for Devices I and II.

### 3.5 Impact of active layer thickness on the output parameters of double absorber device

Fig. 6 illustrates the cumulative sway of the thicknesses of the double perovskite absorber layer (PAL). The  $x$ -axis represents the thickness of  $\text{Sr}_3\text{PI}_3$ , while  $\text{Sr}_3\text{SbI}_3$  thickness is depicted on the  $y$ -axis. Through simulation models varying the PAL

thicknesses from 300 nm to 3000 nm, the compatibility of different thickness combinations is evaluated, as depicted in Fig. 6(a–d). The photovoltaic (PV) outputs of the PSCs, or perovskite solar cells, are scrutinized to discern the optoelectrical qualities beneath AM 1.5G illumination. It is observed that the  $V_{oc}$  peaks at smaller PAL thickness combinations, reaching up to 1.109 V, but declines with increasing PAL





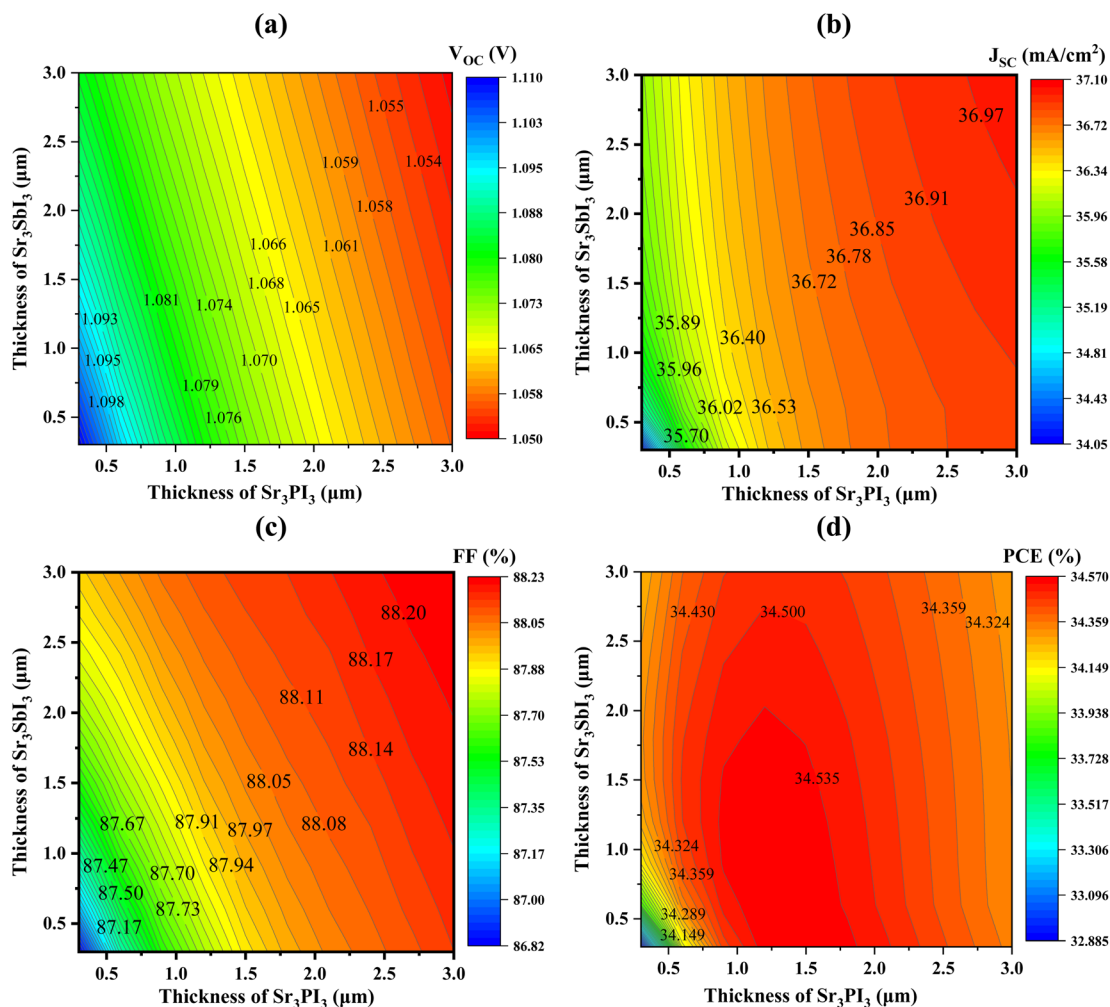


Fig. 6 The electrical parameters, encompassing (a)  $V_{OC}$  (b)  $J_{SC}$  (c) FF and (d) PCE, as determined by altering the thickness of the both layers that are active.

thickness due to heightened recombination rates. Concerning the short-circuit current density ( $J_{SC}$ ), a  $Sr_3PI_3$  thickness of approximately  $1 \mu m$  yields superior results, offering up to  $36.97 \text{ mA cm}^{-2}$ . Conversely, lower thickness values of  $Sr_3PI_3$  and  $Sr_3SbI_3$  lead to reduced  $J_{SC}$  due to inadequate photon absorption within the PALS, achieving around  $34.12 \text{ mA cm}^{-2}$ , thereby adversely affecting efficiency. The contour plot in Fig. 6(c) demonstrates that a double PAL setup yields a maximum fill factor (FF) of 88.22% at variations in thickness values. Lastly, the collective impact of PAL thicknesses on power conversion efficiency (PCE) is depicted in Fig. 6(d), wherein an optimized value of 34.1395% is obtained using a combined thickness of  $0.5 \mu m$  both for  $Sr_3PI_3$  and  $Sr_3SbI_3$ . This aligns with the  $35.61451 \text{ mA cm}^{-2}$   $J_{SC}$  values under  $0.5 \mu m$  and  $0.5 \mu m$  absorber thickness, as PCE is directly proportional to  $J_{SC}$ . The contour analysis furnishes valuable insights into PSC device investigations.

### 3.6 Effect of active layer doping concentration on the performance of double absorber device

The absorption layer within the perovskite material serves to capture photons released by light, thereby generating electron–

hole pairs. Introducing doping to this layer has the potential to enhance carrier concentration, thereby aligning the energy bands of the hybridization with the electron transport layer and consequently enhancing solar cell performance. Our investigation delves into the impact of  $N_A$  variation within the  $Sr_3PI_3$  and  $Sr_3SbI_3$  layers, spanning from  $1 \times 10^{12}$  to  $1 \times 10^{20} \text{ cm}^{-3}$ . Fig. 7(a–d) elucidate the sway of  $N_A$  on the electrical parameters of the two absorber layers. Notably, our findings indicate that the perovskite solar cell prototype exhibits superior performance when the  $N_A$  level in the  $Sr_3PI_3$  and  $Sr_3SbI_3$  layers surpasses  $1 \times 10^{17} \text{ cm}^{-3}$ , as evidenced in Fig. 7(d).

Indeed, when the  $N_A$  in the  $Sr_3PI_3$  layer exceeds that of the  $Sr_3SbI_3$  layer, it facilitates enhanced mobility of holes and electrons within the absorber layer. The fill factor experiences significant influence from variations in  $N_A$ , as depicted in Fig. 7(c). This variation in  $N_A$  levels within the absorber layer instigates an internal electrical field, leading to substantial electron emission from the solar cell. Consequently, this phenomenon results in a reduction in voltage, as demonstrated in Fig. 7(a). Conversely, when the  $N_A$  level in the  $Sr_3SbI_3$  layer surpasses that of the  $Sr_3PI_3$  layer, it impedes the flow of particles, causing the solar panel to function as an open circuit.





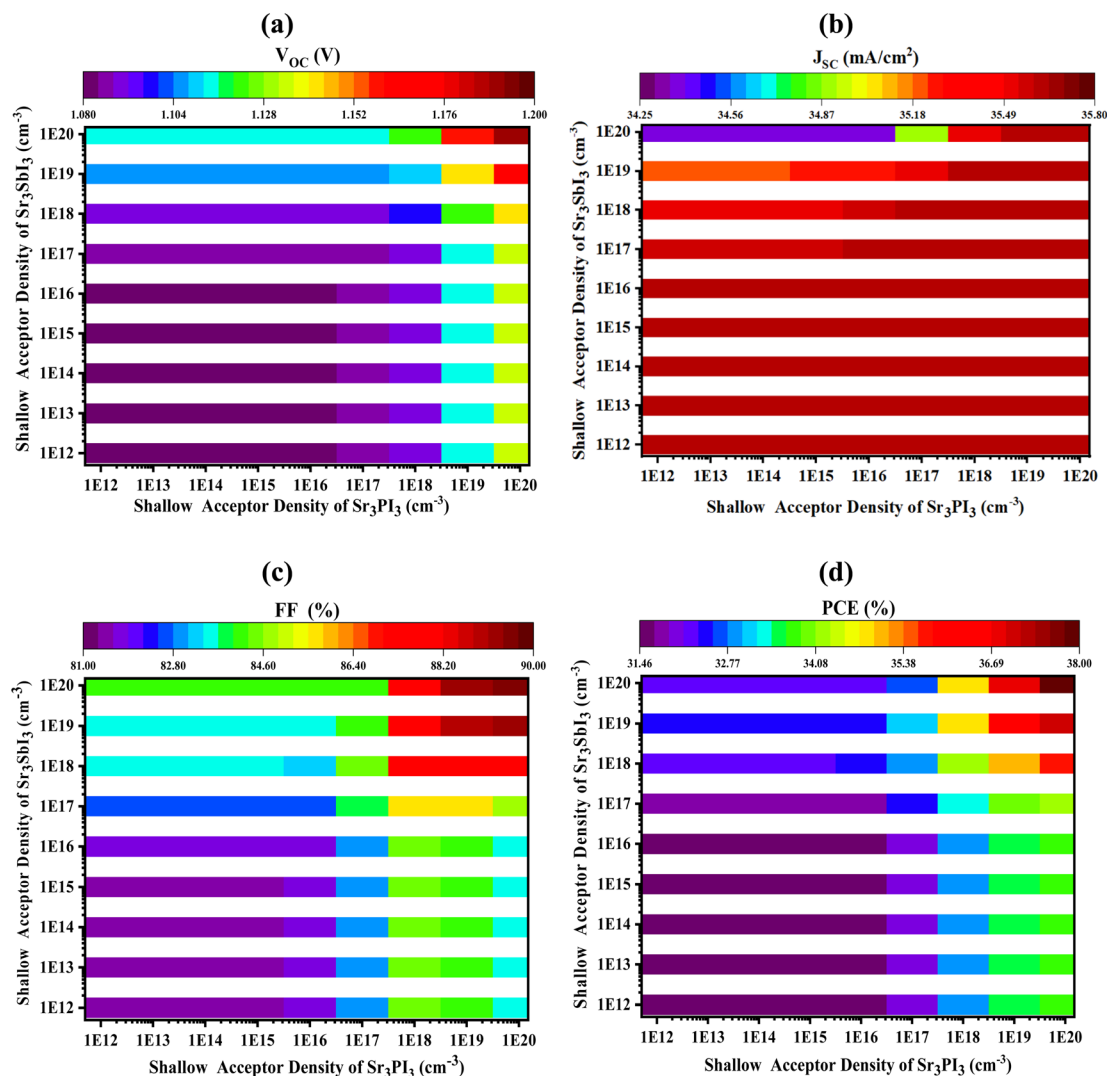


Fig. 7 Effect of active layer doping on electrical properties of PSCs: (a)  $V_{\text{OC}}$  (b)  $J_{\text{SC}}$  (c) FF and (d) PCE.

Fig. 7(d) elucidates that the PCE of the PSC's highest points at a  $N_{\text{A}}$  level of  $1 \times 10^{18} \text{ cm}^{-3}$  for  $\text{Sr}_3\text{PI}_3$  and  $1 \times 10^{18} \text{ cm}^{-3}$  for  $\text{Sr}_3\text{SbI}_3$  perovskite materials, achieving approximately 34.13% with a thickness of 500 nm and 500 nm for  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$ , respectively. As  $N_{\text{A}}$  increases, all electrical characteristics of the PSC improve except for the  $J_{\text{SC}}$ . However, the  $V_{\text{OC}}$  reaches 1.098137 V at the optimum  $N_{\text{A}}$  of  $1 \times 10^{18} \text{ cm}^{-3}$  for both  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  perovskite materials (Fig. 7(a)). At the optimized  $N_{\text{A}}$  for both PALs, the maximum  $J_{\text{SC}}$  reaches 35.61451  $\text{mA}/\text{cm}^2$  (Fig. 7(b)). Additionally, the FF reaches 87.2919% at this optimized  $N_{\text{A}}$  (Fig. 7(c)).

### 3.7 Impact of active layer defect density on the performance of double absorber device

Fig. 8(a–d) depict the variance in defect density ( $N_{\text{t}}$ ) within the perovskite absorber layer (PAL), spanning from  $1 \times 10^{10}$  to  $1 \times 10^{18} \text{ cm}^{-3}$ . Our findings reveal that  $N_{\text{t}}$  exerts a significant influence on the electrical parameters, as demonstrated in Fig. 8(a–d). The investigation focuses on both the  $\text{Sr}_3\text{PI}_3$  and

$\text{Sr}_3\text{SbI}_3$  absorber layers. Photovoltaic characteristics exhibit a decline with increasing  $N_{\text{t}}$  in the absorber layer, indicating a clear correlation between  $N_{\text{t}}$  and carrier trapping within the solar cell.<sup>39</sup> Higher  $N_{\text{t}}$  accelerates carrier recombination by trapping carriers, resulting in energy loss as carriers collide within the crystal lattice, thereby facilitating recombination due to reduced carrier energy levels. The escalating recombination process with increasing trap density leads to a deterioration in PSC performance, potentially causing device overheating. Thus, maintaining  $N_{\text{t}}$  within acceptable limits, approximately  $10^{12} \text{ cm}^{-3}$ , is crucial, based on acceptable current and voltage thresholds from both the  $\text{Sr}_3\text{SbI}_3$  layer (1.307 eV) and the  $\text{Sr}_3\text{PI}_3$  layer (1.258 eV).

Fig. 8(d) demonstrates that the PCE peaks at a  $N_{\text{t}}$  of  $1 \times 10^{12} \text{ cm}^{-3}$  for both perovskite materials, reaching nearly 34.13% for a thickness of 500 nm for  $\text{Sr}_3\text{PI}_3$  and 500 nm for  $\text{Sr}_3\text{SbI}_3$  PALs. As  $N_{\text{t}}$  increases, all electrical characteristics of the PSC decrease. However, the  $V_{\text{OC}}$  extends its peak value of 1.098137 V at a  $N_{\text{t}}$  of  $1 \times 10^{12} \text{ cm}^{-3}$  for both perovskite materials (Fig. 8(a)). The  $J_{\text{SC}}$



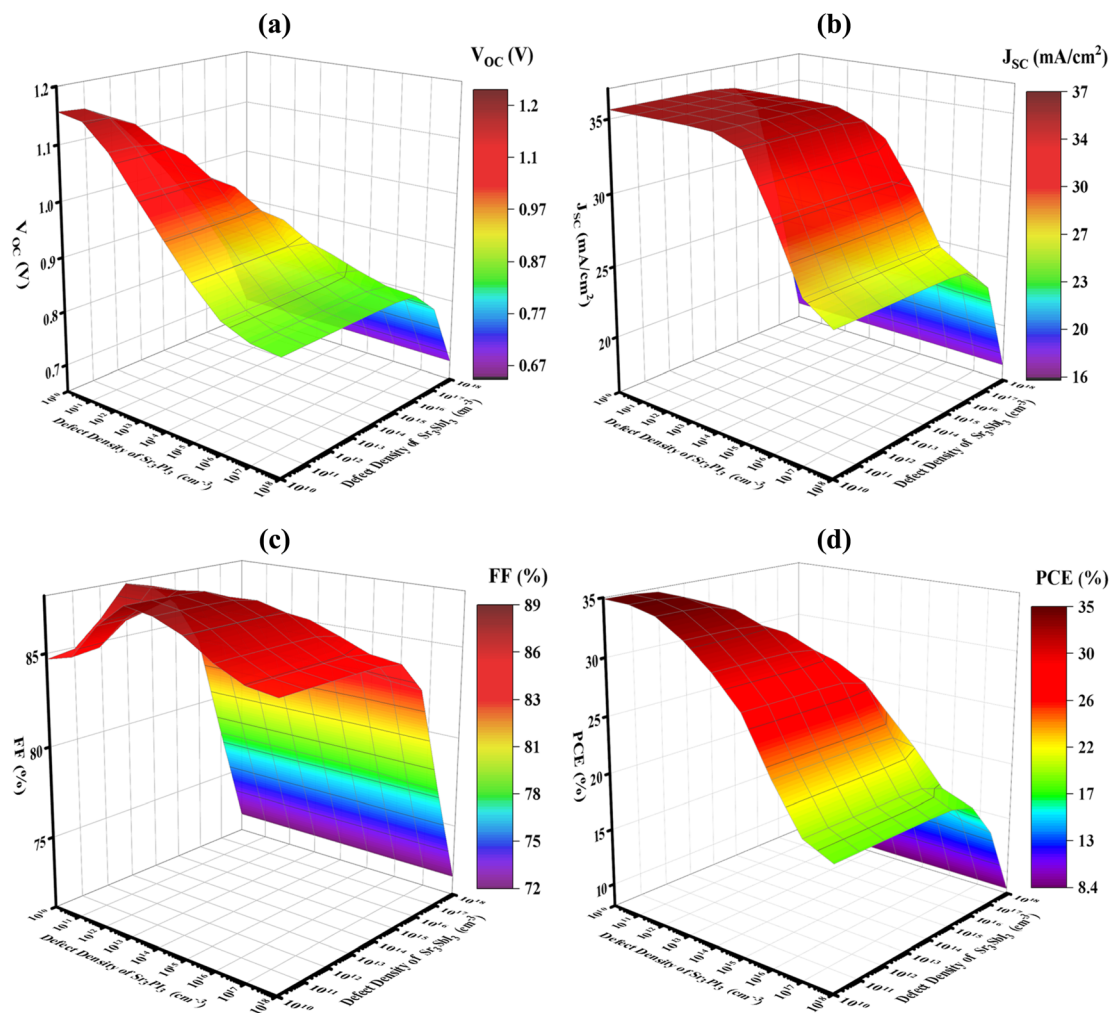


Fig. 8 Influence of active layer defect density on electrical properties of PSCs: (a)  $V_{OC}$  (b)  $J_{SC}$  (c) FF and (d) PCE.

exhibits a continuous decrease with increasing  $N_t$ , sharply declining at elevated levels. At an optimized  $N_t$  of  $1 \times 10^{12} \text{ cm}^{-3}$  for both PALs, the maximal  $J_{SC}$  reaches  $35.61451 \text{ mA cm}^{-2}$  (Fig. 8(b)). Additionally, FF reaches 87.2919% at this optimized  $N_t$  (Fig. 8(c)).

### 3.8 Effects of the ETL's thickness and doping density

The thickness of the ETL layer significantly affects the power output of solar energy systems,<sup>40</sup> as Fig. 9(a) illustrates. By allowing charged particles to travel more readily from the absorber layer towards the electrode, buffer layers improve the durability and effectiveness of these kinds of devices. The thickness of the ETL layer impacts a number of PV device qualities, comprising energy carrier recombination, light absorption, and resistance to layer-to-layer contact. More expansive band gaps and narrower ETL layers successfully transport virtually all incoming photons to the  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  absorber layers, increasing the absorption of light in the cells. The  $V_{OC}$  and  $J_{SC}$  for Devices I, II, and III stayed nearly constant at 1.063, 1.092, 1.098 V, and 32.397, 33.931, 35.601  $\text{mA cm}^{-2}$ ,

respectively, in spite of the rise in the thickness of the ETL stratum. For Device II, the FF and PCE values varied from 86.71% to 83.93% and 32.24 to 31.10%, but for Devices I and III, they were constant at 88.63%, 87.29%, and 30.54%, 34.12%, respectively.

Fig. 9(b) displays the PV qualities of Devices I, II, and III in relation to the donor concentration ( $N_D$ ) of ETL. As  $N_D$  increased from  $10^{12}$  to  $10^{20} \text{ cm}^{-3}$ , FF and PCE for Devices I, II, and III stayed constant at 87.60, 84.53, 86.33%, and 30.22, 31.37, 33.78%. After that, there was a discernible rise in PCE and FF, from 30.22 to 30.60%, 31.37 to 32.99%, 33.78 to 34.20%, and 87.60 to 88.75%, 84.53 to 87.93%, 86.33 to 87.41%, respectively, for Devices I, II, and III. However, despite the rise in the  $N_D$  of the ETL layer, the  $V_{OC}$  and  $J_{SC}$  for Devices I, II, and III remained almost unchanged at 1.064, 1.093, 1.098 V and 32.403, 33.938, and 35.615  $\text{mA cm}^{-2}$ , respectively. The ideal configuration was determined to be Devices I, II, and III with an  $N_D$  of  $10^{17} \text{ cm}^{-3}$ . This improvement in FF might possibly be attributed to the significant decrease in series resistance ( $R_s$ ) and the increase in the internal electric field. The outcomes of this investigation are in line with earlier findings.<sup>41,42</sup>



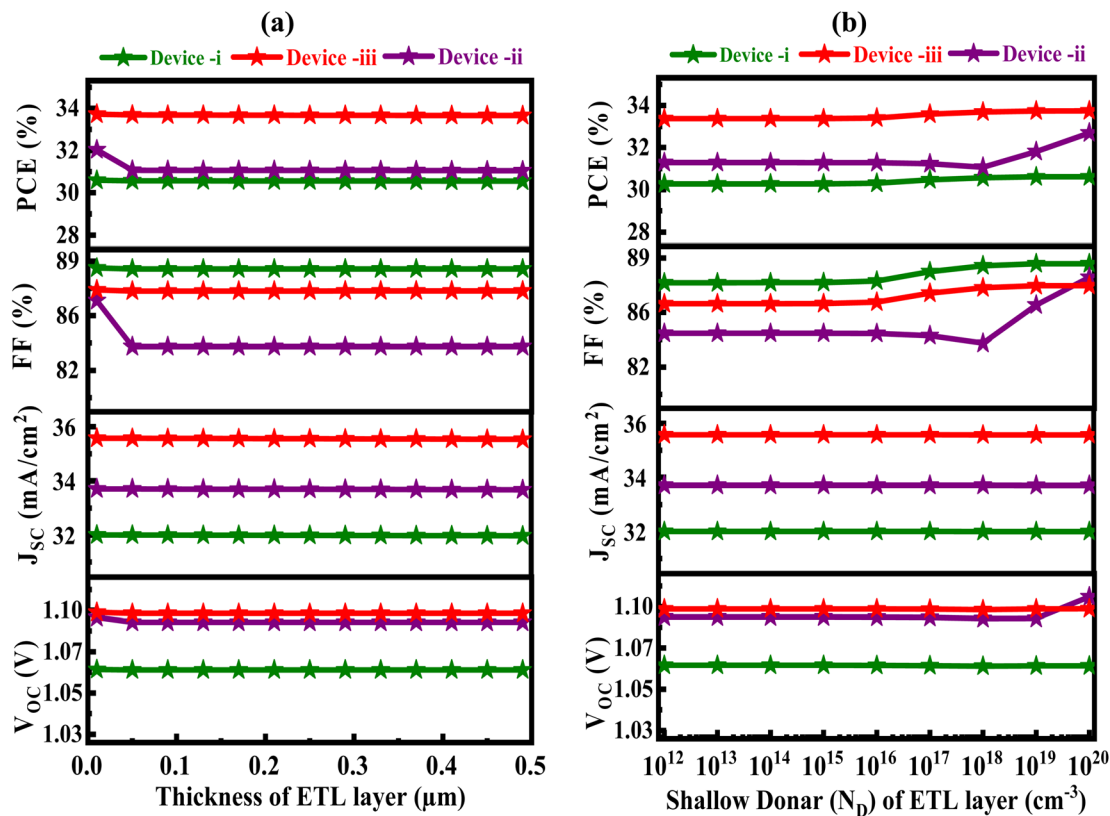


Fig. 9 Effects on the solar cell's performance caused by the (a) thickness and (b) doping level of the (ZnSe) electron transport layer, respectively.

### 3.9 Impact of the interface defect density

Interface defects ( $N_{\text{if}}$ ) develop from structural flaws throughout the solar cell manufacturing process. These flaws worsen the effectiveness of the solar panel by promoting charge carrier recombination at the interface.<sup>43</sup> For this reason, it is essential to evaluate their effects and choose the ideal parameters for realistic manufacturing. All simulations in this study used a neutral  $N_{\text{if}}$  of  $10^{10} \text{ cm}^{-2}$  at the  $\text{Sr}_3\text{PI}_3/\text{ZnSe}$  (Device I),  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device II),  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  (Device III), and  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device III) interfaces, and all PV cells' defect levels were kept at 0.6 eV, as illustrated in Fig. 10. By changing the  $N_{\text{if}}$  from  $10^9$  to  $10^{18} \text{ cm}^{-2}$ , we may assess its impact on the PV parameters in this instance. PCE, FF, and  $V_{\text{OC}}$  were significantly reduced with increasing  $N_{\text{if}}$  from 30.58 to 11.82%, 88.70 to 73.33%, and 1.064 to 0.498 V for  $\text{Sr}_3\text{PI}_3/\text{ZnSe}$  (Device I), 32.94 to 6.17%, 86.94 to 62.20%, and 1.116 to 0.293 V for  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device II), 34.59 to 17.75%, 87.67 to 85.20%, and 1.107 to 0.846 V for  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  (Device III), 34.18 to 13.12%, 87.36 to 73.46%, and 1.098 to 0.502 V for  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device III). Recombination centers that are produced by  $N_{\text{if}}$  can reduce the device's carrier transport efficiency, which lowers FF and  $V_{\text{OC}}$ . But with increasing  $N_{\text{if}}$ ,  $J_{\text{SC}}$  remained almost stable for all interfaces except the  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  (Device III) interface, where it reduced from 35.615 to 24.606  $\text{mA cm}^{-2}$ . Series resistance may rise substantially in the presence of interface difficulties.<sup>44</sup> When  $N_{\text{if}}$  increases, there is an increased rate of interface carrier recombination, which results in a decrease in performance.<sup>45,46</sup>

Consequently, it is suggested that a significant element affecting the performance attributes of PV devices is  $N_{\text{if}}$  at the  $\text{Sr}_3\text{PI}_3/\text{ZnSe}$  (Device I),  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device II),  $\text{Sr}_3\text{PI}_3/\text{Sr}_3\text{SbI}_3$  (Device III), and  $\text{Sr}_3\text{SbI}_3/\text{ZnSe}$  (Device III) interfaces.<sup>47,48</sup>

### 3.10 Impact of the absorber layer's thickness on the G-R profile

Fig. 11(a) and (b) exhibit the carrier production and recombination rates for the Device I, II, and III structures over a wide range of locations. An electron forms duo of electrons and holes during carrier formation when it migrates from the valence band (VB) to the conduction band (CB), with the hole remaining in the VB.<sup>49</sup>  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  undergo this transition, releasing electrons and holes and producing additional carriers.<sup>50,51</sup> Notably, the generation rate is lowest at around 1  $\mu\text{m}$  and maximum at about 0.5  $\mu\text{m}$  for Device I and II structured PSCs, but lowest at 1.04  $\mu\text{m}$  and highest at roughly 1  $\mu\text{m}$  for Device III. This mismatch results from different photon absorption rates at different places. Eqn (8) makes it easier to find  $G(x)$ , and the SCAPS-1D model's  $N_{\text{phot}}(\lambda, x)$  evaluates the output of electron and hole duos based on the arriving photon flux.<sup>35</sup>

$$G(\lambda, x) = \alpha(\lambda, x)N_{\text{phot}}(\lambda, x) \quad (8)$$

In the conduction band of solar systems, electrons and holes recombine. In tastefully constructed and optimized PSCs, the



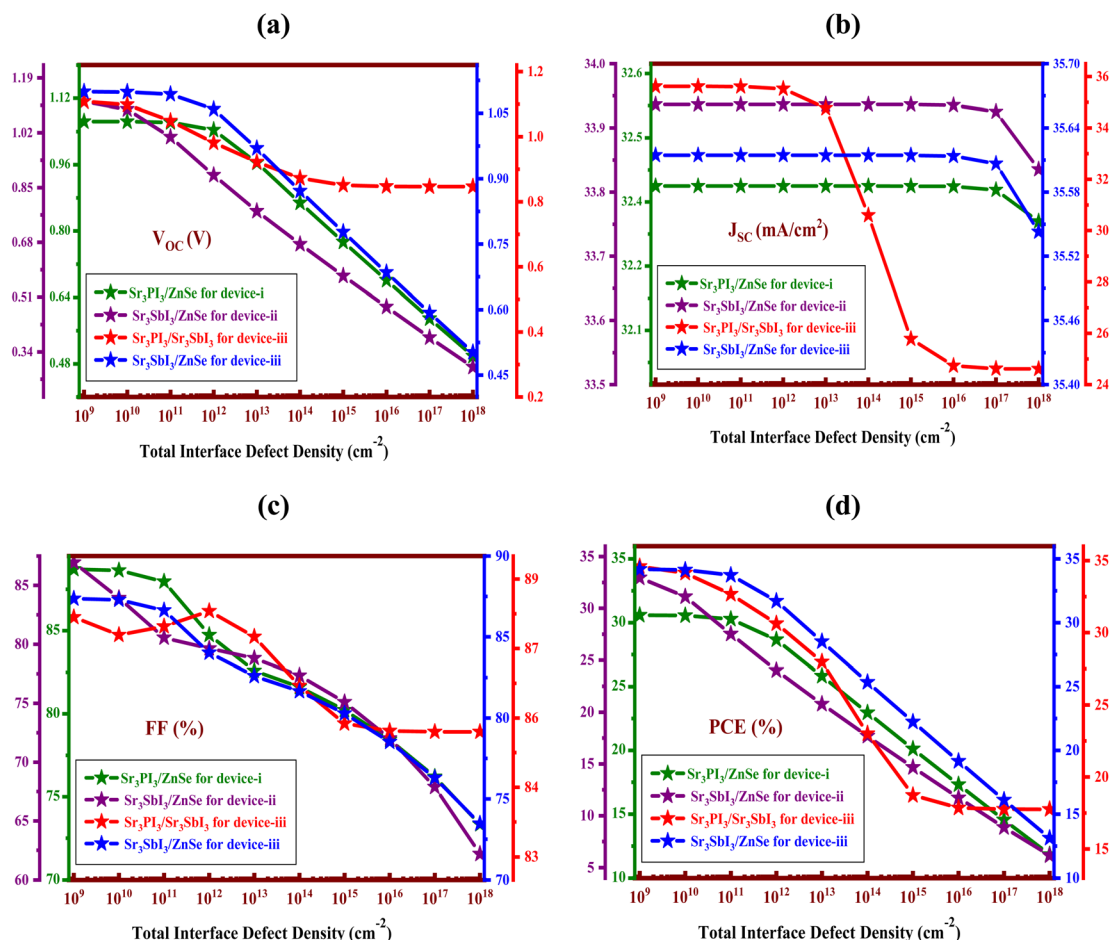


Fig. 10 The impact of interface defect densities on the outputs of the PSC: (a)  $V_{OC}$  (b)  $J_{SC}$  (c) FF and (d) PCE.

density and durability of these charge carriers greatly influence the recombination rates. Each layer's defect states have a major impact on PSC recombination as well. When electrons cross the energy barrier, there are more of them that pair with holes in the valence band of the conduction band. Moreover, the energy levels associated with this transition affect the electron-hole recombination rates. Fig. 11(c) and (d) show the variations in absorber layer thickness, ETL, and their effects on electron and hole carrier concentrations. These differences in absorber thickness have an effect on the hole concentration in the absorber because they produce distinct densities of states (DOS) within the valence bands. Larger carrier concentrations are more significant, especially when comparing electron and hole densities  $d_{slb}$ . This study indicates that the efficiency of the absorber material can be increased by utilizing ZnSe as the ETL in combination with the  $(Sr_3PI_3/Sr_3SbI_3)$  absorber, as this reduces electron-hole recombination and boosts carrier generation. These developments could pave the way for the development of PSCs that are incredibly successful.

### 3.11 Influence of shunt and series resistances

Fig. 12 illustrates how the performance of solar panel parameters is impacted by both series ( $R_s$ ) and shunt resistance ( $R_{sh}$ ).

Series resistance reflects the electrical hindrance caused by the connection of the device to external loads through its front and back contacts, while  $R_{sh}$  represents the leakage current occurring at the solar panel's edges. The  $R_s$  of a solar cell are determined by the circuit's overall impact of bulk resistance, both front and back metal contact resistance, and final resistance.<sup>52</sup> In the study,  $R_s$  and  $R_{sh}$  were adjusted within the ranges of 0–10  $\Omega\text{ cm}^2$  and 10– $10^{10}$   $\Omega\text{ cm}^2$ , respectively. The analysis demonstrates that both series and shunt resistance play significant roles in determining the PCE, as depicted in Fig. 12(d). For the PSC to operate more efficiently, lower  $R_s$  and greater  $R_{sh}$  are necessary.<sup>53</sup> Specifically, the  $V_{OC}$ , illustrated in Fig. 12(a), exhibits a stronger correlation with lower values of shunt resistance rather than series resistance. Conversely, the  $J_{SC}$  is more affected by higher values of series resistance compared to shunt resistance, as depicted in Fig. 12(b). Moreover, the FF demonstrates a notable dependency on changes in series resistance, as seen in Fig. 12(c). The data presented in Fig. 12 suggests that when the  $R_s$  and  $R_{sh}$  vary from 0 to 10  $\Omega\text{ cm}^2$  and 10 to  $10^{10}$   $\Omega\text{ cm}^2$ , correspondingly, the PCE, FF,  $J_{SC}$ , and  $V_{OC}$  change from 34.13% to 1.58%, 87.29 to 24.93%, 35.61 to 17.80  $\text{mA cm}^{-2}$ , and 1.098 to 0.356 V. These findings indicate that optimal PCE is achieved when the leakage current is minimized



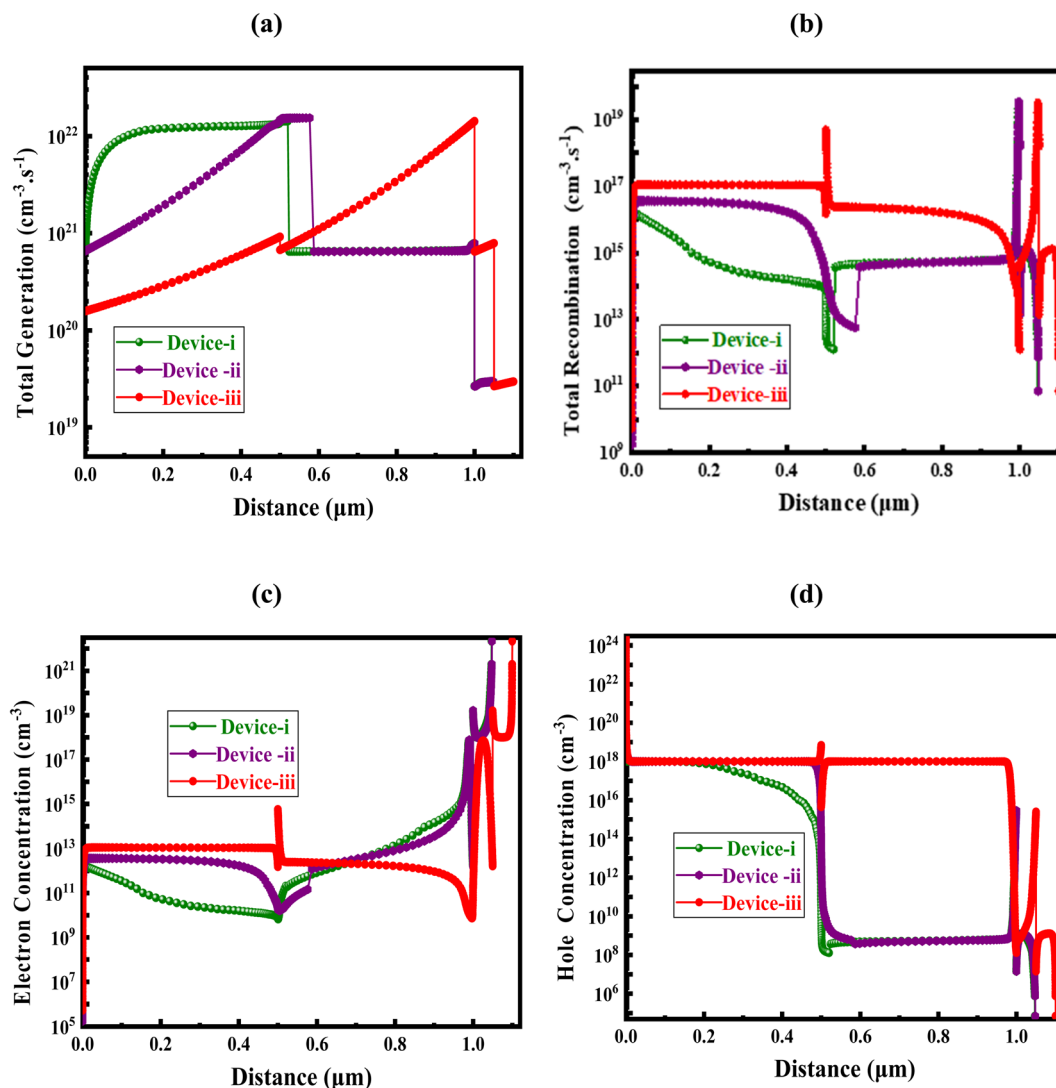


Fig. 11 Impact of (a) concentration of electron, (b) concentration of hole, (c) generation, and (d) recombination regarding the thickness of absorber layer.

(elevated shunt resistance) and series resistance is minimized to facilitate effective carrier collection by the metal electrode.

### 3.12 The impact of operating temperature on the performance of a solar cell

Fig. 13 illustrates how temperature affects Device I, II, and III's performance over a 275–475 K temperature range. The results reveal that as temperature increases, there's a tendency for  $J_{\text{SC}}$  to stay stable while FF,  $V_{\text{OC}}$ , and PCE decrease. This observation suggests that elevated temperatures enhance the thermal mobility of carriers within the solar panel, potentially leading to a higher  $J_{\text{SC}}$ . However, increased temperatures may also cause the absorber layer to behave as an ohmic conductor, impeding carrier flow and resulting in the conversion of electrical energy into heat, thereby reducing FF,  $V_{\text{OC}}$ , and PCE.<sup>54,55</sup> The limited thermal dissipation within different components of the PSC can exacerbate temperature rise, posing a risk of device damage. Therefore, it is crucial to carefully consider the operational

limits of each absorber layer during the creation of such interconnection solar cells. The temperature dependence is evident in the constant  $J_{\text{SC}}$  values of 32.40, 33.93, and 35.61  $\text{mA cm}^{-2}$ , accompanied by a reduction in  $V_{\text{OC}}$  from 1.100 to 0.801 V, 1.105 to 0.925 V, and 1.117 to 0.916 V for Devices I, II, and III. Conversely, FF decreases from 89.45 to 80.44%, 84.21 to 80.38%, and 87.88 to 81.39% for Devices I, II, and III, with increasing temperature. The efficiency reaches its highest value of 31.89, 31.58, and 34.97% at lower temperatures, declining to 20.88, 25.24, and 26.58% for Device I, II, and III as temperatures rise (see Fig. 13).

### 3.13 $J$ - $V$ and $Q$ - $E$ characteristics

A class of photovoltaic devices known for their cheap manufacturing costs and excellent efficiency is perovskite solar cells, which have drawn a lot of interest. The  $J$ - $V$  (current density–voltage) and  $Q$ - $E$  (quantum efficiency) qualities are two important aspects of these cells' operation to comprehend.<sup>18,19</sup>





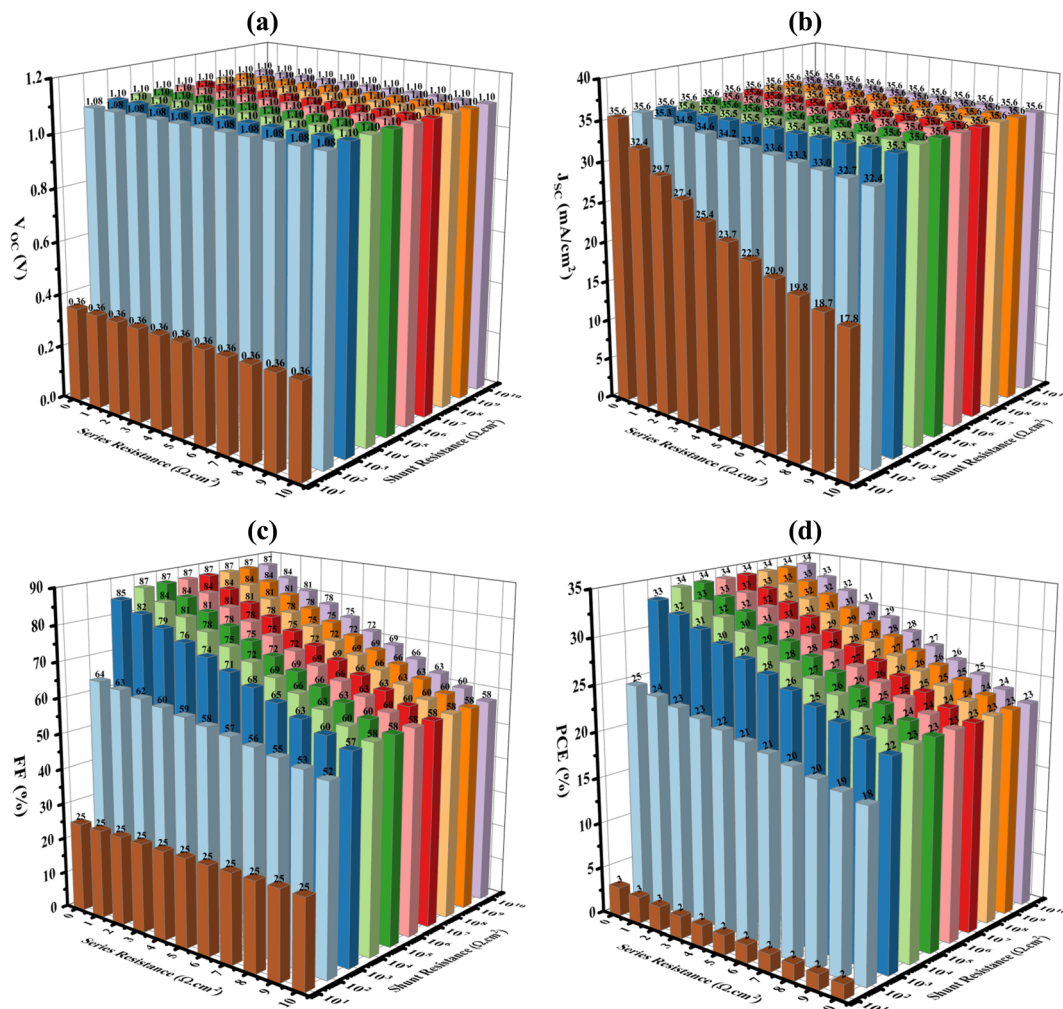


Fig. 12 Impact of shunt and series resistance on electrical properties of PSCs: (a)  $V_{OC}$  (b)  $J_{SC}$  (c) FF and (d) PCE for the optimum Al/FTO/ZnSe/double absorber ( $Sr_3Pb_3/Sr_3SbI_3$ )/Au structure.

The greatest current the cell can generate in an illuminated environment is shown by the current density at zero voltage. The voltage at which there is no current—the highest voltage that the cell is capable of producing. The ratio of charge carriers the cell accumulates to photons impinging on the cell is known as  $Q-E$ .<sup>56,57</sup> It gauges the cell's capacity to transform incident photons into electrical current that can be used. The cell's efficiency is demonstrated throughout the solar spectrum by  $Q-E$ , which changes with the wavelength of incident light. This aids in the comprehension of the spectrum regions that the cell uses most efficiently.  $Q-E$  analysis can help guide advances in cell design by identifying losses resulting from non-radiative recombination, reflection, and transmission.

The  $J-V$  and  $Q-E$  qualities for Device-I, II, and III constructions are displayed in Fig. 14(a and b). With FF values of 88.63, 83.93, and 87.291%,  $J_{SC}$  values of 32.40, 33.93, and 35.61 mA cm<sup>-2</sup>, and  $V_{OC}$  values of 1.0639, 1.0928, and 1.0981 V, the optimized setup's PCE for Devices I, II, and III reached a maximum of 30.55, 31.12, and 34.13%. It is noteworthy that with regard to Devices I, II, and III, the current density of the

optimized structure zeroes out at 1.08, 1.098, and 1.1 V. Remember that prior research has repeatedly demonstrated that current density declines with growing voltage,<sup>58,59</sup> as Fig. 14(a) demonstrates. As seen in Fig. 14(b), the  $Q-E$  profiles cover a wavelength range of 300–1100 nm. For Device I, II, and III structures, the  $Q-E$  begins at around 100% and progressively drops to 0% as the wavelength gets closer to 950, 990, and 990 nm. This drop in  $Q-E$  correlates with the  $J-V$  profile conclusions. Table 4 summarizes the optimized simulated outputs for the final solar cells so that they can be further compared with earlier works.

#### 4. Plan for experimental validation

$Sr_3Pb_3/Sr_3SbI_3$  solar cell technologies should be experimentally evaluated using a comprehensive and multifaceted approach to increase the accuracy of simulation results. This strategy covers material synthesis, device production, characterization, performance analysis, and stability testing. This is a comprehensive plan:



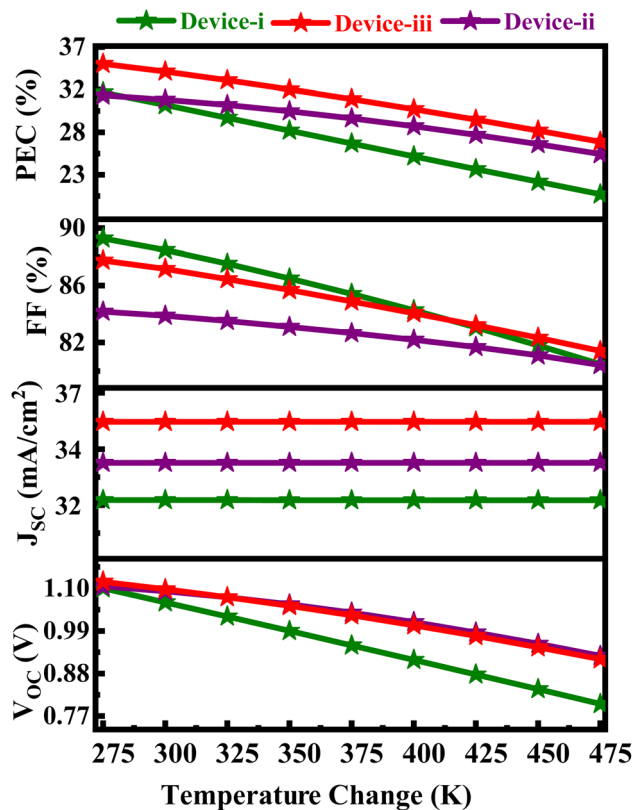


Fig. 13 The effect of temperature changes on solar cells.

## 4.1 Synthesis and Preparation of Materials

### 4.1.1 Production of $\text{Sr}_3\text{PI}_3$ and $\text{Sr}_3\text{SbI}_3$

**4.1.1.1 Chemical procedures.** Solid-state synthesis, solution processing, or chemical vapor deposition (CVD) can be used to produce high-purity  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  perovskite materials. Sustain repeatability by following a specified protocol.

**4.1.1.2 Characterization.** X-ray diffraction (XRD) is used to confirm the crystalline structure and phase purity.

Transmission electron microscopy (TEM) and scanning electron microscopy (SEM) are useful for studying morphology and microstructure.

**4.1.2 Compositional engineering and doping.** To maximize the stability and electrical properties, experiment with different doping levels and compositional modifications. Use energy-dispersive X-ray spectroscopy (EDS) with inductively coupled plasma mass spectrometry (ICP-MS) for precise compositional analysis.

## 4.2. Manufacturing of devices

### 4.2.1 Solar cell construction

**4.2.1.1 Layer deposition in the construction of solar cells.** Layers can be deposited sequentially using spin-coating, thermal evaporation, or sputtering techniques. Typically, a setup may consist of a metal electrode,  $\text{Sr}_3\text{PI}_3$  and  $\text{Sr}_3\text{SbI}_3$  active layer, and electron transport layer (ETL).

**4.2.1.2 Controlled environment.** Manufacture in a glove box with an inert environment to prevent damage from oxygen and moisture.

**4.2.2 Quality control.** Analyze layer thickness and coverage using profilometry and atomic force microscopy (AFM) to ensure uniformity and durability.

## 4.3 Evaluation of stability

**4.3.1 Stability of the environment.** (i) Permit devices to be exposed to ambient conditions (oxygen, humidity), and monitor the gradual decline in device performance over time with recurring  $I$ - $V$  measurements.

(ii) Conduct accelerated ageing trials at high temperatures and continual illumination to simulate long-term operation conditions.

**4.3.2 Mechanical and thermodynamic stability.** (i) Perform thermal cycling studies to evaluate the stability in the presence of temperature changes.

(ii) Perform mechanical stress testing, if appropriate, to assess the resilience of flexible devices.

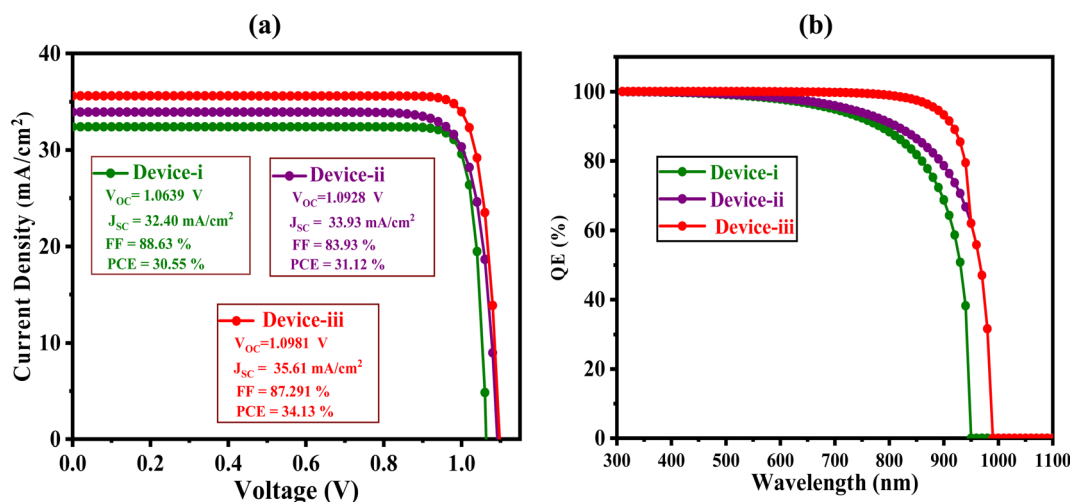


Fig. 14 (a)  $J$ - $V$  and (b)  $Q$ - $E$  curves of Device-I, II, and III structures.



**Table 4** The photovoltaic (PV) metrics obtained in this study with those reported for other double absorber configurations in existing literature (note: E = experimental work and T = theoretical work)

Structures	Type of works	$V_{OC}$ (V)	FF (%)	$J_{SC}$ ( $\text{mA cm}^{-2}$ )	PCE (%)	Ref.
Device-I	T	1.0639	88.63	32.4022	30.55	This work
Device-II	T	1.0928	83.93	33.9365	31.12	This work
Device-III	T	1.0981	87.29	35.6145	34.13	This work
FTO/SnS <sub>2</sub> /Sr <sub>3</sub> SbI <sub>3</sub>	T	0.93	34.67	87.31	28.05	20
FTO/SnS <sub>2</sub> /Sr <sub>3</sub> PI <sub>3</sub>	T	0.92	34.65	34.65	28.15	21
CsPbI <sub>3</sub> /Cs <sub>0.25</sub> FA <sub>0.75</sub> PbI <sub>3</sub>	E	1.20	76.00	18.91	17.39	60
CsPbI <sub>3</sub> /FAPbI <sub>3</sub>	E	1.22	74.00	17.26	15.60	61
MASnI <sub>3</sub> /MASnBr <sub>3</sub>	T	1.04	78.18	31.77	25.91	62
CsPbI <sub>3</sub> /CsGeI <sub>3</sub>	T	1.19	86.19	23.45	24.06	63
MASnI <sub>3</sub> /MAPbI <sub>3</sub>	T	1.15	85.29	30.87	30.29	64
CsPbI <sub>3</sub> /FAPbI <sub>3</sub>	T	1.10	74.00	24.50	19.94	65
CsPbI <sub>3</sub> /CsSnI <sub>3</sub>	T	0.96	78.41	26.59	19.99	66

#### 4.4 Evaluation by comparison and benchmarking

**4.4.1 A reference cells.** Create and evaluate reference solar cells utilizing silicon or other perovskites, such as MAPbI<sub>3</sub>, to act as a performance standard.

**4.4.2 Simulation correlation.** This is comparing the results of the simulations with the data from the experiment, with special focus to crucial factors like charge carrier lifetimes, PCE,  $V_{OC}$ , and  $J_{SC}$ . Based on deviations, modify the simulation models.

#### 4.5 More complex characterization methods

**4.5.1 Analysis of interface and defects.** (i) Use techniques like X-ray photoelectron spectroscopy (XPS) and Fourier-transform infrared spectroscopy (FTIR) to analyze chemical states and interface features.

(ii) Examine defects and trap states using deep-level transient spectroscopy (DLTS).

**4.5.2 Microscopic methods.** (i) Utilizing Kelvin probe force microscopy (KPFM), map the work function and oscillations in the surface potential.

(ii) Local electrical characteristics can be examined using conductive AFM, or c-AFM.

By following this detailed approach, it will be possible to validate Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub> solar cell technologies experimentally and produce high-quality, dependable results that support and enhance simulation predictions, ultimately contributing to the creation of high-performance solar cells.

## 6. Conclusions

The purpose of this work was to use SCAPS-1D software to model a lead-free heterojunction PSC produced from Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub>. The simulation process for this novel PSC prototype commenced with the creation of the absorber layer, which incorporates two components of perovskites, Sr<sub>3</sub>PI<sub>3</sub>/Sr<sub>3</sub>SbI<sub>3</sub>, alongside ZnSe as the electron transport layer (ETL) within the SCAPS-1D software environment. The investigation evaluated the effect of absorber layer thicknesses, doping levels, and defect densities, followed by the influence of ETL thickness and doping. Furthermore, utilizing the SCAPS-1D platform,

simulations were run to evaluate the impact of temperature, shunt, and series resistance on the electrical properties of this new prototype under standard test conditions (STC). The findings revealed that the maximum simulated efficiency of the new prototype reached 34.1395% with  $V_{OC}$  of 1.098137 V, FF of 87.2919%, and  $J_{SC}$  of 35.61451  $\text{mA cm}^{-2}$ , when the Sr<sub>3</sub>PI<sub>3</sub> thickness was approximately 500 nm and the Sr<sub>3</sub>SbI<sub>3</sub> thickness was around 500 nm. Optimal doping levels were determined to be approximately  $10^{18} \text{ cm}^{-3}$  for Sr<sub>3</sub>SbI<sub>3</sub> and Sr<sub>3</sub>PI<sub>3</sub>, with a recommended defect density of around  $10^{12} \text{ cm}^{-3}$  for both absorber layers. Hence, within the production process of this particular PSC, only considerations regarding the absorber layer, FTO, and ETL are crucial for assessing stability and efficiency. Furthermore, it was recommended to maintain the temperature of the fresh PSC prototype at approximately 300 K for optimal performance. For future research directions, experimental investigations are warranted to evaluate the steadiness and longevity of this new device under real-time weather circumstances. Additionally, further studies should explore the effects of different HTL, ETL, and FTO materials on the relationship and performance of this prototype.

## Ethical approval

All the authors declare that the manuscript does not have studies on human subjects, human data or tissue, or animals.

## Data availability

Data will be made available on reasonable request.

## Author contributions

Avijit Ghosh: conceptualization, methodology, software, validation, formal analysis, visualization, investigation, data curation, supervision, writing—original draft, and review and editing. Mohammad Fokhrul Islam Buian, Md. Maniruzzaman, Md Mahfuz Hossain, and Abul Kalam Azad: methodology, software, validation, formal analysis, writing—original draft, and review and editing. Asif Ahammad Miazee, Islam Ragab,



Abeer A. Hassan, H. A. Alrafai, and Siham Khalaf Alla Abdelrahim: software, validation, formal analysis, writing—original draft, and review and editing.

## Conflicts of interest

The authors have no conflicts of interest.

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