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## 1. Introduction

The rapid development of renewable energy sources and the increasing demand for portable electronics and electric vehicles have intensified the need for efficient and high-capacity energy storage solutions.<sup>1–3</sup> Among the diverse range of energy storage technologies, electrochemical capacitors, also known as supercapacitors, stand out as promising options due to their high power density, fast charge and discharge rates, and extended cycle life. Supercapacitors store energy via the electrostatic adsorption of ions at the interface between the electrode and electrolyte, making them an ideal complement to batteries for applications that demand quick energy release and rapid recharging.<sup>4,5</sup> Supercapacitors are classified into three types based on their charge storage mechanisms: electric double-layer capacitors (EDLCs), pseudocapacitors (PCs), and hybrid capacitors, which integrate both EDLC and PC technologies. This classification reflects their methods of energy storage, which involve electrostatic interactions and redox reactions.6,7 EDLCs based on carbonaceous electrode materials show high specific capacitance and long cycle

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## Synergetic effect towards high electrochemical performance in LaMnO<sub>3</sub>-Co<sub>3</sub>O<sub>4</sub> composites

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Electrochemical energy storage devices, especially supercapacitors, require electrode materials with high specific capacitance, excellent stability, and efficient charge transfer kinetics. This study presents LaMnO<sub>3</sub>(LMO)-Co<sub>3</sub>O<sub>4</sub> composites as advanced electrode materials designed to enhance specific capacitance for electrochemical applications. The xLMO-(100% - x) Co<sub>3</sub>O<sub>4</sub> composites (with wt% x values of 100%, 90%, 70%, 50%, and 0%) were synthesized using an auto-combustion method followed by calcination at 900 °C. X-ray diffraction analysis confirmed the presence of the individual compounds in the intended ratios. N<sub>2</sub> adsorption/desorption measurements revealed that the LMO- $Co_3O_4$  composites have a mesoporous structure with a high surface area, with the LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites achieving the highest specific surface area of 6.78 m<sup>2</sup> g<sup>-1</sup>. The electrochemical performance of these composites was evaluated using cyclic voltammetry, charge-discharge, and electrochemical impedance spectroscopy in a three-electrode system with a 1 M KOH electrolyte. The battery-type LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites exhibited outstanding electrochemical performance, showing a specific capacitance of 1614 F  $g^{-1}$  at a scan rate of 1 mV s<sup>-1</sup> and 660 F  $g^{-1}$  at a current density of 0.5 A  $g^{-1}$ , along with energy and power densities of 33 W h kg<sup>-1</sup> and 203 W kg<sup>-1</sup>, respectively. This hybridization approach leverages the strengths of each material to enhance overall electrochemical performance.

> life, facilitating efficient charge storage.<sup>1,8-10</sup> However, their relatively low energy density limits the widespread adoption of supercapacitors in commercial applications. To address this challenge, a promising approach is integrating pseudocapacitors (PCs), which utilize redox reactions during charging and discharging cycles to enhance energy density. This approach includes materials such as metal-based oxides, polymers, and perovskites.<sup>11</sup> Some metal oxide RuO<sub>2</sub> has high specific capacitance but is expensive to commercialize.

> Perovskite oxide materials have recieved more attention in various fields, including solar cells, gas sensing, fuel cells, magnetic data storage devices, metal-air batteries, and PCs due to their physical and structural stability as well as catalytic properties.<sup>12-17</sup> Among them, LaMnO<sub>3</sub>, a perovskite oxide, has attracted significant attention as an energy storage material due to its inherent properties, particularly oxygen vacancy, which significantly enhance the specific capacitance of the material.<sup>18</sup> Further, LMO offers good specific capacitance, primarily through the  $Mn^{3+}/Mn^{4+}$  redox couple, typically exhibits faster ionic diffusion and better electronic conductivity, leading to a higher power density, making LMO more suitable for applications requiring rapid energy delivery, and generally offers better stability, especially in alkaline electrolytes, and can maintain performance over more extended cycling periods, making it more durable in long-term applications.

> Recently, composite electrode materials have garnered significant attention to achieve synergistic enhancements in

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#### Paper

electrochemical performance. By combining multiple materials with complementary properties, such as high conductivity, large surface area, and electrochemical stability, composite electrodes offer the potential to overcome the limitations of individual components and optimize overall energy storage performance. V. V. Deshmukh *et al.* synthesized the  $Co^{3+}$  doped LaMnO<sub>3</sub> by following the sol-gel method and got a specific capacitance of 651.54 F  $g^{-1}$  in 5 mV  $s^{-1}$  scan rate for  $La_{0.8}Co_{0.2}MnO_3$ compound.<sup>19,20</sup> Na Zhang et al. synthesized LaCoO<sub>3</sub>/Co<sub>3</sub>O<sub>4</sub> perovskites composites via the hydrothermal method. They found 1055.0 mA h g<sup>-1</sup> in 100 mA g<sup>-1</sup> current density.<sup>20</sup> A. Dhakal *et al.* synthesized LaMnO<sub>3</sub>-Mn<sub>3</sub>O<sub>4</sub> (70%:30%) composites through the auto-combustion method with a specific capacitance of 584 F  $g^{-1}$ at a scan rate of 1 mV s<sup>-1,21</sup> Hongwei Tian et al. synthesized LaMnO<sub>3</sub>@NiCo<sub>2</sub>O<sub>4</sub> composites by a facile hydrothermal method and reported a specific capacitance of 811 C  $g^{-1}$  at a current density of 0.5 A g<sup>-1</sup> in 6 M KOH electrolyte.<sup>22</sup> By using the electrodeposition process, Pianpian Ma et al. synthesized LaMnO<sub>3</sub>/MnO nano-arrays and exhibited a specific capacitance of 260 F  $g^{-1}$  at a current density of 0.5 A  $g^{-1}$  in 0.5 M Na<sub>2</sub>SO<sub>4</sub>.<sup>23</sup> Zhiyi Lu et al. synthesized Co<sub>3</sub>O<sub>4</sub>(a)Ni-Co-O via a hydrothermal process and found 1525 F  $g^{-1}$  at a current density of 30 mA cm<sup>-2</sup> in 1 M KOH electrolyte.<sup>24</sup> Graham W. Piburn et al. synthesized LaMnO<sub>3</sub>-SiO<sub>2</sub> by direct overgrowth around the short channel version of SBA-15 silica and obtained a specific capacitance of 200 F  $g^{-1}$  at a current density of 1 A  $g^{-1}$  in 1 M KOH electrolyte.<sup>25</sup>

The rationale behind integrating LMO and Co3O4 lies in their complementary characteristics. LMO and Co<sub>3</sub>O<sub>4</sub> have different redox potentials and mechanisms. Combining them can enhance capacitance due to the broader range of redox reactions available. This synergy can increase the overall specific capacitance of the hybrid material. Further, LMO and Co<sub>3</sub>O<sub>4</sub> operate through different redox couples (Mn<sup>3+</sup>/Mn<sup>4+</sup> and Co<sup>2+</sup>/  $Co^{3+}/Co^{4+}$ ), which can result in a more balanced electrochemical profile. This balance can lead to consistent performance across a range of operating conditions. LMO contributes to high power density due to its good ionic and electronic conductivity. When combined with Co<sub>3</sub>O<sub>4</sub>, which may have slower kinetics but higher energy density, the hybrid can achieve a balance between high energy and high-power densities. By adjusting the ratio of LMO to  $Co_3O_4$ , the electrochemical properties of the hybrid material can be fine-tuned to meet specific application requirements, such as prioritizing energy or power density.

## 2. Experimental methods

#### 2.1. Materials and reagents

La(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O (lanthanum(III) nitrate hexahydrate), Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (cobalt(II) nitrate hexahydrate), Mn(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O (manganese(II) nitrate tetrahydrate), C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>·H<sub>2</sub>O (citric acid monohydrate), polyvinylidene fluoride (PVDF), and *N*-methylpyrrolidone (NMP) were purchased from Sigma Aldrich with 99% purity. These chemicals were directly used in the synthesis of LMO–Co<sub>3</sub>O<sub>4</sub> composites without purification.

#### 2.2. Synthesis of LaMnO<sub>3</sub>-Co<sub>3</sub>O<sub>4</sub> composites

The synthesis of composites (LMO, Co<sub>3</sub>O<sub>4</sub>, LMO-Co<sub>3</sub>O<sub>4</sub> (90%: 10%), LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%), LMO-Co<sub>3</sub>O<sub>4</sub> (50%:50%)) with different wt% was carried out by one-pot auto-combustion process.<sup>26</sup> The stoichiometric ratio of  $La(NO_3)_3 \cdot 6H_2O$ ,  $Mn(NO_3)_2$ :4H<sub>2</sub>O, and C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>·H<sub>2</sub>O dissolved in the 20 mL of DI water and placed on the magnetic stirring. Simultaneously, the Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, and C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>·H<sub>2</sub>O dissolved in another 20 mL of DI water and subjected to magnetic stirring for 15 minutes. The solution of Co(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O, and C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>·H<sub>2</sub>O was added to the La(NO<sub>3</sub>)<sub>3</sub>·6H<sub>2</sub>O, Mn(NO<sub>3</sub>)<sub>2</sub>·4H<sub>2</sub>O, and C<sub>6</sub>H<sub>8</sub>O<sub>7</sub>·H<sub>2</sub>O mixture and placed on a hot plate at 120 °C with continuous magnetic stirring. The sample was allowed to undergo auto-ignition, after which the sample was kept in a hot furnace and maintained at 900 °C overnight. The resulting product was the composite of LMO-Co<sub>3</sub>O<sub>4</sub>. The chemical reaction for the formation of LMO- $Co_3O_4$  composites can be expressed as eqn (1), and a schematic diagram for the composite synthesis is presented in Fig. 1.

$$\begin{array}{l} La(NO_3)_3 \cdot 6H_2O + Mn(NO_3)_2 \cdot 4H_2O + 3Co(NO_3)_2 \cdot 6H_2O + C_6H_8O_7 \cdot \\ H_2O \rightarrow LaMnO_3 + Co_3O_4 + 11N_2 + 6CO_2 + 33H_2O + 17/2O_2 \\ (1) \end{array}$$

#### 2.3. Preparation of electrode

As a working electrode, the nickel foam (thickness 1.67 mm), measuring 1 cm  $\times$  1 cm, was thoroughly cleaned *via* ultrasonication in a 37 wt% HCl solution (25 mL) for 10 minutes, followed by rinsing several times with deionized (DI) water and additional ultrasonication in DI water for 10 minutes. Subsequently, it was ultrasonicated in ethanol for 10 minutes and dried in a furnace for 2 hours at 100 °C. For electrode preparation, a solution containing 6 mg of sample composites and 1 mg of PVDF in 1 mL of NMP was stirred for 6 hours to ensure uniform distribution. Then, 0.6 mL of this solution was applied to the nickel foam surface. The sample-loaded Ni foam was heated at 100 °C in a furnace for 20 hours for drying and adhesion. The weight of the sample was determined by subtracting the initial weight of the nickel foam from the weight of the sample-coated nickel foam after drying.

#### 2.4. Characterization

The crystalline structure of the LMO–Co<sub>3</sub>O<sub>4</sub> composites was analyzed using a Bruker D8 Advance X-ray diffraction (XRD) equipped with a CuK<sub> $\alpha$ </sub> radiation source ( $\lambda = 0.15406$  Å), operating at 40 kV and 40 A, with a step size of 0.02 and a scan rate of 0.2 min per step within the 2 $\theta$  range of 20°  $\leq 2\theta \leq 70^{\circ}$ . The morphology of the prepared composites was investigated using a Hitachi S-4700 field emission scanning electron microscope (FE-SEM) operated at 20 kV and 10 mA, while energy dispersive X-ray spectroscopy (EDX) analysis utilized the Bruker Esprit 2.3 system. X-ray photoelectron spectroscopy (XPS) of samples was performed using a Thermo Scientific K-Alpha XPS system with a step size of 0.1 eV. The surface area and pore size distribution were analyzed using a Quantachrome Nova Touch NT2LX-2 surface area analyzer, with nitrogen (N<sub>2</sub>) as the adsorbate gas at a temperature of 77 K. Electrochemical analysis was carried out



using a Gamry IFC 1000-07045 system. The electrochemical properties of samples were investigated in a three-electrode configuration, with a voltage range of 0 to +0.6 V in 1 M KOH electrolyte solutions. The counter electrode was a platinum plate, the reference electrode was Ag/AgCl (Basi), and the working electrode was sample-loaded nickel foam.

## 3. Result and discussion

#### 3.1. Structure and morphology

**3.1.1.** X-ray diffraction study. Fig. 2(a) shows the XRD patterns of the LMO– $Co_3O_4$  composites. The XRD sharp peaks show the presence of orthorhombic LMO (PDF 075-7697) and cubic  $Co_3O_4$  (PDF 076-7802). The diffraction peaks at 22.93, 32.50, 32.81, 40.15, 46.85, 52.57, 57.98, and 68.07 can be indexed to (012), (110), (104), (202), (024), (122), (300), and (220) plane of the LMO crystalline, respectively. Additionally, 31.32, 36.90, 38.60, 44.88, 55.74, 59.45, and 65.344 can be

indexed to (220), (311), (222), (400), (422), (511), (400) plane of the  $Co_3O_4$  crystalline, respectively. No extra peaks were observed in all the composites, confirming the presence of a pure phase of LMO and  $Co_3O_4$  in the sample. Fig. 2(b) shows the Rietveld refined XRD data plot of LMO- $Co_3O_4$  composites using the GSAS-II. The estimated composition percentage from the Rietveld refined XRD data for the LMO- $Co_3O_4$  composites reveals that the compositions closely match the intended ratios. The estimated composition of samples is LMO- $Co_3O_4$  (89.9%:10.1%), LMO- $Co_3O_4$  (69%:31%), and LMO- $Co_3O_4$  (48%:52%), close to the expected composition of the composites.

**3.1.2.** Field emission scanning electron microscopy. Fig. 3 presents the FESEM images, EDX elemental mapping patterns, and spectra of the LMO– $Co_3O_4$  composites. Fig. 3(a) illustrates the spongy, porous structure of the LMO sample. The  $Co_3O_4$  morphology appears to be hollow structures that interconnect, forming chain-like configurations that create interior cavities and loose structures (Fig. 3(b)). The fluffy, porous nature of LMO is retained in the LMO– $Co_3O_4$  (90%:10%) composites, but



Fig. 2 (a) XRD patterns (left) and (b) Rietveld refined XRD data (right) of LMO-Co<sub>3</sub>O<sub>4</sub> composites.



Fig. 3 FESEM images of (a) LMO, (b)  $Co_3O_4$ , (c) LMO- $Co_3O_4$  (90%:10%), (d) LMO- $Co_3O_4$  (70%:30%), and (e) LMO- $Co_3O_4$  (50%:50%) and elemental mapping patterns of the different composites of LMO- $Co_3O_4$ ; La (green), Mn (blue), O (red), and Co (Crane) color. (f)–(j) EDX spectra of LMO- $Co_3O_4$  composites (NA – not applicable).

these composites exhibit small interior cavities due to the presence of  $Co_3O_4$  (Fig. 3(c)). As the ratio of  $Co_3O_4$  in the composite increases, the morphology of LMO– $Co_3O_4$  (70%:30%) composites remains consistent but evolves into a more chain-like structure (Fig. 3(d)). Additionally, the degree of aggregation of  $Co_3O_4$  compounds on the LMO surface increases in the LMO– $Co_3O_4$  (50%:50%) composites (Fig. 3(e)) with cavities or voids. Fig. 3(f)–(j) of the EDX elemental map depicts the presence of La, Mn, Co, and O elements. The sharp peaks observed between 0 to 1 keV and 6 to 8 keV confirm the presence of Co, while peaks observed between 0 to 1 keV confirmed the presence of oxygen. The spectra also show the presence of gold (Au) due to the gold coating applied to samples before capturing the images.

**3.1.3.** Surface adsorption/desorption analysis. The materials' surface area and pore size distribution were characterized by  $N_2$  adsorption-desorption isotherm analysis of LMO-Co<sub>3</sub>O<sub>4</sub> composites measured at 77 K, presented in Fig. 4. All the samples display similar isotherms with different hysteresis loops and can be categorized as type-IV isotherms.<sup>27</sup> The multipoint BET surface area, pore volume, and pore size distribution

were calculated using Brunauer–Emmett–Teller (BET) methods and summarized in Table 1. The surface area and average pore radius of LMO–Co<sub>3</sub>O<sub>4</sub> (90%:10%) is 3.73 m<sup>2</sup> g<sup>-1</sup> and 3.11 nm, which is further increased in the LMO–Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites and reached the highest values of 6.79 m<sup>2</sup> g<sup>-1</sup> and 13.48 nm, respectively. Usually, an increase in the specific surface area and average pore size (radius) of the samples corresponds to an increase in its specific capacitance due to enhanced surface area, more interaction with electrolytes and electrodes, larger pores allowing better access for electrolyte ions, shorten diffusion pathways for ions, reducing resistance, and faster ion transport in charge/discharge conditions.

**3.1.4. XPS.** XPS tests were conducted on the LMO–Co<sub>3</sub>O<sub>4</sub> composites to investigate their elemental valence states and components. The binding energy of the La  $3d_{3/2}$  and La  $3d_{5/2}$  orbitals (Fig. 5(a)) in LMO–Co<sub>3</sub>O<sub>4</sub> composites were estimated to be 833.5 and 850.3 eV, respectively, with spin–orbit splitting ~ 16.8 eV,<sup>28</sup> which proves the presence of La ion in the trivalent state. In the Co 2p spectrum of Fig. 5(b), two major peaks located at 795.6 and 780.2 eV can be detected, corresponding to the Co  $2p_{3/2}$  and Co  $2p_{1/2}$  peaks, with a spin energy separation



 Table 1
 Specific surface area and pore size distribution of LMO-Co<sub>3</sub>O<sub>4</sub> composites

Composites	Mass (g)	BET surface area $(m^2 g^{-1})$	Average pore size (radius nm)	Total pore volume (cc g <sup>-1</sup> )			
LMO	0.22	2	05.91	0.007			
$Co_3O_4$	0.18	3	03.18	0.005			
$LMO-Co_3O_4$ (90%:10%)	0.21	4	03.11	0.006			
$LMO-Co_{3}O_{4}(70\%:30\%)$	0.20	7	13.48	0.050			
LMO- $Co_3O_4$ (50%:50%)	0.19	6	02.72	0.008			

of 15.4 eV.<sup>29</sup> The binding energy of Mn  $2p_{3/2}$  and Mn  $2p_{1/2}$  is centered at 654.1 and 642.4 eV, respectively, with energy separation between them at 11.8 eV (Fig. 5(c)), which is matched with the previously reported values.<sup>30,31</sup> The Mn 2p<sub>3/2</sub> signal was separated into three peaks at around 640.5 (Mn<sup>2+</sup>), 641.4 (Mn<sup>3+</sup>), and 643.0 eV (Mn<sup>4+</sup>). The Mn  $2p_{1/2}$  signals are at around 652.0 (Mn<sup>2+</sup>), 653.0 (Mn<sup>3+</sup>), and 654.6 eV (Mn<sup>4+</sup>).<sup>32</sup> The major two peaks of Co (Fig. 5(d)) from the signal Co  $2p_{3/2}$  are at 780.2 ( $Co^{3+}$ ) and 781.9 eV ( $Co^{2+}$ ), and for Co  $2p_{1/2}$  also are at 794.9 ( $Co^{3+}$ ), and 796.3 eV ( $Co^{2+}$ ), respectively.<sup>33</sup> Here, the ratio of Mn<sup>2+</sup>, Mn<sup>3+</sup>, and Mn<sup>4+</sup> ions decreases, while Co<sup>3+</sup> and Co<sup>2+</sup> ions' concentration naturally rises as the Co3O4 content increases in the composite. The increase in Co<sup>2+</sup> and Co<sup>3+</sup> ions may help to optimize the interfacial interaction, enhancing the specific capacitance. In Fig. 5(e), the O 1s spectra are deconvoluted into two compounds of the lattice oxygen (Co<sub>3</sub>O<sub>4</sub>) at 529.4 eV for the main lattice oxygen and a second much more intense peak at 530.8 eV.<sup>34</sup> For the LMO, O 1s spectra are deconvoluted into three peaks, and they correspond to lattice oxygen in either La or manganese oxide (OL), surface adsorbed oxygen species or OH<sup>-</sup> (O<sub>A</sub>), physisorbed or chemisorbed H<sub>2</sub>O molecules (O<sub>W</sub>), and

located at ~529.0, ~529.6, ~531.0, ~532.6 eV, respectively.<sup>35,36</sup> Among the three oxygenated species,  $O_A$  species are closely related to the oxygen vacancy and are beneficial for enhancing the electrochemical properties of the materials.<sup>37</sup>

#### 3.2. Electrochemical analysis

**3.2.1.** Cyclic voltammetry test. The electrochemical behavior of the LMO– $Co_3O_4$  composites is measured by a cyclic voltammetry (CV) test in a three-electrode electrochemical setup in the 1 M KOH electrolyte. Fig. 6 represents the comparative CV curves at a constant scan rate, 10 mV s<sup>-1</sup> of LMO– $Co_3O_4$  composites in the potential window 0 to 0.6 V. All the REDOX peaks in the CV curves pointed towards the pseudocapacitive behavior.

Fig. 7 represents the CV curves of LMO–Co<sub>3</sub>O<sub>4</sub> composites obtained at scan rates from 1 to 300 mV s<sup>-1</sup> to analyze the chemical kinetics. The graph shows that the CV curves are affected by the scan rates. With increasing scan rate, the anodic peaks current shifts more positive potentials, and reduction peaks shift enormously towards the negative potential. The peak anodic and cathodic voltage difference,  $\Delta E_{a,c}$ , increases





Fig. 5 High-resolution spectrum of (a) La 3d and (b) Co 2p, deconvoluted peaks of (c) Mn 2p, (d) Co 2p, and (e) O 1s of LMO-Co<sub>3</sub>O<sub>4</sub> composites.



Fig. 6 Cyclic voltammetry of LMO–Co $_3O_4$  composites at 10 mV s $^{-1}$  scan rate in 1 M KOH electrolyte.

with increasing the sweep rate. Generally, the difference between the anodic and cathodic peak positions,  $\Delta E_{a,c}$ , and the voltage shift of the anodic and cathodic peaks with changing voltage defines the level of the reversibility of the electrochemical reactions. The  $\Delta E_{a,c}$  is generally small for pseudocapacitors having good reversibility and remains constant over a wide scan rate range. In contrast, a large  $\Delta E_{a,c}$  value is attributed to battery-type materials that could undergo phase

transformation during the electrochemical process.<sup>38,39</sup> The REDOX peaks are attributed to the alternation of valence states of Mn ( $Mn^{2+}$ ,  $Mn^{3+}$ , and  $Mn^{4+}$ ) in LMO and Co ( $Co^{2+}$  and  $Co^{3+}$ ) in Co<sub>3</sub>O<sub>4</sub> facilitating the ionic intercalation/deintercalation over the electrode material. As demonstrated by LMO-Co<sub>3</sub>O<sub>4</sub> composite electrodes, the battery-type behavior ensues from the long diffusion and intercalation of ions accompanied by faradaic reactions. The fast scan rates wash out oxidation peaks in 10 and 30 wt% composite due to reactions not keeping pace with the rapid potential changes. As the scan rate increases, the peaks may shift, and the intensity of the peaks changes significantly, reflecting the slower ion diffusion. At higher scan rates, the time available for the electron transfer reactions (oxidation or reduction) to occur decreases. If the electrochemical reaction kinetics are slow compared to the faster potential sweep, the peak current may not reach its maximum, leading to a less pronounced oxidation peak. Further, at higher scan rates, the electrode surface may become saturated with reaction products, preventing further oxidation. If the products remain on the surface and are not adequately removed, they can inhibit the oxidation reaction from occurring. Further, capacitive currents (due to double-layer charging) can dominate the response at higher sweep rates, overshadowing the faradaic (redox) currents. This can lead to broadening and flattening of the peaks.

Based on the CV and XPS results provided, along with the previously reported article,<sup>15,40</sup> the electrochemical storage

**Energy Advances** 



Fig. 7 (a)-(e) Cyclic voltammetry of LMO-Co<sub>3</sub>O<sub>4</sub> composites at different scan rates from 1 to 300 mV s<sup>-1</sup> in 1 M KOH electrolytes.

mechanism of LMO perovskites and Co3O4 in an alkaline electrolyte involves the intercalation of oxygen and hydroxide ions. This process is driven by the oxidation of Mn atoms (B-site cations) for LMO and Co atoms for Co<sub>3</sub>O<sub>4</sub>; the phenomenon can be represented by eqn (2)-(5).<sup>35,41</sup>

$$La[Mn_{2\delta}^{2^+}, Mn_{1-2\delta}^{3^+}]O_{3-\delta} + 2\delta OH^- \leftrightarrow LaMn^{3^+}O_3 + \delta H_2O + 2\delta e^-$$
(2)

 $LaMn^{3+}O_3 + 2\delta OH^- \leftrightarrow La[Mn_{2\delta}^{4+}, Mn_{1-2\delta}^{3+}]O_{3+\delta} + \delta H_2O + 2\delta e^-$ (3)

$$Co_3O_4 + OH^- + H_2O \leftrightarrow 3CoOOH + e^-$$
 (4)

$$CoOOH + OH^- \leftrightarrow CoO_2 + H_2O + e^-$$
(5)

In CV measurements, the total current measured under a potential sweep rate can be interpreted as the sum of the current elated to the slow diffusion-controlled process  $(i_{diff})$ and the current required to charge the double layer at the electrolyte interface or to initiate fast faradaic reactions on the exposed electrode surface  $(i_{cap})$ . To understand these contributions, the following empirical power-law relationship between the current and scan rate is used (eqn (6) and (7)): $^{42,43}$ 

$$i = i_{\rm cap} + i_{\rm diff} = av^b \tag{6}$$

or

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$$\log(i) = \log(a) + b\log(v) \tag{7}$$

where, *i* represents peak current, v is scanning rate, and *a* and *b* are the constants.

Parameter *b* is determined from the slope of the linear plot of log(i) vs. log(v), which provides kinetic information about the

electrochemical reactions (Fig. 8(a)). Typically, two well-defined conditions for the *b* value are b = 0.5 and b = 1. A *b* value of 1 indicates contributions from rapid near-surface processes, such as fast surface redox reactions and the charging/discharging of electric double-layer capacitors (EDLCs). In contrast, when b =0.5, the charge storage mechanism is diffusion controlled.44 Fig. 8(a) shows a slope change in the linear plot at around 90 mV  $s^{-1}$  scan rate, signifying a change in the reaction kinetics. Corresponding *b* values are plotted in Fig. 8(d). This plot clearly shows that LMO-Co<sub>3</sub>O<sub>4</sub> (90%:10%) and LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites have dominant diffusion contributions at lower scan rates with increased dominance of capacitive contributions in higher scan rate regions. Their b values  $\sim 0.5$  at a lower scan rate represent the slow semi-infinite diffusion-controlled faradaic process that occurs in the bulk, such as battery-type processes. However, limiting diffusion processes from the ohmic contribution, such as active material resistance and solid-electrolyte interphase resistance, could not be ignored.45,46

As discussed above, parameter *b* is desirable for distinguishing between capacitive processes and diffusion-controlled intercalation. This distinction is essential for gaining a deeper understanding of the underlying charge storage mechanisms and can greatly inform the selection of materials and the design of devices. When surface-dominant reactions control the process, the response current varies linearly with v (*i.e.*, di/dv =constant = capacitance). If the process is controlled by semiinfinite diffusion, the response current varies linearly with  $v^{1/2}$ (*i.e.*,  $di/dv^{1/2}$  = constant). Thus, the general expression for current with the mixed presses is expressed as, eqn (8) and (9),<sup>47</sup>

$$i(V) = i_{\rm cap} + i_{\rm diff} = k_1 v + k_2 v^{1/2}$$
(8)



Fig. 8 (a) Relationship between log(*i*<sub>0</sub>) and log (mV s<sup>-1</sup>), (b) the capacitive and diffusion contribution percentage to the total charge storage, (c) relationship between peak current and square root of scan rate from 10 to 300 mV s<sup>-1</sup> scan rate, and (d) bar graph of b-values of LMO–Co<sub>3</sub>O<sub>4</sub> composites.

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$$\frac{i(V)}{v^{1/2}} = k_1 v^{1/2} + k_2 \tag{9}$$

where i(v) is the peak current, function of scan rate (v), and both  $k_1$  (slope) and  $k_2$  (Y-intercept) are constants (Fig. 8(b)). The electrode material will store charge through surface contribution when  $k_1 \neq 0$  and  $k_2 = 0$ ; or charge stored through diffusioncontribution when  $k_1 = 0$  and  $k_2 \neq 0$ ; or when  $k_1 \neq 0$  and  $k_2 \neq 0$ the charge storage contributions contributed by both the capacitance and the diffusion. The LMO-Co<sub>3</sub>O<sub>4</sub> composites have non-zero  $k_1$  and  $k_2$  values, indicating a mixture of diffusion and capacitive control contribution to the charge storage mechanism. In a low scan rate, the  $k_1$  values are much less near zero than the  $k_2$  values, indicating that diffusion is a dominating contribution to the charge storage mechanism. With increasing scan rate, diffusion contribution decreases, or capacitive contribution increases due to insufficient time for electrons to penetrate the electrode. Most composites still have a higher percentage of diffusion contribution, even at 300 mV s<sup>-1</sup>.

The positive and negative voltammetric peak currents in Fig. 8(c) have been used to calculate the chemical diffusion coefficient of LMO-Co<sub>3</sub>O<sub>4</sub> composites by the Randles-Sevcik equation, eqn (10):48

$$i_{\rm p} = 2.69 \times 10^5 A C_0 n^{3/2} D^{1/2} v^{1/2} \tag{10}$$

where  $i_p$  is the peak current, A is the electrode area (cm<sup>2</sup>), n is the number of electrons involved in the reaction of the redox couple, D is the diffusion coefficient (cm<sup>2</sup> s<sup>-1</sup>),  $C_0$  is the concentration of electroactive material (mol cm<sup>-3</sup>), and  $\nu$  is the scan rate. Fig. 8(c) shows a linear relationship between the peak current and the square root of the scan rate, confirming that diffusion-controlled mechanisms dominate the electrochemical process in LMO-Co<sub>3</sub>O<sub>4</sub> composites. The higher slope implies a higher diffusion coefficient, which implies that the electroactive species can move quickly through the electrolyte to the electrode surface. Here, LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites display a higher slope, which could be an optimized composite for achieving higher diffusion rates.

The area enclosed by the current-potential curve is directly proportional to the specific capacitance of the material. The specific capacitance was calculated from the CV curves by integrating the area under the current-potential curve, eqn (11):<sup>49</sup>

$$C_{\rm sp} = \frac{1}{m(V_{\rm c} - V_{\rm a})} \int_{V_{\rm a}}^{V_{\rm c}} I(V) \mathrm{d}V$$
(11)

where  $C_{sp}$  (F g<sup>-1</sup>) is the specific capacitance, *m* is the mass of the active material in the electrode,  $\nu$  (mV s<sup>-1</sup>) is the scan rate,  $V_{\rm c}$  –  $V_{\rm a}$  is a potential window, and I(V) is the response current. The integral part gives the area under the current potential curve. LMO and  $Co_3O_4$  have specific capacitances of 307 F g<sup>-1</sup> and 479 F  $g^{-1}$  at 1 mV  $s^{-1}$  scan rate. The values increased to 756 F  $g^{-1}$ 



Fig. 9 Specific capacitance,  $C_{\rm sp}$ , of LMO–Co<sub>3</sub>O<sub>4</sub> composites at different scan rates.



LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites (Fig. 9). These optimal specific capacitances may be due to the synergetic effect of LMO and Co<sub>3</sub>O<sub>4</sub>. However, a further increase in the ratio of Co<sub>3</sub>O<sub>4</sub> in the LMO; LMO-Co<sub>3</sub>O<sub>4</sub> (50%:50%) composites decrease the specific capacitance to 577 F  $g^{-1}$ . A decrease in specific capacitance with increased  $Co_3O_4$  content could be attributed to (1) excess of  $Co_3O_4$  might disrupt the optimal electron or ion pathways in the composites, (2) the  $Co_3O_4$  might not mix properly, or LMO and  $Co_3O_4$  exist separately, which can reduce the effective interface area and leads poor charge transfer and lower capacitance, and (3) excess of Co<sub>3</sub>O<sub>4</sub> in LMO may form larger cavities or voids, which can reduce the contact between conductive particles within the electrode, leading to increased internal resistance, hindering charge transport, and decreasing specific capacitance. The formation of larger voids is evident in the SEM images in Fig. 3(e). The specific capacitance of LMO-Co<sub>3</sub>O<sub>4</sub> composites at a scan rate of 1 mV s<sup>-1</sup> is presented in Table 2. The LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites have a higher specific capacitance.

**3.2.2.** Chronopotentiometry test. The chronopotentiometry test is generally used to evaluate the performance of electrode materials by examining their response to constant current. This helps assess the material's conductivity, stability, and electrochemical activity. Especially for supercapacitor evaluation, it helps understand how the devices perform under constant current conditions and provides information on charge and discharge characteristics. The chronopotentiometry test is conducted at the current densities of 0.5 to 15 A g<sup>-1</sup>. Fig. 10 shows

Table 2 Specific capacitance,  $C_{sp}$ , of LMO-Co<sub>3</sub>O<sub>4</sub> composites at 1 mV s<sup>-1</sup> scan rate measured from voltammetry

Sample	$C_{ m sp}$ (F g <sup>-1</sup> )
LMO	307.4
Co <sub>3</sub> O <sub>4</sub>	479.3
LMO-Co <sub>3</sub> O <sub>4</sub> (90%:10%)	755.8
LMO-Co <sub>3</sub> O <sub>4</sub> (70%:30%)	1614.0
LMO-Co <sub>3</sub> O <sub>4</sub> (50%:50%)	576.8



Fig. 10 Charge/discharge curves of LMO-Co<sub>3</sub>O<sub>4</sub> composites at 1 A  $g^{-1}$  current density in 1 M KOH electrolyte.

the chronopotentiomety charge/discharge (charge/discharge) curve of LMO– $Co_3O_4$  composites at a scan rate of 1 A g<sup>-1</sup> current density. The discharge time is directly proportional to the specific capacitance of the compounds. Here, the LMO– $Co_3O_4$ (70%:30%) composite displays a longer discharge time, suggesting that its specific capacitance could be higher than others. Also, an increased plateau region is observed with  $Co_3O_4$  content, indicating that the electrochemical process is occurring at a relatively constant potential due to the nature of the reaction and the kinetics involved. This suggests that the material is undergoing a process where the reaction rate or the electrochemical dynamics stabilize over a range of potentials. This typical asymmetric charge–discharge process is common to batteries where diffusion, phase transition, or polarization plays a distinct role.

Charge/discharge curves at different current densities (0.5 to 15 A g<sup>-1</sup>) were conducted to understand the charge/discharge kinetics, mechanisms, and rate capability of LMO–Co<sub>3</sub>O<sub>4</sub> composites (Fig. 11). The discharge time is longest at a current density of 0.5 A g<sup>-1</sup> but decreases with increasing current density. The decrease in discharge time at higher current densities due to the diffusion of ions within the electrode materials becomes less efficient, and the electrochemical reactions are increasingly confined to the surface of the electrodes. From the charge/discharge curve, the specific capacitance ( $C_{\rm sp}$ ) was calculated using eqn (12),<sup>50</sup> and the values are presented in Table 3.

$$C_{\rm sp} = \frac{I_{\rm m} \times \Delta t}{\Delta V} \tag{12}$$

where  $I_{\rm m}$  is the current density, *m* is the mass of the active material,  $\Delta t$  is the discharge time, and  $\Delta V$  is the potential window.

Fig. 12(a) shows the relationship between the specific capacitance and the current density of the LMO–Co<sub>3</sub>O<sub>4</sub> composites. The specific capacitance of LMO, Co<sub>3</sub>O<sub>4</sub>, LMO–Co<sub>3</sub>O<sub>4</sub> (90%:10%), LMO–Co<sub>3</sub>O<sub>4</sub> (70%:30%), and LMO–Co<sub>3</sub>O<sub>4</sub> (50%:50%) is 356, 223, 493, 660, and 266 F g<sup>-1</sup>, respectively at 0.5 A g<sup>-1</sup> current density presented in Table 3. Here, increasing the ratio of Co<sub>3</sub>O<sub>4</sub> in the LMO, the specific capacitance increases and has a maximum at



Fig. 11 (a)-(e) Charge/discharge curves of LMO-Co<sub>3</sub>O<sub>4</sub> composites at different current densities

the LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%). However, the specific capacitance decreases with a further increase in  $Co_3O_4$  content in the LMO.

The energy density (E; W h kg<sup>-1</sup>) and power density (P; W kg<sup>-1</sup>) are calculated from the following eqn (13) and (14):<sup>51</sup>

$$E = \frac{0.5 \times C_{\rm sp} \times \Delta \nu^2}{3.6} \tag{13}$$

$$P = \frac{3600 \times E}{\Delta t} \tag{14}$$

where *E* is the energy density (W h kg<sup>-1</sup>),  $C_{sp}$  represents specific capacitance (F g<sup>-1</sup>), and  $\Delta v$  is the voltage window (V), *P* is the power density (W kg<sup>-1</sup>), and *t* is the discharge time (s).

The Ragone plot of  $LMO-Co_3O_4$  composites at different current densities are plotted in Fig. 12(b), gives the optimum power-energy characteristics, where the energy density of 31 W h kg<sup>-1</sup> at power density 349 W kg<sup>-1</sup> for  $LMO-Co_3O_4$  (70%:30%) composites at 659.9 F g<sup>-1</sup> of specific capacitance and shown in Table 3. Comparing these values, it is evident that the synergistic effects in  $LMO-Co_3O_4$  are at play in improving the energy and power densities of the composite.

In order to better understand the stability performance in the electrochemical analysis, we conducted the charge/discharge 2000 cycles test at a current density of 10 A g<sup>-1</sup>. Fig. 13 depicts the relationship between specific capacitance and the number of cycles. After testing for 2000 cycles, the specific capacitance retention is 94, 88, 96, 99, and 93% for LMO,  $Co_3O_4$ , LMO- $Co_3O_4$  (90%:10%), LMO- $Co_3O_4$  (70%:30%) and LMO- $Co_3O_4$  (50%:50%) from 169.8, 83.2, 231.7, 274.7, and 67.3 F g<sup>-1</sup> to 160.1, 73.4, 223.5, 271.9, and 62.4 F g<sup>-1</sup>, respectively. High cyclic stability indicates that the charge-discharge Table 3 Specific capacitance, energy, and power density of the LMO–  $\rm Co_3O_4$  composites at 0.5 A  $g^{-1}$  current density

Composites	Specific capacitance, $C_{\rm sp}$ (F g <sup>-1</sup> )	Energy density, E (W h kg <sup>-1</sup> )	Power density, $P(W \text{ kg}^{-1})$
LMO	355.8	17.8	172.7
$Co_3O_4$	223.4	11.2	180.4
LMO-Co <sub>3</sub> O <sub>4</sub> (90%:10%)	492.8	24.6	177.5
LMO-Co <sub>3</sub> O <sub>4</sub> (70%:30%)	660.0	33.0	202.7
LMO-Co <sub>3</sub> O <sub>4</sub> (50%:50%)	266.2	13.3	176.8

process is highly reversible. For battery-type capacitors, where energy is stored via redox reactions, reversibility ensures that no significant side reactions or irreversible changes in the chemical composition occur, leading to minimal loss of active materials over time. Further, the sustained performance across cycles reflects that ion transport (e.g., diffusion of lithium ions, protons, etc.) within the electrode materials remains effective over time. It suggests that the pathways for ion diffusion are not obstructed or degraded even after many cycles of operation. Coulombic efficiency measures how effectively electrical charge is input into useful electrical output during charge and discharge cycles. It is calculated for LMO-Co3O4 composites at 10 A g<sup>-1</sup> using  $\eta = (t_D/t_c) \times 100\%^{52}$  and inset in Fig. 13. Where  $t_D$ and  $t_{\rm C}$  are the discharge and charging time. Here, the coulombic efficiency is almost 100% over 2000 cycles. High coulombic efficiency means that most of the charge added during charging is recovered during the discharging, implying no loss or minimal loss of charge through side reactions or other inefficiencies.



Fig. 12 (a) Specific capacitance vs. current density and (b) the Ragone plot, relation between the log energy density and power density of LMO–Co<sub>3</sub>O<sub>4</sub> composites.



Fig. 13 Cyclic-stability and coulombic efficiency test (inset) of LMO– $Co_3O_4$  composites of chronopotentiometry charge–discharge at a current density at 10 A g<sup>-1</sup> for 2000 cycles.

Table 4 summarizes the electrochemical performance of  $LaMnO_3$  and  $Co_3O_4$ -based electrode materials and composites. The table compares the energy and power densities obtained from the literature with the electrode developed in this work.



Fig. 14 Nyquist plot of LMO-Co<sub>3</sub>O<sub>4</sub> composites.

The LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites have relatively higher specific capacitance than the previously reported values.

**3.2.3. EIS fitting.** The Electrochemical Impedance Spectroscopy (EIS) analysis was carried out across a frequency range of 10 mHz to 100 kHz (Fig. 14). The EIS diagram is categorized into three distinct sections. The high-frequency region is

Table 4	Comparison	of specific	capacitance,	energy,	and p	power	density	of LM	D-Co <sub>3</sub> O <sub>4</sub>	composites	with	previously	reported	values	or r	relative
compour	nds															

Material	Current density or scan rate	Electrolyte (Na <sub>2</sub> SO <sub>4</sub> )	Specific capacitance, $C_{\rm P} ({\rm F g}^{-1})$	Energy density, E (W h kg <sup>-1</sup> )	Power density, $P(W \text{ kg}^{-1})$	Ref.
$LaMn_{1\pm x}O_3$	$1 \mathrm{A} \mathrm{g}^{-1}$	1 M KOH	549 mA h $g^{-1}$	_	_	31
LaCoO <sub>3</sub>	$1 \text{ A g}^{-1}$	1 M KOH	203	—	—	53
La <sub>0.5</sub> Ca <sub>0.5</sub> MnO <sub>3</sub>	$1 \text{ A g}^{-1}$	1 M KOH	170	7.6	160	24
LMO-Co <sub>3</sub> O <sub>4</sub> (70%:30%)	$0.5 \ { m \AA g}^{-1}$	1 M KOH	660.0	33.0	202.7	Present work
Hollow dendritic Co <sub>3</sub> O <sub>4</sub> /CeO <sub>2</sub>	$0.5 \text{ A g}^{-1}$	6 M KOH	276.3	—	_	54
Hollow spherical La <sub>2</sub> CoMnO <sub>6</sub>	$1 \text{ A g}^{-1}$	1 M	376	—	_	55
LaMnO <sub>3</sub> @NiCo <sub>2</sub> O <sub>4</sub> Ni	$0.5 \ { m \AA g}^{-1}$	6 M KOH	$811 \text{ C g}^{-1}$	—	_	22
La <sub>0.85</sub> Sr <sub>0.15</sub> MnO <sub>3</sub> /NiCo <sub>2</sub> O <sub>4</sub>	$0.5 \text{ A g}^{-1}$	1 M Na <sub>2</sub> SO <sub>4</sub>	1341	63.5	900	56
$La_{0.7}Sr_{0.3}CoO_{3-\delta}$	$2 \text{ A g}^{-1}$	1 M	747.75	34.8	400	57
LaMnO <sub>3</sub> -Mn <sub>3</sub> O <sub>4</sub> (70%:30%)	$1 \text{ A g}^{-1}$	6 M KOH	478.8	23.9	355.7	21
NiO/NiCo <sub>2</sub> O <sub>4</sub> /Co <sub>3</sub> O <sub>4</sub>	$5 \text{ mA cm}^{-2}$	2 M KOH	1717	_	_	58
LaMnO <sub>3</sub> /CeO <sub>2</sub>	$1 \text{ A g}^{-1}$	1 M	262.0	_	_	59

(cc)

Composites	$R_{1}\left(\Omega\right)$	$R_2(\Omega)$	$W_0\left(\Omega, imes 10^{-3} ight)$	$\text{CPE}_1(\alpha)$	$\text{CPE}_1\left(Q;\Omega^{-1}\;s^{\alpha}\right)$	$\text{CPE}_2(\alpha)$	$\text{CPE}_2\left(\mathbf{Q},\mathbf{\Omega}^{-1}\;\mathbf{s}^{\alpha}\right)$	Goodness of fit ( $\times 10^{-3}$ )
LMO	1.901	38.31	0.183	0.703	0.005	0.906	0.003	0.152
$Co_3O_4$	1.709	11.37	0.086	0.716	0.005	0.894	0.002	0.261
LMO-Co <sub>3</sub> O <sub>4</sub> (90%:10%)	1.913	11.36	0.398	0.624	0.001	0.866	0.003	0.108
LMO-Co <sub>3</sub> O <sub>4</sub> (70%:30%)	0.57	7.12	0.186	0.608	0.008	0.976	0.002	0.186
LMO-Co <sub>3</sub> O <sub>4</sub> (50%:50%)	1.834	34.99	0.173	0.698	0.003	0.928	0.002	1.132

Table 5 Equivalent fitting values of Nyquist plot of LMO-Co<sub>3</sub>O<sub>4</sub> composites

marked by the initial intercept, known as the comprehensive resistance  $(R_s \text{ or } R_1)$ . This resistance includes the contact resistance between the electrode material and the collecting fluid, the resistance associated with ion transport within the electrolyte, and the inherent resistance of the electrode material. The intermediate-frequency region features a semicircular curve representing the charge transfer resistance  $(R_2)$ . In our analysis, the absence of this semicircle indicates a very low charge transfer resistance and a high diffusion coefficient. The low-frequency region is characterized by a linear plot, representing the Warburg impedance  $(W_0)$  resulting from the diffusion of ions at the electrolyte-electrode interface.60 A steeper line slope would mean a smaller diffusion impedance in low-frequency regions. The inset plot shows the fitted equivalent circuit diagram of the LMO-Co<sub>3</sub>O<sub>4</sub> composites by using the Gamry Echem Analyst software. That equivalent circuit contains  $R_1$ ,  $R_2$ ,  $W_0$ , and constant phase element (CPE<sub>1</sub> and CPE<sub>2</sub>). The impedance of the CPE is  $Z_{\text{CPE}} = 1/Q(i\omega)^{\alpha}$ . Where O is the CPE constant, related to the admittance of the element. The exponent  $\alpha$  in the CPE represent the phase deviation from the ideal scenario, where the impedance plot  $(Z_{re} vs. Z_{im})$  would form a vertical line perpendicular to the real axis and parallel to the imaginary axis. When  $\alpha = 1$ , the CPE behaves like a pure capacitor; when  $\alpha = 0$ , it resembles a resistor; and when  $\alpha = 0.5$ , it behaves as Warburg impedance.

The charge transfer resistance ( $R_2$ ) was calculated to be 38.31, 11.37, 11.36, 7.12, and 35.00  $\Omega$  for LMO, Co<sub>3</sub>O<sub>4</sub>, LMO– Co<sub>3</sub>O<sub>4</sub> (90%:10%), LMO–Co<sub>3</sub>O<sub>4</sub> (70%:30%), and LMO–Co<sub>3</sub>O<sub>4</sub> (50%:50%) composites, respectively and presented on Table 5. The decrease in  $R_2$  trends from the LMO samples to LMO– Co<sub>3</sub>O<sub>4</sub> (50%:50%) composites should be associated with the increased electrode and electrolyte interface contact area. Its  $W_0$ value is also highest at 0.389  $\Omega$ , indicating ions' diffusion between the electrode and electrolyte interface.

The specific capacitance of pure LMO and  $\text{Co}_3\text{O}_4$  is lower compared to their composites, which can be attributed to several synergistic factors: (1) the composite has a higher specific surface area and pore radius, LMO– $\text{Co}_3\text{O}_4$  (70%:30%) has the highest specific surface area, 6.79 m<sup>2</sup> g<sup>-1</sup>, and average pore size (radius) 13.48 nm, respectively provide more accessible active sites for electrochemical reactions, enhancing ion adsorption and desorption, (2) LMO is known for its good pseudocapacitive properties due to the multiple valence states of Mn, but its tendency to aggregate limits its effectiveness. On the other hand,  $\text{Co}_3\text{O}_4$  is naturally porous. When combined, LMO and  $\text{Co}_3\text{O}_4$  form composites that reduce LMO aggregation, resulting in a more porous structure. This enhanced porosity is beneficial for electrochemical analysis, as it increases the surface area available for reactions, improves ion diffusion, and ultimately enhances the overall electrochemical performance of the composite, (3) both materials undergo multiple oxidation states, contributing significantly to the overall charge storage, (4) increased  $Co_3O_4$  content may create oxygen vacancies in LMO, enhancing electrochemical performance, and (5) improved interfacial interaction between LMO and  $Co_3O_4$  facilitates efficient electron transfer and ion exchange, leading to higher specific capacitance.

### 4. Conclusion

In this study, LMO-Co<sub>3</sub>O<sub>4</sub> composites were synthesized using the autocombustion method to enhance supercapacitor performance. The LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites with relatively high surface area and pore density demonstrated a significantly high specific capacitance of 1614 F  $g^{-1}$  at a scan rate of 1 mV  $s^{-1}$ and 660 F  $g^{-1}$  at a current density of 0.5 A  $g^{-1}$ , which are 5.25 and 1.85 times greater, respectively, than those of LMO alone. This substantial increase in specific capacitance is attributed to the synergistic effects between LMO and Co<sub>3</sub>O<sub>4</sub>. The Co<sub>3</sub>O<sub>4</sub> component effectively mitigates kinetic challenges related to charge transfer and ion transport within the LMO-Co<sub>3</sub>O<sub>4</sub> (70%:30%) composites. These composites exhibit excellent cyclic stability with battery-type behavior, retaining 99% of their capacity after 2000 cycles. These impressive attributes make LMO-Co<sub>3</sub>O<sub>4</sub> composites a promising and effective electrode material for highperformance supercapacitors and energy storage devices.

## Data availability

Data for this article, including BET, electrochemical analysis, XPS, and XRD of LMO– $Co_3O_4$  composites are available at Zenodo at https://zenodo.org/uploads/14159771.

## Conflicts of interest

There are no conflicts to declare.

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