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## communication

## Gas permeation properties of hollow glass-crystalline microspheres

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5 Permeation of He, H<sub>2</sub> and Ne was studied for hollow glasscrystalline microspheres. Microspheres demonstrated high permeability to helium with high selectivity for  $He/H_2$  and He/Ne owing to the composition and structure of their shells.

Helium is a key component in many high-tech industries. <sup>10</sup> The modern industrial technology for the production of highpurity helium (99.9950 vol %) is based on its release from the natural gas using the energy-intensive cryogenic process. This process includes the low-temperature condensation stage with the formation of a helium concentrate containing

15 approximately 80 vol % He, followed by several stages of its purification from methane, hydrogen, oxygen, nitrogen, argon, and neon.<sup>1</sup>

An alternative helium production direction is the energyefficient diffusion-sorption technology<sup>2</sup> combining pressure

- 20 swing adsorption (PSA) and membrane separation. An implementation of the membrane separation in practice requires the use of membrane materials with high helium permeability and selectivity, high chemical and thermal stability, high strength, and low cost.
- It is known that polymeric materials exhibit a high permeability to helium (Table 1). However, the selectivity for He/CH<sub>4</sub> of different polymers varies in the range from 6 to 184 and, in rare cases, reaches a value of the order of  $10^{3.3}$  In addition to the poor selectivity, the disadvantages of
- 30 polymeric membranes are the low strength, low thermal stability, and, in some cases, high cost and synthesis complexity. For these reasons, among several hundreds of known polymeric materials, only few have been used by industry for the isolation of H<sub>2</sub>, production of O<sub>2</sub> and N<sub>2</sub>, and 35 CO<sub>2</sub> extraction.<sup>5</sup>

Carbon molecular sieve membranes,<sup>6</sup> which can be produced by pyrolysis of polymeric precursor, are characterized by a high temperature operations but a low selectivity for He/CH<sub>4</sub>.

- By their permeability to helium, polymeric materials correspond to nanoporous and microporous materials (Table 1), in particular, zeolite T membranes prepared by the hydrothermal synthesis on porous mullite tubes<sup>8</sup> and metalorganic frameworks (MOFs) membranes.9,10 These materials,
- 45 as well as polymers, are characterized by a low selectivity for He/CH<sub>4</sub>. Moreover, it is problematic for them to obtain defectfree layers of large surface area.

<b>Table 1</b> Permeability and selectivity of membrane materials									
Sample	Temperature	Permeability Selectiv		vity	Ref.				
*	(K)	coefficient for He	He/CH <sub>4</sub>	He/Ne					
	$(mol \cdot m)/(m^2 \cdot s \cdot Pa)$								
Polymeric membranes									
Polypyrrolone	298	98 8·10 <sup>-15</sup>			3				
Polyimide	308	$7 \cdot 10^{-15}$	92		4				
Teflon AF-2400	298	$1 \cdot 10^{-12}$	6		3				
Carbon molecular sieve membranes									
C-HBPI-1	308	$2 \cdot 10^{-13}$	33		7				
Nano- and microporous membranes									
Zeolite T	378	$2 \cdot 10^{-13}$	25-51		8				
Cu-MOF	298	3.10-11 - 6.10-14	2-7		9, 10				
Ultra microporous glass hollow-fiber	473	$2 \cdot 10^{-14}$	10 <sup>4</sup>		12				
Microporous glass	300	$3 \cdot 10^{-13}$	$10^{4}$		13				
Silicate glasses									
	298	3.10-17		$10^{3}$	1.5				
Silica glass	553	$1 \cdot 10^{-15}$			15,				
0	673	3.10-15	$10^{6}$		16				
CCW 7740	298	5.10-18			17				
CGw-//40	553	5·10 <sup>-16</sup>		$10^{2}$	1/				

Permeability coefficients are given in the SI units:  $1 \pmod{m^2 \cdot s \cdot Pa} =$ 50 2.9·10<sup>15</sup> Barrer

A specific direction is the preparation of porous membrane maretials by chemical etching of silicate glasses.<sup>11-13</sup> The ultra-microporous and microporous membranes thus produced are characterized by a high permeability to helium and the ss selectivity for He/CH<sub>4</sub> at a level of  $10^4$ , which significantly exceeds the corresponding value for polymers (Table 1).

Taking into account the technical requirements to helium quality,<sup>14</sup> in which the concentration of impurities should not exceed 0.005%, including neon (no more than 0.004%), the 60 most suitable for selective extraction of helium are silicate glasses characterized by high values of selectivity for He/CH<sub>4</sub> and He/Ne (Table 1).<sup>15-17</sup> The diffusion properties of silicate glasses are determined by their composition and structure. With a decrease in the content of network modifier oxides 65 (Al<sub>2</sub>O<sub>3</sub>, K<sub>2</sub>O, Na<sub>2</sub>O, MgO, CaO, Fe<sub>2</sub>O<sub>3</sub>), their permeability to helium increases<sup>15</sup> due to its diffusion primarily through the silica-rich phase.<sup>17</sup> The silica glass structure, presenting a three-dimensional network of multi-membered rings formed by the SiO<sub>4</sub> tetrahedra, was described for the first time by the 70 theoretical model proposed by Zachariasen<sup>18</sup> and confirmed experimentally by transmission electron microscopy of silica glass supported on graphene.<sup>19</sup>

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Fig. 1. SEM images of cenospheres HM-P-5A 1273 K, O<sub>2</sub>

- <sup>5</sup> In this communication, we present results of investigation into the permeability of hollow glass-crystalline microspheres to helium, hydrogen, and neon as a function of the composition and structure of their shells. We used the fractions of nonmagnetic nonperforated aluminosilicate <sup>10</sup> cenospheres (Fig. 1) with narrow size distributions of globules with a certain composition, morphology, and thickness of glass-crystalline shell.<sup>20-22</sup> The extraction of cenosphere narrow fractions was carried out from cenosphere concentrates of fly ash with the use of a technological setup,<sup>20</sup>
- <sup>15</sup> which included the stages of hydrodynamic separation, sizing, magnetic separation, and aerodynamic classification with the subsequent hydrostatic isolation of the destroyed globules. The average diameter of cenospheres in the fraction -0.063+0.05 mm is equal to 58-61 µm, with the shell thickness
- <sup>20</sup> being 2.5-3.1  $\mu$ m.<sup>21</sup> According to the chemical composition, the cenospheres are considered as a multi-component system with the contents of the major components SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub> in the ranges of 58-61 and 26-37 wt %, respectively. The cenosphere shell consists of the glass phase and crystalline <sup>25</sup> phases, such as mullite, quartz, and calcite. The outer and

inner surfaces of the globules are covered with a nanometer-sized (30-50 nm) film.  $^{23,\,24}$ 

In order to increase the content of crystalline phases and to decrease the content of network modifier oxides in the glass <sup>30</sup> phase, the cenospheres were subjected to thermal treatment at temperatures of 1273 and 1373 K in an oxygen or argon atmosphere (Table 2). This resulted in the formation of an additional mullite (I) phase, which differed from the original mullite (0) by smaller crystallite sizes and different lattice <sup>35</sup> parameters. In some cases, the cristobalite phase also appeared (Table 2).

The composition of the mullite (I) phase depends on the thermal treatment atmosphere, as evidenced by variations in its lattice parameters. The formation of this phase in an <sup>40</sup> oxygen atmosphere is accompanied by the oxidation of Fe<sup>2+</sup> ions to Fe<sup>3+</sup>, their extraction from the glass phase, and incorporation into the Al<sup>3+</sup> ion positions of the crystallized mullite lattice. This results in the formation of a defective iron-containing phase of mullite (I), whose lattice parameters <sup>45</sup> exceed the data available in the literature over the entire range of possible Al/Si ratios in mullite.<sup>25, 26</sup> The lattice parameters

Table 2 Phase con	nposition of	cenospheres	(wt %)
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Sample	Mullite (0)	Mullite (I)	Quartz	Cristobalite	Calcite	Glass phase			
Initial cenospheres									
H-0.08	3.7	0	3.0	0	0.6	92.7			
HM-M-5A	8.4	0	1.5	0	0.7	89.4			
HM-P-5A	30.1	0	1.4	0	0.3	68.2			
Cenospheres after thermal treatment in different gas atmospheres									
HM-M-5A	9.5	20.9	1.7	0	0	67.9			
1273 K, O <sub>2</sub>						07.9			
HM-P-5A	31.3	5.9	2.4	0.5	0	59.9			
1273 K, O <sub>2</sub>									
HM-P-5A	37.0	11.4	2.1	14.1	0	35 /			
1373 K, O <sub>2</sub>	57.0					55.4			
HM-M-5A	8.6	21.2	2.9	0	0	673			
<i>1273 K,</i> Ar						07.5			
HM-M-5A									
<i>1273 K</i> , Ar	9.4	23.6	2.6	0.4	0	64.0			
1273 K, O <sub>2</sub>									

of mullite (I) formed in an inert atmosphere of argon are characterized by systematically lower values corresponding to s defect-free phases.

The permeability of cenosphere shells was investigated in comparison with synthetic hollow glass microspheres  $3M^{TM}$  (Glass Bubbles K37, fraction -0.063+0.05 mm) with the average globule diameter of 57 µm and the shell thickness of <sup>10</sup> 1.4 µm, in which the content of the major components was as

- follows: 70.62 wt % SiO<sub>2</sub>, 13.67 wt % CaO, and 8.90 wt %. The glass microspheres contained 1 wt % of cristobalite.
- The permeability of the cenospheres and microspheres to single gas He, H<sub>2</sub>, and Ne was investigated in a vacuum <sup>15</sup> apparatus under the conditions of gas diffusion from the reactor volume into globules at a pressure of  $3 \cdot 10^4$  Pa in the temperature range from 298 to 623 K for helium and from 553 to 773 K for hydrogen and neon.<sup>21</sup> The diffusion of gases through the globule shells occurred as a result of the
- <sup>20</sup> difference between the gas partial pressures outside and inside the globules. The permeability determination of the microsphere and cenosphere shells was based on measuring the time-dependence of the gas pressure drop after the repassage into the reactor filled with the sample. The relative
- <sup>25</sup> error in the determination of the permeability does not exceed 10%. The permeability coefficient values K of the glass phase were calculated taking into account its content and keeping in mind that the permeability of the crystalline phases is several orders of magnitude lower than that of the glass phase.<sup>27</sup> The

<sup>30</sup> selectivity was defined as ratio of K for single gases.

The increase in the mullite phase content led to respective increase in the cenosphere shell permeability for the studied gases over the entire temperature range. Figure 2 shows the dependences of the permeability coefficients  $K_{\text{He}}$ ,  $K_{\text{H2}}$ , and

- <sup>35</sup>  $K_{\text{Ne}}$  at 553 K on the mullite phase content in the cenospheres. Exceptions were cenospheres in which the crystallization of mullite (I) occurred in an inert atmosphere. In this case, there was no oxidation of Fe<sup>2+</sup> ions to the Fe<sup>3+</sup> state in which iron could be embedded into the lattice of the mullite formed,
- <sup>40</sup> which was confirmed by the decreased values of its lattice parameters. The iron ions remaining in the glass phase hindered the diffusion of helium. A subsequent oxidation Fe<sup>2+</sup>



Fig. 2 Dependences of glass phase permeability of cenospheres to He, H<sub>2</sub>, and Ne at 553 K on the content of mullite formed during thermal treatment in O<sub>2</sub> (closed symbols ) and Ar (open symbols).

 $\rightarrow$  Fe<sup>3+</sup> (sample HM-M-5A 1273 K, Ar 1273 K, O<sub>2</sub>) did not lead to any significant changes in the diffusion properties of the cenospheres, since the iron ions were kept in the glass <sup>50</sup> phase.

The crystallization of mullite in an oxidizing atmosphere led to a decrease in the content of network modifier cations in the glass phase and to an increase in the permeability of the cenosphere shell with high values of selectivity for He/H<sub>2</sub> and <sup>55</sup> He/Ne. The cenospheres with the maximum mullite phase content (48.4 wt %) are characterized by the permeability coefficient  $K_{\text{He}}$  corresponding to the level of silica glass (Table 1), which is several orders of magnitude higher than the permeability coefficient  $K_{\text{He}}$  for synthetic glass-<sup>60</sup> microspheres 3M K37. The values of the selectivity for He/H<sub>2</sub> and He/Ne at a temperature of 553 K are equal to 32 and 221, respectively. The activation energies for He, H<sub>2</sub>, and Ne diffusion are equal to 25, 30, and 42 kJ/mol, respectively.

In conclusion, microsphere materials with a high 65 permeability to helium and a high selectivity for He/H<sub>2</sub> and He/Ne have been prepared by thermal treatment of narrow fractions of fly ash cenospheres in an oxygen atmosphere. The mullite phase formed during the high-temperature crystallization favors both purification of the silicate glass 70 phase from network modifier cations and additional strengthening of the cenosphere shell. The use of these materials underlies the energy-efficient diffusion technology for the separation of gas mixtures.<sup>2,28</sup> The modules on the base of cenosphere are characterized by a large surface area per  $_{75}$  unit volume 60000 m<sup>2</sup>/m<sup>3</sup>, which higher than the value for membrane cells fabricated from hollow fibers (20000 m<sup>2</sup>/m<sup>3</sup>) and exceeds that of rolling  $(1000 \text{ m}^2/\text{m}^3)$  and flat membranes (100  $m^2\!/m^3)$  by several orders of magnitude.  $^{29}$  Moreover, such modules possess reliable gas-separation properties for a long

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time, because the efficiency of the process does not depend on the damage of individual globules. These advantages, in combination with high values of permeability to helium and the selectivity for He/H<sub>2</sub> and He/Ne, can provide high efficiency of the diffusion process for helium isolation and

- s efficiency of the diffusion process for helium isolation and purification. The present results are promising for actual applications of glass-crystalline microspheres for helium capture.
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Table of contents

Microsphere materials for helium capture have been prepared on the base of narrow fractions of fly ash cenospheres.

