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**Biogas dry reforming for syngas production: Catalytic performance of nickel supported on waste-derived SiO<sub>2</sub>**

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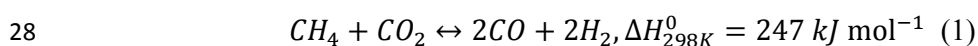
1 **Abstract**

2 SiO<sub>2</sub> synthesized from photovoltaic waste by a vapor-phase hydrolysis method  
3 was applied as the support for a nickel catalyst in a biogas dry reforming process for  
4 the first time. The results were compared with the catalytic performance of  
5 commercial precipitated SiO<sub>2</sub> and ordered mesoporous SiO<sub>2</sub>. Nickel supported on  
6 waste derived SiO<sub>2</sub> had a high CH<sub>4</sub> conversion (92.3%) and a high CO<sub>2</sub> conversion  
7 (95.8%) at 800°C, and there was no deactivation after 40 h-on-stream test. Catalyst  
8 characterization results revealed that the S<sub>BET</sub> values and pore properties of catalysts  
9 affected the catalytic performance. A higher pore volume/S<sub>BET</sub> ratio led to a smaller  
10 crystal metal size and higher metal dispersion; thus the catalyst was less prone to  
11 deactivation. This discovery will help improve catalyst design. The use of nickel  
12 supported on waste-derived SiO<sub>2</sub>, which is competitive to commercial and  
13 mesoporous one, provides a use for photovoltaic waste as a high value-added product,  
14 and also can deliver a cheap and environmentally benign support for catalysts in the

15 biogas dry reforming process.

## 16 **1. Introduction**

17 Biogas is a mixture of mainly methane and carbon dioxide that is produced by  
18 the anaerobic digestion of residual biomass, such as landfilled waste, municipal  
19 sludge, and food waste. With the growing concern regarding global climate change  
20 due to anthropogenic CO<sub>2</sub> emissions, biogas recycling for energy-related applications  
21 has received much attention.<sup>1</sup> Therefore, biogas dry reforming for syngas production  
22 (Equation 1) is a recycling option with several advantages: (i) biogas dry reforming  
23 processes can simultaneously consume the two main greenhouse gases (CH<sub>4</sub> and CO<sub>2</sub>);  
24 (ii) the H<sub>2</sub>/CO ratio is close to 1, which makes it suitable for further use in the  
25 carbonylation, hydroformylation, and Fischer–Tropsch synthesis of long chain  
26 hydrocarbons;<sup>2</sup> and (iii) the process avoids the separation of CO<sub>2</sub>, which is an energy  
27 intensive and costly process.<sup>3-5</sup>



29 The high cost and energy consumption of biogas dry reforming has restricted its  
30 industrial application.<sup>6</sup> Because biogas dry reforming is a strong endothermic process  
31 (see equation 1), the high reaction temperature will achieve a relatively high  
32 conversion of reactants.<sup>7,8</sup> In addition, catalysts also play a vital role in the catalytic  
33 dry reforming process, which increases the cost substantially. Improving the stability  
34 and choosing relatively cheap raw materials to prepare the catalyst, without a loss in  
35 catalyst activity, is important.

36 The main obstacle to stability is the deactivation of catalysts, which is caused  
37 mainly by the deposition of inactive carbon and the sintering of active metal.<sup>9, 10</sup> To  
38 improve catalyst stability, many studies have been conducted to optimize the active  
39 metals, catalyst supports, and catalyst preparation methods.<sup>3, 11-14</sup> During these  
40 processes, the low-cost and availability of the raw materials used for catalyst  
41 preparation is important. Ni-based catalysts are commonly used in dry reforming  
42 process due to their reasonably good activity and low cost compared to noble metals,  
43 although they are more sensitive to coke formation than the noble metals.<sup>2, 10, 13, 15</sup>  
44 Many dioxides, including SiO<sub>2</sub><sup>12, 16-18</sup>, ZrO<sub>2</sub>,<sup>19</sup> MgO,<sup>20</sup> TiO<sub>2</sub>,<sup>8</sup> CeO<sub>2</sub>,<sup>11</sup> Al<sub>2</sub>O<sub>3</sub>,<sup>3, 21</sup> and  
45 their hybrids<sup>15, 22, 23</sup> have been used as catalyst supports in reforming process due to  
46 their high specific surface area and high thermal stability. Of these, SiO<sub>2</sub> and  
47 SiO<sub>2</sub>-based catalyst supports are the most widely used and the most promising for the  
48 industrial application of the dry reforming process due to their availability and various  
49 phase morphologies. Frontera, et al.<sup>12</sup> investigated the activity and stability of several  
50 nickel catalysts supported on different types of highly crystalline silica zeolites,  
51 including Ni-ITQ-6, Ni-silicalite-1, and Ni-MCM-41, and found that the  
52 heterogeneity of the support surface strongly affected the catalyst performance. Ning  
53 Wang, et al.<sup>18</sup> also found that the pore topology of different types of SiO<sub>2</sub> affected the  
54 particle dispersion, reducibility, and catalytic behavior of catalysts. The synthesis of  
55 silica zeolites consumes large amounts of organic template agents, and these zeolites  
56 are currently not commercially available in large quantities.<sup>24</sup> Therefore, the  
57 development of new silica materials, with a high specific surface area, high thermal

58 stability, and most importantly, the potential for large-scale production is essential.

59 In our previous study, polyporous nano-silica synthesized from photovoltaic  
60 waste  $\text{SiCl}_4$  using a low temperature vapor-phase hydrolysis method (designated as  
61  $\text{SiO}_2\text{-H}$ ) was shown to have a relatively high specific surface area and high thermal  
62 stability.<sup>25</sup> Considering the large-scale production and poor treatment condition of  
63 photovoltaic waste  $\text{SiCl}_4$ , the production of  $\text{SiO}_2\text{-H}$ , and its further application as a  
64 catalyst support for biogas dry reforming represents a useful conversion of  
65 photovoltaic waste to a high value-added product, as well as providing a cheap and  
66 environmentally benign support for catalysts in the biogas dry reforming process.  
67 Using  $\text{SiO}_2\text{-H}$  as a waste-derived  $\text{SiO}_2$  support in biogas catalytic dry reforming  
68 applications has not been reported previously.

69 A comprehensive evaluation of the catalytic performance of nickel supported on  
70 waste derived  $\text{SiO}_2$  in biogas dry reforming was undertaken.  $\text{SiO}_2\text{-H}$  was used as  
71 support for nickel catalyst in a biogas dry reforming process for the first time, and  
72 commercial precipitated  $\text{SiO}_2$  and mesoporous  $\text{SiO}_2$  were also considered for  
73 comparison. Catalytic tests of the three different nickel supported catalysts and the  
74 related characterization of both fresh and spent catalysts were undertaken  
75 systematically.

## 76 **2. Materials & Methods**

### 77 **2.1 Support and Catalyst Preparation**

78 A low temperature vapor-phase hydrolysis method was used to synthesize

79 SiO<sub>2</sub>-H as previously reported.<sup>25</sup> Silicon tetrachloride (99%: LDK Solar Ltd., Xinyu,  
80 China) was vaporized and hydrolyzed with water vapor at a temperature of 200°C, a  
81 retention time of 5 s, and a H<sub>2</sub>O/SiCl<sub>4</sub> molar ratio of 2. Silica powder was collected  
82 and dried at 105°C for 2 h.

83 Commercial precipitated SiO<sub>2</sub> (designated as SiO<sub>2</sub>-P) and ordered mesoporous  
84 silica (SBA-15) were purchased (Sigma–Aldrich, St Louis, MO, USA). All three of  
85 the SiO<sub>2</sub> supports were calcined at 700°C for 4 h to enhance their thermal stability and  
86 remove surface moisture.

87 An ultrasonic-assisted wetness impregnation method was used to prepare  
88 Ni/SiO<sub>2</sub> catalysts with a 10 wt% Ni. The metallic precursor solution was obtained by  
89 dissolving Ni(NO<sub>3</sub>)<sub>2</sub>·6H<sub>2</sub>O (99%: Sigma–Aldrich) in ethanol with a Ni-ethanol ratio  
90 of 2g/L. The three SiO<sub>2</sub> supports were dispersed into ethanol after ultrasonic  
91 oscillation to obtain a SiO<sub>2</sub> colloidal solution. The Ni precursor solution was then  
92 added dropwise to the SiO<sub>2</sub> colloidal solution under magnetic stirring. The solution  
93 was agitated at 70°C for 12 h to remove the ethanol. The catalysts were dried at 60°C  
94 for 6 h in a vacuum oven and calcined at 800°C for 4 h. Catalysts synthesized from  
95 the SiO<sub>2</sub>-H, SBA-15, and the SiO<sub>2</sub>-P supports were designated Ni/SiO<sub>2</sub>-H, Ni/SBA-15,  
96 and Ni/SiO<sub>2</sub>-P, respectively.

## 97 **2.2 Catalyst Characterization**

98 XRD patterns were obtained with a D8 Advance X-ray diffractometer (Siemens,  
99 Munich) using Cu-K $\alpha$  radiation ( $\lambda = 0.15406$  nm), with a  $2\theta$  range of 0.3–80°. The  
100 Scherrer equation was used to estimate the mean Ni crystallite size based on the

101 diffraction peaks of the Ni (200) facet. Analysis of the Ni loading of catalysts was  
102 undertaken using an XRF analyzer (XRF-1800, Shimadzu).

103 Textual properties were measured by a Surface Area and Porosity Analyzer  
104 (ASAP2020 HD88, Micromeritics) through the nitrogen adsorption–desorption  
105 isotherms at 77 K. The samples were degassed at 90°C for 60 min and held at 160°C  
106 for 120 min before analysis. A Barrett–Emmett–Teller (BET) model was used to  
107 calculate the specific surface area and a Barrett–Joiner–Halenda (BJH) model was used  
108 to calculate the pore volume distribution.

109 Transmission electron microscopy (TEM) (JEM-2011, JEOL Ltd) was used to  
110 observe the morphology and distribution of metal sites. The samples were first  
111 dispersed in ethanol, and then one drop of ethanol solution was placed on a copper  
112 grid pre-coated with a Formvar film and dried in air. And SEM (S-5500, Hitachi) was  
113 also used to observe the morphology the samples.

114 The H<sub>2</sub> temperature-programmed reduction (H<sub>2</sub>-TPR) was employed to analyze  
115 the reduction behavior of catalysts using a Chemisorption Analyzer (AutoChem II  
116 2920, Micromeritics). Catalyst samples (50 mg, 20–40 mesh) were pretreated at  
117 400°C for 1 h under flowing Ar (30 ml/min). Upon cooling to 50°C, the sample was  
118 heated from room temperature (RT) to 1000°C with a temperature ramp of 10°C/min  
119 under a 5 vol% H<sub>2</sub>/Ar stream (50 mL/min).

120 The TGA-MS method was applied to investigate the carbon deposition with a  
121 TGA/DSC 1 STARe system (METTLER TOLEDO) and a Thermostar mass  
122 spectrometer (Pfeiffer). Samples were treated at a rate of 10°C/min from RT to 900°C

123 under an oxygen stream of 20 mL/min with nitrogen as protection gas.

## 124 2.3 Catalytic Tests

125 Catalytic tests of biogas dry reforming were conducted in a fixed-bed reactor  
126 with a quartz glass tube (diameter = 6 mm) under atmospheric pressure. 200 mg of the  
127 samples (20–40 mesh) were loaded in the center of the tube reactor. Before the test,  
128 the catalysts were reduced at 800°C in situ for 1 h in a flow of 10 vol% H<sub>2</sub>/N<sub>2</sub>. A flow  
129 rate of 50 mL/min mixture gas (CH<sub>4</sub>:CO<sub>2</sub>:N<sub>2</sub> = 0.4:0.4:0.2) was used, in which N<sub>2</sub> was  
130 the reference gas for end gas analysis. The products were analyzed using on-line GC  
131 apparatus (GC-2014: Shimadzu) with a combined PC-1, MC-1, and MC-2  
132 chromatographic column and a thermal conductivity detector. Catalytic activity of all  
133 of the samples, including a blank sample (20–40 mesh SiO<sub>2</sub> support without Ni) was  
134 tested at temperatures from 600 to 900°C after being in a steady state for 1 h. Stability  
135 tests of Ni/SiO<sub>2</sub>-H, Ni/SBA-15, and Ni/SiO<sub>2</sub>-P were conducted at 800°C for 40 h  
136 on-stream, and the products were analyzed every 30 min. The conversion (X) and the  
137 H<sub>2</sub>/CO ratio were calculated as follows:

$$138 \quad X_{CH_4} (\%) = \frac{[CH_4]_{in} - [CH_4]_{out}}{[CH_4]_{in}} \times 100$$

$$139 \quad X_{CO_2} (\%) = \frac{[CO_2]_{in} - [CO_2]_{out}}{[CO_2]_{in}} \times 100$$

$$140 \quad \frac{H_2}{CO} \text{ ratio} = \frac{\text{mole of } H_2 \text{ produced}}{\text{mole of } CO \text{ produced}}$$

## 141 3 Results and Discussion

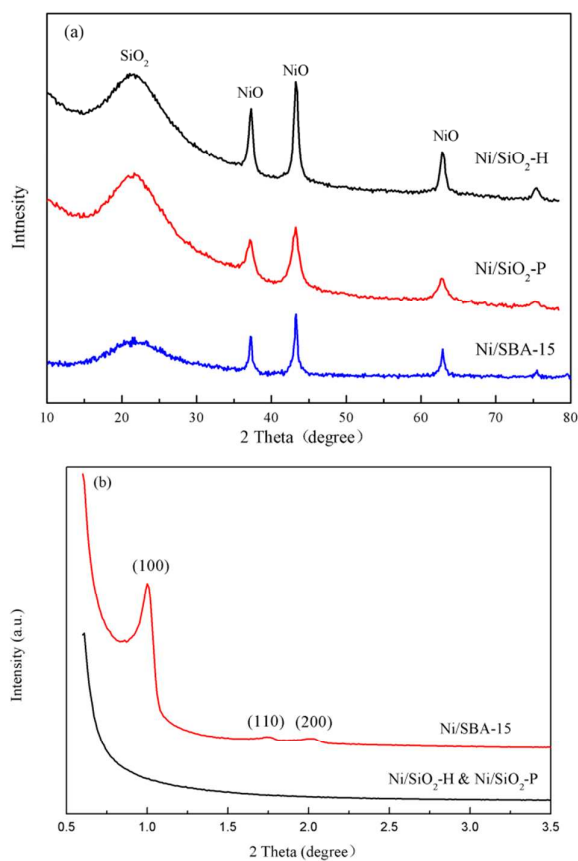
### 142 3.1 Characterization of Fresh Catalysts



143 The XRD patterns of fresh catalysts are shown in Figure 1. Reflections of SiO<sub>2</sub>  
144 and NiO were detected in all three fresh SiO<sub>2</sub> supported nickel catalysts in their  
145 wide-angle XRD patterns (Figure 1a). Three sharp peaks were clearly visible at 37.3°,  
146 43.3° and 62.9°, which corresponded to the crystal NiO structure for (111), (200), and  
147 (220) reflections, respectively (PDF#47-1049). Strong and broad diffractions with a  
148 wide 2θ range at 15–30° were assigned to amorphous SiO<sub>2</sub>.<sup>26</sup> Compared to Ni/SiO<sub>2</sub>-H  
149 and Ni/SiO<sub>2</sub>-P, Ni/SBA-15 had a less erratic diffraction peak at 15–30°. This may be  
150 because SBA-15 has a highly ordered mesoporous structure. This was confirmed by  
151 the small-angle XRD patterns (Figure 1b). Ni/SBA-15 had remarkable peaks of  
152 ordered mesoporous silica (100), (110), and (200) planes, indicating a high degree of  
153 hexagonal mesoscopic organization.<sup>27, 28</sup> No peaks were found in the small-angle  
154 XRD patterns of Ni/SiO<sub>2</sub>-H and Ni/SiO<sub>2</sub>-P, indicating a heterogeneous porosity.

155 The average crystallite size of NiO was determined by the diffraction peak of the  
156 NiO (200) plane in XRD patterns, using the Scherrer equation (Table 1). The average  
157 crystal metal size increased in the order Ni/SiO<sub>2</sub>-P < Ni/SiO<sub>2</sub>-H < Ni/SBA-15,  
158 indicating a decreasing Ni-dispersion order Ni/SiO<sub>2</sub>-P > Ni/SiO<sub>2</sub>-H > Ni/SBA-15.<sup>26</sup>  
159 <sup>29</sup> The BET specific surface area (S<sub>BET</sub>) value and pore properties of catalyst supports  
160 and freshly prepared catalysts are shown in Table S1. After impregnation, the S<sub>BET</sub>  
161 value and pore volume decreased in all three of the catalysts. This phenomenon might  
162 be caused by pore blocking during the impregnation process. The S<sub>BET</sub>, pore volume,  
163 average pore size, and average Ni-loading of freshly prepared catalysts are also  
164 presented in Table 1. The largest pore volume and largest average pore size were

165 found in Ni/SiO<sub>2</sub>-P, while Ni/SBA-15 had the largest S<sub>BET</sub> value. There was no  
166 obvious connection between the S<sub>BET</sub> value and pore volume of catalysts, but the pore  
167 volume/S<sub>BET</sub> ratio decreased in the order Ni/SiO<sub>2</sub>-P > Ni/SiO<sub>2</sub>-H > Ni/SBA-15,  
168 which was in accordance with the Ni-dispersion order, and Bappy Saha<sup>30</sup> also proved  
169 that a high pore volume/S<sub>BET</sub> ratio contributes to high catalytic performance. The XRF  
170 results in Table 1 show that the Ni-loading was slightly higher than the set value of 10  
171 wt%. This might be caused by weight loss during the pre-calcination of the supports,  
172 resulting in a higher Ni content in the catalysts.



**Figure 1.** XRD patterns of fresh 10% Ni/SiO<sub>2</sub> catalysts (before reduction). (a)

Wide-angle XRD patterns, (b) small-angle XRD patterns.

**Table 1.** The main textural properties of fresh catalysts.

Catalysts	Ni loading <sup>a</sup> wt. (%)	Average crystal size <sup>b</sup> nm	S <sub>BET</sub> <sup>c</sup> m <sup>2</sup> /g	Pore volume cm <sup>3</sup> /g	Average pore size Å	Pore volume to S <sub>BET</sub> ratio 10 <sup>-9</sup> m
Ni/SiO <sub>2</sub> -H	10.55	8.38	153	0.40	107	2.6
Ni/SBA-15	10.90	10.23	332	0.42	50	1.3
Ni/SiO <sub>2</sub> -P	10.15	6.25	279	0.88	126	3.2

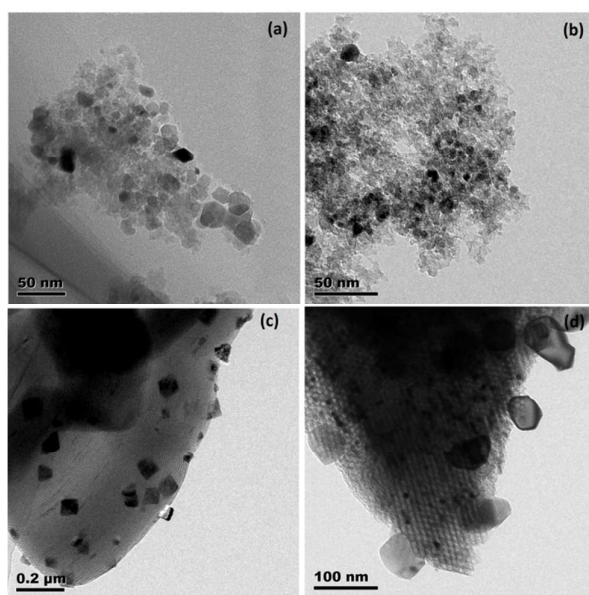
a Determined by the XRF method.

b Determined by the Scherrer equation from the Ni (200) plane of XRD.

c. Specific surface area calculated by BET method.

173 SEM images of the three supports were shown in Figure S1. From the SEM  
174 images of supports, we can see that both SiO<sub>2</sub>-H and SiO<sub>2</sub>-P have a loose and porous  
175 structure with a non-uniform pore size, while SBA-15 have an uniform cylindrical  
176 pores. TEM images of fresh catalysts are shown in Figure 2. The translucent particles  
177 with an irregular shape are supports of Ni/SiO<sub>2</sub>-H and Ni/SiO<sub>2</sub>-P catalysts (Figure 2a  
178 and 2b),<sup>25</sup> and crystal NiO particles were uniformly supported on SiO<sub>2</sub>-H and SiO<sub>2</sub>-P.  
179 In contrast, Ni/SiO<sub>2</sub>-P had a smaller NiO particle size and greater homogeneity in  
180 metal dispersion. In Figure 2c and 2d, a two-dimensional hexagonal texture is  
181 assigned to SBA-15.<sup>15, 31</sup> The pores of Ni/SBA-15 were of a uniform size of ~5 nm  
182 (Figure S2), which is also confirmed by the BET results in Table 1. Some NiO  
183 particles were uniformly loaded on the outside surface of SBA-15, which differed

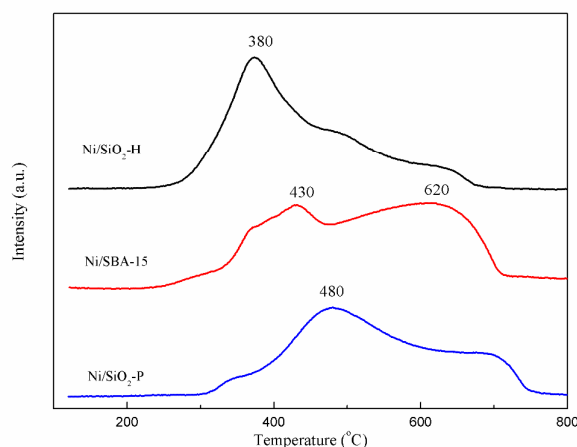
184 greatly from the crystallite sites inside the porous structure. The regulated growth of  
185 crystals inside the narrowly distributed channels might have been responsible for the  
186 difference in NiO particle size, resulting in less homogeneity of NiO particles than in  
187 Ni/SiO<sub>2</sub>-P and Ni/SiO<sub>2</sub>-H. The particle size of supported NiO increased in the order of  
188 Ni/SiO<sub>2</sub>-P < Ni/SiO<sub>2</sub>-H < Ni/SBA-15, which was in agreement with the Scherrer  
189 equation results.



**Figure 2.** TEM images of fresh catalysts (before reduction): (a) Ni/SiO<sub>2</sub>-H, (b) Ni/SiO<sub>2</sub>-P, (c) and (d) Ni/SBA-15.

190 The reducibility and different Ni species in the SiO<sub>2</sub> supported nickel catalysts  
191 were investigated using H<sub>2</sub>-TPR (Figure 3). All of the catalysts had a broad and  
192 overlapping H<sub>2</sub> consumption peak from 300 to 800°C, indicating the presence of  
193 nickel oxides that had different interactions with the supports.<sup>16,32</sup> The highest H<sub>2</sub>  
194 reduction temperature of Ni/SiO<sub>2</sub>-H, Ni/SBA-15, and Ni/SiO<sub>2</sub>-P was 680°C, 700°C,

195 and 750°C, respectively, in the order Ni/SiO<sub>2</sub>-H < Ni/SBA-15 < Ni/SiO<sub>2</sub>-P, suggesting  
196 an enhancement of NiO-SiO interactions.<sup>26, 33</sup> In addition, two separate reduction  
197 regions can be seen in the Ni/SBA-15 catalyst; i.e., the broad peak at 430°C and the  
198 shoulder peak around 620°C. These peaks might relate to the reduction of NiO  
199 particles supported on the outside surface and inside the porous structure of SBA-15,  
200 respectively, which can also be clearly distinguished in the TEM results. The H<sub>2</sub>-TPR  
201 profiles also confirmed that 800°C was the appropriate pre-reduction temperature for  
202 the reduction of reducible catalysts.



**Figure 3.** H<sub>2</sub>-TPR profiles of Ni/SiO<sub>2</sub> catalysts (reduced in a 5 vol% H<sub>2</sub>/Ar stream at a temperature ramp of 10°C/min).

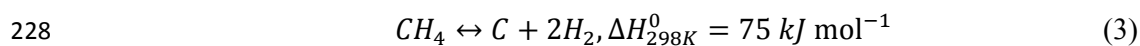
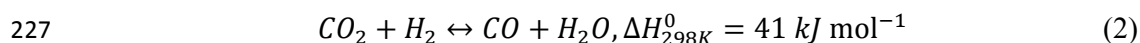
### 203 3.2 Catalytic Performance in Biogas Reforming

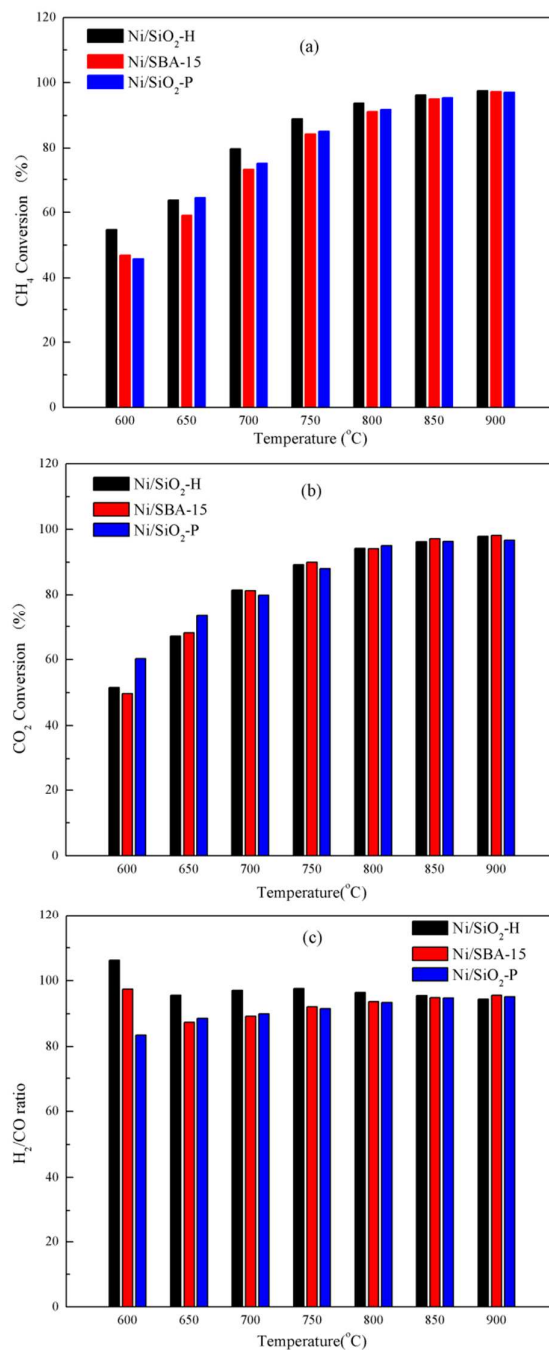
#### 204 Effect of temperature

205 The dry reforming activity of catalysts is indicated by the conversion of CH<sub>4</sub> and  
206 CO<sub>2</sub>, and the selectivity is expressed in terms of the H<sub>2</sub>/CO ratio. Figure 4 shows the  
207 activity and selectivity results for all the three types of SiO<sub>2</sub> supported nickel catalysts

208 from 600 to 900°C. Generally, the conversion of both CH<sub>4</sub> and CO<sub>2</sub> increased as the  
209 temperature increased from 600 to 900°C. This may be because the dry reforming  
210 reaction of biogas is a strong endothermic reaction (Equation 1), and a higher  
211 temperature will increase the conversion rate, as observed in earlier studies.<sup>6, 7, 34</sup> Of  
212 the different catalysts, the CH<sub>4</sub> conversion of Ni/SiO<sub>2</sub>-H was the highest during the  
213 whole temperature range, and when the temperature was higher than 650°C, the CH<sub>4</sub>  
214 conversion of Ni/SiO<sub>2</sub>-P was slightly higher than that of Ni/SBA-15. As the  
215 temperature increasing, less difference was observed in the CO<sub>2</sub> conversion between  
216 different catalysts. Taking Ni/SiO<sub>2</sub>-H as an example, the CH<sub>4</sub> conversion increased  
217 from 55% to 98% and the CO<sub>2</sub> conversion increased from 52% to 98% when  
218 temperature increased from 600 to 900°C. When the temperature was 800°C, both  
219 CH<sub>4</sub> and CO<sub>2</sub> conversion exceeded 90%. There is only slight increase in CH<sub>4</sub> and CO<sub>2</sub>  
220 conversions at temperatures >800 °C

221 The H<sub>2</sub>/CO ratio of different catalysts at various temperatures is shown in Figure  
222 4c. When the temperature was higher than 650°C, the H<sub>2</sub>/CO ratio of all samples was  
223 < 1. The reverse water-gas-shift reaction (RWGS, Equation 2) can consume the  
224 additional H<sub>2</sub> and produces CO, which lowers the H<sub>2</sub>/CO ratio.<sup>9</sup> When the temperature  
225 was < 850°C, the H<sub>2</sub>/CO ratio of Ni/SiO<sub>2</sub>-H was slightly higher than that of  
226 Ni/SBA-15 and Ni/SiO<sub>2</sub>-P, indicating a smaller contribution from the RWGS reaction.



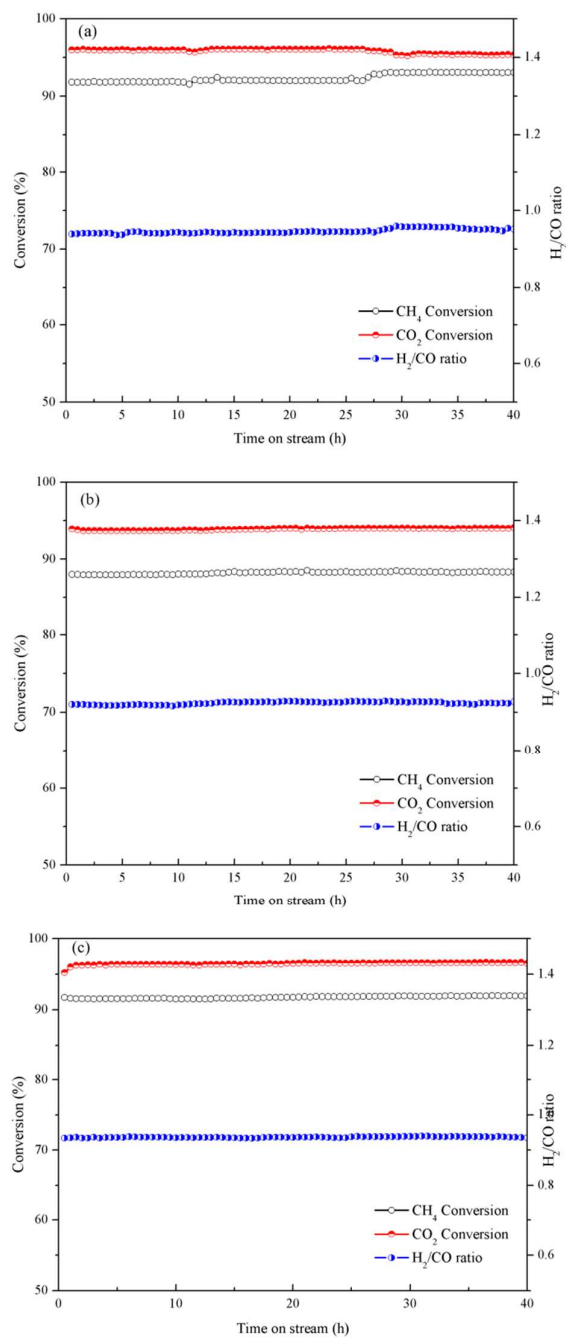


**Figure 4.** The influence of temperature on the catalytic activity of Ni/SiO<sub>2</sub> catalysts: (a) CH<sub>4</sub> conversion, (b) CO<sub>2</sub> conversion, and (c) H<sub>2</sub>/CO ratio. (GHSV = 15 000 mL•g<sub>cat</sub><sup>-1</sup>•h<sup>-1</sup>, atmospheric pressure)

230 Temperature tests indicated that at 800°C, both CH<sub>4</sub> and CO<sub>2</sub> conversion was  
231 high (> 90%). Blank tests showed that when the temperature was higher than 750°C,  
232 H<sub>2</sub> and CO was detected in the outlet gas (Figure S3), which might be caused by  
233 RWGS reaction (Equation 2) and methane decomposition reaction (Equation 3).  
234 Therefore, 800°C was chosen as the appropriate temperature to conduct stability tests.  
235 Figure 5 shows the 40-h-on-stream catalyst test results for all catalyst samples at  
236 800°C. All three of the samples showed good stability during the 40 h on-stream, and  
237 no decay of activity was found in all samples. The conversion of CH<sub>4</sub> was slightly  
238 lower than the conversion of CO<sub>2</sub> and the H<sub>2</sub>/CO ratio was < 1.

239 The average CH<sub>4</sub> conversion, CO<sub>2</sub> conversion, and H<sub>2</sub>/CO ratio are summarized  
240 in Table 2. The average CH<sub>4</sub> conversion increased in the order Ni/SBA-15 <  
241 Ni/SiO<sub>2</sub>-P < Ni/SiO<sub>2</sub>-H, and the average CO<sub>2</sub> conversion increased in the order  
242 Ni/SBA-15 < Ni/SiO<sub>2</sub>-H < Ni/SiO<sub>2</sub>-P. The contribution of the RWGS reaction  
243 increased the conversion of CO<sub>2</sub> and decreased the H<sub>2</sub>/CO ratio. The higher the degree  
244 of the reverse water gas shift reaction process, the larger the difference between CH<sub>4</sub>  
245 and CO<sub>2</sub> conversion, and the lower the H<sub>2</sub>/CO ratio. These theoretical considerations  
246 are confirmed by the actual test results shown in Table 2. The highest average H<sub>2</sub>/CO  
247 ratio of Ni/SiO<sub>2</sub>-H indicated that the secondary reaction was minimized to a greater  
248 extent than in Ni/SBA-15 and Ni/SiO<sub>2</sub>-P.





**Figure 5.** Stability tests of Ni/SiO<sub>2</sub> catalysts under 800°C for 40 h: (a) Ni/SiO<sub>2</sub>-H, (b) Ni/SBA-15, and (c) Ni/SiO<sub>2</sub>-P. (GHSV = 15 000 mL•g<sub>cat</sub><sup>-1</sup>•h<sup>-1</sup>, atmospheric pressure)

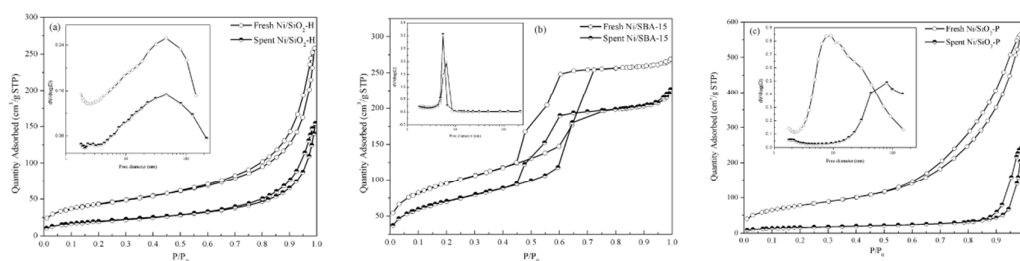
**Table 2.** Average catalytic activity of all three of the catalyst samples during 40 h-on-stream.

Catalysts	Average CH <sub>4</sub> conversion (%)	Average CO <sub>2</sub> conversion (%)	Conversion difference (%)	Average H <sub>2</sub> /CO ratio
Ni/SiO <sub>2</sub> -H	92.3	95.8	3.5	0.946
Ni/SBA-15	88.2	93.9	5.7	0.924
Ni/SiO <sub>2</sub> -P	91.8	96.5	4.7	0.937

### 249 3.3 Post-reaction Characterization.

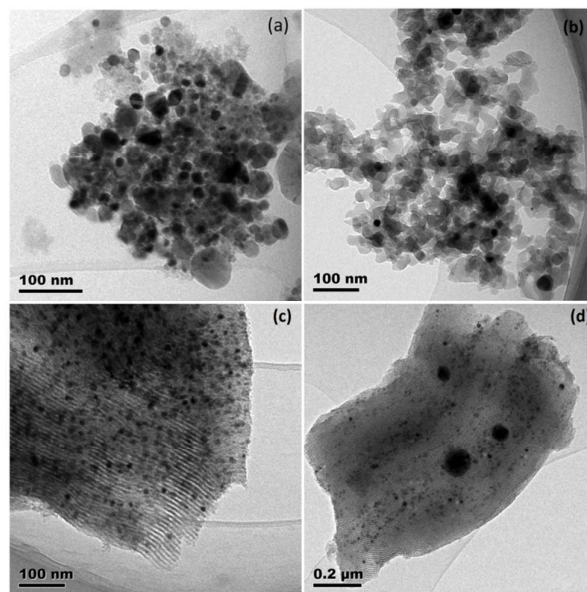
250 Figure 6 shows the N<sub>2</sub> adsorption-desorption isotherms and BJH desorption pore  
251 size distribution analysis of fresh and spent catalysts. The N<sub>2</sub> adsorption-desorption  
252 isotherms of both fresh and spent Ni/SiO<sub>2</sub>-H (Figure 6a) and Ni/SiO<sub>2</sub>-P (Figure 6c)  
253 catalysts displayed an approximate type IV isotherm as defined by the International  
254 Union of Pure and Applied Chemistry (IUPAC). The presence of a type H3 hysteresis  
255 loop indicates the existence of mesopores, and the unlimited adsorption at high P/P<sub>0</sub>  
256 values suggests that aggregates of plate-like particles give rise to slit-shaped pores.<sup>24,</sup>  
257 <sup>35</sup> The results were also confirmed by Figures 2a and 2b. The N<sub>2</sub>  
258 adsorption-desorption isotherms of both fresh and spent Ni/SBA-15 (Figure 6b)  
259 catalysts displayed a typical Type IV isotherm and a standard H1 type hysteresis loop  
260 as defined by the IUPAC, and were characteristic of mesoporous materials with highly  
261 uniform cylindrical pores,<sup>27</sup> which also supports the XRD and TEM results. The fresh  
262 Ni/SiO<sub>2</sub>-H and Ni/SiO<sub>2</sub>-P catalysts had a wide BJH desorption pore size distribution,  
263 while fresh Ni/SBA-15 had a highly narrow size distribution with a mean diameter of  
264 5.0 nm, which was in accordance with the HR-TEM results (Figure S2).

265 After the 40-h-on-stream tests, there was a decrease in the BET surface area and  
266 pore volume, and an increase in average pore size in all of the spent catalysts (see  
267 Table S1). This agreed with the BET analysis results for Ni/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> reported by  
268 Srinivas Appari.<sup>36</sup> The catalytic reaction process did not change the shape of the N<sub>2</sub>  
269 adsorption-desorption isotherms of Ni/SiO<sub>2</sub>-H and Ni/SBA-15, or their BJH  
270 desorption pore size distribution, and only a slight change in the average pore size was  
271 observed due to a slight blocking phenomenon. There was a difference in the  
272 hysteresis loop for Ni/SiO<sub>2</sub>-P between fresh and spent catalysts. The shifting of the  
273 relative pressure of the hysteresis loop to a higher value was observed, leading to an  
274 obvious change in the BJH desorption pore size distribution, with the average pore  
275 size shifted greatly from 126 to 270 nm. According to Aziza<sup>27</sup>, the hysteresis loops at  
276 lower and higher relative pressures represent the intra- and inter- particle porosity,  
277 respectively. There might be a decrease in intra-particle porosity and an increase in the  
278 inter-particle porosity of Ni/SiO<sub>2</sub>-P after a stability test, therefore the decrease of  
279 smaller pore size due to intra-particle porosity may result in an increase in the average  
280 pore size.



**Figure 6.** N<sub>2</sub> adsorption-desorption isotherms and the BJH desorption pore size distribution for fresh and spent catalysts: (a) Ni/SiO<sub>2</sub>-H, (b) Ni/SBA-15, and (c) Ni/SiO<sub>2</sub>-P. The inset shows the pore size distribution.

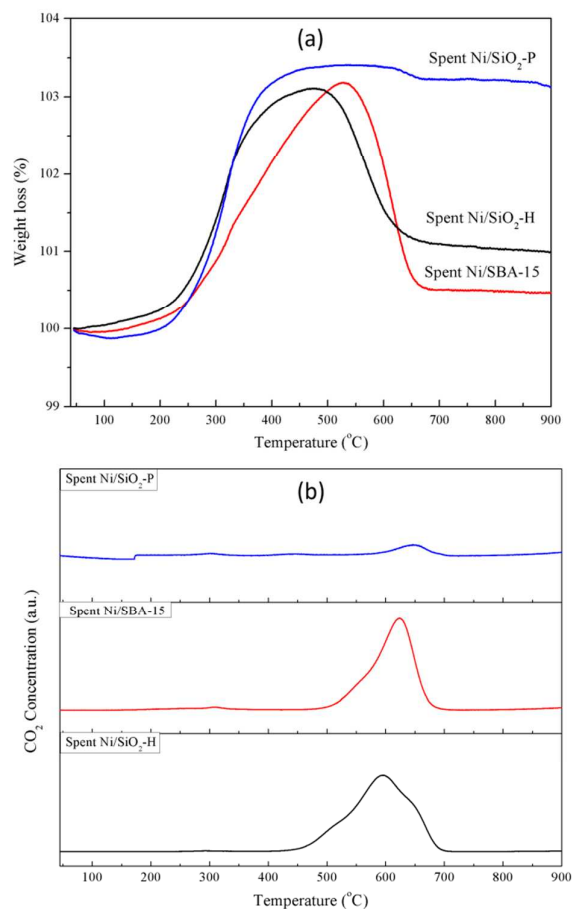
281 Figure 7 shows TEM images of spent catalysts. The original structure of all  
282 catalysts was maintained after 40-h-on-stream tests. Spent Ni/SiO<sub>2</sub>-H and Ni/SiO<sub>2</sub>-P  
283 catalysts kept their amorphous structure, and Ni/SBA-15 kept its two-dimensional  
284 hexagonal texture. However, there was an obvious pore size increase in the spent  
285 Ni/SiO<sub>2</sub>-P catalyst (Figure 7b), which was supported by the BJH pore size distribution  
286 results shown in Figure 6c. A slight metal agglomeration phenomenon was observed  
287 in spent Ni/SiO<sub>2</sub>-H and Ni/SiO<sub>2</sub>-P catalysts (Figures 7a and 7b). The two-dimensional  
288 hexagonal channel of spent Ni/SBA-15 limited the agglomeration of active metals  
289 inside the pore (Figure 7c), while the active metals supported on the outside surface  
290 experienced significant agglomeration, and even detached from the SBA-15 support  
291 (Figure 7d). Ilenia Rossetti, et al. also reported that large particles exposed a small  
292 interface with the support surface, which led to a weaker interaction, thus, easy to  
293 detach from the support.<sup>26</sup> No carbon was found in any of the three spent catalysts,  
294 indicating negligible coke deposition.



**Figure 7.** TEM images of spent catalysts: (a) Ni/SiO<sub>2</sub>-H, (b) Ni/SiO<sub>2</sub>-P, (c) and (d) Ni/SBA-15.

295 The results of the TGA-MS analysis of the spent catalysts are shown in Figure 8.  
296 The thermo-grams can be divided into two different temperature regions (Figure 8a).  
297 All of the spent catalysts experienced an increase in weight at low temperature ranges  
298 and a decrease in weight at high temperature ranges. The oxidation of nickel particles  
299 at temperatures above 200°C caused the weight increase, and the 3% weight increase  
300 of spent catalysts was inconsistent with the theoretical weight increase of 10% due to  
301 nickel particle oxidation, which was also reported by Jianqiang Zhu<sup>17</sup>. Weight loss at  
302 temperatures above 400°C was ascribed to the oxidation of deposited carbon.<sup>37</sup> CO<sub>2</sub>  
303 MS signals from TPO process of three spent catalysts were shown in Figure 8b. Since  
304 O<sub>2</sub> was used as react gas and N<sub>2</sub> was used as protection gas, the signal of molecular  
305 weight at 44 was only supposed to be CO<sub>2</sub>, which was generated by the oxidation of

306 deposited carbon. The CO<sub>2</sub> generation peak range of spent Ni/SiO<sub>2</sub>-H, Ni/SBA-15,  
307 and Ni/SiO<sub>2</sub>-P were 450-700°C, 500-700°C, and 580-700°C, respectively,  
308 corresponding to the weight loss temperature ranges of the three catalysts. Although  
309 MS is a semi-quantitative method, we can still distinguish that a higher weight loss  
310 amount of TGA resulted in a higher MS signal intensity. So a very weak CO<sub>2</sub> signal  
311 intensity of spent Ni/SiO<sub>2</sub>-P implied its lowest carbon deposition. The amount of coke  
312 deposited on spent Ni/SiO<sub>2</sub>-H, Ni/SBA-15, and Ni/SiO<sub>2</sub>-P catalysts was calculated to  
313 be 2.1, 2.7 , and 0.3 wt.%, respectively, which was in the low range of carbon  
314 deposited (0.89–6.56 wt.%) on Ni/SiO<sub>2</sub> catalysts after a 30-h test, as reported by  
315 Zhu.<sup>17</sup> In conclusion, the results showed that little coke was deposited on the catalysts,  
316 and the formation of coke was related to the metal dispersion of the catalysts. The  
317 smaller crystal size of metal catalysts will lead to a catalyst that is less prone to  
318 deactivation.



**Figure 8.** (a) TGA profiles of spent Ni/SiO<sub>2</sub> catalysts, (b) MS signals of CO<sub>2</sub> (20 mL/min O<sub>2</sub> stream under a temperature ramp of 10°C/min with N<sub>2</sub> as protection gas).

#### 319 4 Conclusions

320 In summary, Waste-derived SiO<sub>2</sub> obtained from photovoltaic waste SiCl<sub>4</sub> by a  
321 vapor-phase hydrolysis method was applied as the support for a nickel catalyst in a  
322 biogas dry reforming process for the first time. Catalytic tests results showed that the  
323 conversion of CH<sub>4</sub> and CO<sub>2</sub> increased as temperature increased from 600 to 900°C.  
324 When temperature was 800°C, it reached a high CH<sub>4</sub> conversion (92.3%) and a high  
325 CO<sub>2</sub> conversion (95.8%), and there was no deactivation after 40 h-on-stream test.

326 Compared to commercial precipitated SiO<sub>2</sub> and ordered mesoporous SiO<sub>2</sub>, the  
327 catalytic activity of waste-derived SiO<sub>2</sub> is equivalent to those of commercial  
328 precipitated SiO<sub>2</sub>, and even superior to those of mesoporous SiO<sub>2</sub>. The coke deposition  
329 amount after stability tests follows the order commercial precipitated SiO<sub>2</sub> <  
330 waste-derived SiO<sub>2</sub> < mesoporous SiO<sub>2</sub>. It is further demonstrated that coke  
331 deposition in biogas dry reforming process is related to the textural properties of  
332 catalysts. A higher pore volume/S<sub>BET</sub> ratio will lead to a smaller crystal metal size and  
333 higher metal dispersion; thus the catalyst is less prone to deactivation. This discovery  
334 will help improve catalyst design.

335 In conclusion, waste-derived SiO<sub>2</sub> used as catalyst support in biogas dry  
336 reforming process shows a high catalytic activity and good stability, which is  
337 competitive to commercial and mesoporous one. Considering the large-scale  
338 production and poor treatment condition of photovoltaic waste SiCl<sub>4</sub>, the production  
339 of waste-derived SiO<sub>2</sub>, and its further application as a catalyst support for biogas dry  
340 reforming represents a useful conversion of photovoltaic waste to a high value-added  
341 product, as well as providing a cheap and environmentally benign support for  
342 catalysts in the biogas dry reforming process.

#### 343 **ASSOCIATED CONTENT**

344 Supporting Information

345 Supplementary materials for online publication are available via the Internet at

346 <http://pubs.rsc.org>.



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352 The authors declare no competing financial interest.

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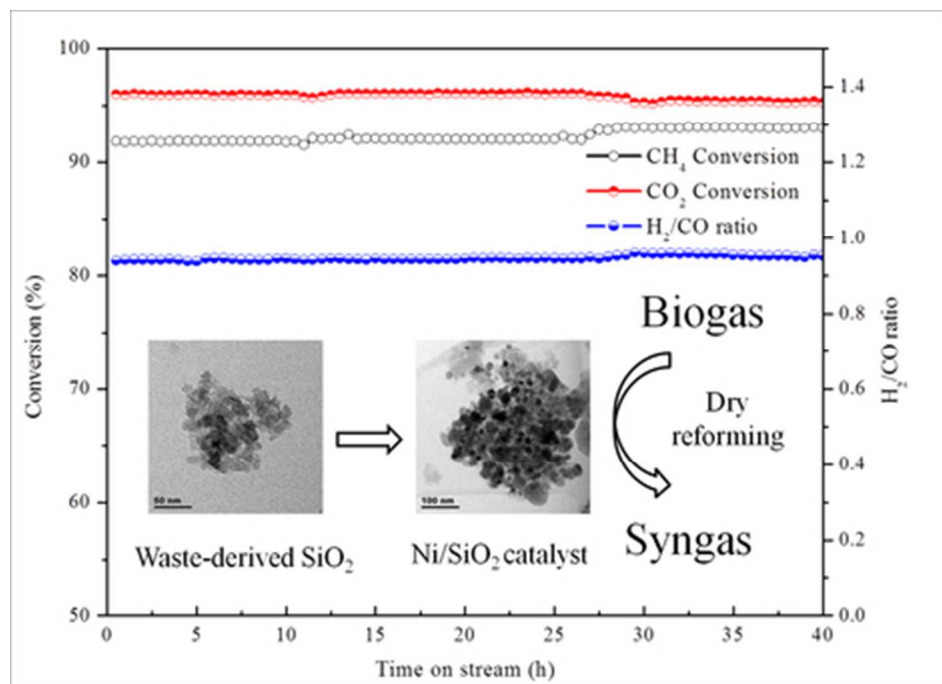
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Waste-derived  $SiO_2$  was used as catalyst support in biogas dry reforming process, which showed a high catalytic activity and good stability.  
39x28mm (300 x 300 DPI)