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2 The Effect of Temperature on the Dynamics of a

3 Homogeneous Oscillatory System Operated in Batch and

4 Under Flow

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15

16 **Abstract**

17 The effect of temperature on a network of chemical reactions is non-obvious,
18 especially when compared to the effect exerted on elementary steps. There are few
19 reports regarding the estimation of parameters such as activation energies for
20 oscillating chemical systems. Still less investigated is the importance of the relative
21 distance from thermodynamic equilibrium on the way in which temperature
22 influences the oscillators' dynamics – a crucial aspect for the understanding of
23 chemical and bio-chemical oscillating networks. In this paper we use the
24 bromate/oxalic acid and acetone/cerium oscillatory system to study the influence of
25 temperature under close and far-from-equilibrium regimes. The research was carried
26 out under identical conditions for batch and flow (in a continuous flow stirred tank
27 reactor, CSTR) regimes, and the main oscillation features were preserved, so that it
28 was possible to isolate the effect of flow. Overall, increasing the flow results in an
29 increase of the oscillatory frequency. The apparent oscillatory activation energy was
30 found to decrease from $72 \pm 6 \text{ kJ mol}^{-1}$, for the system operated in batch, to $50 \pm 2 \text{ kJ}$
31 mol^{-1} , under flow regime. The role of the distance from the thermodynamic
32 equilibrium on the temperature dependence is generalized and discussed in connection
33 with other systems. Numerical simulations using the Brusselator model under batch
34 and flow regimes further helped the discussion of the main experimental results.

35

36 **Keywords:** oscillating reactions, temperature, activation energy, batch, CSTR.

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39

40 1. Introduction

41 A network of chemical reactions under oscillatory regime might display rather
42 unusual response to temperature changes. Examples include non-Arrhenius behaviors
43 such as temperature compensation and overcompensation.^{1,2,3,4-5} These infrequent
44 effects play a decisive role, for instance, in temporally organized patterns found in
45 living systems which are commonly known to be rather insensitive to temperature and
46 other parameters such as pH, etc. Temperature compensation is particularly important
47 as part of the wide-ranging homeostatic mechanism, and it underlies many oscillatory
48 mechanisms in living systems (c.f. circadian, ultradian and some neuronal rhythms),
49 c.f. ref. ⁶ and references therein. In terms of individual reactions, temperature
50 compensation results from the balance among the weighted activation energies of
51 frequency-increasing and frequency-decreasing elementary steps in a reaction
52 network.^{1,2,7}

53 Despite the comparable simplicity of chemical oscillators, results obtained in
54 such designed *in vitro* systems can provide valuable information on some structural
55 aspects of more complex and sometimes less tractable biochemical oscillators.^{8-9,10}
56 Indeed, the observation of temperature compensation in comparable simpler
57 (electro)chemical oscillators^{5,11-12} attests their importance as model systems. In most
58 cases, the effect of temperature in these oscillators has been discussed in terms of the
59 temperature dependence of the oscillatory frequency, as firstly suggested by Körös.¹³

60 One of the most prominent feature of living systems is that their internal
61 organization is kept at the expense of exporting entropy to the environment. In order
62 to stay alive, these open systems import (or are fed with) high free energy materials
63 and reject the degraded ones. Already in 1950, von Bertalanffy¹⁴ recognized that
64 “from the physical point of view, the characteristic state of the living organism is that

65 of an open system”, and as such, living systems can thrive by “maintaining
66 themselves in exchange of materials with environment, and in continuous building up
67 and breaking down of their components”. Therefore, the position with respect to the
68 thermodynamic equilibrium is a key parameter to the understanding and description
69 of the actual state of open systems. In chemical systems, the departure from the state
70 of thermodynamic equilibrium can be tuned by the rate at which reactants are fed and
71 products (and also unreacted species and intermediates) are removed from the
72 reaction vessel. Tuning this parameter results on non-trivial changes in most reaction
73 rates. Hence, the effect exerted by temperature is expected to depend on the distance
74 from thermodynamic equilibrium.

75 A literature survey reveals a lack of reports dealing with the influence of the
76 relative position with respect to thermodynamic equilibrium on the way in which
77 temperature influences the oscillators’ dynamics. In a seminal report, Rössler¹⁵
78 conjectured on the importance of flow when designing a temperature-compensated
79 homogenous chemical oscillator. The discussion was carried out in terms of a
80 theoretical model for a relaxation oscillator. Insofar, however, it seems that no
81 verification of this expectation has been provided. Ruoff and co-workers¹⁶ studied the
82 effect of temperature on the dynamics of some bromate oscillators catalyzed by
83 cerium, and reported a considerable decrease in the activation energy when the system
84 was operated in a continuous flow stirred tank reactor (CSTR), when compared with
85 the batch regime. The effect of flow and/or temperature on the dynamics has been
86 reported for some oscillatory systems such as the hydrogen
87 peroxide/thiosulfate/sulfite flow system,^{11,17} pH oscillators,¹² and the Bray reaction.¹⁸
88 We have recently studied¹⁹ the time evolution of the apparent oscillatory activation
89 energy for a BZ-like oscillator operated in batch approaches the thermodynamic

90 equilibrium. As the main result, we observed that the apparent oscillatory activation
91 energy increases as reactants are consumed and products accumulate inside the
92 reactor. A detailed investigation of formic acid electro-oxidation on platinum⁵
93 revealed the predominance of highly non-Arrhenius temperature dependence over a
94 wide parameter window. The system was characterized in terms of the distance from
95 the thermodynamic equilibrium and temperature compensation was found to prevail at
96 considerably high applied currents or, equivalently, at the farthest distance from
97 equilibrium.

98 The present contribution results from our interest to understand the combined
99 effect of temperature and distance from the thermodynamic equilibrium. We decided
100 to undergo such an investigation using the bromate-oxalic acid-acetone-cerium
101 system^{20,21} as a model system. This system was chosen mainly because of its
102 robustness and low sensitivity of its properties, such as the oscillation morphology, on
103 temperature and flow rates. The constancy of such features might indicate that the
104 underlying chemistry remains unchanged at distinct flow rates and temperatures. As
105 far as the effect of temperature is concerned, this system has been studied under both
106 batch and flow regimes.^{22,23,24,25} In contrast to previous reports by other authors,
107 however, the systematic experiments reported here allowed isolate as much as
108 possible the contribution of the flow on the temperature dependence. We initially
109 optimized the system in order to compare the effect of temperature in batch and flow.
110 In this way, the open and closed systems were studied under identical conditions of
111 stirring rate, temperature, and concentrations. In order to go deeper in the
112 understanding of the distance from the thermodynamic equilibrium on the system's
113 dynamics, we carried out some numerical simulations using the Brusselator model

114 under batch and flow regimes. Finally, the results are discussed in connection with
115 other processes in electro-, bio- and chemical systems.

116

117 **2. Experimental Section**

118 The cylindrical glass reactor employed in all experiments is 90 mm high and
119 47 mm in diameter. The temperature was controlled by water circulation through its
120 glass jacket, with the aid of thermostatic bath (Microquimica, model MQBTC99-20)
121 and monitored using a digital thermometer (Tec-Lab). The Teflon reactor cap contains
122 the holes to allow the use of a platinum electrode and a reversible hydrogen electrode,
123 filled with aqueous sulfuric acid solution at identical concentration than that used
124 inside the reactor. The potential difference was followed by means of a multimeter
125 (Minipa, ET2201). Further experimental details can be found elsewhere.^{19,26} For open
126 reactor experiments (CSTR) two peristaltic pumps (Milan, 640) were used. The
127 system was fed with three aqueous H₂SO₄ solutions: solution A (CH₃COCH₃ and
128 (COOH)₂), solution B (NaBrO₃), and solution C (Ce₂(SO₄)₃). In this case, all solutions
129 were placed in jacketed flasks and kept inside a thermostatic bath to assure the same
130 temperature to that inside the reaction vessel. The solution inside the reactor was
131 mixed by the use of a magnetic stirrer (Marconi, MA089) and a magnetic Teflon bar
132 15 mm long and 5.7 mm of diameter. All experiments were carried out with a stirring
133 rate of 700 rpm.

134 All chemicals were used as received: H₂SO₄ (Mallinckrodt, AR 96.0 wt %),
135 oxalic acid (Sigma Aldrich, 99,0%), Ce(SO₄)₂ (Sigma Aldrich, 98%), Ce₂(SO₄)₃
136 (Sigma Aldrich, 97%), sodium bromate (Sigma Aldrich, 99%), acetone (J. T. Baker,
137 99.7%). Ultrapure water (Millipore system, 18.2 MΩ cm) was used in all solutions
138 and general cleaning.

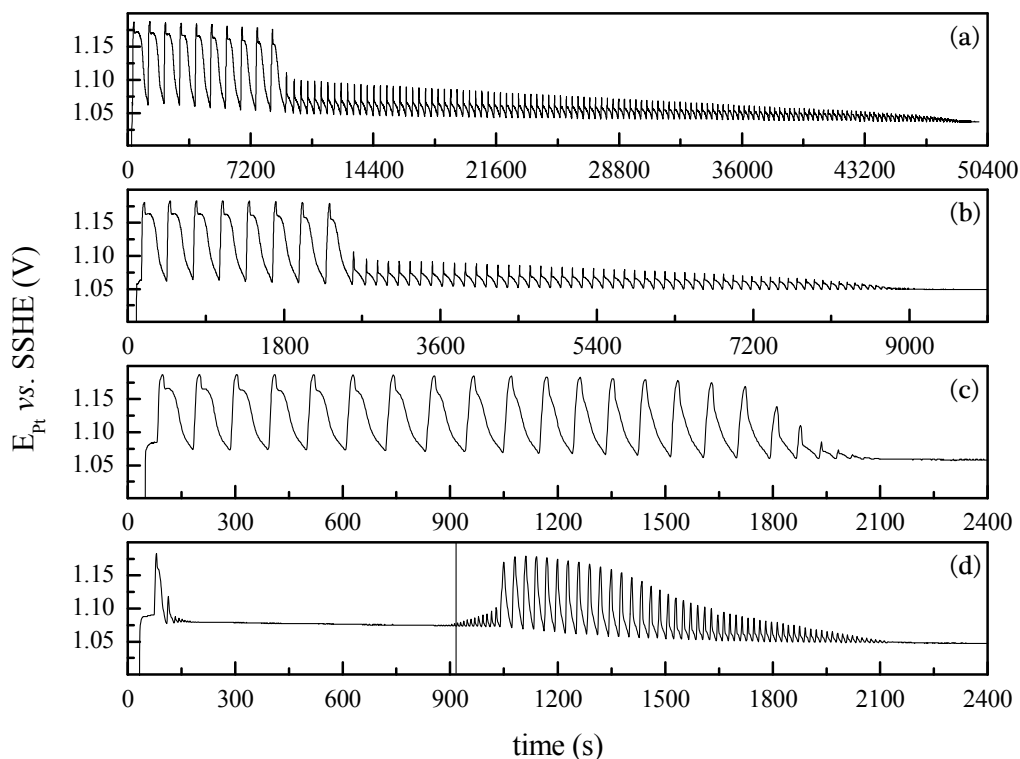
139 The oscillating frequency, ω , for each experiment was taken as an average for
140 the high amplitude set of oscillations, eventually discarding the first or the last value,
141 if it is out of the range of the others. The frequency of low amplitude oscillations was
142 not considered because this regime has shown to be more irregular.

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144 **3. Results and Discussion**

145 **3.1 Experiments**

146 ***Oscillations in batch.*** The effect of temperature was firstly investigated in the system
147 operated in batch. Figure 1 shows the time-series for the bromate/oxalic
148 acid/acetone/cerium system operated in batch at different temperatures from 5 to 35
149 °C. As a first noteworthy aspect, it is seen that temperature affects only slightly the
150 morphology of the main, high amplitude, oscillations, suggesting that, in the range
151 investigated, there is no change in the mechanism underlying the oscillatory
152 dynamics. In contrast to what is observed when Ce^{4+} ions are present, there is no
153 induction period when Ce^{3+} is used.²⁶ Moreover, the use of Ce^{4+} results in
154 considerable scattering in the Arrhenius plots. Therefore, all experiments presented
155 here were carried out with Ce^{3+} , performed in triplicate, and all time-series presented
156 are representative of the system's dynamics and reproducible.



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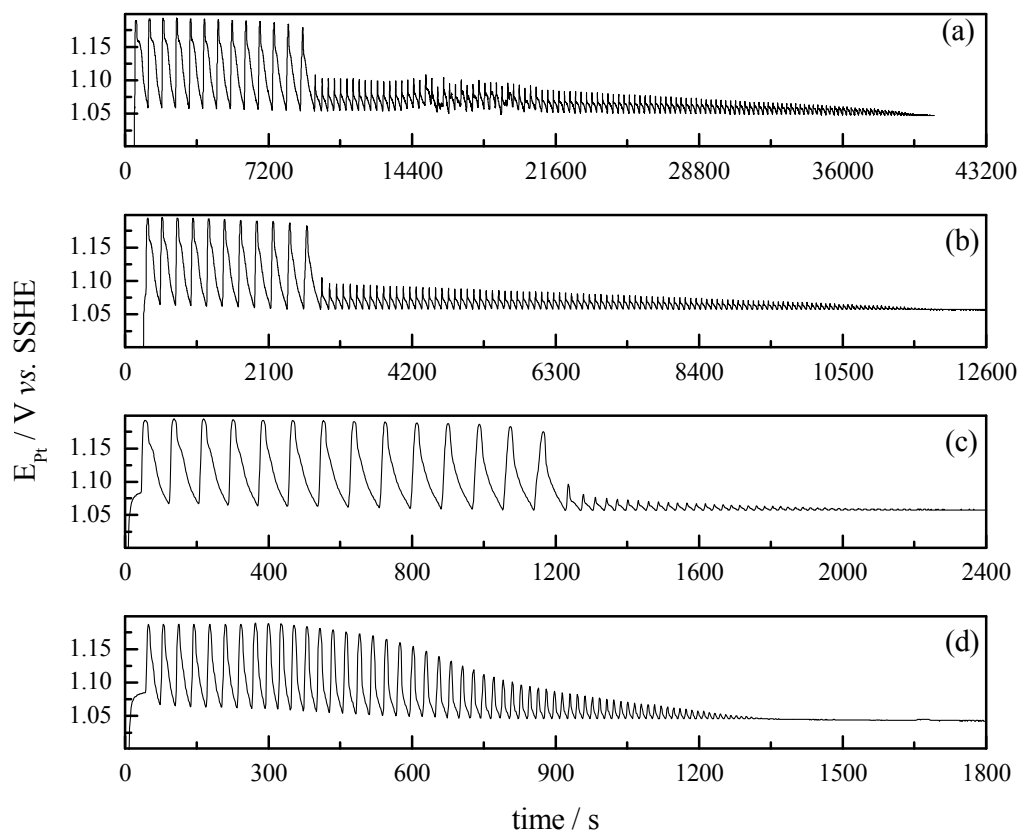
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Figure 1: Time-series of the platinum electrode for the bromate/oxalic acid/acetone/cerium oscillatory system operated in batch at (a) 5, (b) 15, (c) 25 and (d) 35 °C. Initial concentrations: $[\text{H}_2\text{SO}_4]_0 = 1.42 \text{ mol L}^{-1}$; $[\text{NaBrO}_3]_0 = 0.010 \text{ mol L}^{-1}$; $[(\text{COOH})_2]_0 = 0.025 \text{ mol L}^{-1}$; $[\text{CH}_3\text{COCH}_3]_0 = 0.115 \text{ mol L}^{-1}$ and $[\text{Ce}_2(\text{SO}_4)_3]_0 = 0.0005 \text{ mol L}^{-1}$. The vertical line in panel (d) indicates the addition of 0.37 mL of acetone in the reactor vessel.

At 35 °C the system did not oscillate under the given conditions. The addition of a small aliquot (0.37 mL) of acetone at the instant indicated by the vertical line, produced the emergence of transient oscillations, as shown in Figure 1(d). To circumvent the absence of oscillations at 35 °C, we performed experiments with slightly higher acetone concentration, namely 0.157 mol L^{-1} , and the results are presented in Figure 2.

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Figure 2: Time-series of the platinum electrode for the bromate/oxalic acid/acetone/cerium oscillatory system operated in batch at (a) 5, (b) 15, (c) 25 and (d) 35 °C. Initial concentrations: $[\text{H}_2\text{SO}_4]_0 = 1.42 \text{ mol L}^{-1}$; $[\text{NaBrO}_3]_0 = 0.010 \text{ mol L}^{-1}$; $[(\text{COOH})_2]_0 = 0.025 \text{ mol L}^{-1}$; $[\text{CH}_3\text{COCH}_3]_0 = 0.157 \text{ mol L}^{-1}$ and $[\text{Ce}_2(\text{SO}_4)_3]_0 = 0.0005 \text{ mol L}^{-1}$.

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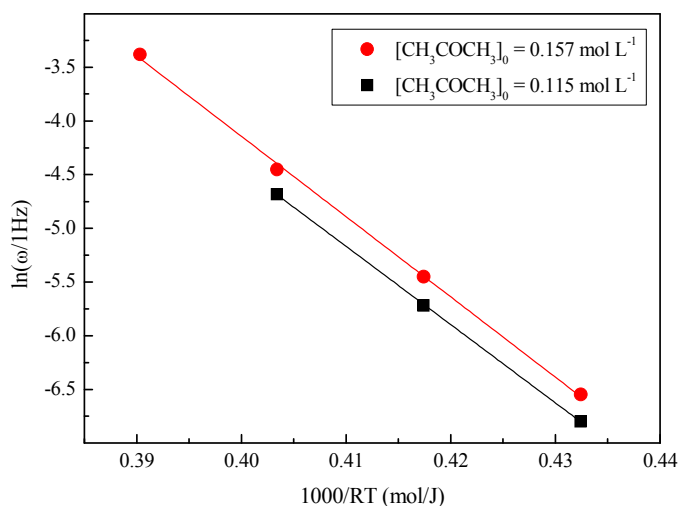
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Overall, the high amplitude oscillations presented in Figures 1 and 2 have comparable waveform and amplitude. Only a small discrepancy in the oscillatory frequency is observed for distinct acetone concentrations. The initial and uniform high amplitude oscillations were used to estimate the apparent oscillatory activation energy. Figure 3 shows the Arrhenius plot for the data presented in Figures 1 and 2, and illustrates the effect of temperature on the dynamics of the bromate/oxalic acid/acetone/cerium oscillatory system. The, apparent oscillatory activation energies, E_{ω} , calculated in these plots¹³ were found to amount to $72 \pm 2 \text{ kJ mol}^{-1}$ (for

189 $[\text{CH}_3\text{COCH}_3] = 0.115 \text{ mol L}^{-1}$), and to $74 \pm 1 \text{ kJ mol}^{-1}$ (for $[\text{CH}_3\text{COCH}_3] = 0.157 \text{ mol}$
 190 L^{-1}). Experiments were done in triplicate and these results represent the averaged
 191 values. Pastapur and Kulkarni²² studied the effect of temperature in the
 192 bromate/oxalic acid/acetone system in batch using Ce^{3+} and Mn^{2+} , as catalysts. The
 193 study was performed at 25, 30, 35, and 40 °C and the activation energy obtained under
 194 oscillatory regime for the system with Ce^{3+} was 73 or 82 kJ mol^{-1} , depending on the
 195 method used to estimate. The discrepancies between these values and the ones we
 196 found in the present work could be attributed to the differences in the concentrations
 197 and temperature range used in each case.



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199 **Figure 3:** Arrhenius plots using the oscillatory frequency ω , for the
 200 bromate/oxalic acid/acetone/cerium system operated in batch at two
 201 distinct initial concentrations of acetone: 0.115 mol L^{-1} (black squares)
 202 and 0.157 mol L^{-1} (red circles). Other concentrations: $[\text{H}_2\text{SO}_4]_0 = 1.42$
 203 mol L^{-1} ; $[\text{NaBrO}_3]_0 = 0.010 \text{ mol L}^{-1}$; $[(\text{COOH})_2]_0 = 0.025 \text{ mol L}^{-1}$; and
 204 $[\text{Ce}_2(\text{SO}_4)_3]_0 = 0.0005 \text{ mol L}^{-1}$.

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206 An important remark to be done at this point is that although no oscillations
 207 were found in batch at 35 °C for the lower acetone concentration used, the apparent
 208 oscillatory activation energy depicted in Figure 3 ($\sim 72\text{--}74 \text{ kJ mol}^{-1}$) is representative
 209 of the system operated in batch in the temperature range investigated. The flow

210 experiments were carried out with $[\text{CH}_3\text{COCH}_3] = 0.115 \text{ mol L}^{-1}$ and the main results
211 are summarized in the following.

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213 ***Experiments in a CSTR.*** As already mentioned, one of the aims of the present work
214 consists in the investigation of the effect that temperature exerts on the systems'
215 dynamics under different regimes, namely the distance from thermodynamic
216 equilibrium. Therefore, the study in the open system started with the investigation of
217 the flow rate effect on the dynamics. The oscillations' morphology and amplitude
218 were barely affected by the flow rate in the range investigated. The effect of the flow
219 rate on the systems dynamics at 25 °C is displayed in Figure 4. The vertical lines
220 indicate the instant at which the flow was interrupted.

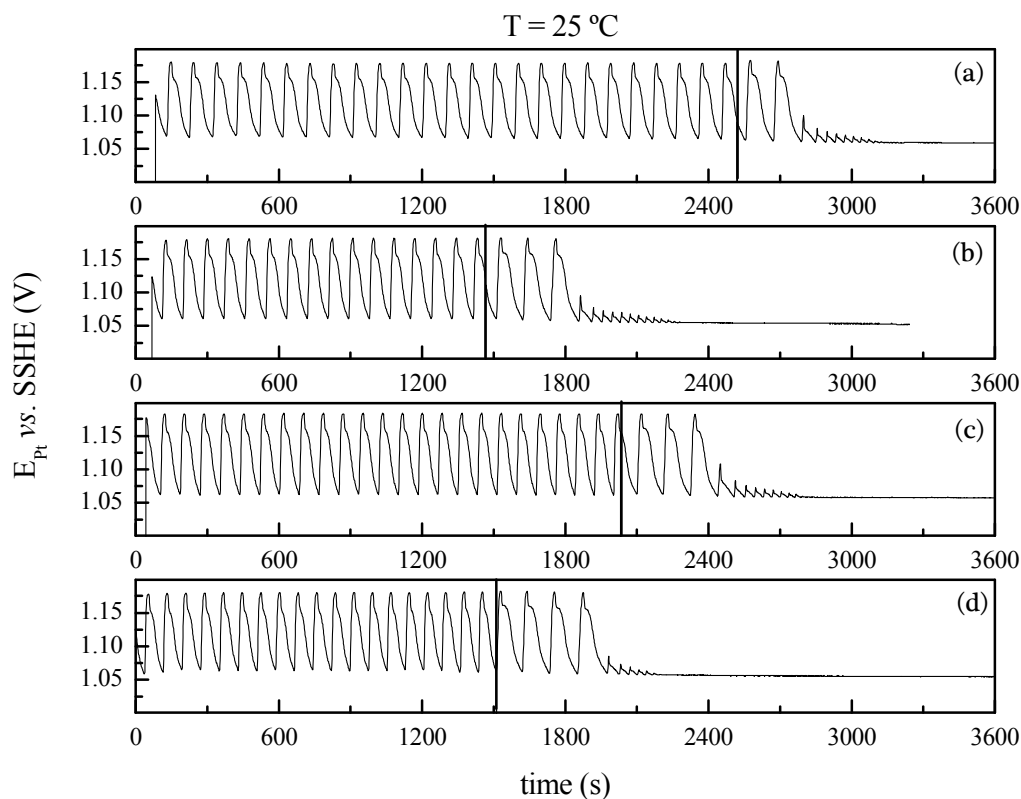
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 227 **Figure 4:** The influence of the flow rate on the dynamics of the
 228 bromate/oxalic acid/acetone/cerium oscillatory system at 25 °C.
 229 $[\text{H}_2\text{SO}_4]_0 = 1.42 \text{ mol L}^{-1}$; $[\text{NaBrO}_3]_0 = 0.010 \text{ mol L}^{-1}$; $[(\text{COOH})_2]_0 =$
 230 0.025 mol L^{-1} ; $[\text{CH}_3\text{COCH}_3]_0 = 0.115 \text{ mol L}^{-1}$; $[\text{Ce}_2(\text{SO}_4)_3]_0 = 0.0005$
 231 mol L^{-1} . $k_0 =$ (a) 0.0059 s^{-1} , (b) 0.0104 s^{-1} , (c) 0.0150 s^{-1} , and (d) 0.020
 232 s^{-1} .

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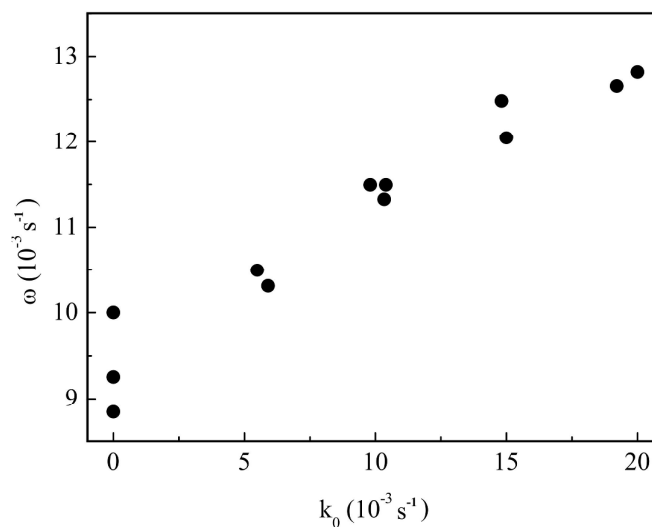
234 The observed oscillation periods in this figure were: 97 s (at $k_0 = 0.0059 \text{ s}^{-1}$),
 235 87 s (at $k_0 = 0.0104 \text{ s}^{-1}$), 83 s (at $k_0 = 0.0150 \text{ s}^{-1}$), and 78 s (at $k_0 = 0.020 \text{ s}^{-1}$). Figure 5
 236 summarizes the effect of flow rate on the oscillatory frequency for all experiments. As
 237 can be seen, the oscillatory frequency increases, almost linearly, with the flow rate.
 238 Data points in batch, i.e. $k_0 = 0$, account for three different experiments.

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245 **Figure 5:** Oscillatory frequency as a function of the flow rate. Identical
246 conditions as in Figure 4.

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248 Our results are in line with that reported by Pereira and Faria,²¹ who observed
249 a comparable behavior and reported a decrease of about 20 % on the oscillation period
250 for an increase in k_0 from 0.0119 to 0.0352 s^{-1} , for the oscillatory bromate-oxalic acid-
251 acetone-cerium system. General increase of the oscillatory frequency when increasing
252 flow rates has been also found for the hydrogen peroxide/ thiosulfate/sulfite flow
253 system.¹¹ The difficulty in comparing previously published data is due to the
254 commonly observed problem that the system is studied under different conditions
255 (mainly concentration of chemicals) in batch and flow. As already mentioned, this is
256 not a problem in the present case.

257 In homogeneous systems, the decrease in oscillatory frequency, which follows
258 the reduction of flow rate can be tentatively interpreted as a damping caused by a
259 decrease in the concentration of reacting species and the corresponding reduction of
260 reaction rates of all reactions. As the flow rate increases, the concentrations of
261 reacting species inside the reaction vessel are maintained high because of the efficient
262 replenishment of fresh reactants, and also the removal of products.

263 For most of the homogeneous systems operated in batch, the degree of
264 decrease of the oscillatory frequency in time reflects the strength of the damping; see
265 below more on this aspect. We have explained this phenomenon before in somewhat
266 different terms,¹⁹ but the concept is equivalent in both cases. This is a known effect
267 that calls for a special care on the definition of the procedure for estimating the
268 activation energy under oscillatory regime.²⁷ Moreover, the damping observed in
269 batch can also be observed in the oscillation amplitude in addition to the damping in
270 frequency. This interpretation is valid for the same type of oscillations, and thus does
271 not include sequential oscillations witnessed in batch.^{19,28,29,30-31} In fact, sequential
272 oscillations are dynamics states located at different regions in the phase space that are
273 visited as an uncontrollable parameter slowly varies.^{32,33} As such, there is no
274 particular trend to be expected for the oscillations' frequency and amplitude in
275 sequential oscillations.

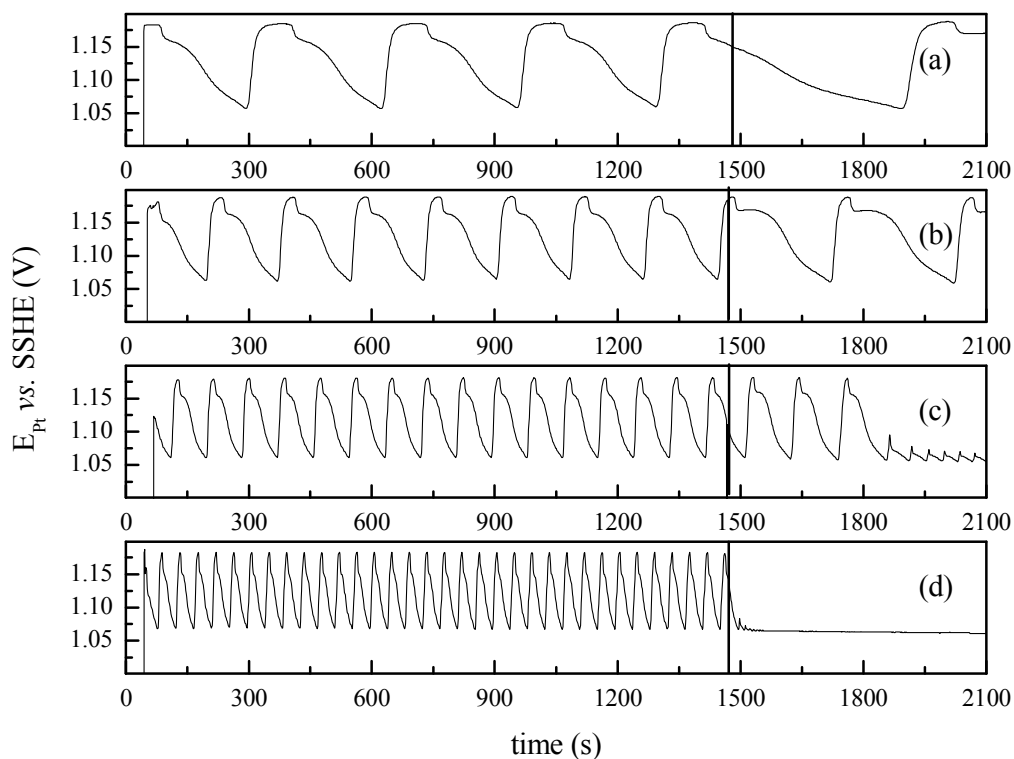
276 When compared to chemical systems, the relative position with respect to the
277 thermodynamic equilibrium in electrochemical systems can be controlled either via
278 potentiostatic or galvanostatic mode.³⁴ In both cases, the parameter, i.e. the potential
279 or the current, respectively, readily informs on the distance with respect to the
280 thermodynamic equilibrium. Nevertheless, the departure from the equilibrium is even
281 more transparent since the flow of electrons through the interface is controlled. In
282 agreement with the present findings, the oscillatory frequency also increases with the
283 applied current for the electro-oxidation of formic acid on platinum⁵ and on platinum-
284 tin surfaces.³⁵ Again, these examples are for a situation where the same kind of
285 oscillations is compared at different applied currents. As a final observation on the
286 comparison between chemical and electrochemical systems in the context of the
287 present discussion, it is remarkable the peculiarity of chemical systems in the sense

288 that the situation for $k_0 = 0$ cannot be obtained in electrochemical systems.
289 Consequently, the range of k_0 explored in Figure 5 is in principle broader than that
290 registered in electrochemical systems. Even considering the problem in properly
291 normalizing the distance from thermodynamic equilibrium, this fact allows for further
292 generalizations.

293 The effect of temperature was also investigated using a system with identical
294 composition as in Figure 4, but with $k_0 = 0.0098 \text{ s}^{-1}$. Figure 6 shows the effect of
295 temperature on the time-series for the bromate/oxalic acid/acetone/cerium oscillatory
296 system under flow regime. The vertical lines indicate when the flow was stopped.
297 After interrupting the feeding, the system oscillates for a while, just as observed when
298 operated in batch, *vide supra*. In agreement with the results at 35 °C for the system
299 operated in batch for this acetone concentration, the oscillations die out earlier when
300 the temperature is increased, and as shown in Figure 6(d). As it was observed in
301 batch, a regular, Arrhenius-like behavior is also found for the flow regime and both
302 oscillations' waveform and amplitude remain very similar at all temperatures.

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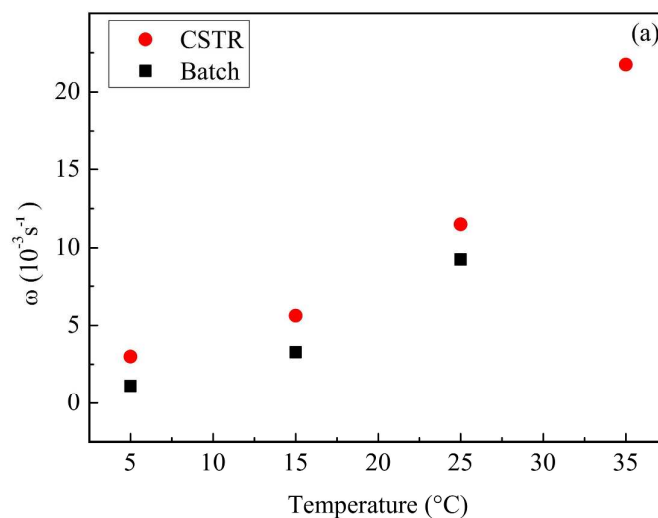
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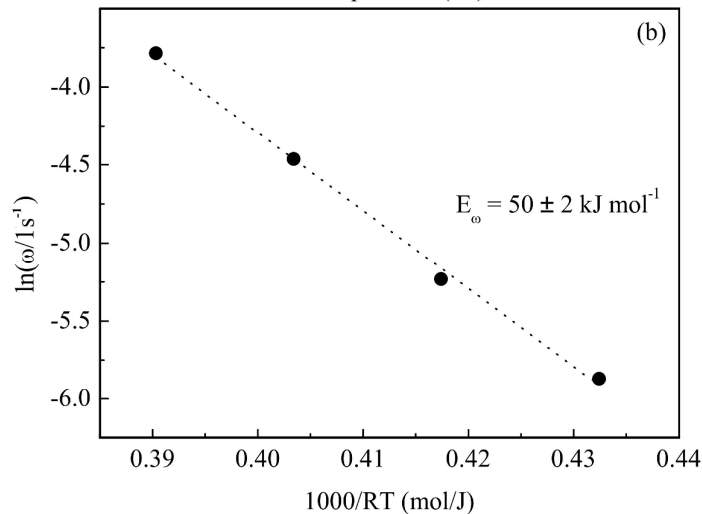
Figure 6: Time evolution of the bromate/oxalic acid and acetone/cerium oscillatory system at (a) 5, (b) 15, (c) 25 and (d) 35 °C, and at $k_0 = 0.0098 \text{ s}^{-1}$. Vertical lines indicate when the pumps were switched off. $[\text{H}_2\text{SO}_4]_0 = 1.42 \text{ mol L}^{-1}$; $[\text{NaBrO}_3]_0 = 0.010 \text{ mol L}^{-1}$; $[(\text{COOH})_2]_0 = 0.025 \text{ mol L}^{-1}$; $[\text{CH}_3\text{COCH}_3]_0 = 0.115 \text{ mol L}^{-1}$; $[\text{Ce}_2(\text{SO}_4)_3]_0 = 0.0005 \text{ mol L}^{-1}$.

The effect of temperature on the oscillatory frequency under both batch and open regimes is summarized in Figure 7(a). The missing point in the data for the batch system accounts for the fact that no oscillations are observed at 35 °C for the lower acetone concentration, c.f. Figure 3. The oscillatory frequencies at different temperatures taken from Figure 6 were used to estimate the activation energy for the CSTR regime.¹⁹ The Arrhenius plots for the CSTR regime are presented in Figure 7(b). An excellent linearity is observed and an apparent oscillatory activation energy of $50 \pm 2 \text{ kJ mol}^{-1}$ results.

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Figure 7: (a) The effect of temperature on the oscillatory frequency ω , for the bromate/oxalic acid/acetone/cerium system operated in batch and also in a CSTR. (b) Arrhenius plots using the oscillatory frequency, ω , for the system operated in a CSTR. Data for experiments in batch as in Figure 1 and for the open system as in Figure 6.

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335 As already anticipated in Figure 5, it is clear from Figure 7(a) that the open
336 system oscillates faster than the one operated in batch, for the whole range of
337 temperature studied. The apparent oscillatory activation energy decreases from 72 ± 2
338 kJ mol^{-1} , in batch, to $50 \pm 2 \text{ kJ mol}^{-1}$ under flow. As the batch regime is virtually at k_0

339 = 0, if other k_0 values higher than 0.0098 s^{-1} were employed an oscillatory activation
340 energy still lower should be found. These two aspects are central in the present study
341 and will be further discussed below.

342 Experimental results for other systems are in line with our findings, as already
343 mentioned in the Introduction.^{16,19} Nogueira *et al.*¹⁹ in particular, clearly show the
344 increase of the apparent oscillatory activation energy as the system approaches the
345 thermodynamic equilibrium. As already stressed, in order to isolate as much as
346 possible the effects of interest, namely the operation mode and temperature, it is
347 mandatory to keep, if possible, all the other parameters constant, as in the present
348 case. In this respect, we are not aware of a comparable report. Taking specifically the
349 work by Kulkarni and co-workers,^{22-23,24,25} who investigated the effect of temperature
350 under comparable conditions for the same system studied here, besides the different
351 concentrations used in some experiments in batch and under flow, the authors also
352 used Ce^{4+} as the catalyst in some experiments, and this might lead to misleading
353 results. In fact, we have shown that Ce^{3+} is the needed catalyst to observe oscillations
354 in the bromate-oxalic acid-acetone-cerium system.^{21,26} In batch, no induction period is
355 observed when Ce^{3+} is used, and in a CSTR, oscillations were found with Ce^{3+} and
356 with aged solution of Ce^{4+} , after partial conversion of Ce^{4+} to Ce^{3+} by reaction with
357 acetone. The use of Ce^{4+} results in long induction times and leads to imprecision. In
358 terms of the influence of temperature, we have observed that the Arrhenius plots are
359 less linear when Ce^{4+} is used instead of Ce^{3+} .

360 Back to the main results, in summary, we observed that, as the system is
361 moved out from the state of thermodynamic equilibrium, its oscillatory frequency
362 generally increases and its apparent oscillatory activation energy decreases. The first
363 aspect, the frequency increasing with the distance from equilibrium was already

364 discussed. We focus now on the temperature dependence, as discussed in terms of
365 apparent activation energy for the oscillatory system. The activation energy of an
366 elementary reaction step accounts for the energy barrier that molecules have to
367 overcome in order to form products. For more complex processes, however, the
368 presence of different steps and intermediates results in the existence of several energy
369 barriers. In the case of an oscillating network consisting of many reactions and
370 chemical species, the apparent oscillatory activation energy, as measured by the
371 oscillatory frequency, informs on the temperature dependence of the oscillator, as it is
372 based on a single reaction. As presented by Körös,¹³ the system can be regarded as ‘a
373 series of autocatalytic reaction bursts occurring with a certain frequency’. In our case,
374 the apparent oscillatory activation energy decrease as the system is kept far from
375 equilibrium, and it is equivalent to saying that it becomes less sensitive to temperature
376 changes. As a consequence, the relative independence of the physiological rhythms in
377 living systems on the environmental temperature, known as temperature
378 compensation, might indeed be favored under significantly far from equilibrium
379 regime. It is well-known that dynamic self-organization,³⁶ such as the temporally
380 organized rhythms, that characterizes all living structures, occurs only in open and far
381 from equilibrium systems. What our results reinforce is that the distance from
382 equilibrium favors the decrease of temperature sensitivity.

383 Curiously enough, but also in line with our observations, our previous study
384 on the electro-oxidation of formic acid on platinum and in acidic media,⁵ showed that,
385 even for a system having a highly non-Arrhenius temperature dependence,
386 temperature compensation is found under considerably far from equilibrium regime.

387 The role of flow in the temperature compensation has been explored by Otto
388 Rössler in an often cited proceeding paper.¹⁵ The author discusses the temperature-

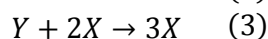
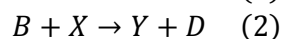
389 sensitivity as resulting of a combination of kinetic and flow parameters and draw
390 some particular conditions for achieving temperature compensation for the case
391 studied, namely a relaxation oscillator. Importantly, the author mentions the role
392 eventually played by membranes. In bio-systems, membranes are key components
393 that control the inflow and outflow of species and preserve the internal organization
394 by keeping the system under far from equilibrium regime. However, besides the
395 magnitude of flow itself, the selectivity, or its effect on particular species, is also a
396 key aspect when discussing properties such as the temperature dependence on the
397 oscillatory frequency. This aspect will be further discussed below.

398 In the following we present some numerical results that explore some aspects
399 raised by our experiments. Given the lack of a well-established model for the studied
400 system, we used a general and very simple model to investigate the effect of flow and
401 temperature.

402

403 **3.2 Numerical solutions of the Brusselator model**

404 The chosen model to test the ideas just discussed was the Brusselator,^{37,38} a
405 very simple, classical example of a limit cycle oscillator. The model consists of the
406 following hypothetical steps:



407 where A and B are the initial reactants whose concentrations are assumed to be
408 constant, D and E are final products, X and Y are intermediate species that oscillate
409 under a suitable choice of the rate of reactions and initial concentrations of A and B.
410 This mechanism can be translated to a set of differential equations:

411

$$\begin{aligned}\frac{dX}{dt} &= k_1 * A_0 - k_2 * B_0 * X + k_3 * X^2 * Y - k_4 * X \\ \frac{dY}{dt} &= k_2 * B_0 * X - k_3 * X^2 * Y\end{aligned}\quad \text{ODE 1}$$

412 These equations describe how the concentrations of the two intermediate
413 species X and Y change as a function of their concentration and that of the initial
414 reactants A and B . In the original formulation of the Brusselator model,^{37,38} $[A]$ and
415 $[B]$ are held constant which implies continuous inflow for those species, and the
416 system represents, thus, a semi-batch oscillator. In our case, the original equations
417 were modified to directly incorporate the effect of reactant inflow and outflow fluxes,
418 as we shall describe in the following. Specific routines were built using the
419 Mathematica[®] software to solve the resulting ODEs as well as analyze the resulting
420 time series as a function of selected parameter changes. Runge-Kutta with variable
421 step size was the preferred method for numerical integration.

422

423 ***The effect of the flow.*** In order to explicitly incorporate the effect of the flow of
424 reactants in a continuously fed well-stirred tank reactor (CSTR) it is necessary to add
425 two other equations accounting for the addition and removal of the initial reactants A
426 and B , where k_f stands for the flow rate:

427

$$\begin{aligned}\frac{dA}{dt} &= k_f * A_0 - k_1 * A - k_f * A \\ \frac{dB}{dt} &= k_f * B_0 - k_2 * B * X - k_f * B\end{aligned}\quad \text{ODE 2}$$

428

429 The final set of equations describing the CSTR system can be achieved with a minor
430 intervention on the original ODEs to account for the removal of the intermediate
431 species. The final set of equations for the CSTR oscillator then becomes:

432

$$\begin{aligned}\frac{dA}{dt} &= k_f * A_0 - k_1 * A - k_f * A \\ \frac{dB}{dt} &= k_f * B_0 - k_2 * B * X - k_f * B \\ \frac{dX}{dt} &= k_1 * A - k_2 * B * X + k_3 * X^2 * Y - k_4 * X - k_f * X \\ \frac{dY}{dt} &= k_2 * B * X - k_3 * X^2 * Y - k_f * Y\end{aligned}\quad \text{ODE 3}$$

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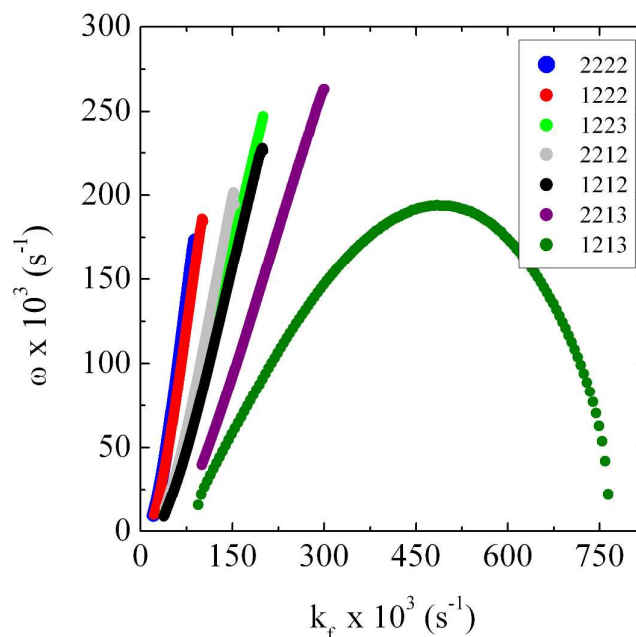
434 Oscillations may be found for this system of equations after numerical
435 integration and a sensible choice of the parameters. In what follows, the values of A_0
436 and B_0 were fixed at 20, and the oscillatory frequency analyzed as a function of the
437 flow rate, k_f , for some selected sets of the constants $\{k_1, k_2, k_3, k_4\}$ which were
438 representative of the overall model behavior. Numerical results of the effect of the
439 flux of reactants through the reactor on the oscillatory frequency are displayed in
440 Figure 8.

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445 **Figure 8:** Simulated dependency of the oscillatory frequency on the
 446 parameter k_f that represents the flux of reactants through the reactor (set
 447 ODE 3). The curves were obtained for several sets of the rate constants
 448 $\{k_1, k_2, k_3, k_4\}$, indicated in the insert.
 449

450
 451 The majority of curves presented in Figure 8 reveal a general increase in the
 452 values of oscillatory frequency as the flow rate increases, in line with our
 453 experimental findings, c.f. Figure 5. This behavior was found for six combinations of
 454 the rate constants $\{k_1, k_2, k_3, k_4\}$ and for the whole range of flow in which oscillations
 455 exists. One exception was found for the set $\{1, 2, 1, 3\}$, but the deviation occurs only
 456 for a very high k_f , namely k_f higher than 0.5 s^{-1} , i.e. in an extreme parameter region. In
 457 terms of the mechanism, the decrease of oscillatory frequency when increasing the
 458 flow rate was found only for a combination of the smallest value for the rate of step 1
 459 ($A \rightarrow X$) with the highest value for the rate of step 4 ($X \rightarrow E$), and only for very high
 460 flow rates. Under these conditions the decrease of the oscillatory frequency can be
 461 attributed to the small concentrations of X (low formation and fast removal) and also
 462 to its low residence time within the reactor. Finally, we observed that the range of
 463 flow rate in which oscillations can be found generally increases with the decrease of
 464 k_3 and with the increase of k_4 . It was mentioned in the experimental section that, in

465 batch, a possible explanation for the slower dynamics was the general decrease in the
 466 concentration of active species caused by their consumption in a closed system. This
 467 effect is absent in our simulations since we used constant concentrations for A and B
 468 in the simulations for the original Brusselator, which prevents any damping and
 469 produces only stable oscillations as for the system under explicit flow.

470 As seen in the set ODE 3, the flow rate parameter k_f is found to impact several
 471 terms of the differential equations' set. It is possible to evaluate how each one of these
 472 terms affects the overall oscillatory frequency. To do so, we can discriminate each k_{fi}
 473 which appear in the set ODE 4:

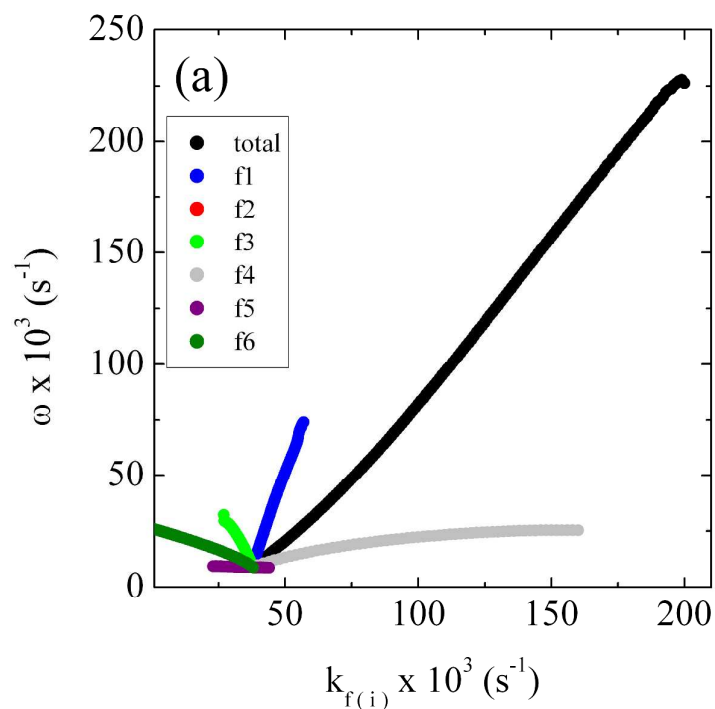
$$\begin{aligned}
 \frac{dA}{dt} &= k_{f1} * A_0 - k_1 * A - k_{f2} * A \\
 \frac{dB}{dt} &= k_{f3} * B_0 - k_2 * B * X - k_{f4} * B \\
 \frac{dX}{dt} &= k_1 * A - k_2 * B * X + k_3 * X^2 * X - k_4 * X - k_{f5} * X \\
 \frac{dY}{dt} &= k_2 * B * X - k_3 * X^2 * Y - k_{f6} * Y
 \end{aligned}
 \tag{ODE 4}$$

475
 476 Altogether, there are six flow rate terms, four of them which increase (k_{f1} and
 477 k_{f3}) and decrease (k_{f2} and k_{f4}) the concentrations of A and B, and two related with the
 478 withdraw of the intermediate species X and Y (k_{f5} and k_{f6}). We can vary each of those
 479 k_{fi} individually while keeping the remaining values constant at a control value. It is
 480 important to note, at this point, that this is merely a mathematical procedure, aiming
 481 to explore how these parameters, individually, influence the overall oscillatory
 482 dynamics for the model, and that there is no direct physical counterpart associated to a
 483 variation on a specific value of k_{fi} , since it would violate volume conservation. Still,
 484 one can see the variation in those parameters as a mean of increasing or decreasing
 485 the relative abundances of the reactants A, B, X, and Y. With this thought in mind,

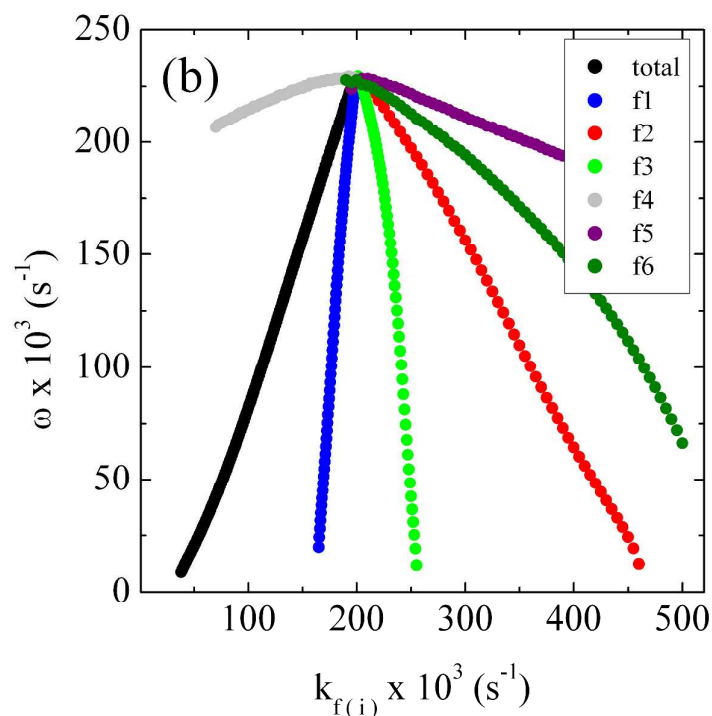
486 and the tool in hands, important insights can be achieved as of the role of availability
487 of each of the reactant and its effect on oscillatory properties.

488 Figure 9 shows the effect of the variation of each k_{fi} value on the oscillatory
489 frequency for the CSTR version of the Brusselator. On panel (a) the results of such
490 procedure are shown for values of k_{fi} starting from a low flow rate value ($k_0 = 40$),
491 while (b) displays the results for a high flow rate value ($k_0 = 200$). The set of four k_i
492 values used were $\{1,2,1,2\}$, but the general trend is similar for other sets of k_i .

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Figure 9: The curve in black shows how oscillatory frequency depends on the flow rate for the CSTR version of the Brusselator model using the {1,2,1,2} rate constants set. The colorful lines indicate the dependency of the oscillatory frequency on the individual rate constants k_{fi} found in the set ODE 4, at low and high flow values, $k_0 = 40$ in (a), and $k_0 = 200$ in (b). $A_0 = B_0 = 20$.

508 Figure 9 shows that each different constant is associated with different effects
509 on the oscillatory frequency. A common feature, however, is that a given rate constant
510 plays the same role either at low or high flow rate. It is possible to quantify the
511 magnitude of individual flow rate parameters k_{fi} on the overall behavior of frequency
512 by introducing a sensitivity coefficient. Such coefficients have been used in biological
513 contexts to evaluate the response of specific living organelles' functions for variations
514 of important chemical species or physical parameters such as temperature.³⁹ In our
515 specific case, it is intuitive to introduce the sensitivity coefficient for the oscillatory
516 frequency:

$$S_{k_{f,i}}^{\omega} = \left(\frac{\partial \omega}{\partial k_{f,i}} \right)_{k_{f,i} \rightarrow k_{f,control}}$$

517 Here, a specific sensitivity coefficient $S^{\omega}_{k_{f,i}}$ relates how the oscillatory
 518 frequency ω changes as function of a variation on a specific flow rate parameter $k_{f,i}$.
 519 The partial derivative is evaluated in the vicinities of the control flow rate, rendering
 520 thus a special physical meaning to the sensitivity coefficients, since the change in
 521 volume of the reactor is infinitesimal for that limit.

522 Table I presents the overall dependency of the oscillatory frequency on the increase in
 523 each of the $k_{f,i}$ constants as well as the specific control coefficients. It can be seen that
 524 parameters k_{f1} and k_{f2} related with the addition and removal of A, respectively,
 525 increase and decrease the oscillatory frequency. On the other hand, parameters k_{f3} and
 526 k_{f4} , associated with the addition and removal of B, display the opposite effect. This
 527 result is in accordance with the simulated original Brusselator system where
 528 integration of the original ODE 1 set reveals that an increase in the concentration of A
 529 leads to higher oscillatory frequencies, while an increase for B promotes the opposite
 530 trend. Finally, Table I shows that an increase in the values of k_{f5} and k_{f6} promotes a
 531 decrease in oscillatory frequency, which means that depletion on the concentration of
 532 the intermediates X and Y has a negative effect on this property.

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Table I: Dependence of oscillatory frequency on the variation of individual constants associated with flow rate.

| Parameter | Effect on ω | $S^{\omega}_{k_{f,i} \rightarrow 40}$ | $S^{\omega}_{k_{f,i} \rightarrow 200}$ |
|---------------|--------------------|---------------------------------------|--|
| k_{f1} | ↑ (+) | + 3.6 | + 4.0 |
| k_{f2} | ↓ (-) | - 0.19 | - 0.71 |
| k_{f3} | ↓ (-) | - 2.7 | - 1.5 |
| k_{f4} | ↑ (+) | + 0.34 | + 0.088 |
| k_{f5} | ↓ (-) | - 0.33 | - 0.19 |
| k_{f6} | ↓ (-) | - 0.75 | - 0.33 |
| $k_{f,total}$ | ↑ (+) | + 0.99 | + 1.4 |

536

537 In this way, we can see that the individual flow rate parameter operates on
 538 several terms of the set of differential equations and that each one of them has a

539 particular effect on the oscillatory frequency, since it is specifically associated to the
540 increase/withdraw of a particular reactant. Back to our specific results, a closer look
541 in Figure 9 reveals that the constants k_{f1} and k_{f3} related to the addition of reactants A
542 and B, respectively, display the most pronounced effect on frequency, with k_{f1}
543 promoting its increase while k_{f3} producing its decrease. Thus we can explain the
544 overall increase of frequency as the flow rate is increased (curve in black in Figure 9),
545 as a function of a higher weight of the term related with k_{f1} . In summary, the results
546 shown in Figure 9 can be rationalized as the net increase in the oscillatory frequency
547 is a result of an increasingly surplus of the initial reactant A.

548 As represented by the black curve in Figure 9, simple experiments in a CSTR
549 would result in overall increase of the oscillatory frequency with the increase in the
550 flow rate. The selective removal or addition of a given species in the reaction network
551 would result in the increase or decrease of the oscillatory frequency. An interesting
552 aspect that emerges from these results consists of the opposite effects exerted by the
553 removal or addition of a given species. This feature opens the possibility of exploring
554 the selective role of a given species to achieve properties such as temperature
555 compensation. Indeed, the high selectivity of cellular membrane might play a role in
556 keeping unaltered biological rhythms despite of changes in the environment. The
557 importance of the interactions between membrane ion transport and ion concentration
558 gradients in circadian rhythms has been discussed in the Njus-Sulzman-Hastings or
559 membrane model.⁴⁰ Despite the criticisms to some aspects of this earlier model,
560 Nitabach *et al.*⁴¹ stressed the essential role that the ion fluxes through the membrane
561 play in the mechanism of the core oscillator. Therefore, this discussion suggests that,
562 instead of the robustness of a given biochemical network, it would be thus more
563 adequate to consider the confined system (chemistry and membrane) as whole. The

564 use of methods to investigate the reaction mechanism in complex systems^{42, 43} is
 565 certainly of help in this direction.

566

567 ***The effect of temperature.*** Temperature variation will affect directly the overall
 568 oscillatory frequency through its influence on each specific reaction rates k_i . This
 569 effect can be mathematically treated through the use of control coefficients:^{1,2,3-4}

$$570 \quad C_{k_i}^{\omega} = \frac{\partial \ln \omega}{\partial \ln k_i} \quad \text{e1}$$

571 The overall effect of temperature on frequency can be understood as the sum:

$$572 \quad \frac{\partial \ln \omega}{\partial T} = \sum_{i=1}^4 \frac{\partial \ln \omega}{\partial \ln k_i} * \frac{\partial \ln k_i}{\partial T} \quad \text{e2}$$

573 Through reference to Arrhenius' law, the following equation can be derived:

$$574 \quad \frac{\partial \ln k_i}{\partial T} = \frac{E a_i}{RT^2} \quad \text{e3}$$

575 Which finally produces:

$$576 \quad \frac{\partial \ln \omega}{\partial T} = \frac{1}{RT^2} * \sum_{i=1}^4 C_{k_i}^{\omega} * E a_i \quad \text{e4}$$

577 Here it is possible to see that each specific reaction will influence the overall
 578 frequency change with respect to its specific control coefficient and activation energy.

579 The overall activation energy can be calculated as:

$$580 \quad E_{\omega} = \sum_{i=1}^4 C_{k_i}^{\omega} * E a_i \quad \text{e5}$$

581 For the Brusselator model, this expression actually translates into:

$$582 \quad E_{\omega} = (C_{k_1}^{\omega} * E a_1 + C_{k_2}^{\omega} * E a_2 + C_{k_3}^{\omega} * E a_3 + C_{k_4}^{\omega} * E a_4) \quad \text{e6,}$$

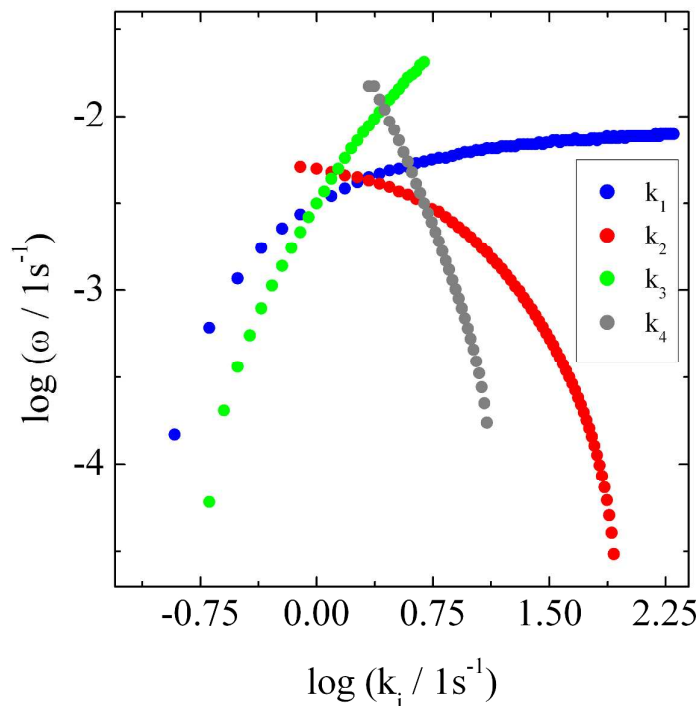
583 which indicates how the apparent oscillatory activation energy relates with the
 584 activation energies of individual steps. Figure 10 portraits the influence of the reaction
 585 rates on the oscillatory frequency for the CSTR version of the Brusselator model.

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Figure 10: Influence of each k_i on the oscillatory frequency for the CSTR version of the Brusselator model, set ODE 3 with $k_f = 0.10 \text{ s}^{-1}$. Each rate constant was varied individually while the others would obey the following set $\{1,2,1,2\}$. $A_0 = B_0 = 20$.

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Results in Figure 10 describe the impact of the rate constants on the oscillatory frequency. Coefficients $C_{k_i}^\omega$ were estimated and indicate that: steps 1 ($A \rightarrow X$) and 3 ($Y + 2X \rightarrow 3X$) contribute to increase the oscillatory frequency as the temperature increases, whereas steps 2 ($B + X \rightarrow Y + D$) and 4 ($X \rightarrow E$) belong to the frequency decreasing set. In short, steps that produce X increase the oscillatory frequency and the ones that consume X decrease the oscillatory frequency. In general, this trend was also found for almost all combinations of constants investigated.

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According to equation (e6), the apparent oscillatory activation energy for the Brusselator model would thus result of positive contributions of the activation energies of steps 1 and 3, and negative ones of steps 2 and 4. The impact of individual rate constants on the oscillatory frequency can be readily compared to the role of

607 selective feeding of different species discussed above. For instance, saying that step
608 steps 1 ($A \rightarrow X$) contributes to increase the oscillatory frequency as the temperature
609 increases, as evidenced by its positive control coefficient, is equivalent to the
610 observation that the addition/removal of species A contributes to the increase/decrease
611 of the oscillatory frequency, as discussed above.

612

613 **4. Summary and Conclusions**

614 We investigate in this article the coupled effects of temperature and of the
615 distance from thermodynamic equilibrium on the dynamics of a homogeneous
616 oscillatory system. Experiments were carried out with the bromate/oxalic acid and
617 acetone/cerium system under different temperatures and flow rates, by means of a
618 continuous flow stirred tank reactor (CSTR). The conclusions on the effect of the
619 distance from thermodynamics equilibrium was validated by the nearly identical
620 oscillation's features under both batch and flow regimes. The experimental results
621 were discussed in connection with numerical simulations using the Brusselator model,
622 in its conventional formulation and also in a modified one to explicitly include the
623 effect of flow.

624 The experiments reveal a general increase of the oscillatory frequency when
625 the flow rate is increased, in line with our previously published experiments in some
626 homogeneous (chemical) and also heterogeneous (electrochemical) oscillators.
627 Numerical simulations with the CSTR version of the Brusselator confirm this
628 tendency but also disclose a tiny parameter region (for one specific set of rate
629 constants and at extremely high flow rates) in which the increase of the flow rate
630 results in a decrease in the oscillatory frequency. The effect of flow rate was also
631 explored for each species of the Brusselator. Remarkably, we observed that, although

632 the increase of the flow rate typically increases the oscillatory frequency, the feed
633 concentration of each species impacts in a particular way the overall oscillatory
634 frequency. This finding further stresses the role of flow rate in reacting systems, an
635 important aspect for engineering artificial oscillators for specific applications.

636 The apparent oscillatory activation energy obtained via Arrhenius plots using
637 the oscillatory frequency, was found to amount to $72 \pm 6 \text{ kJ mol}^{-1}$, in batch, and to 50
638 $\pm 2 \text{ kJ mol}^{-1}$, under flow. Unlike previous reports, these results were obtained under
639 identical concentrations of all species and thus allowed to separate the effects of flow
640 and temperature dependence. The decrease of the apparent oscillatory activation
641 energy from batch to flow was interpreted as a result of the maintenance of the
642 concentration of reactants, in contrast to their decrease caused by their consumption in
643 batch, which is in line with our previous results.¹⁹ Numerical simulations with the
644 CSTR version of the Brusselator were explored in terms of the control coefficients,
645 $\partial \ln \omega / \partial \ln k_i$,^{1,2,3-4} for each reaction step i of the model. The results uncover the
646 existence of two steps that are associated to the frequency-increasing set and two to
647 the frequency-decreasing one, whose role remains unchanged despite the operational
648 conditions. Furthermore, and as already mentioned, the particular manner at which the
649 feeding rate of each species affects the oscillatory frequency further reinforces the
650 role played by the selectivity of biological membranes in this respect.

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672 **References**

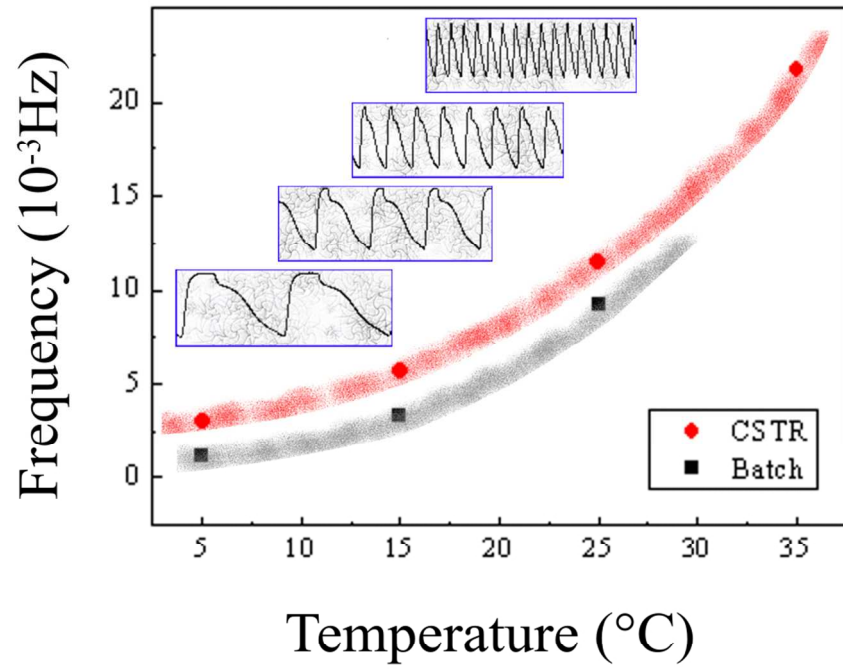
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Dependence of the oscillation frequency on the temperature under flow and batch regimes