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A Langmuir-like desorption model for reflecting the inhomogeneous pore structure of coal and its

experimental verification

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ABSTRACT: A Langmuir-like model was established to describe the desorption kinetics of methane in coal with inhomogeneous pore structure. Two Chinese coal samples were selected to study the initial CH₄ desorption rate in coals with the volumetric method under five equilibrium pressures. The results show that the pressure has a significant influence on desorption kinetics of methane in coal. At a constant temperature, desorption volume increases with the rising of pressure. And at a given desorption time, the desorption volume appears to have a Langmuir-like relationship with pressure. Also, the relationship between the parameters in the Langmuir-like model and desorption time is power function. Thus, we can obtain the changing law of desorption volume with equilibrium pressure and desorption time from the Langmuir-like model. This model is a valuable option to the prediction of lost gas content and identification of coal and gas outburst.

Keywords: Methane; desorption kinetics; Langmuir-like model; inhomogeneous pore structure

1 Introduction

Coalbed methane has always been a major problem in underground coal mining and can cause a variety of problems including mining hazards of explosions and outbursts, pollution of the environment, and climate change¹⁻³. Thus, in order to improve mining safety and to reduce greenhouse gas emission, the research of gas transportation of methane in coal is very important $4-7$.

Desorption kinetics of methane in coal has been studied since 1950 and the conventional approach for modeling matrix gas transport mainly focuses on the relative desorption volume rather than the absolute desorption volume⁸⁻¹⁵. For example, the unipore diffusion model⁸⁻¹³ and the bidisperse pore diffusion model¹⁴, these models play an important role in understanding details of the desorption law. However, the application of absolute desorption volume plays an important role in predicting the coal and gas outburst. And researchers have proposed many equations to describe the relationship between the absolute desorption volume and desorption time, such as the H.M.BCTMHOB equation($Q_t = v_0 \left((1+t)^{1-n} - 1 \right) / (1-n)$), Barrier equation ($Q = k \sqrt{t}$) and Sun Chong-xu equation $(Q = at^i)^{16}$. In which, the Barrier equation was proposed on the basis of unipore

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diffusion model and has its own theoretical foundation, and the Barrier equation was verified to fit well with the experimental desorption data in a short time but not good for a longer time. The H.И.BCTИHOB and Sun Chong-Xu equations were proposed by fitting the experimental data and belongs to empirical formula, and these equations were proved not to be suitable for all coal samples because of the complex coal characteristics¹⁷.

Coal is a complex polymeric material, its pore structure is inhomogeneous ¹⁸⁻²⁰, and as a potential reservoir for coalbed methane (CBM), the pore structure has great effects on gas transport²¹⁻²³. Therefore, for seeking the best fit for the desorption kinetics of methane in coal, two Chinese coal samples were applied to do the desorption experiment and a desorption model for reflecting the inhomogeneous pore structure of coal was established. The desorption model can describe the relationship between the absolute desorption volume and desorption time at a given pressure, and this is important in predicting the coal and gas outburst.

2 Theory of the Langmuir-like equation

Coal is a porous media with macromolecule structure resulting in the inhomogeneous pore structure¹⁸⁻²⁰. Suppose there are *N* kinds of adsorption center at the coal surface. As total rate is the difference between desorption rate and adsorption rate, it can be expressed in Eq. (1):

$$
R_{t} = \frac{d\theta_{t}}{dt} = R_{t}^{d} - R_{t}^{a} = \sum_{n=1}^{N} f_{n} R_{n}^{d} - \sum_{n=1}^{N} f_{n} R_{n}^{a}
$$
(1)

where *t* is the desorption time, *n* is the *nth* adsorption center number, θ , is gas coverage on the coal surface at the desorption time of t based on assumption of monolayer adsorption type. f_n is the fraction of the *nth* adsorption center. For the ideal gas, R_n^d and R_n^a are separately the desorption and adsorption rate for the *nth* adsorption center. R_n^d is proportional to θ_n defined as the gas coverage at the *nth* adsorption center, then R_n^a is proportional to 1– θ_n defined as the empty adsorption sites at the *nth* adsorption center, also, R_n^a is proportional to α defined as the ratio of absorbed molecule number to total molecules hitting the coal surface, so the total rate can be given by Eq.(2)

$$
R_{t} = \frac{d\theta_{t}}{dt} = \sum_{n=1}^{N} f_{n}k_{n}^{d}\theta_{n} - \alpha\mu\sum_{n=1}^{N} f_{n}k_{n}^{a}(1-\theta_{n})
$$
\n(2)

where k_n^d and k_n^a are separately the constants of desorption and adsorption rate, μ is the total number of molecules hitting 1cm^2 coal surface per second, and can be expressed in 2 *p* $\mu = \frac{P}{\sqrt{2\pi MRT}}$ according to the

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kinetic theory of gas. *T* is the absolute temperature; *P* is the gas pressure; *M* is the molecule weight of the gas; R is the gas constant.

When the types of adsorption center is large enough, $Eq.(2)$ can be expressed in a simple style given in Eq. (3) :

$$
R_t = \frac{d\theta_t}{dt} = \overline{k}^d \theta_t^{1/\nu_t} - \alpha_t \mu \overline{k}^a (1 - \theta_t)^{1/\nu_t}
$$
 (3)

where 1 *L* $\sum_{l=1}^t J_l \mathcal{O}_l$ $\theta_t = \sum f_i \theta_i$ $=\sum_{i=1}^{L} f_{i} \theta_{i}$; \overline{k}^{a} and \overline{k}^{d} are separately the average constants of adsorption and desorption rate for the whole inhomogeneous coal surface; α_t is the ratio of absorbed molecule number to the total molecules hitting the coal surface at time t ; v_t is a parameter representing the inhomogeneous level of coal surface($0 < v < 1$) at time *t* when the time $t \to \infty$, The adsorption rate is equal to the desorption rate, then Eq.(3) becomes:

$$
\theta_{t}|_{t\to\infty} = \frac{Q_{pt}}{a_{t}}|_{t\to\infty} = \frac{\left(\frac{p}{\sqrt{2\pi MRT}}\alpha_{t}\overline{k}^{a}\right)^{v_{t}}}{\left(\overline{k}^{d}\right)^{v_{t}} + \left(\frac{p}{\sqrt{2\pi MRT}}\alpha_{t}\overline{k}^{a}\right)^{v_{t}}|_{t\to\infty}}
$$
(4)

where Q_{pt} is the volume of gas desorbed at time t , a_t is the limit desorption volume at time t under the equilibrium pressure P , representing the adsorption capacity of coal, the larger the value of a_t , the stronger the adsorption forces and the steeper the desorption curve.

Let
$$
b_t|_{t\to\infty} = \left(\frac{\overline{k}^a}{\overline{k}^d} \frac{\alpha_t}{\sqrt{2\pi MRT}}\right)^{v_t}|_{t\to\infty}
$$
, then Eq.(4) becomes

$$
Q_{pt}|_{t\to\infty} = \frac{a_t b_t P^{v_t}}{1 + b_t P^{v_t}}|_{t\to\infty}
$$
(5)

From Eq.(5) it can obtain that the relationship between the desorption volume with the pressure under the equilibrium pressure *P* at the time $t \to \infty$. b_t is the Langmuir desorption constant at the time $t \to \infty$, and its reciprocal is the Langmuir pressure that is corresponding to the pressure at which half of the Langmuir volume $a_{\mu\to\infty}$ is reached and from Eq.(5) we can see that $b_{\mu\to\infty}$ reflects the ratio of adsorption and desorption rate and the larger the value of $b_{i\to\infty}$ the higher the desorption rate and the steeper the desorption curve.

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As for a given pressure, the adsorption/desorption volume changes over time before equilibrium, thus from Eq.(5), we can assume that: a limit desorption volume (a_i) and a Langmuir desorption constant (b_t) always exists corresponding to a given time t_t during the adsorption/desorption process under a given pressure, and the inhomogeneous level of coal always changes over time because of the adsorption of methane to coal surface. Thus for a given time t , there always exists an index of v_t , thus, the desorption rate for a given pressure *P* at a given time *t* would be given in the following form:

$$
Q_{pt} = \frac{a_i b_i P^{v_i}}{1 + b_i P^{v_i}}
$$
\n(6)

In order to verify the applicability of Eq. (6) in the methane desorption from coal, we did some desorption experiments and the changing law of parameters over time in Eq.(6) were also be confirmed.

3 Experimental verification of the Langmuir-like desorption model

3.1 Proximate and Petrographic analysis of coal samples

Two coal samples were collected from TieFa(TF), TunLan(TL) coal mines. Upon collection, coal blocks were immediately wrapped tightly with plastic, indexed, and transported to the laboratory. The blocks were then ground and sieved to a size range of 0.2~0.25 mm. After crushing, the samples were kept in airtight packets and refrigerated to prevent oxidation. **Table 1** summarizes the Proximate and Petrographic analysis results of the coal samples.

Coal			Petrographic analysis (vol.%)			THEIR T I TOMINIQUE THAT CHOLOGIC CHILI (SID OF THO CHINGS COME SAMPLES Proximate analysis (wt .%)		
	V Rr $(\%)$	Vitrinite	Intertinite	Mineral	$M_{\rm ad}$	Ađ	V_{daf}	
TF	0.60	91.60	5.50	2.90	6 77	19 75	38.77	
TL	L.85	88.65	2.30	9.05	0.89	22.89	19.63	

Table 1 Proximate and Petrographic analysis of two Chinese coal samples

From Table 1 it can be seen that TL coal samples has the higher coal rank, mineral and ash contents, Vitrinite group macerals are the most abundant maceral group in this two coal samples, no liptinites were found in this two coal samples, the possibly reason is that Liptinite/Exinite often accumulated in a specific position in the coal bed, which means that the Liptinite/Exinite in coal seams are unevenly distributed, some positions may be rare in Liptinite/Exinite, while some coal positions may be rich in Liptinite/Exinite. The distribution of Liptinite/Exinite is mainly controlled by coal-forming materials. Another possibly reason is that the Liptinite/Exinite has fine grain size, occurs in other components, and it is always difficult to analyze accurately 24 .

3.2 Pore structure by nitrogen adsorption

Liquid nitrogen adsorption method was used to study the inhomogeneous pore surface structure of coal, the specific surface area was calculated with BET method, the pore volume was calculated with the BJH

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equation. To better understand the effects of pore structure on the gas desorption kinetics, a combined classification from IUPAC ²⁵ and Hodot²⁶ for coal pore size was used in this work: ultra-micropores(<10 nm), mesopores (10–100 nm), macropores (>100nm).The results are shown in Table2:

Coal	Average	the total specific surface area/ $\rm (m^2/g)$	Percentage of the specific surface area of the pore-size spectrum /%			Total pore	The Specific pore volume of the pore-size spectrum /%		
sample	pore diameter/nm		$<$ 10nm	10-100nm	>100 nm	volume/ (mL/g)	$<$ 10nm	10-100nm	>100 fuu
TF	7.525	5.84	72.964	24.387	2.649	9.02E-03	65.9	5.9	28.2.
TL	22.02	0.998	37.201	54.656	8.143	2.96E-03	4.38	74.2	21.42
	illustrated in Fig. 1. 5 $\overline{4}$ Volume (mL/g)	TF	-Desorption - - Adsorption	changing trend of pore structure parameters with coal rank runs through a minimum.	2.0 TL 1.5 Volume (mL/g) 1.0 0.5	From table2 we can see that the TF coal sample has the smaller average pore diameter, the higher total and segmented specific surface area, the larger percentage of the micropore specific surface area, the lower percentage of mesopore and macropore specific surface area, the larger total pore volume and the percentage of the micropore and macropore pore volume, the lower percentage of mesopore pore volume comparing with the TL coal sample. The changing law of pore structure parameters with coal rank are consistent with the results reported by Levy et al., $(1997)^{27}$; Gürdal and Yalçın $(2001)^{28}$; Bustin and Clarkson $(1998)^{29}$ that a Based on the nitrogen adsorption method, two types of N_2 adsorption/desorption isotherms were \blacksquare Desorption \blacksquare Adsorption			SC Advances Accepted Manu
	0.0	0.2	0.4 0.6 Relative pressure P/P	0.8 1.0	0.0 0.0	0.4 0.2 Relative pressure P/P	0.6 0.8	1.0	

Table 2 pore structure parameters obtained from the liquid nitrogen adsorption method

Fig.1 N₂ adsorption/desorption isotherms at low temperature (77 K) of TF and TL coal samples From Fig.1 we can see that the adsorption capacity of the liquid nitrogen in TF coal sample is larger than in TL coal sample. No hysteresis loops between the adsorption/desorption isotherms exist in both of the two coal samples, the possibly reason is that proportion of the micro-pore is too large, and hysteresis characteristic

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exists in the desorption process. Another possible reason may be the variation of pore structure in coal, such as the swelling of coal during adsorption³⁰. The differences between the two coal samples are as follow:

The $N₂$ adsorption/desorption isotherms of TF coal sample increases slowly at the lower relative pressure and rapidly at the relative pressure near 1. When the relative pressure is less than 0.42, the adsorption isotherm is essentially coincident with the desorption branch, indicating that small pores are accessible via a single pore throat. As the relative pressure rises, the resulting inflection point occurs can be attributed to the difference between the adsorption and desorption mechanisms, corresponding to condensation and evaporation, respectively, and a steep fall exists in the desorption isotherm at the 0.42-0.6MPa interval. According to the kelvin equation, the pore size corresponding to the relative pressure of $0.42 MPa$ is 3.3nm. The pores with the size lower than 3.3nm is mainly cylinder-shaped pores with one open end and the pores with the size upper 3.3nm are mainly inkbottle-shaped and slit-shaped. The pore structure in TF coal sample has good condition in coalbed methane storage resulting in high methane volume and rapid desorption rate.

The N_2 adsorption/desorption isotherms of the TL coal sample increases slowly within the 0.1-0.9 relative pressure and rapidly with the relative pressure near 0.9 and does not show any adsorption limitation. According to the previous research results, these linear indicates that pores in the TL coal samples are mainly slit-shaped pores and few cylinder-shaped pores with two open end, few inkbottle-shaped pores and wedges-shaped pores. And these pore shape structure is disadvantage in coal bed methane storage resulting in low methane volume and slow desorption rate.

3.3 Desorption kinetics

Core sampling method was used to prepare the coal samples for the standard desorption tests. The collected coal samples were crushed into particles of 0.2~0.25 mm using a sampling machine. The gas used for the desorption tests were CH4 with a purity of about 99.99% and the experiments were conducted with the bath temperature of 303.15 K.

For the analysis of different gas desorption characteristics of coal samples, we corrected the desorption volume to standard atmospheric condition with the dry ash-free basis according to the Eq.(7) to comparatively study the desorption characteristics of the two Chinese coal samples.

$$
Q_{i} = \frac{273.15}{101325(273.15 + t_w)} \times (P_{\text{atm}} - 9.81h_w - P_0) \times Q_{i} \times \frac{100}{100 - M_{ad} - A_{ad}}
$$
(7)

where Q_i is the total desorption volume corrected to standard atmospheric condition, ml; Q_i is the desorption volume obtained during the experimental process, ml; t_w is the ambient temperature, \mathcal{C} ; P_{atm} is the atmospheric pressure, MPa; h_w is the height of liquid column in the desorption cylinder, mm; P_0 is the saturated vapor pressure at the temperature of t_w , MPa. The corrected data on the basis of the experimental

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data and the Eq. (7) for the desorption kinetics of $CH₄$ at the equilibrium pressure are shown in Fig.2.

Fig. 2. CH4 desorption data under different pressures of two Chinese coal samples

We can see from Fig. 2 that the shapes of the desorption kinetics are similar and have strong regular. The desorption rate of CH4 depends strongly on pressure, and the cumulative amount of desorption volume presents the positive interrelated relationship to the pressure, The reason is the increasing of initial gas concentration with adsorption content at higher equilibrium pressure, thus, when gas diffusion begins, greater gas concentration gradient exists at higher equilibrium pressure and finally resulting in the faster gas diffusion speeds ²⁶. The slope of desorption curve is higher at the later point of time than the former point, and the slope in the first 10min is very high. This phenomenon indicates that at the higher equilibrium pressure, the adsorption of the coal to methane is stronger and the desorption volume is larger, also, we can obtain the result that the desorption rate becomes smaller along with the time. According to the molecular diffusion theory, the reason for this phenomenon is the dependency of desorption rate on concentration difference exists between the external and internal surface of pore because of the highly enriched methane on the inner surface of pore. This concentration difference forces the methane to diffuse, and as time goes on, the concentration difference reduces gradually resulting in the gradually reduced desorption rate. It is observed from **Fig. 2** that for CH4, the lower-ranked TF coal sample generally exhibited higher desorption rate compared to the higher-ranked TL coal sample. This difference may be related to the evolution of coal pore structure with changing rank ¹⁷. And also this difference may caused by the surface area of coal that is higher in low rank TF coal sample.

To verify the Eq.(6), six vertical lines at the time of 5min, 10min, 15 min, 20 min, 25 min, 30 min were marked on each sub-graph **in Fig. 2**, and these vertical lines will intersect the desorption lines, then the vertical coordinates of this intersections were defined as Q_{pt} , which means the desorption volume at the time t with the equilibrium pressure P . By applying the Eq.(6), the points of (p, Q_{pt}) were marked on **Fig. 3.**

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Fig. 3. Diagram of $P \sim Q_{pt}$ on the two Chinese coal samples with CH₄

From **Fig.3**, we can see that correlation coefficients are all above 0.95, which means that the relationship between Q_{pt} and *P* can be well described by Eq.(6). The parameters of a_t , b_t in Eq.(6) are shown in table3.

		TF		TL				
t /min	a_t	b_t	\mathcal{U}_t	\hat{R}^2	a_{t}	b_{t}	\mathcal{U}_t	$\hat{\mathcal{R}}^2$
5	21.8153	0.2266	0.1993	0.99659	8.5246	0.4286	0.0459	0.9970
10	25.7842	0.2376	0.2107	0.9991	10.6904	0.4204	0.0320	0.9984
15	29.7602	0.2253	0.2365	0.9987	12.3416	0.4065	0.0308	0.9984
20	35.5151	0.1964	0.2749	0.9976	13.3787	0.4139	0.0179	0.9995
25	39.8553	0.1802	0.2918	0.9956	14.6383	0.3975	0.0237	0.9990
30	40.9812	0.1816	0.2950	0.9946	15.6035	0.3922	0.0230	0.9990

Table 3. Parameters of the Langmuir-like model on the two Chinese coal samples with CH₄ absorbed

It can be seen from **Table 3** that the ultimate desorption volume a_t in TF coal sample are larger than that in TL coal sample, consisting with pore structures of the two coal samples. And the trend of a_t increasing with the desorption time is consistent with the desorption curve. And the decreasing of b_t with the desorption time shows that the desorption rate decreases with the desorption time, consisting with the desorption curve. And the increasing of v_t in TF coal sample and decreasing of v_t in TL coal sample with *t* may due to the different pore structures of the two samples. The changing law of the parameters can be seen intuitively from **Fig. 4**.

Fig. 4. Changing law of the Langmuir-like model Parameters on the two Chinese coal samples for CH⁴ Through the fitting results of the data (t, a_t) and (t, b_t) in Fig. 4, we can conclude that the relationship between a_t , b_t and t are all in the form of power function:

$$
a_t = c_d t^{d_a} \tag{8}
$$

$$
b_i = c_b t^{d_b} \tag{9}
$$

$$
v_t = c_v t^{d_v} \tag{10}
$$

where parameters of c_a , c_b , c_c , d_a , d_b , d_c are the coefficient of the power functions and are listed in Table 4.

			$q \rightarrow q$, $q \rightarrow q$, $q \rightarrow q$, $q \rightarrow q$				
Coal sample	U	\mathbf{u}_a	\mathbf{c}_h	u_h	$\mathbf{U}_{\mathbf{n}}$	u_{ν}	
TF	10.80988	0.39422	0.4644	-0.0463	0.12353	0.25809	
TL	4.92097	0.338	0.4649	-0.047	0.0932	-0.44754	

Table 4 Parameters of c_a c_b *c* , *a* d_a , d_b , d_v in TF and TL coal samples

After taking the Eq. (8), (9), (10) into the Eq. (6), the Eq. (11) that can describe the relationship between Q_{pt} and *P* at random time *t* was obtained:

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$$
Q_{pt} = \frac{At^B P^{Et^F}}{1 + Ct^D P^{Et^F}}
$$
 (11)

where $A = c_a \cdot c_b$, $B = d_a + d_b$, $C = c_b$, $D = d_b$, $E = c_v$, $E = d_v$

Eq. (11) is called as Langmuir-like desorption model and the desorption curve it presents is as follow: the desorption volume increases with pressure, the slope of the curve at the low pressure is larger, and the slope of the curve decreases gradually with pressure. This is because the desorption volume is proportion to the surface coverage fraction of methane. The coverage rate of methane on coal gradually decreases with the increasing pressure because of the gradually saturated adsorption coal surface. Under a certain pressure, the desorption pressure at the initial period is large, then as time goes on, the desorption rate gradually decreases.

Through Eq.(11), we can predict the desorption rate at any given pressure and time for coal samples obtained from the working face by doing several desorption kinetics experiments for corresponding given pressure *P* to confirm values of parameters in Langmuir-like model, which plays an important role in lost gas estimation and the prediction of mine outburst.

4 Conclusions

Pressure has a significant influence on the desorption kinetics of gases in coal. At a constant temperature, the desorption volume increases with the pressure regardless of the coal rank and gas type. And at a given desorption time, the desorption volume appears to have a Langmuir-like relationship with pressure. Also, the relationship between a_t , b_t , v_t in the Langmuir-like model and the desorption time t are in the form of power function. Thus, a Langmuir-like desorption model expressed in the form of 1 *F F B Et* $Q_{pt} = \frac{At^{B}P^{Et^{c}}}{1+Ct^{D}P^{Et^{c}}}$ $Ct^{\prime\prime}P^{\prime}$ = + was

established, which plays an important role in lost gas estimation and the prediction of mine outburst.

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