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1 **Combustion Characterization and Modeling of Novel Nanoenergetic Composites of**  
2 **Co<sub>3</sub>O<sub>4</sub>/nAl**

3 Vinay Kumar Patel<sup>1</sup>, Jayant Raj Saurav<sup>1</sup>, Keshab Gangopadhyay<sup>2</sup>, Shubhra Gangopadhyay<sup>2</sup>,  
4 Shantanu Bhattacharya<sup>\*,1</sup>

5 <sup>1</sup>Microsystems Fabrication Laboratory, <sup>1</sup>Department of Mechanical Engineering,

6 <sup>1</sup>Indian Institute of Technology Kanpur, Kanpur 208016, Uttar Pradesh, India

7 <sup>2</sup>Department of Electrical and Computer Engineering, University of Missouri Columbia, MO  
8 USA

9  
10 \*Corresponding author: [bhattacs@iitk.ac.in](mailto:bhattacs@iitk.ac.in)

11 Tel- +915122596056; fax- +915122597408  
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24 Nanoenergetic materials have been widely explored for obtaining rapid release of energy, burn-  
25 speeds and high pressurization rates. In this study, we have synthesized  $\text{Co}_3\text{O}_4$  nanobelts *via* a  
26 simple solid-state process and further integrated as-prepared  $\text{Co}_3\text{O}_4$  and calcined  $\text{Co}_3\text{O}_4$  (at 400  
27 °C for 4 hr) ( $\text{Co}_3\text{O}_4$ -400) with nano-aluminum (nAl) to realize novel bulk nanoenergetic systems  
28 of  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4$ -400/nAl respectively. The heat of reaction and combustion  
29 performance of these nanoenergetic systems are studied by thermogravimetric and differential  
30 scanning calorimetry (TG-DSC), combustion front-wave speed and pressure-time characteristics  
31 measurements. The heat of reaction has been measured to be  $0.96 \text{ kJ g}^{-1}$  for  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $1.02$   
32  $\text{kJ g}^{-1}$  for  $\text{Co}_3\text{O}_4$ -400/nAl nanoenergetic systems. The  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetic system is able to  
33 develop mild peak pressure ( $12.6 \pm 1$  to  $20 \pm 2$  MPa) and pressurization rate ( $0.08 \pm 0.05$  to  
34  $0.14 \pm 0.05$  MPa/ $\mu\text{s}$ ) having a characteristics of low gas generation, which can be harnessed in low  
35 intensity pressure-pulse based microporation of soft matters like bacterial cells without any lysis.  
36 The calcined  $\text{Co}_3\text{O}_4$  oxidizer is capable to develop more reactive nanoenergetic system than  
37  $\text{Co}_3\text{O}_4/\text{nAl}$ , reflecting the generation of moderate peak pressure ( $26 \pm 2$  to  $32.6 \pm 3$  MPa) and  
38 pressurization rate ( $0.29 \pm 0.1$  to  $0.47 \pm 0.1$  MPa/ $\mu\text{s}$ ). The propagating flames of ( $\text{Co}_3\text{O}_4/\text{Co}_3\text{O}_4$ -  
39 400)/nAl are observed accelerating during instrumented burn tube combustion experiment with  
40 front combustion front-wave speed ranging from  $480 \pm 25$  to  $830 \pm 75$  m/s. Through this paper, the  
41  $\text{Co}_3\text{O}_4$  nanoenergetic oxidizers can be utilized in the generation of low to moderate pressure  
42 pulses to transport biological materials to soft matters.

43 **KEYWORDS:** cobalt oxide, Al/ $\text{Co}_3\text{O}_4$ , nanothermites, nanoenergetic materials, combustion,  
44 metastable intermolecular composites

45

## 46 I. INTRODUCTION

47 Nanoenergetic materials, a new class of metastable intermolecular composites, comprising  
48 nanoscale fuel (aluminum) and oxidizer (CuO, Fe<sub>2</sub>O<sub>3</sub>, Bi<sub>2</sub>O<sub>3</sub>, MoO<sub>3</sub> *etc.*) produce rapid release of  
49 heat and pressure upon thermite reaction.<sup>1</sup> There are a wide range of possible combinations of  
50 metals and oxidizers for energetic material formulations.<sup>2</sup> Aluminum nanopowder is most widely  
51 used as fuel in these materials due to its low cost, easy availability and favorable physical  
52 properties such as high oxide reducing potential, low vapor pressure, low melting temperature  
53 and high thermal conductivity.<sup>3</sup> The nanoscale structuring of oxidizer materials increases their  
54 surface area to a wider exposure and reduces the diffusion distances from the close packed fuel  
55 particles, thus reducing the atomic length scales of heat and mass transfer between the reactants.  
56 This leads to enhancement in both ignition sensitivity and reaction/propagation rate at minimum  
57 heat losses.<sup>4</sup> The high speed combustion generating high pressure/shock front-waves found  
58 useful applications in microthrusters<sup>5</sup>, safe arm and fire devices,<sup>6</sup> drug/gene delivery micro-  
59 devices<sup>7</sup> *etc.* Also, it has been widely observed that the energy density and combustion kinetics  
60 of nanoenergetic materials are significantly affected by changing the combination of fuel and  
61 oxidizer, their nanostructuring and following various preparation/assembling strategies.<sup>8</sup> The  
62 most effective nanoenergetic materials can be generated by selection of right fuel-oxidizer  
63 combination and their nanostructuring (*viz.*, the shape and size distribution) and assembling at  
64 right stoichiometry.

65 Cobalt oxide (Co<sub>3</sub>O<sub>4</sub>, p-type semiconductor) has attracted the research community for its wide  
66 range of applications in many areas such as electrode materials in rechargeable Li-ion batteries,<sup>9-</sup>  
67 <sup>10</sup> gas sensors<sup>11</sup>, catalyst,<sup>12</sup> energy storage,<sup>13</sup> solar energy absorber,<sup>14</sup> magnetic materials,<sup>15</sup> and  
68 electronic devices.<sup>16</sup> Owing to its unique physicochemical properties of one dimensional

69 nanostructures, the various methods such as micro-emulsion-based methods,<sup>17</sup> hydrothermal  
70 methods,<sup>18</sup> solvo-thermal methods,<sup>19</sup> co-precipitation/digestion methods,<sup>20</sup> heating cobalt foils in  
71 air,<sup>21</sup> sol-gel method<sup>22</sup> *etc.* were developed for the synthesis of  $\text{Co}_3\text{O}_4$  nanorods,<sup>17-19</sup> nanowires<sup>21</sup>  
72 and nanofibers.<sup>22</sup> In this work we have developed  $\text{Co}_3\text{O}_4$  nanobelts by a simple solid-state  
73 method *via* modification of a mechano-chemical method.<sup>23</sup>

74 In recent years, a rapid growth in design and development of nanoenergetic systems has been  
75 observed with scientific and technological advancements in various shape and size metal oxide  
76 nanomaterials. Among the various metal oxides,  $\text{CuO}$ ,  $\text{Bi}_2\text{O}_3$ ,  $\text{MoO}_3$ ,  $\text{Fe}_2\text{O}_3$  and  $\text{WO}_3$  are widely  
77 explored as nanoenergetic oxidizers. The various synthesis methodologies and processing of  
78  $\text{CuO}$  nanomaterials have developed nanoenergetic composites with moderate to excellent  
79 combustion reactivity (combustion front-wave speed and pressurization rate).<sup>24-26</sup> S.  
80 Gangopadhyay and groups<sup>24</sup> demonstrated that the  $\text{CuO}/\text{Al}$  nanocomposites were capable to  
81 deliver wide-range combustion performance (combustion front-wave speed:  $1500 \pm 50$  to  $2400 \pm$   
82  $100$  m/s; peak pressure:  $22 \pm 3$  to  $70 \pm 10$  MPa; pressurization rate:  $2.5 \pm 0.3$  to  $5.7 \pm 0.7$  MPa/ $\mu\text{s}$ ) by  
83 adopting various processing methodologies such as vacuum drying and calcination of  $\text{CuO}$   
84 nanorods at different temperature and time as well as with/without self-assembling the  $\text{CuO}$   
85 nanorods with aluminum nanoparticles. M. R. Zachariah and groups<sup>25</sup> developed hollow  $\text{CuO}$   
86 sphere of thin shell thickness using aerosol spray pyrolysis method, which exhibited excellent  
87 gas generating and rapid oxygen releasing capabilities, resulting in a high pressurization rate of  
88  $0.745$  MPa/ $\mu\text{s}$  with nanoaluminum combustion. In a similar effort, S. Bhattacharya and groups<sup>26</sup>  
89 fabricated super-reactive  $\text{CuO}$  nanorods by simple biogenic solid-state and sonoemulsion routes  
90 utilizing Aloe-vera as green surfactant, which manifested a high combustion performance  
91 (average combustion front-wave speed:  $620 \pm 50$  to  $1780 \pm 75$  m/s; maximum peak pressure:  $65.4$

92 MPa; maximum pressurization rate: 1.09 MPa/ $\mu$ s) with nanoaluminum combustion. K. S.  
93 Martirosyan and groups<sup>27</sup> evaluated the maximum pressure rise of eight nanoenergetic  
94 formulations (each of 0.5 g quantity) using commercial grade metal oxides and nanoaluminum in  
95 a constant volume (0.342 L) combustion chamber and demonstrated the increasing order of  
96 maximum pressure rise ( $\text{Fe}_2\text{O}_3/\text{Al} < \text{Fe}_3\text{O}_4/\text{Al} < \text{MoO}_2/\text{Al} < \text{WO}_3/\text{Al} < \text{MnO}_2/\text{Al} < \text{MoO}_3/\text{Al} <$   
97  $\text{CuO}/\text{Al} < \text{Bi}_2\text{O}_3/\text{Al}$ ) with observation of highest pressure peak of 2.9 MPa with  $\text{Bi}_2\text{O}_3/\text{Al}$ .  
98 However, when Martirosyan and groups<sup>28</sup> experimented the combustion of nanoenergetic  
99 formulation (0.5 g mixture) containing nanoaluminum and combustion synthesized high quality  
100 nanocrystalline  $\text{Bi}_2\text{O}_3$  oxidizer (size: 40-50 nm, wt%: 80%), a very high combustion performance  
101 (peak pressure:  $\sim 12$  MPa; front combustion velocity:  $\sim 2500$  m/s; pressurization rate: 650 GPa/s)  
102 than that of commercial grade  $\text{Bi}_2\text{O}_3$ -based nanoenergetics were achieved. Martirosyan and  
103 groups<sup>29</sup> also developed another high reactive nanoenergetic system of  $\text{Al}/\text{I}_2\text{O}_5$ , which  
104 propagated with a velocity of  $\sim 2000$  m/s and created a maximum peak pressure of  $\sim 11$  MPa and  
105 pressurization rate of  $\sim 2750$  GPa/s comparable to (combustion synthesized  $\text{Bi}_2\text{O}_3$ )/ $\text{Al}$ <sup>28</sup>  
106 nanoenergetic system. M. Pantoya and groups<sup>30</sup> ignited the composites  $\text{I}_2\text{O}_5/\text{Al}$  and  $\text{Ag}_2\text{O}/\text{Al}$  by  
107 impact and demonstrated higher average flame propagation rate of  $1305 \pm 28$  m/s with  $\text{I}_2\text{O}_5/\text{Al}$   
108 than that of  $\text{Ag}_2\text{O}$  (flame rate of  $531 \pm 32$  m/s). In another investigation of pressurization rate of  
109 various metal oxide ( $\text{CuO}/\text{SnO}_2/\text{Fe}_2\text{O}_3/\text{WO}_3$ )/nanoaluminum composites (fixed mass of 25 mg)  
110 in a combustion cell (free volume: 13 cc) by M R Zachariah and groups,<sup>31</sup>  $\text{CuO}$  and next  $\text{SnO}_2$   
111 were observed creating rapid pressurization rate owing to their high rate of decomposition and  
112 release of gaseous oxidizers resulting in pressurization rate in such a descending order of  $\text{CuO}/\text{Al}$   
113 ( $11.1$  Psi/ $\mu$ s),  $\text{SnO}_2/\text{Al}$  ( $7.7$  Psi/ $\mu$ s),  $\text{Fe}_2\text{O}_3/\text{Al}$  ( $0.017$  Psi/ $\mu$ s) and  $\text{WO}_3$  ( $0.028$  Psi/ $\mu$ s). In an  
114 experimental study of the effect of stoichiometry on the combustion behavior of nanoscale

115 MoO<sub>3</sub>/nAl thermite, Dutro *et al.*<sup>32</sup> characterized the propagation velocity and pressure output in a  
116 burn tube experiment and reported a steady propagation velocity (~100 to ~1000 m/s) for  
117 ~nanoaluminum proportions from 10 to 65 wt% and peak pressures over 8 MPa near  
118 stoichiometric compositions.

119 Cobalt oxide has not been explored as bulk nanoenergetic composites except a recent  
120 development in thin-film based nanoenergetic materials onto a silicon substrate.<sup>33</sup> This report<sup>33</sup>  
121 talks in details about the formulation of a core-shell structure of Co<sub>3</sub>O<sub>4</sub> nanorod coated with  
122 aluminum film. Although films deposited in this manner may have a benefit of micro-patterning  
123 and may thus possess good integrability with MEMS/nEMS devices still it is always easy to tune  
124 the combustion behavior of the bulk nanoenergetic materials. Further bulk materials can be  
125 packed in micro-tubes or capillaries to generate high pressurization rate and also shock waves.  
126 Their packaging ratio can be easily changed and various oxidizers and tune morphology of the  
127 oxidizers can be used in customized applications. In this study, we have synthesized nanoscale  
128 Co<sub>3</sub>O<sub>4</sub> oxidizer and developed a novel nanoscale energetic composites system with nano-  
129 aluminum. We have mathematically estimated the pressure-time characteristics for combustion  
130 of our nanoenergetic systems in a pressure-cell chamber based on established gas dynamics  
131 model<sup>34</sup>, Chapman–Jouguet (CJ) theory.<sup>35</sup> The exploration of this system has been carried out as  
132 a basis to create lower pressures and a higher pressurization rate which is very suitable for the  
133 application of delivering particles/genes into soft extra-cellular structures of micro-organisms.  
134 We have investigated the combustion front-wave speed and peak pressure/ pressurization rates  
135 by igniting these composites.

## 136 II. Experimental Section

### 137 **A. Synthesis of Co<sub>3</sub>O<sub>4</sub> nanobelts**

138 All chemical reagents used in the synthesis process were of analytical grades and applied  
139 without processing. Co<sub>3</sub>O<sub>4</sub> nanobelts were synthesized by simple solid-state chemical mixing of  
140 CoCl<sub>2</sub>.6H<sub>2</sub>O (Source: RFCL Ltd, India, Purity: 98%) and sodium bicarbonate (Source: Fisher  
141 Scientific, India, Purity: 99%) in presence of water and hexamethylenetetramine (HMTA)  
142 (Source: Merck Specialties Pvt Ltd, India, Purity: 99.99 %). In a typical synthesis process, 2.38 g  
143 CoCl<sub>2</sub>.6H<sub>2</sub>O and 2.1 g NaHCO<sub>3</sub> were mixed and ground together in presence of 0.280 g HMTA  
144 for few minutes in a mortar and pestle. After getting a homogeneous mixture, 2 ml of de-ionized  
145 water was added and mixing was carried on up to 20-30 minutes till a pink homogeneous paste  
146 was obtained. The pink paste was extracted from the mortar as well as the pestle and washed  
147 several times with water and ethanol in order to get pure cobalt oxide precursor. This precursor  
148 was observed to be an intermediate step and after heating the paste in an oven for 180 °C for 4 hr,  
149 black-colored pure Co<sub>3</sub>O<sub>4</sub> was obtained.

### 150 **B. Preparation of nanoscale energetic composites**

151 Nanoenergetic composite of 0.225 g quantity was prepared by homogeneous dispersion of  
152 accurately weighed Co<sub>3</sub>O<sub>4</sub> oxidizer nanobelts with aluminum nanoparticles in 30 ml of 2-  
153 propanol solution using a sonic wand. These materials were further mixed at different  
154 equivalence ratios<sup>36</sup> which was calculated after considering the actual active aluminum content in  
155 the aluminum nanoparticles by subtracting the aluminum oxide layer. The aluminum  
156 nanoparticles utilized in nanoenergetic composites were of spherical shape with average  
157 diameter of 80 nm (Source: Neo Ecosystems and Software Private Ltd. India, Purity: 99%). The  
158 sonication process promoted a better homogenized mixing of fuel and oxidizer nanostructures  
159 and also helped in breaking up agglomerates if any were formulated by coupling sonic waves to



160 the particulate system. After sonication for about 3-5 minutes, the well homogenized slurry  
161 obtained was poured out in a glass petri-dish and dried at 90° C to evaporate out the 2-propanol  
162 dispersant media completely. The dried nanoenergetic composites were carefully retrieved by  
163 scrapping off very carefully with a pre-cleaned end of spatula and vacuum stored. The retrieval  
164 process of the composite is a skillful step as too much pressure of scrapping off may ignite the  
165 material and thus standard precautions at this step are advised.

### 166 C. Nanomaterials Characterization

167 The crystal structure and composition of Co<sub>3</sub>O<sub>4</sub> nanobelts was determined by powder X-ray  
168 diffraction (XRD) analysis using PANalytical X'Pert Pro diffractometer in the 2θ range of 30–  
169 80° at scan rate of 0.02 s<sup>-1</sup> with Cu Kα radiation of wavelength 1.5418 Å. The surface  
170 morphology of Co<sub>3</sub>O<sub>4</sub> nanobelts was characterized by transmission electron microscopy (TEM)  
171 at accelerating voltage of 200 kV using FEI Technai, 20 UT. The surface morphology of  
172 aluminum nanoparticles and its nanoenergetic composites with Co<sub>3</sub>O<sub>4</sub> nanobelts were  
173 characterized by scanning electron microscopy (Supra 40 VP, Zeiss Germany).

174 Combustion Characterization of nanoenergetic composites were conducted *via* TGDSC  
175 measurements, combustion front-wave speed measurements and pressure–time characteristics  
176 measurements at different equivalence ratio. The equivalence ratio was evaluated by considering  
177 the actual active aluminum content of Al(core)/Al<sub>2</sub>O<sub>3</sub>(shell) nanoparticles. The equivalence ratio  
178 (φ) was calculated by the Eqn. (1), in which *m* refers to the mass of fuel/oxidizer, and the  
179 subscripts *act* and *st* imply actual ratio and stoichiometry ratio respectively.

$$\varphi = \frac{(m_{Al}/m_{Co_3O_4})_{act}}{(m_{Al}/m_{Co_3O_4})_{st}} \quad (1)$$

180

181 The thermogravimetric mass changes and the heat of reaction of  $\text{Co}_3\text{O}_4$  based nanoenergetic  
182 composites were experimentally measured by thermogravimetric and differential scanning  
183 calorimetric (TG-DSC) analysis conducted on Netzsch STA 449F3 instrument. The TG-DSC  
184 analysis was conducted from 50 to 800 °C at a heating rate of 10 K  $\text{min}^{-1}$  under nitrogen gas  
185 supply (99.999 % purity).

186 The combustion front-wave speed was measured by initiating the combustion of 0.225 g of  
187 nanoenergetic composites filled in a constant volume polycarbonate burn tube of inside diameter  
188 of 3.18 mm and volume of 0.8  $\text{cm}^3$ . The nanoenergetic combustion was initiated from either side  
189 of the burn tube by Nichrome wire connected to a 9V DC power source. The combustion front-  
190 wave propagation was optically detected by four fiber optics (Thor Labs) coupled photo-  
191 detectors (Thor Labs, DET 10A/M) placed in-line at inter-fiber distance of 25 mm over the burn  
192 tube. The combustion front-wave speed was measured by the estimation of inter-fiber response  
193 time recorded in Tektronix oscilloscope DPO 3054 after the successive flame propagation  
194 distance of 25 mm from the previous optical fiber position.

195 The pressure and pressurization rate of nanoenergetic composites was measured by conducting  
196 the combustion experiment of 30 mg of  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetic composites in a constant  
197 volume pressure cell (diameter=6.25 mm, depth= 5 mm). The nanoenergetic composites were  
198 loosely filled in the pressure cell with a packing density of 0.2  $\text{g cm}^{-3}$ . A piezoelectric based  
199 pressure sensor PCB119B12 (PCB Piezotronics) was rigidly fixed to the pressure cell to measure  
200 the pressure-time characteristics of nanoenergetic combustion. The pressure-time characteristics  
201 output was recorded by Tektronix digital oscilloscope DPO3054. The details of  
202 pressure/pressurization rate and combustion front-wave speed measurements can be found in our

203 previous publication<sup>26</sup> and these measuring set ups are shown in supplementary Fig. S1 and S2  
204 respectively.

### 205 **III. Results and Discussion**

206 **A. Morphology and crystallography.** The phase of the as-prepared and calcined nanomaterials  
207 was identified by X-ray diffraction (XRD). The X-ray diffractogram of as-prepared and calcined  
208  $\text{Co}_3\text{O}_4$  ( $\text{Co}_3\text{O}_4$ -400) nanomaterials is shown in Fig. 1. All XRD peaks were compared to the  
209 standard powder XRD data files maintained by Joint Committee on Powder Diffraction  
210 Standards (JCPDS) and were found to consistent with the card number JCPDS 9-418 of spinel  
211  $\text{Co}_3\text{O}_4$  cubic structure. No characteristics peak relates to the CoO which demonstrates the  
212 formation of pure phase  $\text{Co}_3\text{O}_4$ . The XRD peaks of  $\text{Co}_3\text{O}_4$ -400 nanomaterials were found sharper  
213 and of higher intensity than that of  $\text{Co}_3\text{O}_4$ , which demonstrates the higher crystallinity of  
214 calcined  $\text{Co}_3\text{O}_4$  nanomaterials. The morphology and crystallography of as-synthesized  $\text{Co}_3\text{O}_4$   
215 were determined by TEM and selected area electron diffraction (SAED) analysis. Fig. 2 (a) and  
216 (b) represent the TEM image of  $\text{Co}_3\text{O}_4$  samples and related SAED pattern respectively. The  
217 TEM image indicates the formation of nanobelts like structures of  $\text{Co}_3\text{O}_4$ . From the TEM image,  
218 the formation of very small nanoparticles of diameters of  $\sim 3$ -5 nm was also observed. It is  
219 evident from the SAED ring pattern that the  $\text{Co}_3\text{O}_4$  sample is polycrystalline in nature. The X-ray  
220 diffractogram of  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetics clearly indicates the peak of aluminum nanopowder.  
221 Fig. 2 (c) shows the FESEM image of aluminum nanoparticles of average diameter of 80 nm  
222 with the inset high magnification TEM image of nanoaluminum demonstrating the  $\text{Al}_2\text{O}_3$  shell  
223 thickness of  $\sim 4$  nm.

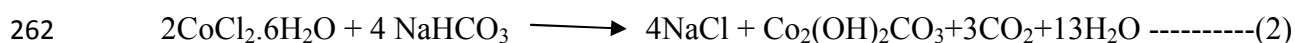
### 224 **B. Fourier Transform Infrared (FTIR) Analysis**

225 The FT-IR Spectrum of  $\text{Co}_3\text{O}_4$  and  $\text{Co}_3\text{O}_4$ -400 nanocrystals are represented in Fig. 3. The  
226 absorption peaks at wave number 3377 and 1624  $\text{cm}^{-1}$  of  $\text{Co}_3\text{O}_4$  and 3435  $\text{cm}^{-1}$  and 1632  $\text{cm}^{-1}$  of  
227  $\text{Co}_3\text{O}_4$ -400 could be attributed to the (OH) stretching and bending mode respectively due to  
228 possible consequence of water adsorptions from the environment and during handling which  
229 causes the surface of the  $\text{Co}_3\text{O}_4$  samples to be hydroxilated. The absorption peak at 1384  $\text{cm}^{-1}$  is  
230 observed only with  $\text{Co}_3\text{O}_4$  which may be related to the surface impurity of  
231 poly(oxymethylene)glycols, remained even washing several times the  $\text{Co}_3\text{O}_4$  precipitates with  
232 deionized water. HMTA is decomposed in to ammonia and formaldehyde and ammonia supplies  
233 hydroxyl ion slowly after further hydrolyzation with water.<sup>37</sup> The formaldehyde is soluble in the  
234 water as it forms a oligomers of poly(oxymethylene)glycols ( $\text{HO}(\text{CH}_2\text{O})_n\text{H}$ ) with water  
235 solution.<sup>38</sup> The contents of formaldehyde which become soluble in water in the form of  
236 poly(oxymethylene)glycols is expected to be removed but the content of  
237 poly(oxymethylene)glycols which form strong surface bonding with the  $\text{Co}_3\text{O}_4$  nanocrystals  
238 remains as an impurity even several times water cleaning. The strong absorption peaks observed  
239 at 563 and 660  $\text{cm}^{-1}$  of  $\text{Co}_3\text{O}_4$  and 566 and 660  $\text{cm}^{-1}$  of  $\text{Co}_3\text{O}_4$ -400 correspond to the stretching  
240 vibrations of metal oxide for tetrahedrally coordinated  $\text{Co}^{+2}$  metal ions and octahedrally  
241 coordinated  $\text{Co}^{+3}$  metal ions.<sup>39</sup>

### 242 C. Possible Formation Mechanism

243 The solid-state synthesis process in presence of HMTA is able to form nanobelts cum  
244 nanoparticles morphology of  $\text{Co}_3\text{O}_4$  than only nanoparticles<sup>23</sup> morphology in the absence of  
245 HMTA which demonstrates the significant role of HMTA for its anisotropic nanobelts  
246 structuring of  $\text{Co}_3\text{O}_4$  in solid phase reaction process. FTIR measurement confirms the presence  
247 of HMTA with  $\text{Co}_3\text{O}_4$  nanocrystals. From the Reaction (2), the nucleation and growth of cobalt

248 hydroxyl carbonate ( $\text{Co}_2(\text{OH})_2\text{CO}_3$ ) can be interpreted. The gradual release of hydroxyl ions by  
249 HMTA during solid state mixing process may be envisioned to transit the occurrence of reaction  
250 process in comparatively higher basic media which furnishes the stable anisotropic growth of  
251 cobalt hydroxyl carbonate nanocrystals. HMTA has been demonstrated to have greater affinity  
252 with a particular facet of  $\text{Co}^{+2}$  nuclei, hence selectively absorbs to this facet depending on the  
253 ratio of  $\text{Co}^{+2}$  and HMTA.<sup>40</sup> In a similar way, the HMTA is proposed to absorb selectively on to  
254 the particular facet of cobalt hydroxyl carbonate and minimizes the energy of this facet. Thus the  
255 high energy facets of cobalt hydroxyl carbonate experience higher driving force of crystal  
256 growth resulting in anisotropic formulation of nanobelt-like structure of cobalt hydroxyl  
257 carbonate. Owing to less homogeneity of solid state mixing than solution phase reactions, some  
258 cobalt hydroxyl carbonate nanocrystals may not experience favorable condition for nanobelts  
259 formulations and thus remains in the form of nanoparticles. The cobalt hydroxyl carbonate  
260 nanocrystals are transformed in to  $\text{Co}_3\text{O}_4$  nanobelts cum nanoparticles when heated at  $180^\circ\text{C}$  in  
261 oven according to the Reaction (3).



#### 264 **D. Thermogravimetric and Differential Scanning Calorimetry (TG/DSC) Measurement**

265 TG/DSC measurements were conducted for  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-}400/\text{nAl}$  nanoenergetic  
266 composites at equivalence ratio of 1.6. From thermogravimetric analysis of nanoenergetics as  
267 shown in Fig. 4, the weight-loss up to  $400^\circ\text{C}$  was found to be greater with  $\text{Co}_3\text{O}_4/\text{nAl}$  (4%) than  
268 the  $\text{Co}_3\text{O}_4\text{-}400/\text{Al}$  (1.56 %). The excess weight-loss of 2.44% can be assigned to the surface  
269 impurity of oligomers of poly(oxyethylene)-glycols ( $\text{HO}(\text{CH}_2\text{O})_n\text{H}$ ) adhered tightly with

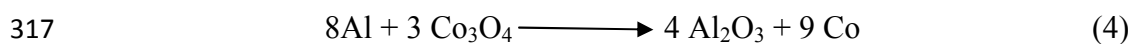
270  $\text{Co}_3\text{O}_4$  nanobelts. In DSC studies, The exothermic peaks were observed at 606 °C (onset  
271 temperature of 536 °C, heat of reaction of 960  $\text{J g}^{-1}$ ) for  $\text{Co}_3\text{O}_4/\text{nAl}$  and at 601 °C (onset  
272 temperature of 534 °C, heat of reaction of 1020  $\text{J g}^{-1}$ ) for  $\text{Co}_3\text{O}_4\text{-400/Al}$ . The higher heat of  
273 reaction associated with  $\text{Co}_3\text{O}_4\text{-400/nAl}$  may be attributed to its higher pure-phase  $\text{Co}_3\text{O}_4\text{-400}$   
274 oxidizer than  $\text{Co}_3\text{O}_4$ . It may be believed that the higher purity of oxidizer enhances the inter-  
275 atomic diffusion reaction with aluminum by releasing oxygen at relatively faster rate. A minor  
276 exothermic peak having heat of reaction of 95  $\text{J g}^{-1}$  was observed at 424 °C for  $\text{Co}_3\text{O}_4\text{-400/Al}$   
277 which may be attributed to low temperature redox reactions or interfacial Al–Co–O  
278 recrystallization. The exothermic heat of reaction of of  $\text{Co}_3\text{O}_4$  based nanoenergetics was  
279 observed greater than that of PEG400 synthesized CuO nanorods based nanoenergetics (heat of  
280 reaction of 850  $\text{J g}^{-1}$ ) as reported in our earlier publication.<sup>26</sup> The heat of reaction (1.02 kJ/g) of  
281 our bulk nanoenergetic system was found ~3.56 times lower than the total heat of reaction of  
282 core( $\text{Co}_3\text{O}_4$ )/shell(Al)<sup>33</sup> nanoenergetic materials prepared on silicon substrate. Core-shell  
283 nanostructuring of fuel and oxidizer can be envisaged to enhance the nanoscale intimacy,  
284 interfacial contact area as well as purity. Thus, core-shell nanoenergetic can be envisioned to  
285 possess higher reactivity due to decreased inter-atomic diffusion path and increased population  
286 of fuel and oxidizer atoms per unit surface-area at any instance during exothermic reaction,  
287 which can be attributed to higher heat of reaction of core-shell ( $\text{Co}_3\text{O}_4/\text{Al}$ ) nanoenergetic  
288 materials as compared to ultrasonically mixed bulk nanoenergetics. Further, the core-shell  
289 ( $\text{Co}_3\text{O}_4/\text{Al}$ ) thermites, owing to oxidation of aluminum in Ar- $\text{O}_2$  plasma, were examined to  
290 possess higher heat of reaction than core( $\text{CuO}$ )/Al(shell)<sup>41</sup> thermites. Thus in a nutshell, the  
291 higher reactivity and aluminum oxidation in Ar- $\text{O}_2$  plasma of core/shell ( $\text{Co}_3\text{O}_4/\text{Al}$ ) thermite can  
292 be attributed for its higher heat of reaction than our bulk nanoenergetic system.

### 293 E. Theoretical Estimation of Pressure Time Characteristics

294 The pressure-time characteristics of low gas generating  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetic composites  
295 (mass: 0.03 g) were theoretically estimated and validated by following the gas dynamic model<sup>34</sup>  
296 which has been proposed for high reactive mass (0.5 g) combustion of high gas generating  
297  $\text{Al}/\text{Bi}_2\text{O}_3$  in a large volume cylindrical chamber. Even though the gas generation with  $\text{Co}_3\text{O}_4/\text{nAl}$   
298 nanoenergetic composites is much smaller than the  $\text{Bi}_2\text{O}_3/\text{Al}$ ,<sup>27-28, 42</sup> the pressurization rate in our  
299 pressure cell (diameter=6.25 mm, depth= 5 mm, Supplementary Fig. S1) can be assumed to be  
300 developed at high level and so considered to be consistent to gas dynamic model because of low  
301 volume of  $0.1534 \text{ cm}^3$  of our pressure-cell as compared to  $85.13 \text{ cm}^3$  applied in gas dynamic  
302 model.<sup>34</sup> In the model, the energy of solid fuels-oxidizers thermite reaction is released instantly  
303 and transferred to the gaseous products. The big explosion based gas dynamic model<sup>34</sup> assumes  
304 the generation and propagation of one-dimensional shock wave in the air-filled cylindrical  
305 pressure-cell. The heat transfer is considered to be adiabatic and the pressure of the shock wave  
306 is assumed to be much greater than the ambient pressure. In big explosion model,<sup>34</sup> the explosion  
307 happens very quickly releasing all the explosion energy into the gas instantly before the shock-  
308 wave leaves the narrow expansion region and a strong discontinuity condition arises because of  
309 the higher pressure magnitude behind the shock wave than the gaseous medium pressure where it  
310 is expanding. The Chapman–Jouguet (CJ) theory also assumes the reaction in the shock to be  
311 completed instantaneously at the continuum level<sup>35</sup> and based on this CJ theory equation of state  
312 for  $\text{CuO}/\text{Al}$  nanothermites have been developed earlier.<sup>43</sup>

313 The gas dynamic model<sup>34</sup> utilizes the conservation of momentum, entropy and mass to arrive the  
314 pressure equation. For theoretical modeling of thermite reaction, we considered the mass of

315 nanoenergetics to be 30 mg. Following reaction was used to calculate the amount of the Al that  
316 would undergo combustion for the given amount of oxidizer.



318 It was kept in mind that about 20% of nano-aluminum is in the form of  $\text{Al}_2\text{O}_3$  initially which  
319 was calculated for aluminum nanoparticles of average particle size of 80 nm possessing outer  
320 shell thickness of  $\text{Al}_2\text{O}_3$  of  $\sim 4$  nm determined from high magnification TEM image as shown by  
321 inset of Fig. 2 (c). Hence, the actual amount of nanoenergetics after the exclusion of non-reactive  
322  $\text{Al}_2\text{O}_3$  was calculated for equivalent ratio of 1.6 which is summarized in supplementary Table S1.  
323 It is assumed that the outer shell of Al *i.e.*  $\text{Al}_2\text{O}_3$  acts as heat sink thus the various level of its  
324 contents in different equivalent ratio of nanoenergetics modify the combustion pressure.

325 The experimental module that is developed for the testing of the nanoenergetic composite  
326 materials is a constant volume pressure cell fully packaged with the composite materials. The  
327 pressure sensor used to measure the pressurization rate and peak pressure in our experiments  
328 have been positioned at the end of the pressure-cell and is supposed to measure the total force  
329 acting on it per unit area which is a function of both the incoming pressure and the drag force  
330 and its value depends heavily on the orientation of the detector.<sup>25</sup> The pressure sensor normally  
331 does not feel any drag force *i.e.*, drag coefficient ( $\gamma$ ) =0, if it is placed along the combustion  
332 propagation direction in the chamber. If it is assembled perpendicular to the drag force, the  
333 effect of drag is maximum and the drag coefficient is assumed to be 2 in that situation. In our  
334 experiments the pressure sensor is placed perpendicular to the direction of propagation of the  
335 pressure wave although due to relatively very less pressure-cell volume and fast pressurization  
336 rate, the drag to combustion propagation is insignificant and we assume the value of ( $\gamma$ ) =0 for



337 all our calculations. A theoretical big explosion gas dynamic model was utilized based on the the  
 338 following equations<sup>25</sup> of combustion pressure.

$$339 \quad P + \frac{1}{2} \gamma \rho v^2 = \left( \frac{4L^2 \rho_1}{9t^2} \right) \left( \frac{1}{\gamma} DZ + \frac{1}{2} \gamma DV^2 \right) \quad (5)$$

340 Where,  $\mathcal{V} \equiv \mathcal{V}(\xi[t])$ ,  $\xi[t] = \left( \frac{\rho_1 L^3 A}{Et^2 \beta^3} \right)^{\frac{1}{3}}$ , Here  $P$ ,  $\rho$  and  $v$  are the gas pressure, gas density and gas  
 341 velocity respectively.  $L$  and  $A$  is the length and cross-section area of the cylindrical pressure-cell  
 342 chamber. The symbol  $\rho_1$  refers to the gas density in front of propagating shock wave whereas  $\beta$   
 343 and  $\xi$  to a dimensionless constant and dimensionless variable. Eqn. (6) is used to calculate the  
 344 magnitude of  $\xi$ .  $E$  is the energy released during the exothermic reaction.  $\mathcal{V}(\xi)$  represents a  
 345 function inverse to the function  $\xi(\mathcal{V})$ . Due to the complexity of the equation below, an indirect  
 346 approach was used to solve it. The limits of  $\mathcal{V}$  vary from  $1/\gamma$  to  $2/\gamma+1$  (from  $\xi=0$  to  $\xi=1$ ) and the  
 347 iterations are performed in MATLAB.  $D$  and  $Z$  are the dimensionless function and can be  
 348 estimated by the Eqn. (7) and (8) respectively.

$$\xi^3 = \frac{4 \left( \frac{\gamma+1}{\gamma-1} (\gamma \mathcal{V} - 1) \right)^{\frac{3(\gamma-1)}{2\gamma-1}} (3 - (1+\gamma)\mathcal{V})^{\frac{5\gamma-4}{2\gamma-1}}}{(1+\gamma)^2 \mathcal{V}^2} \quad (6)$$

$$349 \quad D = \frac{\gamma+1}{\gamma-1} \left( \frac{\gamma+1}{\gamma-1} (1 - \mathcal{V}) \right)^{\frac{-2}{2-\gamma}} \left( \frac{\gamma+1}{\gamma-1} (\gamma \mathcal{V} - 1) \right)^{\frac{1}{2\gamma-1} \times} (3 - (1+\gamma)\mathcal{V})^{\frac{-(5\gamma-4)}{(\gamma-2)(2\gamma-1)}} \quad (7)$$

$$350 \quad Z = - \frac{\gamma(\gamma-1)\mathcal{V}^2(\mathcal{V}-1)}{2(\gamma\mathcal{V}-1)} \quad (8)$$

351 The value of  $\beta$  was considered to be 1.229 for  $\gamma=1.4$ . Following these equations, the pressure v/s  
352 time characteristics was obtained for all the three equivalent ratios assuming the drag coefficient  
353 to be zero.

354 The pressure curve is calculated by solving equations 5 through 8. MATLAB8.2 is used for  
355 calculating the peak pressure and also the pressurization rate. Fig. 5 (a) and (b) show the plot of  
356 estimated gas pressure (in MPa) with respect to time (microseconds) corresponding to an  
357 equivalence ratios 1.6 for  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  respectively. The peak pressure was  
358 estimated to be 25.35 MPa and 36.95 MPa respectively for  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$ .

#### 359 **E. Combustion Performance of $\text{Co}_3\text{O}_4/\text{nAl}$ and $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$ nanoenergetic composites**

360 Combustion front-wave speed, peak pressure and pressurization rate measurement of  $\text{Co}_3\text{O}_4/\text{nAl}$   
361 at equivalence ratio of 1.4, 1.6 and 1.8 has been shown in supplementary Table S2. The pressure-  
362 time characteristics curve of  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  as a function of equivalence ratio  
363 has been drawn and shown in Fig 5 (c) and (d). The peak pressure and pressurization rate of  
364  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  were measured maximum at equivalence ratio of 1.6 developing  
365 peak pressure of  $20\pm 2$  MPa (Pressurization rate= $0.14\pm 0.03$  MPa/ $\mu\text{s}$ ) and  $32.6\pm 3$  MPa  
366 (Pressurization rate= $0.47\pm 0.1$  MPa/ $\mu\text{s}$ ) respectively. The peak pressure so measured rhymes well  
367 with the theoretically predicted value although as estimated earlier the pressurization rate is not  
368 so huge. The time scale of experimental pressure-time characteristics (pressurization rate) is in  
369 fact  $\sim 100$  times more than that predicted theoretically due to diffusional restrictions. In reality,  
370 the exothermic reactivity of nanoenergetic formulation and henceforth the gas release rate during  
371 combustion depends on the population of fuel and oxidizer atoms in contact and inter-atomic  
372 diffusion path which will disallow the pressure wave to travel such a super high rate as predicted

373 in theoretical estimation. The pressure rise time of cobalt oxide based nanoenergetics is  
374 measured to be 70  $\mu\text{s}$  ( $\text{Co}_3\text{O}_4\text{-400/nAl}$  at  $\phi=1.6$ ), which is seven times higher than that of our  
375  $\text{Bi}_2\text{O}_3/\text{Al}^{42}$  based nanoenergetic films. The shorter time scale of  $\text{Bi}_2\text{O}_3/\text{Al}^{42}$  nanoenergetic films  
376 than  $\text{Co}_3\text{O}_4\text{-400/nAl}$  can be attributed to its higher gas generating ability and less diffusional  
377 restriction owing to core-shell nanostructuring. Thus, we may conclude that the time scale of  
378 cobalt oxide based nanoenergetics can be shortened and approached towards theoretical one by  
379 nanotechnological efforts (Fabrication of high-aspect, high purity  $\text{Co}_3\text{O}_4$  nanostructures and their  
380 molecular level as well as stoichiometric assembling with nanoaluminum).

381 The pressure-time characteristics achieved with  $\text{Co}_3\text{O}_4\text{-400/nAl}$  was found better than the PEG  
382 synthesized CuO nanorods ( $\text{CuO}_{\text{peg}}$ ) based nanoenergetics (Peak Pressure= $27.4\pm 2$  MPa,  
383 Pressurization rate= $0.25\pm 0.1$  MPa/ $\mu\text{s}$ ) as reported in our previous findings.<sup>26</sup> In another pressure-  
384 time characteristics experiment,<sup>24</sup> the commercial grade CuO based nanoenergetics developed  
385 lowest peak pressure and pressurization rate of magnitude  $22\pm 3$  MPa and  $2.5\pm 0.3$  MPa/ $\mu\text{s}$   
386 respectively among their all kinds of CuO oxidizers of packing density of  $0.33$  g/cm<sup>3</sup>. Thus the  
387 low pressure-time characteristics of  $\text{Co}_3\text{O}_4/\text{nAl}$  really helps us to achieve a softer system of  
388 delivery of a pressure waves which would not cause much damage to the soft cellular system as  
389 has eventually been the goal behind all the material synthesis reported in this work. The peak  
390 pressure ( $32.6\pm 3$  MPa) of calcined  $\text{Co}_3\text{O}_4$  based nanoenergetics is comparable to that of CuO  
391 nanoparticles (calcined at  $400$  °C for 3 h of CuO-100 nanorods) based nanoenergetics (Peak  
392 Pressure= $35\pm 3$  MPa). The considerably lower pressurization rate of  $\text{Co}_3\text{O}_4\text{-400/nAl}$  than the  
393 CuO nanoparticles (calcined at  $400$  °C for 3 h of CuO-100 nanorods) based nanoenergetics<sup>24</sup> can  
394 be attributed to its lower theoretical gas generations<sup>2</sup>. Theoretical gas release of  $\text{Co}_3\text{O}_4/\text{nAl}$   
395 nanoenergetic composites is about 62 % lesser than the gas release with the CuO/nAl

396 nanoenergetic composites. The combustion behavior of  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetics at equivalence  
397 ratio of 1.8 is observed to be anomalous giving highest combustion velocity but developing  
398 smallest pressurization rate. It can be hypothesized that, since the combustion front-wave  
399 propagation distance in pressure cell is much shorter (i.e. 5 mm) than that in burn-tube  
400 experiment (i.e. 100 mm), therefore the higher thermal conductivity of nanoenergetics associated  
401 with equivalence ratio of 1.8 may not contribute much in pressurizing the combustion front-  
402 waves. The higher available oxygen atoms at equivalence ratio of 1.6 can be believed to increase  
403 the exothermic reaction and thus the pressurization rate.

404 The combustion front-wave speed (correspond to speed between photo-detectors 3 and 4) of  
405  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  nanoenergetics at different equivalence ratios can be seen in Fig.  
406 6. From the inset photo-detector output *vs* time plot of Fig. 6, the interval time between two  
407 photo-detectors is observed decreasing in forward direction, which implies that the combustion  
408 wave-front accelerates in forward direction in confined burn tube. It can be envisioned that the  
409 pressure build-up due to high combustion/exothermic reactivity and gas generation in confined  
410 burn tube during combustion process propel the flame front propagation at a faster rate in  
411 forward direction. The pressure build up may also hypothesized to enhance the ignition  
412 sensitivity of nanoenergetic composites lying ahead of the flame front and therefore the ignition  
413 of nanoenergetic composites happens at early stage of time in forward direction. Thus, the  
414 accelerating rate of combustion flame-front speed may be believed to depend on the intensity of  
415 pressure-build up, forward pressure wave speed and the rate of confinement of burn tube.  
416 However, it can further be envisaged that the pressure wave would accelerate the combustion  
417 flame front propagation only, if it is travelling at a higher speed than the combustion flame front  
418 speed. The combustion front-wave speed of calcined  $\text{Co}_3\text{O}_4$  based nanoenergetic composites

419 was found to be maximum at equivalence ratio of 1.6 where as for  $\text{Co}_3\text{O}_4/\text{Al}$  nanoenergetics, an  
420 increasing trend in combustion front-wave speed with equivalence ratio can be observed. It can  
421 be interpreted that the presence of surface impurity of poly(oxymethylene)glycols to the  
422 uncalcined  $\text{Co}_3\text{O}_4$  may require excess aluminum than that of calcined  $\text{Co}_3\text{O}_4$  oxidizer which may  
423 be the reason of developing higher combustion front-wave speed at equivalence ratio of 1.8 in  
424  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetics. It is also observed from combustion front-wave speed plot that there  
425 is lower deviation in combustion front-wave speed in between equivalence ratio of 1.6 to 1.8  
426 than that between 1.4 to 1.6 which can be explained by considering the higher thermal  
427 conductivity of nanoenergetic composites due to increase in the relative quantity of nano-  
428 aluminum at higher equivalence ratio. The higher thermal conductivity can be believed to create  
429 a faster hot spot at the front of combustion front-wave which may accelerate the combustion  
430 front-wave propagation along the total travel of 100 mm in the burn-tube experiment.

#### 431 **IV. Conclusions**

432 In summary, nanoscale  $\text{Co}_3\text{O}_4$  consisting of small nanoparticles (diameter  $\sim 3\text{-}5$  nm) and  
433 nanobelts (diameter of 5-10 nm, lengths of up to 100 nm) were synthesized by a simple solid-  
434 state method and were characterized by XRD, TEM, SAED and FTIR. The nanoscale  $\text{Co}_3\text{O}_4$  was  
435 utilized as oxidizer in developing novel bulk nanoenergetic composites with nanoaluminum. The  
436 calcined  $\text{Co}_3\text{O}_4$  based nanoenergetic composites *i.e.*  $\text{Co}_3\text{O}_4\text{-}400/\text{nAl}$  exhibited better exothermic  
437 heat of reaction and combustion performance than that of uncalcined one. Based on TGDSC  
438 measured heat of reaction and pressure-cell design parameters, the peak pressure and  
439 pressurization rate were theoretically estimated and when compared to the experimentally  
440 measured pressure-time characteristics, a good agreement between predicted peak pressure and  
441 measured peak pressure was found. The  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-}400/\text{nAl}$  nanoenergetics were

442 able to propagate at a maximum flame-front speed of  $781\pm 50$  and  $830\pm 75$  m s<sup>-1</sup> respectively.  
443 These nanoenergetic systems are able to develop peak pressure ranging from mild ( $12.6\pm 1$  to  
444  $20\pm 2$  MPa with Co<sub>3</sub>O<sub>4</sub>/nAl) to moderate ( $26\pm 2$  to  $32.6\pm 3$  MPa with Co<sub>3</sub>O<sub>4</sub>-400/nAl) during  
445 combustion experiment inside a constant-volume pressure cell experiment with charge density of  
446  $0.2$  g cm<sup>-3</sup>. The maximum peak pressure was obtained at equivalence ratio of 1.6 and was nearly  
447 comparable to the CuO based nanoenergetic system but the maximum pressurization rate with  
448 Co<sub>3</sub>O<sub>4</sub>/nAl ( $0.47\pm 0.1$ MPa/ $\mu$ s) was much below to that of CuO/nAl nanoenergetics owing to low  
449 gas generation during combustion process. The heat of reaction was measured to be  $0.96$  kJ g<sup>-1</sup>  
450 for Co<sub>3</sub>O<sub>4</sub>/nAl and  $1.02$  kJ g<sup>-1</sup> being greater to that of PEG400 synthesized CuO nanorods based  
451 nanoenergetics. Through this work we report a new set of nanoenergetic composite that can be  
452 used for creating mild to moderate pressure waves.

### 453 **Supporting Information**

454 The pressure-time characteristics measuring set-up and combustion front-wave speed  
455 measuring set-up have been shown in supplementary Fig. S1 and S2. Reactive mass  
456 distribution and Combustion (front-wave speed and pressure-time) measurements of  
457 nanoenergetic composites have been listed in supplementary Table S1 and S2 respectively.

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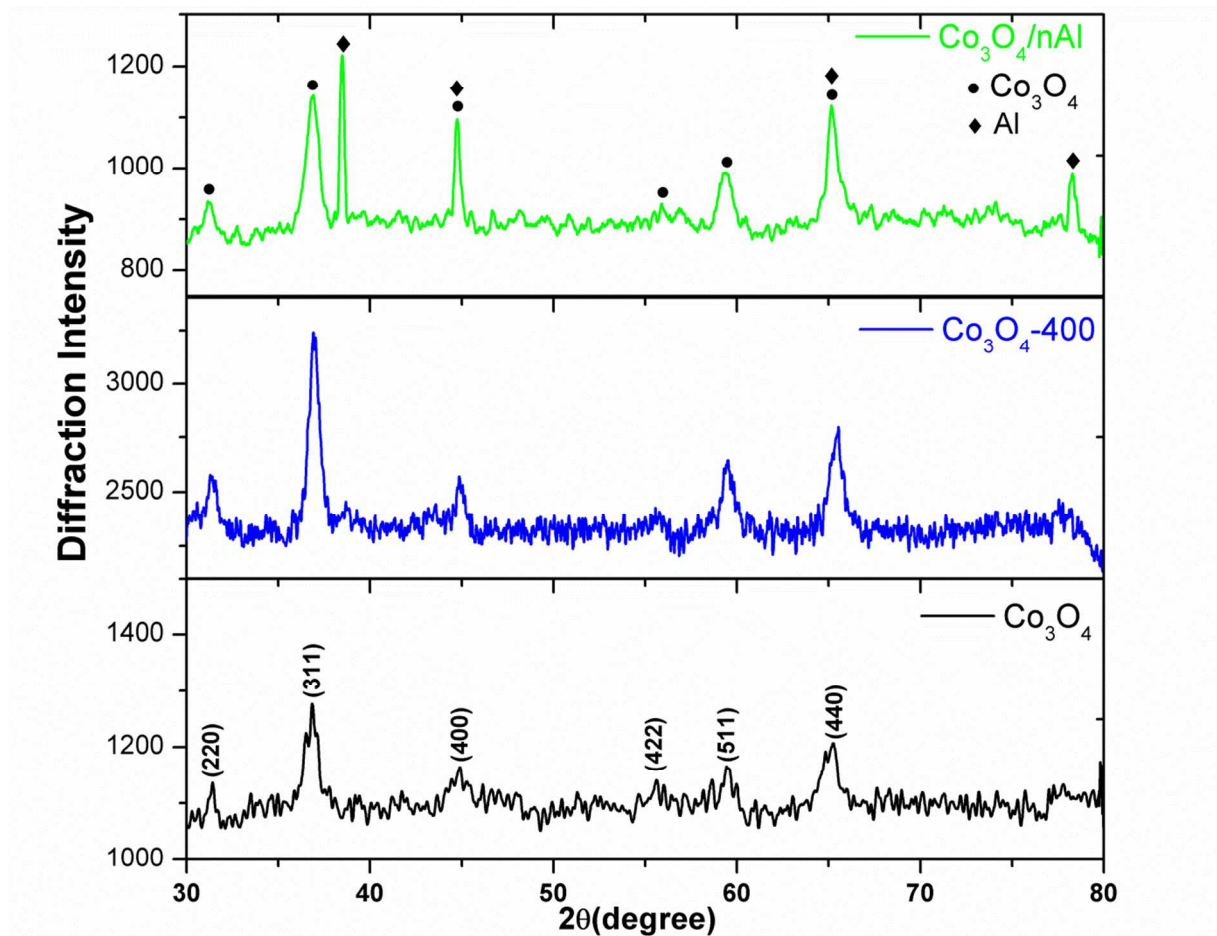
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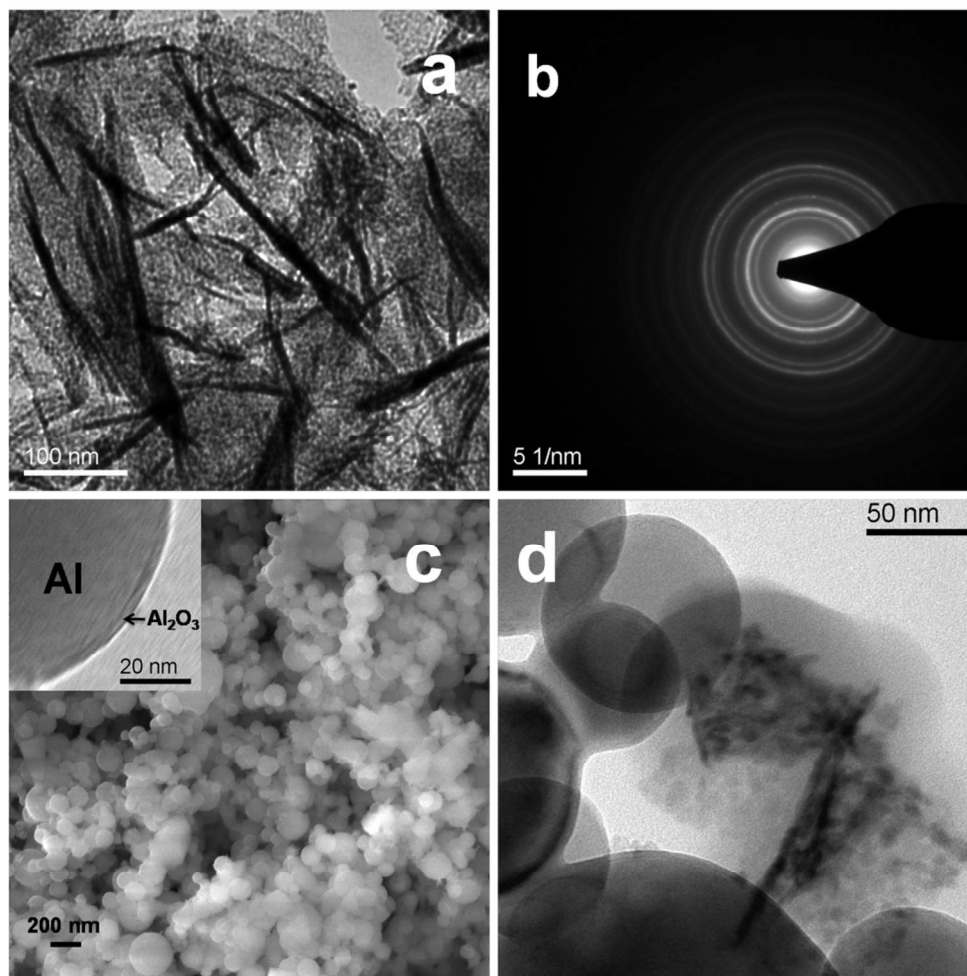
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542 **Fig 1.** Powder X-ray diffraction pattern of  $\text{Co}_3\text{O}_4$  (indicated in black),  $\text{Co}_3\text{O}_4\text{-400}$  (indicated in  
543 blue) and  $\text{Co}_3\text{O}_4/\text{Al}$  nanoenergetics prepared at equivalence ratio of 1.6 (indicated in green)

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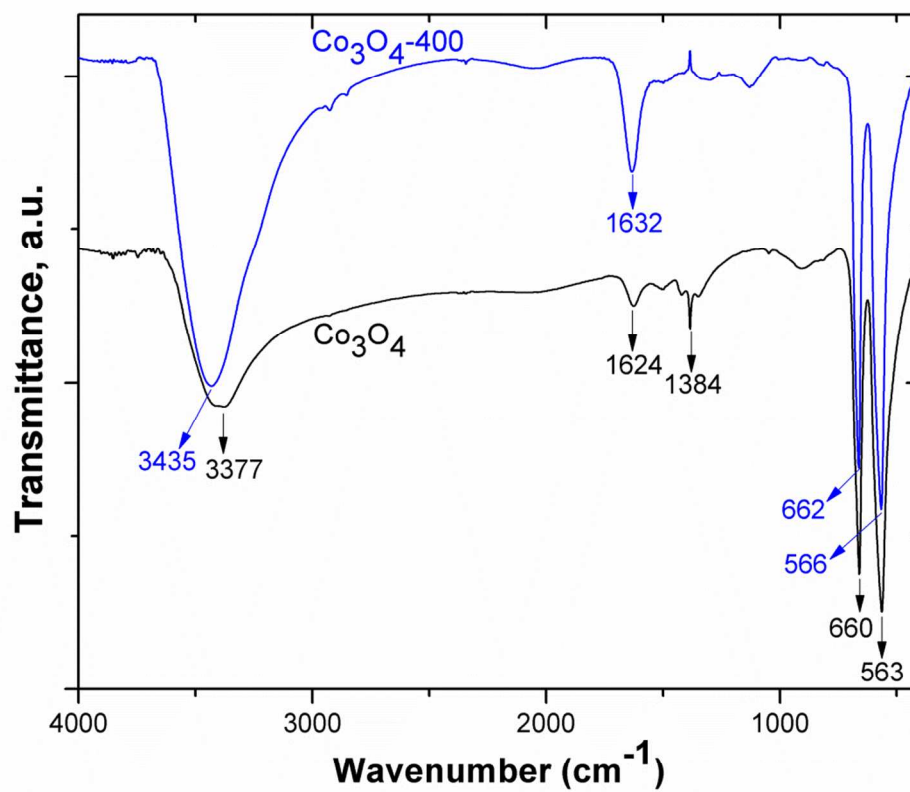
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546 **Fig 2.** (a) TEM image of  $\text{Co}_3\text{O}_4$  nanobelts (b) SAED ring pattern of  $\text{Co}_3\text{O}_4$  nanobelts (c) FESEM  
547 image of aluminum nanoparticles with inset of its high magnification TEM image showing the  
548 core (Al) and shell ( $\text{Al}_2\text{O}_3$ ) (d) TEM image of  $\text{Co}_3\text{O}_4/\text{nAl}$  nanoenergetic composites

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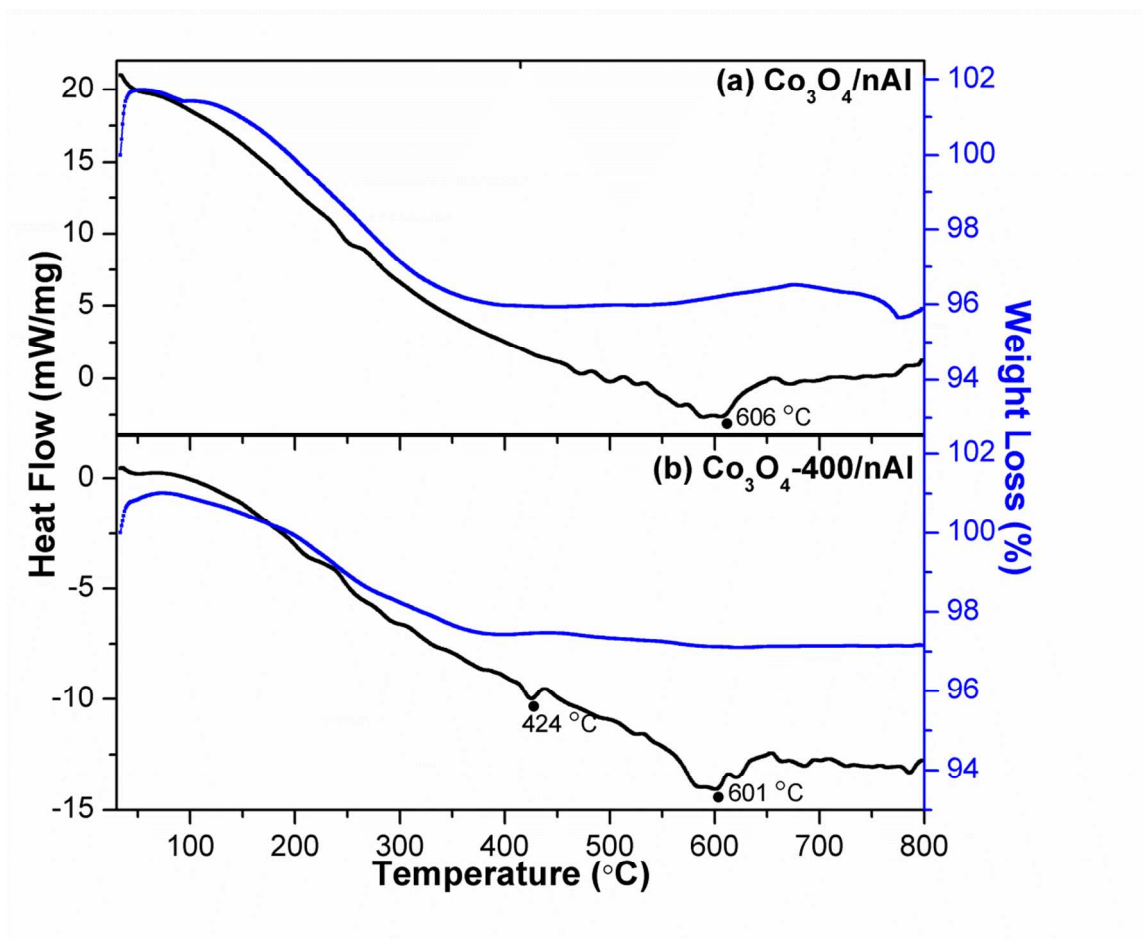
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554 **Fig. 3** FT-IR Spectrum of  $\text{Co}_3\text{O}_4$  (indicated in black) and  $\text{Co}_3\text{O}_4\text{-400}$  (indicated in blue)

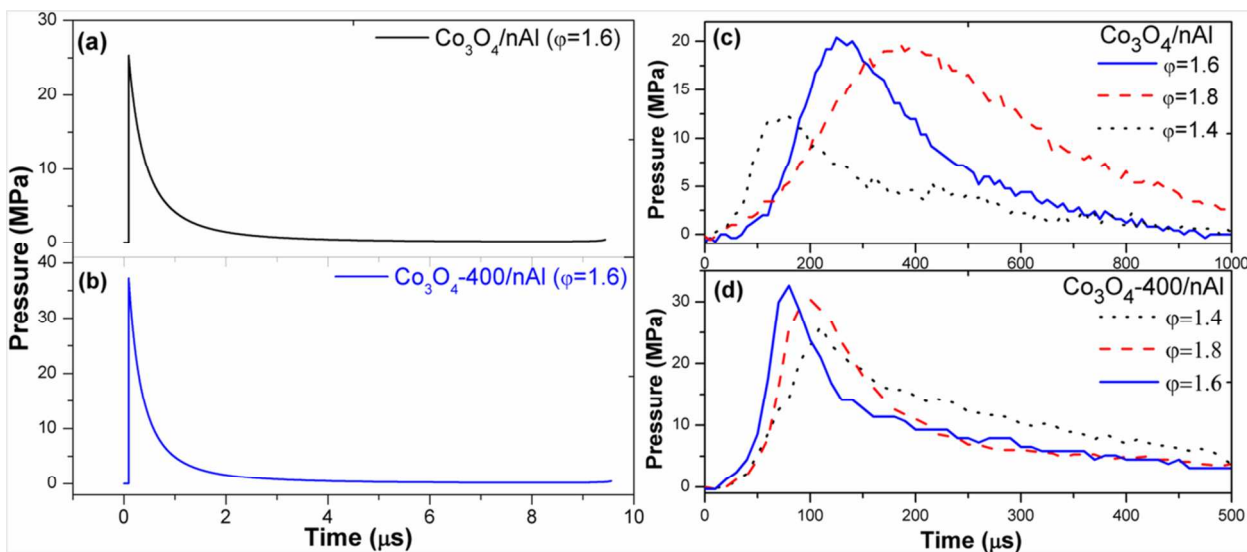
555 nanomaterials.



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557 **Fig 4.** TG-DSC measurements of (a)  $\text{Co}_3\text{O}_4/\text{nAl}$  and (b)  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  nanoenergetics at

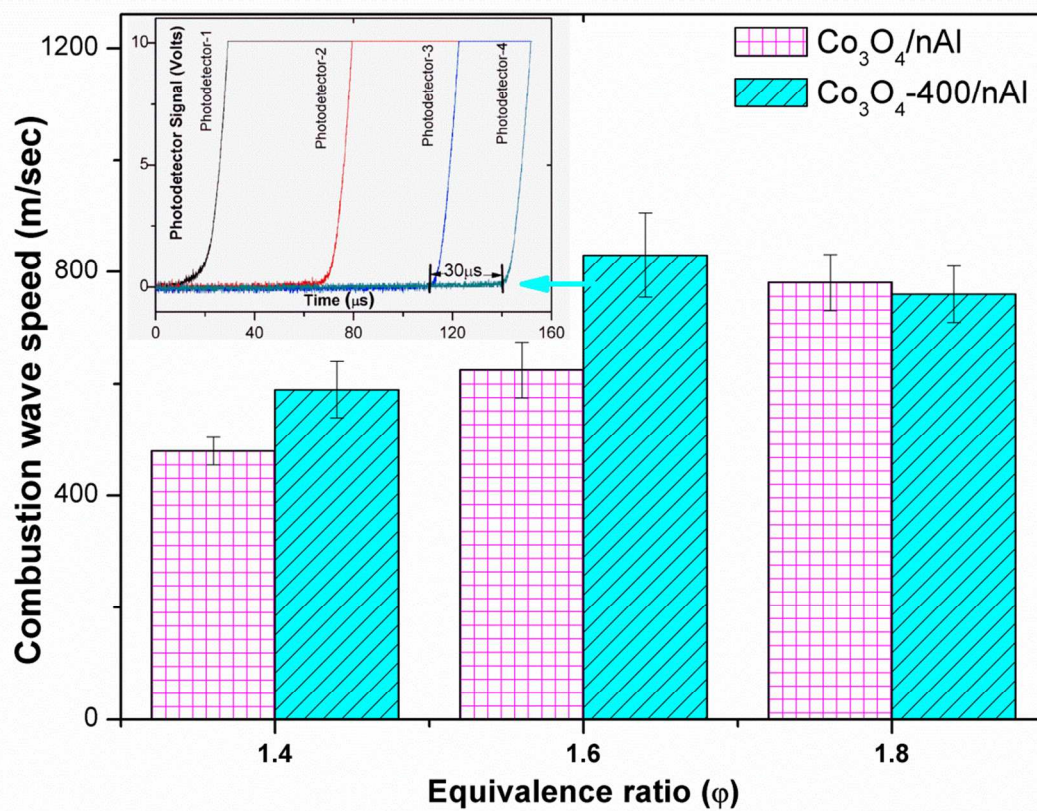
558 equivalence ratio of 1.6.



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560 **Fig. 5** Theoretical Pressure-time characteristics results using MATLAB modeling of big  
561 explosion gas dynamic model at equivalence ratios of 1.6 for (a)  $\text{Co}_3\text{O}_4/\text{nAl}$  and (b)  $\text{Co}_3\text{O}_4\text{-}$   
562 400/nAl, and experimental Pressure-time characteristics of (c)  $\text{Co}_3\text{O}_4/\text{nAl}$  (d)  $\text{Co}_3\text{O}_4\text{-}400/\text{nAl}$  at  
563 different equivalence ratio.

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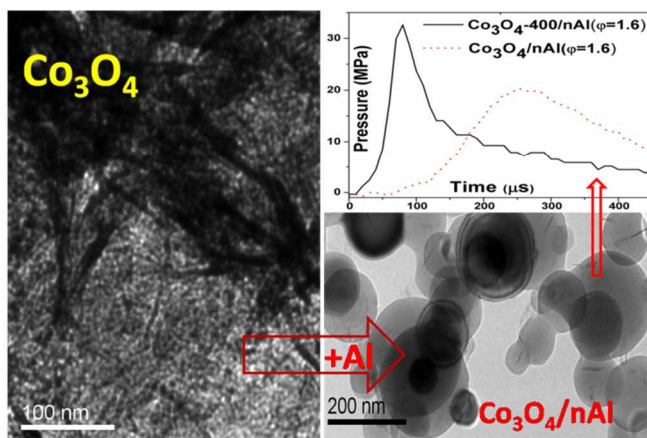
566 **Fig 6.** Combustion front-wave speed measurements of  $\text{Co}_3\text{O}_4/\text{nAl}$  and  $\text{Co}_3\text{O}_4\text{-400}/\text{nAl}$  as a

567 function of equivalence ratio with inset plot of photo-detector output vs time.

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571 Novel  $\text{Co}_3\text{O}_4$  nanobelts based bulk nanoenergetic systems have been developed which are able to

572 generate mild to moderate peak pressure and pressurization rates as demanded in shock wave

573 mediated biomedical applications.

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