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Aluminium-doped SnO2 nanoparticles inhibited a hydroxyl poisoning and enhanced the sensor response in humid atmosphere

Journal Name

ARTICLE

Received 00th January 20xx, Accepted 00th January 20xx

DOI: 10.1039/x0xx00000x

www.rsc.org/

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Inhibition of hydroxyl poisoning of SnO₂ nanoparticles is important to develop a highly sensitive combustible gas sensor that functions in a humid atmosphere. For this purpose, we incorporated Al into $SnO₂$ nanoparticles (Al-doped $SnO₂$) by a precipitation method, and fabricated a thick-film-type sensor using a screen printing method. Bare SnO₂ nanoparticles and Al₂O₃-loaded SnO₂ nanoparticles were also prepared for comparison. The oxygen adsorption amount clearly decreased after Al doping and Al₂O₃ loading, according to temperature programmed desorption measurements. Al doping enhanced the sensor response (sensitivity) to H₂, CO and C₂H₅OH in a humid atmosphere by almost five to ten times. Al₂O₃ loading also slightly increased the sensor response to each gas in a humid atmosphere. The enhancement of the sensor response was attributed to both Al and Al₂O₃ acting as hydroxyl absorbers on the surface of the nanoparticles, thereby providing an oxygen adsorption site for surface combustion reactions in a humid atmosphere. Based on the relationship between the sensor response and C₂H₅OH concentration, it was estimated that Al-doped SnO₂ can detect less than one ppm C₂H₅OH in a humid atmosphere. Therefore, doping with Al, which protects and holds the adsorbed oxygen on the surface of the SnO₂, is important as a surface modification to obtain humidity-tolerant semiconductor gas sensors.

Introduction

Tin dioxide $(SnO₂)$ is well known as one of the multifunctional material having a wide applications such as gas sensors $1-6$, catalyst $6-8$, optoelectronic device $4,5,9-11$, and so on $4,5,12$. In particular, SnO₂ based semiconductors offer great potential for gas sensors because of their detection accuracy and high sensitivity to combustible gases. For example, we developed a highly sensitive H_2S gas sensor using crystallite controlled SnO_2 nanoparticles $\frac{1}{2}$ and a highly sensitive volatile organic compounds (VOCs) gas sensor using clustered (aggregated) Pd/SnO_2 nanoparticles ². Such SnO_2 -based gas sensors allow instant gas detection because $SnO₂$ responds rapidly to combustible gases 13 . Moreover, compact and lowpower gas sensors have recently been investigated for batteryoperated portable devices 14,15. However, the potential of these gas sensors has often been demonstrated in a dry atmosphere because $SnO₂$ has a significantly low tolerance to humidity. Therefore, many researchers are interested in humidity-tolerant

materials as semiconductor gas sensors for monitoring the gas components.

SnO₂-based semiconductors have been recognized as a promising material because of their sensitive response to combustible gases. However, $SnO₂$ is vulnerable to humidity because of its gas detection mechanism. Normally, the electric resistance of $SnO₂$ is strongly dependent on the presence of negatively charged adsorbed oxygen on the particle surface, as explained below.

$$
O_2 + 2e^- \rightarrow 2O^-_{ad} \tag{1}
$$

Here e is a carrier electron in $SnO₂$ and O_{ad} is adsorbed oxygen trapping the electron. This reaction leads to the formation of an electron depletion layer on the particle surface and an increase in the electric resistance. Combustible gases, such as H_2 , are detected by a combustion reaction with adsorbed oxygen on the $SnO₂$ surface. This reaction is shown in the following equation.

$$
H_2 + O_{ad} \rightarrow H_2O + e^-(2)
$$

Consequently, the electric resistance decreases as the electron depletion layer is reduced by the release of the trapped electrons. The difference in the electric resistance is used as a signal for gas detection. However, oxygen adsorption on the SnO² surface is strongly disturbed by hydroxyl poisoning in a humid atmosphere ¹⁶⁻¹⁹. Therefore, detection of combustible gases in a humid atmosphere is difficult. In a commercial gas sensor, the sensing layer is capped by a humidity absorber, such as activated carbon, to avoid hydroxyl poisoning. To develop reduced-size semiconductor gas sensors, it is desirable that the semiconductor materials are resistant to humidity.

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Recent research has focused on protecting the sensor from deterioration due to hydroxyl poisoning. For example, it has been accepted that catalytic Pd loading on the $SnO₂$ particle leads to less hydroxyl poisoning $18,19$. We found that the main oxygen adsorption species of $SnO₂$ and Pd-loaded $SnO₂$ were O and $O²$ in a humid atmosphere ²⁰. Accordingly, $O²$ on PdO prevented hydroxyl adsorption on the $SnO₂$ surface. Furthermore, Kim et al. proposed that NiO, a humidity absorber, protects the $SnO₂$ surface from hydroxyl poisoning according to the results of their diffusion-reflectance Fourier transform IR (DRIFT) spectroscopy measurements 21 . Moreover, Choi et al. reported that CuO also worked as a humidity absorber on the $SnO₂$ surface for $H₂S$ sensing in a humid atmosphere. They proposed that CuO is effective because it has a high affinity towards water vapour 22 . Therefore, protecting and holding adsorbed oxygen on the $SnO₂$ surface is the key to producing a high performance gas sensor in a humid atmosphere.

In this study, we attempted to enhance the sensor response to combustible gases in a humid atmosphere by using $SnO₂$ based semiconductor gas sensors. Aluminium ions and alumina, which have a high affinity for water and hydroxyl adsorption²³⁻ ²⁵, were incorporated into $SnO₂$ nanoparticles to protect the adsorbed oxygen. To investigate the effect of surface modification on the oxygen and hydroxyl adsorption, we prepared conventional spherical bare- $SnO₂$ nanoparticles, Aldoped $SnO₂$ nanoparticles, and $Al₂O₃$ -loaded $SnO₂$ nanoparticles. Sensor responses to combustible gases H_2 , CO, and C_2H_5OH in dry and humid atmospheres were investigated by analysing the electric resistance with considering their crystallite size, specific surface area, pore radius, and amount of oxygen adsorbed. It is noteworthy that Al-doped $SnO₂$ showed a high response to C_2H_5OH in a humid atmosphere even though its crystallite size, specific surface area, and pore radius were almost the same as bare- $SnO₂$. These results show that the developed semiconductor gas sensors can be used in a humid atmosphere without capping and could lead to the development of more compact sensor devices.

Experimental

Material preparation

Bare-SnO² nanoparticles were prepared using a hydrothermal treatment, as reported previously ². Stannic acid gel was prepared by adding an aqueous solution of SnCl₄.5H₂O (1M) dropwise into a $NH₄ HCO₃$ solution (1M). The aqueous dispersion of the stannic acid gel was hydrothermally treated at 200 $^{\circ}$ C for 3 h at 10 MPa with continuous stirring at 600 rpm,

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after removal of Cl- by centrifugation. To prepare a monodispersed solution of smaller $SnO₂$ nanoparticles, the pH of the solution was adjusted to 10.6. The solution was dried at 120 \degree C for 6 h and calcined at 600 \degree C for 3 h to produce a powder of bare-SnO₂ nanoparticles.

Al (0.5 mol\%) -doped SnO₂ nanoparticles were prepared by a conventional precipitation method, reported previously . SnCl₄ 5H₂O and AlCl₃ were used as the starting materials. An appropriate amount of a mixed aqueous solution of SnCl₄ and $AICl₃$ was added dropwise into a $NH₄HCO₃$ solution. After waiting for 12 h to obtain a white precipitate, the hydroxide gel was washed and the Cl was removed by centrifugation. The gel was dried at 120 $^{\circ}$ C and calcined at 600 $^{\circ}$ C for 3 h to obtain a powder of Al-doped SnO₂ nanoparticles.

For comparison with Al-doped $SnO₂$, we prepared $Al₂O₃$ $(0.5 \text{ mol\%}$ Al atom)-loaded SnO₂ nanoparticles using an impregnation method 26 . Carrier SnO₂ nanoparticles were prepared using a conventional precipitation method, in the same manner as the Al-doped $SnO₂$. The stannic acid gel was prepared by adding a $SnCl₄$ aqueous solution (1M) into NH₄HCO₃ solution (1M). The precipitated white gel was dried at 120 and calcined 600 $^{\circ}$ C for 3 h to obtain the carrier SnO₂ powder, after removing Cl- from the gel by centrifugation. The obtained powder was dispersed in deionized water and $Al(NO₃)₃$ (0.5 mol%) was added to the solution by stirring. The Al_2O_3 -loaded Sn O_2 nanoparticles powder was obtained by evaporating the solution at 100 \degree C and calcining the dried powder at $600 °C$ for 3 h.

Preparation of the sensor device and evaluation of the electric resistance

A screen printing method was used to mount the $SnO₂$ based powders on an alumina substrate $(9 \times 13 \times 0.38 \text{ mm})$, which was printed with an Au comb-type electrode (180-um line width, 90-um distance between lines, 64-mm² sensing area). For screen printing, an $SnO₂$ paste was prepared by mixing the SnO_2 -based powders with α -terpineol. The sensing films were deposited on the substrates and sintered at 580 °C for 3 h with flowing synthetic air. The air was controlled using a conventional gas-flow apparatus equipped with an electric furnace (Fig. 1). The flow rate of the synthetic air and sample gases was kept at 80 cm³/min by mass flow controllers (SECseries; HORIBA STEC). Sample gases of H_2 , CO, and C_2H_5OH in air were prepared by diluting the parent synthetic gas mixtures with synthetic air. A humid atmosphere was prepared by blowing the sample gases into pure water (Fig. 1), and humidity was determined using a commercial humidity sensor (TR-77Ui; T&D Corporation). Each sensor device was connected with a standard resistor in series. Voltage across the standard resistor was measured under an applied DC voltage of 4 V to evaluate the electric resistance of the sensors. An electric signal was acquired using an electrometer (2701; Keithley Instruments). The sensor response (S) was defined as the ratio of the electric resistance in air (R_a) to the resistance in the sample gases (R_g) (S = R_a/R_g).

Fig. 1 Schematic image of a gas flow apparatus with an electrical measurement system.

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Results and discussion

Material characterization

 XRD patterns of the bare-SnO₂, Al-doped SnO₂ (Al-SnO₂), and Al_2O_3 -loaded SnO_2 (Al_2O_3 -SnO₂) nanoparticles are shown in Fig. 2a. The obtained XRD patterns correspond well with the cassiterite structure of $SnO₂$ (JCPDS: 41-1445) and no impurity peaks were observed. The estimated crystallite size of each nanoparticle is shown in Table 1. The crystallite size of bare- $SnO₂$ and $Al-SnO₂$ were similar sizes, 14 and 12 nm, respectively. The average crystallite size of bare-SnO₂ prepared using the same conventional precipitation process as for Al-SnO² , was almost 18 nm. Al doping reduces the crystallite size of $SnO₂$ nanoparticles. It is well accepted that metallic ion

doping inhibits the crystal growth of $SnO₂$ ^{9,26}. This is the slight evidence that Al is doped into the $SnO₂$ nanoparticles. A small peak shift of the XRD patterns would also indicate doping of other elements, as reported by Duan et al. ⁹. However, no peak shifts in the XRD patterns were observed because the amount of Al doping was very low. In the case of $Al_2O_3-SnO_2$ nanoparticles, the crystallite size of 19 nm was larger than the other materials because the size of the carrier $SnO₂$ was 18 nm. TEM images of the nanoparticles are shown in Fig. 2b-d, and spherical type $SnO₂$ crystals were observed in each image. The Al_2O_3 -Sn O_2 nanoparticles were discernibly larger than the other nanoparticles. The observed crystallite size of bare-SnO₂, Al- $SnO₂$, and $Al₂O₃$ -SnO₂ were 14, 13, and 22 nm, respectively. These were similar to the crystallite sizes estimated from the XRD patterns.

Table 1 Estimated values of average crystallite size (XRD), specific surface area (BET), peak pore radius (BJH) and O₂ desorption amount (O₂-TPD) for bare-SnO₂ nanoparticles, Al-doped SnO₂ nanoparticles, and Al₂O₃-loaded SnO₂ nanoparticles.

Fig. 2 (a) XRD patterns of nanoparticles and TEM images of (b) $bare-SnO₂$ nanoparticles, (c) Al-doped SnO₂ nanoparticles, and (d) Al₂O₃-loaded SnO₂ nanoparticles.

The pore size distribution of each nanoparticles is shown in Fig. 3a, and the estimated specific surface area and peak pore radius are shown in Table 1. Bare-SnO₂ and Al-SnO₂ nanoparticles had a comparable specific surface area and peak pore radius. Al_2O_3 -Sn O_2 had a smaller specific surface area and a larger peak pore radius because of a larger crystallite size and particle aggregation. SEM images of each nanoparticles on the sensing layer are shown in Fig. 3b-d. The observed pore and particle size of bare-SnO₂ was comparable in size to Al-SnO₂. However, Al_2O_3 -Sn O_2 had larger nanoparticles and pores than bare-SnO₂. Both the bare-SnO₂ and Al-SnO₂ nanoparticles accumulated in a dense packing layer with small particles, whereas the Al_2O_3 -SnO₂ nanoparticles accumulated in a loose packing layer. Thereby, we can investigate the Al doping effect without considering particle size and morphology.

Fig. 3 (a) Pore radius distributions of each nanoparticles and SEM images of (b) bare-SnO₂ nanoparticles, (c) Al-doped SnO₂ nanoparticles, and (d) $\mathsf{Al}_2\mathsf{O}_3$ -loaded SnO₂ nanoparticles.

Figure 4 shows the O_2 -TPD results of bare-Sn O_2 , Al-Sn O_2 , and Al_2O_3 -Sn O_2 nanoparticles. Two large peaks were observed at 100 and 450 $^{\circ}$ C; these were attributed to desorption of adsorbed molecular oxygen (O_2) and adsorbed dissociated oxygen with a negative charge (O or O^2), respectively ¹⁷. The adsorbed oxygen (O or O^2) peaked at 450 °C is attributed to the surface reaction (Equation 2) that causes decreasing of

adsorbed oxygen amount because of the $H₂O$ emission evaluation $17,20$. We estimated the oxygen desorption amount in the range of $350-520$ °C from the amount of adsorbed oxygen using Fig. 4, and listed these values in Table 1 as two different units, μ mol·g⁻¹ and μ mol·m⁻². Bare-SnO₂ desorbed almost two times more adsorbed oxygen (O or O^2) than Al-SnO₂ and Al₂O₃-SnO₂. In previous reports of TPD measurements, Huang et al. revealed that the oxygen desorption peak was observed at approximately 527 °C (800 K) when using γ -Al₂O₃ ²⁷ . Moreover, Putna et al. reported that no oxygen desorption peak was observed using α -Al₂O₃ (0001)²⁸. These results indicate that the presence of Al decreases the oxygen desorption amount because of the reduction of naked oxygen adsorption sites in SnO₂. The oxygen desorption amount per unit area, μ mol·m⁻², of Al-SnO₂ was smaller than Al_2O_3 -SnO₂. Usually, the naked surface area of the carrier material decreases with an increase in dispersity of the doping or loading element. Thus, the Al in Al- $SnO₂$ was more dispersed on the surface than the $Al₂O₃$ in Al_2O_3 -SnO₂, and the Al in Al-SnO₂ effectively disturbed oxygen adsorption on the $SnO₂$ surface. Therefore, Al doping and Al_2O_3 loading decreased the oxygen adsorption on the SnO₂, and Al was probably highly dispersed in the $SnO₂$ nanoparticles.

Fig. 4 Oxygen desorption spectra of $O₂-TPD$ measurement using (a; black line) bare-SnO₂ nanoparticles, (b; red line) Aldoped SnO₂ nanoparticles, and (c; blue line) Al_2O_3 -loaded SnO₂ nanoparticles.

The electric resistance in synthetic air

The electric resistance of $SnO₂$ nanoparticles is greatly influenced by the change in the oxygen adsorption amount and other element doping 26,29 and loading 20,22,26. Figure 5a and b show the electric resistance in synthetic air in dry and humid (45% R.H. at 25 $^{\circ}$ C) atmospheres, respectively. In a dry atmosphere, $AI\text{-}SnO_2$ and $AI_2O_3\text{-}SnO_2$ showed higher electric resistance than bare-SnO₂. In previous work, we prepared Fedoped $SnO₂$ nanoparticles using the same process as with Al- $SnO₂$, and we confirmed that Fe doping into $SnO₂$ nanoparticles increases their electric resistance ²⁶. Hence, increasing the electric resistance of $AI-SnO₂$ was attributed to the replacement of Sn^{4+} with Al^{3+} , leading to a decrease in the donor density. Conversely, mixing Al_2O_3 with SnO_2 prevents electron transport between the SnO2 nanoparticles and increases the electric resistance. This occurs because Al_2O_3 is an insulating material. The amount of oxygen adsorbed by $AI-SnO₂$ and $Al_2O_3-SnO_2$ was less than the bare-SnO₂, as shown in Fig. 4. Therefore, Al doping and Al_2O_3 loading were effective at increasing electric resistance.

In a humid atmosphere, the electric resistance of each sensor decreased (Fig. 5b). It is well accepted that oxygen adsorption is disturbed by hydroxyls adsorbed on the oxygen adsorption site. $AI\text{-}SnO_2$ and $AI_2O_3\text{-}SnO_2$ nanoparticles showed a higher electric resistance than bare- $SnO₂$ nanoparticles, even in a humid atmosphere. The reason for the high electric resistance was caused less by oxygen adsorption and more by Al doping and Al_2O_3 loading. Sensor response to water vapour, which is the ratio of electric resistance in dry air to that in humid air, is shown in Fig. 5c. Sensor response increased with decreasing operating temperature in all samples because hydroxyl poisoning increases with decreasing temperatures. Bare-SnO₂ nanoparticles was clearly more sensitive to humidity than Al-SnO₂ and Al₂O₃-SnO₂ nanoparticles at 250 °C because there are fewer oxygen adsorption sites on $AI-SnO₂$ and $AI₂O₃$ - $SnO₂$ than on bare- $SnO₂$. In addition, our $SnO₂$ -based nanoparticles had a high affinity for hydroxyls.

Fig. 5 Temperature dependence of the electric resistance in synthetic air atmosphere (a) in dry and (b) humid (45 % R.H. at 25 $^{\circ}$ C), and (c) the response to humidity using (\bullet) bare-SnO₂ nanoparticles, (\triangle) Al-doped SnO₂ nanoparticles, and (\triangledown) Al₂O₃loaded SnO₂ nanoparticles.

The sensor response to combustible gases

The sensor response to combustible gases was examined using bare-SnO₂, Al-SnO₂, and Al₂O₃-SnO₂ nanoparticles. The sensor response relies on the surface reaction between adsorbed oxygen and combustible gases, so the amount of oxygen adsorbed strongly affect sensor response. Yamazoe et al. proposed a theoretical approach for estimating sensor response and suggested the following equation to represent the hydrogen response ³⁰:

$$
S2 = (Ra/Rg)2 = (3c/aNd) \cdot PH2 + const.
$$
 (3)

Here $c = k_2/k_1$ is the constant, k_2 is the rate constant of forward reaction of equation (2), *k-1* is the rate constant of the reverse reaction of equation (1), a is the crystal radius, N_d is the donor density of $SnO₂$, and P_{H2} is the partial pressure of hydrogen. According to this equation, reduction of donor density and crystallite size enhances sensor response to H_2 . We have confirmed experimentally that the equation holds true for donor density reduction 26 . However, in the case of Al-SnO₂, there was a reduction in not only the donor density but also the oxygen adsorption amount. According to the equation, these two factors should have an opposite influence on the sensor response.

The temperature dependence of the sensor response to 200 ppm of H_2 , 200 ppm of CO, and 100 ppm of C_2H_5OH in a dry atmosphere is shown in Fig. 6a, b, and c, respectively. In response to H_2 and CO, the sensor response using bare-SnO₂

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nanoparticles went through a maximum at 300 °C. Such volcano-shaped behaviour is typical of a $SnO₂$ sensor and can be explained theoretically by the surface reactions and gas diffusion of $SnO₂$ ³¹. Al-SnO₂ and Al₂O₃-SnO₂ showed a high sensor response at 250 °C even though Al and Al_2O_3 are not strong catalytic materials for surface reactions. The surface combustion reaction makes byproducts H_2O and CO_2 , and these byproducts are adsorbed on the oxygen adsorption site and inhibit oxygen re-adsorption. Accordingly, the sensor response is further increased. At an optimum temperature, the surface reaction activity, gas diffusion, and adsorption/desorption of byproducts are balanced to give the highest possible sensor response. The adsorption capability of the byproducts was probably higher for Al-SnO₂ and Al_2O_3 -SnO₂ than bare-SnO₂ at lower temperatures. The maximum sensor response to H_2 and CO of bare-SnO₂ was higher than to AI -SnO₂ and AI ₂O₃-SnO₂. As mentioned above, the sensor response is related not only to the oxygen adsorption amount but also to the crystallite size and donor density. In both the sensor responses of bare- $SnO₂$ and Al-SnO₂, the oxygen adsorption amount had more effect on the sensor response than the donor density. Thus, the reduced sensor response to $AI-SnO_2$ and $AI_2O_3-SnO_2$ was mainly attributed to the reduction of oxygen adsorption sites on the particle surface. The sensor response to C_2H_5OH , as shown in Fig. 6c, went through a maximum at 250° C for all the nanoparticles. The response of bare- $SnO₂$ to $C₂H₅OH$ was higher than that of $Al-SnO_2$ and $Al_2O_3-SnO_2$. The pore diameter of $Al_2O_3-SnO_2$ was larger than bare-SnO₂ (Fig. 3a), and the Al_2O_3 -Sn O_2 sensing layer was loosely packed. According to previous research, a porous sensing layer should give a higher sensor response to C_2H_5OH than densely packed sensing layer $5,32,33$. However, our sensor response to C_2H_5OH corresponded well with the oxygen adsorption amount. Zeng et al. suggested that C_2H_5OH rapidly reacts with adsorbed oxygen after adsorption and dissociation of the OH, as described in following equation 33 :

$$
C_2H_5OH_{ads} + O_{ads} \rightarrow CH_3CHO + H_2O + e^{\cdot \cdot \cdot} \tag{4}
$$

According to the result shown in Fig. 5c, the $SnO₂$ surface has a high affinity to hydroxyls at 250° C. Thus, the hydrophilic surface of $SnO₂$ is very effective for $C₂H₅OH$ sensing because of a reaction (Equation 4) occurring at low operating temperatures. Additionally, the C_2H_5OH combustion reaction consumes the adsorbed oxygen by successive reactions, as described in previous reports using $Pt/Rh/SnO₂$ ⁷ and Sc/In₂O₃ ³⁴. Although they suggested various pathways for the combustion reaction, the clear root of the surface reaction on the bare- $SnO₂$ is still not clear. Nevertheless, such successive reactions enhance the sensor response to C_2H_5OH , and our $SnO₂$ sensors were more sensitive to $C₂H₅OH$ than to $H₂$ and CO. Therefore, increasing the oxygen adsorption amount is important to enhance the sensor response by accelerating the combustion reaction. Additionally, the sensor response to C_2H_5OH is much higher than that of various SnO_2 based semiconductor gas sensors in the literature $4-6,32,33$.

Fig. 6 The sensor response to (a) 200 ppm H_2 , (b) 200 ppm CO, and (c) 100 ppm C_2H_5OH in dry atmosphere as a function of operating temperature using (\bullet) bare-SnO₂ nanoparticles, (\blacktriangle) Al-doped SnO₂ nanoparticles, and (∇) Al₂O₃-loaded SnO₂ nanoparticles.

Figure 7a–c shows the temperature dependence of the sensor response to H_2 and CO (200 ppm) and C_2H_5OH (100 ppm) in a humid atmosphere (45 % R.H. at 25 $^{\circ}$ C). The sensor responses deteriorated significantly compared with that in a dry atmosphere because of hydroxyl poisoning. The sensor responses to H_2 and CO increased with temperature in all the materials. Increasing the temperature leads to desorption of hydroxyls, resulting in an increase of adsorbed oxygen. Accordingly, the surface reaction rate increases with temperature. For C_2H_5OH , the response went through a maximum at 300 °C because C_2H_5OH is reactive at a lower temperature than H_2 and CO, similar to that observed in the dry atmosphere. This result indicates that the amount of residual adsorbed oxygen at 300 $^{\circ}$ C is more effective than that at 350 $^{\circ}$ C. Amazingly, bare-SnO₂ shows almost no sensitivity to the target gases at 250 and 300 °C because of its high affinity to hydroxyls. This lack of sensitivity indicates that almost no adsorbed oxygen exists on the particle surface. Most importantly, the sensor response using $AI-SnO₂$ and $AI₂O₃$ - $SnO₂$ nanoparticles was higher than bare- $SnO₂$ nanoparticles for all of the target gases. Such a high sensor response implies a large amount of oxygen adsorption. Hence, these results indicate that Al and Al_2O_3 inhibit hydroxyl poisoning on the oxygen adsorption site. This phenomenon is well explained by the humidity-interference effect and the introduction of a hydroxyl absorber on the $SnO₂$ nanoparticles, as described earlier for NiO-doped $SnO₂$ ²¹. Al and $Al₂O₃$ act as a water vapour absorber on the $SnO₂$ surface. Additionally, the sensor response to H_2 and CO in a humid atmosphere using Al-SnO₂ nanoparticles is comparable with that of Pd-loaded SnO_2 ²⁰ and NiO-doped SnO₂²¹ gas sensors, respectively. For C₂H₅OH, the sensor response using $AI\text{-}SnO₂$ nanoparticles is higher than that of porous SnO_2 gas sensors 35,36 , even though the humidity of these measurement is lower than our measurement. The sensor responses to C_2H_5OH using Al-SnO₂ nanoparticles were 2.7 times higher than that of AI_2O_3 -SnO₂ nanoparticles at 300 °C, respectively. The crystallite size and specific surface area of Al2O³ -SnO² were not suitable for obtaining a high sensor response. Additionally, we believe that Al in $AI-SnO₂$ is more highly dispersed in Al_2O_3 in $Al_2O_3-SnO_2$ because of the aggregation of Al₂O₃ (Fig. 4). Hence, highly dispersed Al

effectively absorbs hydroxyls and accelerates oxygen adsorption on the $SnO₂$ surface. Thus, the sensor response to combustible gases in a humid atmosphere was enhanced.

Fig. 7 The sensor response to (a) 200 ppm H_2 , (b) 200 ppm CO, and (c) 100 ppm C_2H_5OH in humid atmosphere (45 % R.H. at 25 $\rm ^{o}$ C) as a function of operating temperature using (\bullet) bare-SnO₂ nanoparticles, (\triangle) Al-doped SnO₂ nanoparticles, and (\triangledown) Al₂O₃loaded SnO₂ nanoparticles.

Figure 8 shows the sensor response to C_2H_5OH as a function of C_2H_5OH concentration at 300 °C in a humid atmosphere (45% R.H. at 25 °C) using bare-SnO₂, Al-SnO₂, and $Al_2O_3-SnO_2$ nanoparticles. The sensor responses were clearly proportional to the C_2H_5OH concentration. According to the extrapolation line, it can be expected that $AI-SnO₂$ nanoparticles detect less than one ppm C_2H_5OH in a humid atmosphere. We believe that optimizing the Al doping amount would give SnO₂-based materials a more sensitive surface in a humid atmosphere.

Fig. 8 The C_2H_5OH concentration dependence of the sensor response at 300 °C in humid atmosphere, using (\bullet) bare-SnO₂ nanoparticles, (\triangle) Al-doped SnO₂ nanoparticles, and (\triangledown) Al₂O₃loaded SnO₂ nanoparticles.

Conclusions

We have successfully developed highly sensitive, surfacemodified $SnO₂$ nanoparticles incorporating Al and $Al₂O₃$ that demonstrate resistance to humidity. Spherical bare-SnO₂, Al- $SnO₂$, and $Al₂O₃$ -SnO₂ nanoparticles were prepared using conventional methods. XRD, TEM, surface analysis, and SEM suggest that the bare-SnO₂ nanoparticle and $AI-SnO₂$ nanoparticle are similar in size while the Al_2O_3 -SnO₂ is larger.

The amount of oxygen adsorbed by bare- $SnO₂$ was clearly greater than that adsorbed by $AI-SnO_2$ and $Al_2O_3-SnO_2$, as confirmed by O_2 -TPD measurement. Bare-Sn O_2 adsorbed more oxygen because it has a high affinity to oxygen ions. In addition, the dispersity of Al in $AI-SnO₂$ was higher than that of Al_2O_3 in Al_2O_3 -SnO₂. The sensor responses to combustible gases using $Al-SnO₂$ and $Al₂O₃-SnO₂$ were lower than bare- $SnO₂$ in a dry atmosphere because incorporating Al reduces the combustion reaction rate with adsorbed oxygen. Conversely, in a humid atmosphere, the response to combustible gases using $Al-SnO₂$ was approximately five to ten times larger than bare-SnO₂. Al₂O₃-SnO₂ also showed a higher sensor response to combustible gases than bare- $SnO₂$. These results indicate that Al and Al_2O_3 inhibit hydroxyl poisoning of SnO_2 nanoparticles by working as hydroxyl absorbers and producing an oxygen adsorption site around them. The Al doping process dispersed Al in SnO₂ nanoparticles discretely, leading to an effective surface for combustion reactions in a humid atmosphere. Additionally, it was expected that $Al-SnO₂$ can detect $C₂H₅OH$ at ppb levels in a humid atmosphere. Therefore, Al doping offers a better surface for combustible gas sensors in a humid atmosphere. These results suggest surface modification as a possible improvement for material design. We believe that further modification of Al-SnO₂, such as morphological regulation and catalytic addition, would create attractive materials for humidity-tolerant semiconductor gas sensors. Therefore, further development of these materials will enable development of the high performance gas sensors with resistance to poisoning gases and more compact gas sensors than are currently available.

Acknowledgment

This work was supported in part by the FIST Foundation for Interaction in Science & Technology, Japan.

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