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1 Etching synthesis of iron oxide nanoparticles for adsorption of arsenic from water

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3 Wei Cheng, Weidong Zhang, Lijuan Hu, Wei Ding, Feng Wu and Jinjun Li*

4 School of Resources and Environmental Sciences, Hubei Key Lab of Bioresources and
5 Environmental Biotechnologies, Wuhan University, Wuhan 430079, China

6 **Corresponding Author*

7 *Tel.: +86 27 68778511. E-mail: ljcbacademy@163.com*

8 *Present address: Wuhan University, No. 129, Luoyu Road, Wuhan, 430079, P. R. China*

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12 *(PZC) of nano-iron oxide, As(III) and As(V) speciation for various pH values, Influence of*
13 *initial H₂O₂ concentration on As(III) removal. See DOI:10.1039/x0xx00000x*

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1 **Abstract**

2 Arsenic contamination in source drinking water has become an alarming issue worldwide. Iron oxides have
3 been recognized as effective adsorbents for arsenic removal. In this study, an etching method was used to
4 synthesize nanosized iron oxide with small primary particle sizes of approximately 4 nm and a high specific
5 surface area of 317 m²/g. The material was used as an adsorbent for arsenic removal from water. The sorption
6 isotherms fit the Langmuir equation, and the derived maximum sorption capability for As(III) and As(V) is 42
7 mg/g at pH 7 and 83 mg/g at pH 3, respectively. Arsenic adsorption obeys pseudo-second-order kinetics. The
8 adsorption sites were located mostly on the external nanoparticle surface, and therefore intraparticle
9 diffusion resistance was avoided and external diffusion was the rate-limiting step. The mechanism of arsenic
10 removal on nanosized iron oxide is chemisorption via inner-sphere surface complexation, and the hydroxyl
11 groups of arsenic species are important for reaction with adsorbent surface hydroxyl groups. Adsorption of
12 As(III) in the presence of hydrogen peroxide and ferrous ion was also studied, and the catalytic oxidation of
13 As(III) promoted its adsorptive removal significantly.

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1. Introduction

Arsenic contamination has become an alarming issue worldwide because of its high toxicity and carcinogenicity.¹⁻³ Chronic exposure to arsenic may cause tumors in the liver, lung, kidney, bladder, skin, and various human tissues; lead to cardio vascular system problems; and impede the mental development of children.⁴⁻⁶ The World Health Organization has lowered the limit of arsenic concentration in drinking water from 50 to 10 $\mu\text{g/L}$.^{2,7} Toxicity, mobility, and bioavailability of arsenic is related to its chemical speciation, oxidation state, and solution pH.⁷⁻⁹ In natural water, arsenic exists mainly as inorganic arsenate As(V) and arsenite As(III).¹ As(V) predominates in oxidizing conditions and is present mainly as H_3AsO_4 ($\text{pH} < 2.2$), H_2AsO_4^- ($2.2 < \text{pH} < 7$), HAsO_4^{2-} ($7 < \text{pH} < 11.5$), and AsO_4^{3-} ($\text{pH} > 11.5$).^{1,4} As(III) is the major arsenic species under reducing conditions and is present mainly as neutral H_3AsO_3 ($\text{pH} < 9.2$), H_2AsO_3^- ($9.2 < \text{pH} < 12$), and $\text{H}_2\text{AsO}_3^{2-}$ ($\text{pH} > 12$).^{1,3}

Adsorption is one of the most promising techniques for arsenic removal from water,¹⁰ and iron oxide is used extensively as an adsorbent because of its high affinity toward arsenic and low cost.^{2,11-13} Nanosized iron oxides are desirable for adsorption applications because of their large surface areas.¹⁴ Various methods such as solvothermal reduction^{11,15} and thermal decomposition^{14,16-18} have been applied in recent years to produce iron oxide nanoparticles. Solvothermal reduction usually involves thermal treatment of ferric salts and organic reducing agents in organic solvents.^{11,15} Thermal decomposition involves the decomposition of iron precursors, such as long-chain iron carboxylates,¹⁶ iron acetylacetonate¹⁷ or iron pentacarbonyl $\text{Fe}(\text{CO})_5$ ^{14,18} in a high-boiling-point organic solvent. These processes are complicated and high-cost, and usually involve toxic organics.¹⁹ Because of these disadvantages, intensive research is underway to introduce new procedures for the synthesis of iron oxide adsorbents.

As(III) is considered to be more toxic and harder to remove by adsorption than As(V).^{20,21} An oxidation step is often used to convert As(III) to As(V) prior to adsorption. As(III) oxidation can be achieved through photocatalytic reaction on TiO_2 ^{22,23} or reactions with oxidizing agents such as manganese oxide.²⁴ Önnby et al.²⁵ found that inorganic As(III) can be oxidized by H_2O_2 on Al_2O_3 via a surface-catalyzed mechanism. Fenton oxidation as a wastewater treatment technology has generated significant interest. A homogeneous Fenton reaction using ferrous ion has problems of iron ion release and iron sludge production.²⁶ These drawbacks can be overcome by introducing heterogeneous Fenton catalysts. Pham et al.²⁷ found that silica-supported iron oxide catalyzed the decomposition of H_2O_2 into oxidants capable of transforming phenol

1 at ~pH 3–10. Chun et al.²⁶ synthesized a magnetite-loaded mesocellular carbonaceous material and found that
2 such material exhibits superior activity as both Fenton catalyst and adsorbent for phenol and arsenic removal.
3 To the best of our knowledge, few studies have used pure iron oxide as both Fenton catalyst and adsorbent for
4 arsenic removal.

5 Recently, we synthesized mesoporous Fe–Si oxide composites using Pluronic P123 as porosity-generating
6 template, and found that the precursors of silica and iron oxide copolymerized to form a homogeneous
7 structure with high iron content.²⁸ In this paper, we will show that a Fe–Si binary oxide composite could be
8 prepared without using an organic template that may be costly, and silica units in the composite could be
9 etched further by alkali to leave nanosized iron oxide. The main objective of this work was to study the
10 adsorption of As(III) and As(V) on nanosized iron oxide and the catalytic oxidation-promoted adsorption of
11 As(III) in the presence of H₂O₂.

12 **2. Materials and methods**

13 **2.1. Chemicals**

14 Iron nitrate nonahydrate, sodium carbonate, and tetraethyl orthosilicate (TEOS) were from Sinopharm
15 Chemical Reagent Company Limited, Shanghai, China. Sodium arsenite (NaAsO₂) and sodium arsenate
16 (Na₂HAsO₄·7H₂O) were from Yikeda Chemical Reagent Corporation, Chengdu, China. All reagents were of
17 analytical grade.

18 **2.2. Sample preparation**

19 In a typical synthesis, Fe(NO₃)₃·9H₂O (0.016 mol) was dissolved in 150 mL of ultrapure water. Na₂CO₃
20 (0.016 mol) was added under vigorous stirring to promote the partial hydrolysis of iron ions. TEOS (0.04
21 mmol) was added to this resultant colloidal dispersion of iron oxide precursors. The solution was stirred
22 continuously at 40°C in a water bath for 1 day to hydrolyze TEOS, forming silica precursors and initially
23 copolymerizing with the iron oxide precursors. The solution was transferred to a Teflon-lined stainless steel
24 autoclave and heated at 100°C in an oven for 1 day to achieve further copolymerization. The solid was
25 collected by suction filtration and washed with 1000 mL of ultrapure water, dried at 100°C and calcined at
26 550°C for 6 h to form a composite of Fe–Si oxide. The composite was immersed in 200 mL of 1 M NaOH at
27 80°C for 8 h with stirring to remove the silica species. The resultant iron oxide product was labeled nano-iron
28 oxide.

2.3. Materials characterization

X-ray diffraction patterns were collected on a X'Pert Pro X-ray diffractometer (PANalytical, Netherlands) with Cu-K α radiation ($\gamma = 1.5406 \text{ \AA}$). Transmission electron microscopy (TEM) images were taken on a JEM-2100 (JEOL, Japan) with an acceleration voltage of 200 kV. Brunauer–Emmett–Teller specific surface area (S_{BET}) was determined using a V-sorb 2800P surface area analyzer (Gold APP, China). Microscopic examinations were performed using a S-3400N scanning electron microscope (HITACHI, Japan) equipped with an energy-dispersive spectrometry microanalyzer. In order to get the point of zero charge (pH_{PZC}) of the material, 10 mL of 0.1 M NaCl solution was taken in different vials and adjusted the initial pH in the range of 4-12 with hydrochloric acid and sodium hydroxide, then 4 mg of the material was added to each vial and these vials were placed on a platform shaker for 24 h at 25°C to reach equilibrium and then the final pH of the suspension was measured, and plot the curve of the difference between initial and final pH vs initial pH, the point at which the curve crossed the pH axis determined the pH_{PZC} of the sorbent.^{29,30}

2.4. Batch adsorption experiments

NaAsO₂ and Na₂HAsO₄·7H₂O were used as As(III) and As(V) sources, respectively. In the adsorption experiment, 10 mL of arsenic solution of a certain concentration was transferred to a 25 mL vial that contained 4 mg of adsorbent. These vials were sealed and shaken continuously on a platform shaker at 250 rpm and 25°C for 12 h to reach adsorption equilibrium. The suspension was centrifuged and the equilibrium concentrations of arsenic in the supernatant solutions were measured using an 8220 atomic fluorescence spectrophotometer (Beijing Jitian Instrument Company, China) with a total lamp current of 80 mA. High-purity argon was used as carrier and shielding gas (supplied at 300 and 800 mL/min, respectively). To detect the arsenic concentration of the arsenate solutions, a solution of ascorbic acid and thiourea was used to reduce the As(V) to As(III) prior to detection. The quantity of adsorbed arsenic at equilibrium (q_e , mg/g) was calculated as follows:

$$q_e = \frac{(C_0 - C_e) V}{m} \quad (1)$$

where C_0 (mg/L) and C_e (mg/L) represent the initial and equilibrium arsenic concentrations in solution, respectively; m (mg) is the mass of adsorbent used; and V (mL) is the solution volume.

The effect of pH on arsenic removal efficiency was evaluated by adjusting arsenic solution from pH 1 to 12 using HCl and NaOH.

The adsorption isotherms of As(III) at pH 7 and As(V) at pH 3 were obtained by varying the initial arsenic concentration from 1–100 mg/L.

1 Adsorption kinetic studies were conducted by varying the adsorption time from 1 to 240 min at an initial
2 arsenic concentration of 10 mg/L. The As(III) solution was kept at pH 7, and the As(V) solution was kept at
3 pH 3.

4 The influence of various competing ions, including HCO_3^- , SiO_3^- , SO_4^{2-} , HPO_4^- , Cl^- , F^- , and NO_3^- , on
5 arsenic removal was assessed. The concentration of each competing ion was 1 mmol/L. The initial arsenic
6 concentration was 1 mg/L (0.013 mmol/L) and As(III) and As(V) solutions were kept at pH 7 and pH 3,
7 respectively.

8 Every batch experiment was repeated three times and average values were used for analysis.

9 **2.5. Regeneration studies**

10 To evaluate the reusability, the adsorbent were first loaded with As(III) or As(V) by stirring the suspension for
11 12 h with an initial arsenic concentration of 1 mg/L and with an adsorbent dosage of 0.4 g/L. After adsorption,
12 the spent adsorbent was stirred with 1 M NaOH solution for 3 h, during which As anions could desorb from the
13 nano-iron oxide nanoparticle surface through hydroxyl exchange and electrostatic repulsion. The adsorbent
14 was collected by centrifugation, washed with ultrapure water, and dried in air at 100°C for the next cycle of
15 use.

16 **2.6. Catalytic oxidation-promoted adsorption of As(III)**

17 Catalytic oxidation of As(III) in the presence of H_2O_2 was used to promote its adsorption. The effects of
18 H_2O_2 concentration and pH were studied. The H_2O_2 concentration varied from 150–600 μM , and the solution
19 acidity varied from pH 3 to 9. The dynamics of As(III) removal in the presence of 300 μM H_2O_2 was also
20 studied. Nano-iron oxide (80 mg) was added to 200 mL of the 10 mg/L As(III) solution with stirring. The
21 solution was sampled and the residual As(III) concentrations were analyzed after a specified time interval.
22 Experiments were also conducted without H_2O_2 addition.

23 **3. Results and discussion**

24 **3.1. Properties of adsorbents**

25 Energy-dispersive spectrometry analysis revealed that the atomic Si/Fe ratio of the as-prepared composite
26 before alkali-etching is 2.8, whereas that of nano-iron oxide is only 0.1 (Fig. S1†), which indicates that
27 alkali-etching can dissolve silicon and leave iron oxide.

28 A typical TEM image of the prepared material indicates the presence of nanoparticles of less than 4 nm
29 (Fig. 1). The X-ray diffraction pattern shows extremely weak diffraction peaks (Fig. S2†), which also

1 indicates that the material is composed of very small particles. On the whole, the weak diffraction peaks
2 could be assigned to α -Fe₂O₃ (JCPDS No. 33-0664) and hydrous iron oxide FeO(OH) (JCPDS No.22-0353).
3 Fig. 2 shows the Fe 2p XPS spectrum of the material. The Fe 2p_{2/3} peaks at 710.7 and 712.6 eV are attributed
4 to Fe³⁺ bonded with O²⁻ in the crystal lattice of α -Fe₂O₃ and with -OH in FeO(OH), respectively.^{31,32,33} The
5 Fe 2p_{1/2} peaks at 724.2 and 725.8 eV may be assigned to α -Fe₂O₃ and FeO(OH), respectively.^{31,33} Therefore,
6 the XPS spectra also indicate that the material is a composite of α -Fe₂O₃ and FeO(OH). For the sake of
7 simplicity, the composite of α -Fe₂O₃ and FeO(OH) is termed as nano-iron oxide in this work. A nitrogen
8 adsorption-desorption isotherm of the nano-iron oxide is used to derive the textural properties. The isotherm
9 features a hysteresis loop (Fig. S3†), which suggests the presence of mesopores in the samples.³⁴ The BJH
10 pore size distribution profile shows that the mesopore pore size is centered at ca. 3.5 nm. The mesopores
11 may consist of voids between the aggregated primary particles as revealed by the TEM images. It is
12 interesting that the derived specific surface area of nano-iron oxide is 317 m²/g, which is high compared with
13 reported data. Analysis of the nitrogen sorption data by the t-plot method indicates that nano-iron oxide has a
14 small internal surface area of 26 m²/g in contrast with its external surface area of 291 m²/g.

15 **3.2. Effect of pH on arsenic adsorption**

16 The pH values of arsenic solutions often influence arsenic removal. Fig. 3 shows the pH-dependence of
17 As(III) and As(V) removal efficiency at an initial arsenic concentration of 10 mg/L and an adsorbent dosage
18 of 0.4 g/L.

19 An optimal As(III) removal (~75%) was achieved at pH 6–8. A further increase in pH resulted in a sharp
20 decrease in removal efficiency, and the As(III) removal efficiency dropped to approximately 30% at pH 12.
21 The surface hydroxyl groups on the iron oxide can be protonated or deprotonated in solution depending on
22 pH.³⁵ Fig. S4† shows that the pHPZC of the nano-iron oxide is about 6.5. At pH values below the pHPZC, the
23 iron oxides would have positive surface charges because of surface hydroxyl group protonation, and above
24 the pHPZC, the reverse would occur. The pH value also determines the As(III) species structures as shown in
25 Fig. S5a†. As(III) is present mainly as neutral H₃AsO₃ below pH 9.2, and H₂AsO₃⁻ becomes dominant above
26 pH 9.2. The As(III) removal efficiencies under various acidities may indicate that neutral H₃AsO₃ molecules,
27 which exist below pH 9, could be captured more easily by iron oxide. Fe-OH and As-OH groups participate
28 in the adsorption reactions to form either inner- or outer-sphere complexes.³⁶ The adsorbent manifests the
29 highest As(III) removal efficiency at pH 6–8 possibly because, under such conditions, the iron oxide surface

1 has a large proportion of unaltered Fe–OH groups that favor reaction with the As–OH groups of H₃AsO₃
2 molecules. At other pH values that deviate from the pHPZC, protonation or deprotonation of Fe–OH groups
3 may disfavor the reaction with As–OH groups and decrease the sorption capacity. Above pH 9.2, electrostatic
4 repulsion may occur between dominant HAsO₃²⁻ species and the deprotonated negatively charged nano-iron
5 oxide surface, which hinders arsenic adsorption.

6 The As(V) removal efficiency was almost 100% at pH 2–4, it decreased gradually with increase in pH
7 from 4 to 10, and a large decrease in removal efficiency occurred with further increase in pH to 11. Fig.
8 S5b† shows the species variation of As(V) with pH. Neutral H₃AsO₄ molecules are dominant species in
9 solution only below pH 2, and they almost disappear above pH 4. From pH 2–12, As(V) is present mainly as
10 negative H₂AsO₄⁻, HAsO₄²⁻, and AsO₄³⁻, and higher pH values indicate that more hydroxyl groups on
11 H₃AsO₄ molecules dissociate to induce negative charges. In literature, it is suggested that at pH < 4.3,
12 positively charged adsorbent surfaces favor As(V) adsorption by electrostatic attraction between H₂AsO₄⁻
13 anions and surface –OH₂⁺.³⁷ It is not clear in this work why, from pH 8–10, the adsorbent surface is still
14 capable of removing more than 60% As(V) despite the repulsive forces between negatively charged
15 deprotonated surface and arsenic anions. We suggest that the As–OH groups also play an important role in
16 As(V) adsorption. At pH 2–4, dominant H₂AsO₄⁻ and H₃AsO₄ species that contain more As–OH groups
17 could be captured more easily by iron oxide. However, the dissociation of As–OH at higher pH hinders their
18 reaction with Fe–OH: for pH > 11, dominant AsO₄³⁻ species contain no As–OH groups, which results in a
19 very poor arsenate uptake.

20 3.3. Adsorption isotherms

21 Fig. 4a shows the adsorption isotherm of As(III) at pH 7 and that of As(V) at pH 3. Langmuir (Fig. 4b) and
22 Freundlich (Fig. 4c) models were used to fit the experimental data.

23 The Langmuir model is derived from the hypothesis that the adsorbent surface is homogeneous and
24 adsorbs only monolayer adsorbates without involving intermolecular forces.^{38,39} The mathematical linear
25 expressions of the Langmuir isotherm can be written as:

$$\frac{1}{Q_e} = \frac{1}{Q_m} + \frac{1}{bQ_m C_e} \quad (2)$$

26 where C_e (mg/L) is the equilibrium arsenic concentration, Q_e (mg/g) is the equilibrium adsorption capacity,
27 Q_m (mg/g) is the maximum sorption capacity, and b (L/mol) is the affinity of binding sites.

1 The Freundlich isotherm is derived by assuming a heterogeneous surface with a nonuniform distribution of
 2 the heat of sorption over the surface. Its linearized form can be expressed by the following formula:

$$\ln Q_e = \ln K_f + \frac{1}{n} \ln C_e \quad (3)$$

3 where C_e (mg/L) is the equilibrium concentration of arsenic, Q_e (mg/g) is the equilibrium adsorption capacity,
 4 and K_f (mg/g) and n are the Freundlich experimental constants related to the adsorption capacity and the
 5 adsorption intensity, respectively.

6 The isotherm parameters and correlation coefficients obtained by nonlinear regression analyses with both
 7 models are listed in Table 1. The correlation coefficients indicate that the As(III) and As(V) adsorption data
 8 could be better fitted into the Langmuir model than the Freundlich one. The maximum adsorption capacity
 9 derived from the Langmuir isotherms for As(III) and As(V) is 42 and 83 mg/g, respectively.

10 The adsorption capacities of the samples for As(III) and As(V) in this work were compared with other
 11 nanostructured iron oxide materials reported in literature as shown in Table 2. The results indicate that
 12 nano-iron oxide possesses a relatively high sorption capacity for As(III) and As(V).

13 3.4. Kinetics of arsenic adsorption

14 Fig. 5a shows the As(III) uptake at pH 7 and As(V) uptake at pH 3 with time on stream. The As(III)
 15 adsorption reached equilibrium in 120 min, whereas that of As(V) was reached in 50 min. This indicates that
 16 nano-iron oxide is more favorable for As(V) removal than As(III), which agrees with the sorption isotherm
 17 results.

18 The kinetics of As(III) and As(V) adsorption were evaluated using pseudo-first- and -second-order models.
 19 The pseudo-first-order model can be written as:⁴⁴

$$\ln(Q_e - Q_t) = \ln Q_e - k_1 t \quad (4)$$

20 The pseudo-second-order model that represents sorption processes controlled by chemical reaction can be
 21 expressed as follows:^{45,46}

$$\frac{t}{Q_t} = \frac{1}{k_2 Q_e^2} + \frac{1}{Q_e} t \quad (5)$$

22 The initial sorption rate h can be defined as:

$$h = k_2 Q_e^2 \quad (6)$$

1 In the two models, k_1 is the rate constant of pseudo-first-order adsorption and k_2 is that of
2 pseudo-second-order adsorption, Q_e is the equilibrium adsorption capacity, and Q_t is the amount of adsorbate
3 adsorbed at time t .

4 The fitted curves based on the two kinetic models are displayed in Fig. 5b and Fig. 5c, and kinetic
5 parameters calculated from experimental data are listed in Table 3. The correlation coefficients suggest that
6 the pseudo-second-order kinetic model fitted better for As(III) and As(V) adsorption, which indicates that
7 chemisorption took place during arsenic uptake onto nano-iron oxide.^{30,46-48} The initial sorption rate for As(V)
8 is approximately seven times faster than that for As(III) (Table 3), which also indicates that nano-iron oxide
9 has a better affinity for the former.

10 An intraparticle diffusion model^{30,49} was used to reveal the rate-determining step for arsenic adsorption.
11 The validity of this model is confirmed by linear plots of the Weber and Morris equation:

$$Q_t = k_p t^{0.5} + c \quad (7)$$

12 where Q_t is the amount of adsorbate adsorbed at time t , k_p is the intraparticle diffusion rate constant, and the
13 intercept c is associated with the boundary layer effect. If the plot of Q_t versus $t^{0.5}$ is linear and passes through
14 the origin, then intraparticle diffusion is the rate-limiting step, otherwise it is not the only rate-limiting
15 step.^{30,49} A larger intercept value c represents a greater boundary layer effect and a greater contribution of
16 boundary layer diffusion in the rate-controlling step.³⁰

17 Linear plots of the intraparticle diffusion model for arsenic are shown in Fig. 6a and the derived
18 parameters are shown in Table 4. Plots for As(III) and As(V) do not pass through the origin, which indicates
19 that intraparticle diffusions were not the only rate-limiting step.³⁰ In many reported works, linear plots of the
20 intraparticle diffusion model could be divided into three steps, namely, the first sharper portion that reflected
21 the external surface adsorption stage, where boundary layer diffusion of solute molecules was
22 rate-controlled, the second gradual portion that reflected the internal surface adsorption stage, where
23 intraparticle diffusion was rate-controlled, and the third horizontal portion that reflected the adsorption
24 equilibrium stage. In this work, only two steps are observed for As(III) and As(V) as shown in Fig. 6a. The
25 first sharper sections represent arsenic diffusion to the external adsorbent surface and occupation of the readily
26 available adsorption sites.²⁰ The second parts are horizontal, which indicates that equilibrium has been
27 reached. The intercept c for As(V) is greater than that for As(III), which suggests that a greater boundary
28 layer effect occurred in As(V) adsorption.³⁰ Because As(V) could be captured more easily by iron oxide, its

1 concentration in the boundary layer would be lower. Therefore, diffusion of As(V) from the bulk solution to
2 the particle surface would influence the adsorption rate more significantly.

3 General adsorbents often possess framework-confined pores and intraparticle surfaces. However, tiny iron
4 oxide nanoparticles possess dominant external surfaces instead of internal surfaces. Furthermore, the
5 nanoparticles can be well-dispersed in water and their surfaces are easily approachable. Because most
6 adsorption sites are located on the external surfaces of nano-iron oxide, intraparticle adsorption may be
7 negligible.

8 An external diffusion model⁵⁰ was also used to fit the experimental data before reaching equilibrium. This
9 model can be expressed as:

$$\ln \frac{C_t}{C_0} = -k_f \frac{A}{V} t \quad (8)$$

10 where C_0 , C_t , A/V , t , and k_f are the initial adsorbate concentration, concentration at time t , ratio of the
11 external sorption area to the total solution volume, sorption time, and external diffusion coefficient,
12 respectively. If the adsorption is controlled by external resistance, a plot of $\ln C_t/C_0$ versus t must be linear.

13 Linear plots of the external diffusion model for arsenic are shown in Fig. 6b and the derived parameters are
14 shown in Table 4. The plots for As(III) and As(V) pass through the origin, which indicates that the external
15 diffusions were the rate-limiting step in arsenic adsorption.

16 3.5. Effect of coexisting ions and ionic strength on As(III) and As(V) sorption

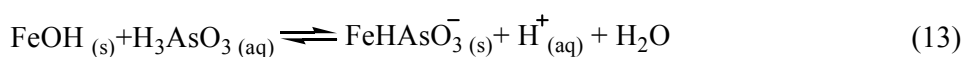
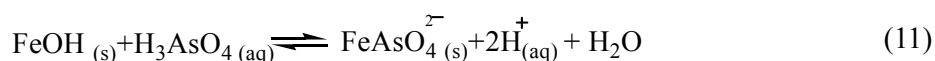
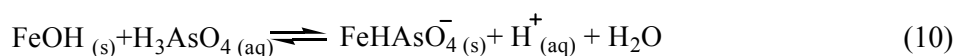
17 The competing effect induced by co-existing anions on arsenic removal was studied, and the results are
18 shown in Fig. 7a. Even though the concentration of competing ions (1 mmol/L) was much higher than that of
19 arsenic (0.013 mmol/L), the presence of HCO_3^- , SO_4^{2-} , Cl^- , F^- , and NO_3^- did not have any effect on arsenic
20 adsorption. In contrast, the presence of HPO_4^{2-} and SiO_3^{2-} showed some deterioration effect, especially for
21 HPO_4^{2-} . Silicate and hydrophosphate tend to retain multi-hydroxyl groups in aqueous system, and these
22 hydroxyl groups may compete with arsenic and react with surface groups on the adsorbent.⁵¹

23 The effect of ionic strength on As(III) and As(V) removal is shown in Fig. 7b. The arsenic removal
24 remained almost constant when the ionic strength increased from 0.001 M NaNO_3 to 0.1 M NaNO_3 , which
25 indicates that arsenic adsorption on nano-iron oxide is unaffected by change in ionic strength. Goldberg et al.³⁶
26 proposed that inner-sphere surface complexation could be a dominant process if the adsorption exhibits either
27 no ionic strength dependence or an increasing adsorption with increasing solution ionic strength. Outer-sphere

1 complexation could be dominant if the adsorption decreases with increasing ionic strength. According to this
 2 theory, the As(III) and As(V) adsorption onto nano-iron oxide is dominated by inner-sphere complexation.

3 **3.6. Mechanism of As(III) and As(V) removal**

4 Studies of adsorption kinetics and the effect of ionic strength suggest that arsenic removal on nano-iron oxide
 5 may be by chemisorption via inner-sphere surface complexation. Goldberg et al.³⁶ summarized the surface
 6 reactions for arsenic adsorption on oxides by inner-sphere surface complexation as follows:



7 In all cases, Fe–OH and As–OH groups participate in the adsorption reactions. Therefore it is not
 8 surprising that an improved arsenic removal efficiency was achieved when arsenic species and iron oxide
 9 contain more hydroxyl groups at suitable pH conditions as discussed previously. Previous researches have
 10 suggested that arsenic removal may depend on the surface density of hydroxyl groups on iron oxides, which
 11 can form complexes with arsenite and arsenate.⁵²⁻⁵⁴

12 Adsorbent X-ray photoelectron spectroscopy (XPS) spectra were recorded to reveal the adsorption
 13 mechanism. Fig. 8 shows a wide-scan XPS spectrum of the O 1s binding energies of the adsorbent before and
 14 after adsorbing arsenic. The O 1s spectrum can be divided into three component peaks with binding energies
 15 of ~530, ~531, and ~532 eV, which can be assigned to O in the form of metal oxide (M–O), hydroxyl group
 16 bonded to metal (M–OH) and adsorbed water (H₂O), respectively.⁵⁵⁻⁵⁷ After As(III) and As(V) adsorption, the
 17 relative ratios of M–OH decreased, which indicates that some surface hydroxyl groups were consumed in
 18 surface reactions. The relative ratios of M–O increased after adsorption, which could be attributed to the
 19 introduction of As–O after surface reactions. Therefore, the XPS spectra verified that the hydroxyl groups on
 20 nano-iron oxide reacted with those on arsenic species during adsorption, to form inner-sphere complexes.

21 **3.7. Regeneration studies**

22 For practical adsorbent use, a high efficiency of adsorbent regeneration and reusability is very important. In
 23 this work, the used adsorbent was regenerated in aqueous alkali solution. Fig. 9 shows the efficiency of

1 As(III) or As(V) removal by nano-iron oxide nanoparticles during five adsorption–regeneration cycles. The
2 removal efficiency after five cycles remained almost unchanged, which indicated that the adsorbent could be
3 easily regenerated and is promising for practical applications.

4 **3.8. Catalytic oxidation-promoted As(III) removal**

5 H₂O₂ was used to induce As(III) oxidation to promote its adsorptive removal. By varying H₂O₂
6 concentrations from 0 to 600 μM at pH 7, it was found that optimal As(III) removal was achieved at a H₂O₂
7 concentration of 300 μM (Fig. S6†). Above 300 μM, the As(III) removal efficiency no longer increased and
8 even showed a slight decrease because the higher-concentration H₂O₂ can scavenge •OH radicals.⁵⁸ Fig.10
9 shows the XPS spectra of the As 3d binding energies of the spent adsorbents. The As 3d binding energies for
10 As(III) and As(V) were reported to be 44.3–44.5 and 45.2–46.1 eV, respectively.^{59,60} In the absence of H₂O₂,
11 the As 3d binding energy of the spent adsorbent was 44.5 eV, indicating it is As(III). In the presence of 300
12 μM H₂O₂, it was shifted to 45.7 eV, indicating that As(III) was converted into As(V).

13 Fig. 11 shows the As(III) removal on nano-iron oxide with time on stream in the presence and absence of
14 300 μM H₂O₂ at various pH values. Within pH 3–9, the addition of H₂O₂ promoted As(III) removal, which
15 could be attributed to the simultaneous oxidation and adsorption of As(III). It should be mentioned that As(III)
16 oxidation in aqueous H₂O₂ solution without metal oxide is very slow and requires up to 30 d.⁶¹ In this work,
17 nano-iron oxide might catalyze fast As(III) oxidation, and it played a dual role of catalyst and adsorbent. At
18 pH 11, H₂O₂ actually declined the arsenic removal. As discussed previously, under highly alkaline
19 conditions, the severe dissociation of hydroxyl groups on As(V) species could hinder arsenic adsorption onto
20 iron oxide surfaces, and the As(V) uptake was even lower than As(III) at pH 11 (Fig. 3). Therefore, due to
21 conversion of As(III) to As(V) in the presence of H₂O₂, the arsenic removal declined at pH 11.

22 It is well known that Fe²⁺ is capable of catalyzing H₂O₂ decomposition to generate oxidative hydroxyl
23 radicals. We added Fe²⁺ to the nano-iron oxide and H₂O₂ system, and found that a higher As(III) removal rate
24 was achieved in the presence of 600 μM Fe²⁺ (Fig. 12). This indicates that H₂O₂ coupled with Fe²⁺ could
25 promote As(III) oxidation. Furthermore, spontaneous sedimentation of nano-iron oxide in water was slow,
26 most likely because of their small particle sizes and good dispersion in water; however, if Fe²⁺ were present,
27 sedimentation was more rapid and most likely because the ionic iron species could act as a flocculation
28 agent. This could be helpful in practical applications because adsorbent can be separated easily.

1 4. Conclusions

2 Nanosized iron oxide was prepared by an etching method and used as an adsorbent for effective As(III) and
3 As(V) removal from water. The nanosized iron oxide had a high specific surface area of 317 m²/g and primary
4 particle size of approximately 4 nm. Arsenic adsorptions were pH dependent, and pH 6–8 and 2–4 are most
5 favorable for As(III) and As(V) removal, respectively. As(III) and As(V) adsorption could be fitted well into
6 the Langmuir model, and the maximum adsorption capacity for As(III) and As(V) was 42 mg/g and 83 mg/g,
7 respectively. The adsorption kinetics obeyed a pseudo-second-order model and the rate-limiting step was
8 external diffusion. Phosphate and silicate anions decreased the arsenic removal to some extent, whereas other
9 co-existing anions and ionic strengths had no effect on arsenic removal. The mechanism of arsenic removal on
10 nano-iron oxide may be chemisorption via inner-sphere surface complexation, and hydroxyl groups on the
11 iron oxide and arsenic species were involved in adsorption. As(III) removal can be promoted by catalytic
12 oxidation in the presence of H₂O₂. The high arsenic uptake capability of nanosized iron oxide makes it a
13 potentially attractive adsorbent for arsenic removal from aqueous solution.

14 Acknowledgments

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16 the Natural Science Foundation of Hubei Province (2014CFB182).

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- 1 **List of tables**
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Table 1 Isotherm parameters for As(III) and As(V) adsorption

	Langmuir isotherm			Freundlich isotherm		
	Q_m (mg/g)	b (L/mg)	R^2	K_f (mg/g)	n	R^2
As(III)	42	0.4	0.9789	11.3	2.1	0.9214
As(V)	83	0.8	0.9989	28.6	3.1	0.8288

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Table 2 Arsenic adsorption capacity compared with other iron oxide materials

Adsorbents	Specific surface area (m ² /g)	Adsorption capacity (mg/g)		Initial As concentration (mg/L)		Ref.
		As(III)	As(V)	As(III)	As(V)	
Nano-iron oxide	317	42	83	1–100	1–100	This study
Fe ₃ O ₄ loaded PCL	–	32	28	10–80	10–80	1
Ultrafine α-Fe ₂ O ₃	162	95	47	0–200	0–200	11
γ-Fe ₂ O ₃ –TiO ₂	154	33	–	0.1–50	–	22
Fe ₃ O ₄ -silica	294	14.7	121	5–750	5–750	12
Magnetic wheat Straw	4.7	3.9	8.1	1–28	1–28	40
Resin/FeMn	48	13.5	14.5	5–150	5–200	20
Ascorbic acid-coated Fe ₃ O ₄	179	46.1	16.6	0–70	0–50	21
Ferrihydrite	202	526.4	219.3	20-2000	20-2000	41
Ferrihydrite	–	175.5	135.8	0-150	0-150	42
Zn-Fe-LDH	11.9	–	151.4	–	2-100	43

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Table 3 Kinetic parameters for arsenic adsorption

	Pseudo-first order			Pseudo-second order			
	k_1 (min ⁻¹)	Q_e (mg/g)	R ²	k_2 (g mg ⁻¹ min ⁻¹)	Q_e (mg/g)	h (mg g ⁻¹ min ⁻¹)	R ²
As(III)	0.018	11.0	0.9779	0.0036	19.5	1.4	0.9976
As(V)	0.073	15.2	0.9280	0.017	23.7	9.6	0.9993

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Table 4 Internal and external diffusion model parameters for arsenic adsorption

	Internal diffusion model			External diffusion model	
	k_p (mg g ⁻¹ min ^{-0.5})	C (mg g ⁻¹ min ^{-0.5})	R ²	k_f (cm/min)	R ²
As(III)	1.4	4.1	0.9889	5.8×10^{-5}	0.9922
As(V)	2.1	10	0.9733	1.6×10^{-5}	0.9907

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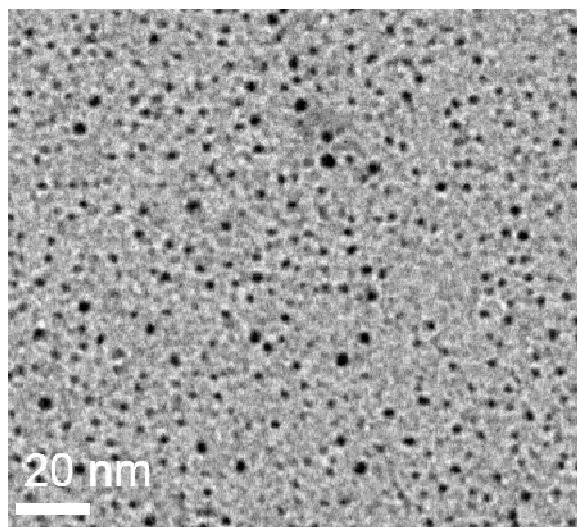
14 **Fig. 9** As(III) and As(V) removal efficiency on regenerated nano-iron oxide.

15 **Fig. 10** Wide-scan X-ray photoelectron spectroscopy spectra of the As 3d binding energies of
16 As(III)-adsorbed adsorbents (a) in the presence and (b) absence of H₂O₂.

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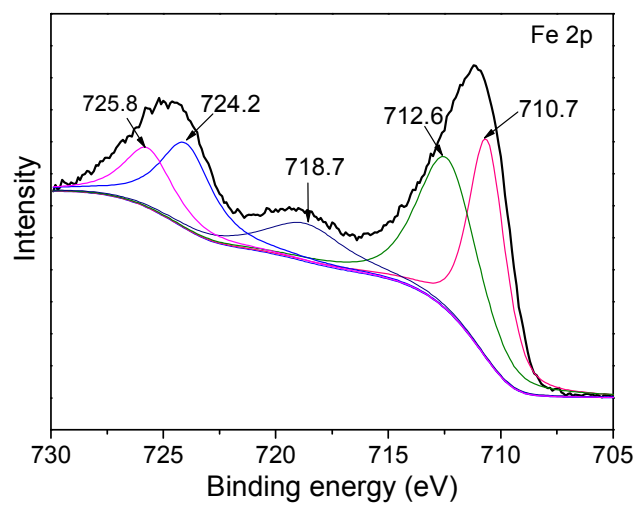
18 **Fig. 12** Change in total arsenic concentration with time on stream (pH 7, initial concentrations: As(III) = 10
19 mg/L, H₂O₂ = 300 μM, Fe²⁺ = 600 μM).

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Fig. 1 TEM image of nano-iron oxide.



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Fig. 2 Wide-scan X-ray photoelectron spectroscopy spectrum of the Fe 2p binding energies of nano-iron oxide.

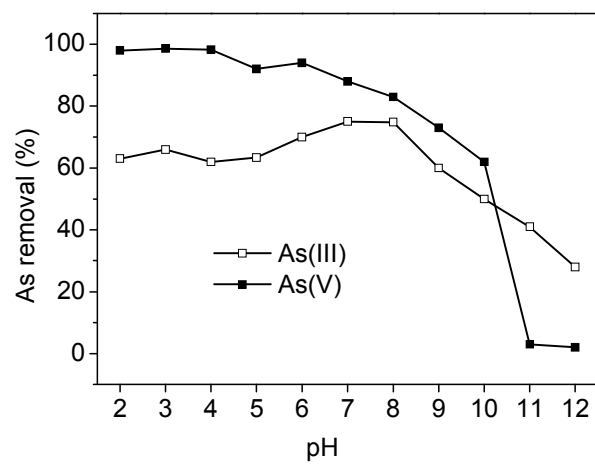
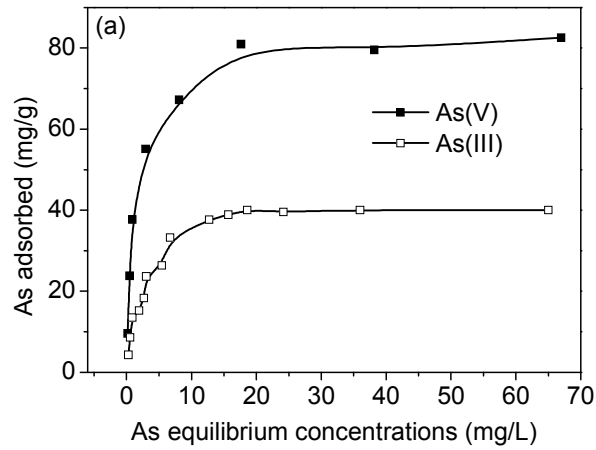


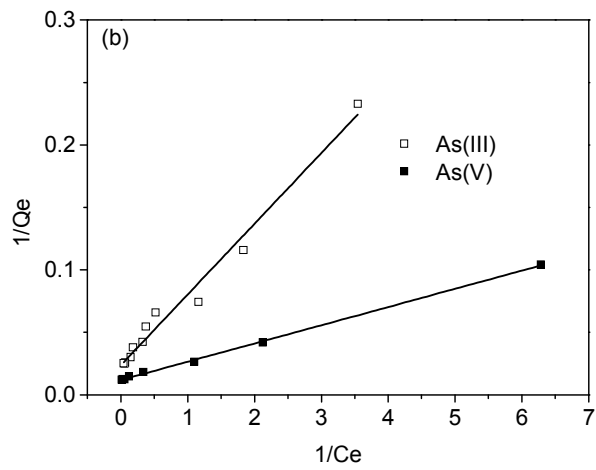
Fig. 3 Influence of pH on As(III) and As(V) adsorption.

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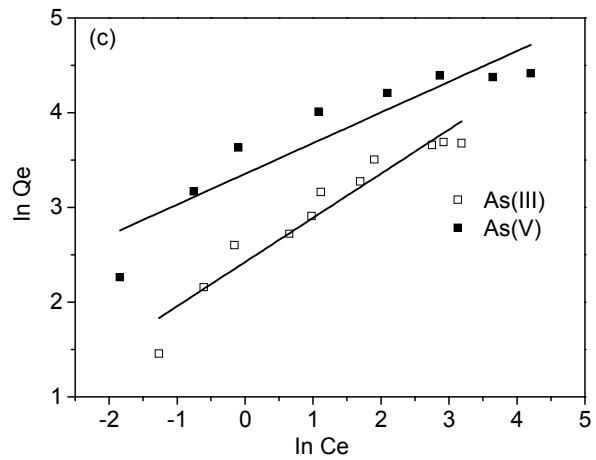
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5 **Fig. 4** (a) Arsenic adsorption isotherms at 25°C, (b) Langmuir isotherm plots, and (c) Freundlich isotherm
6 plots.

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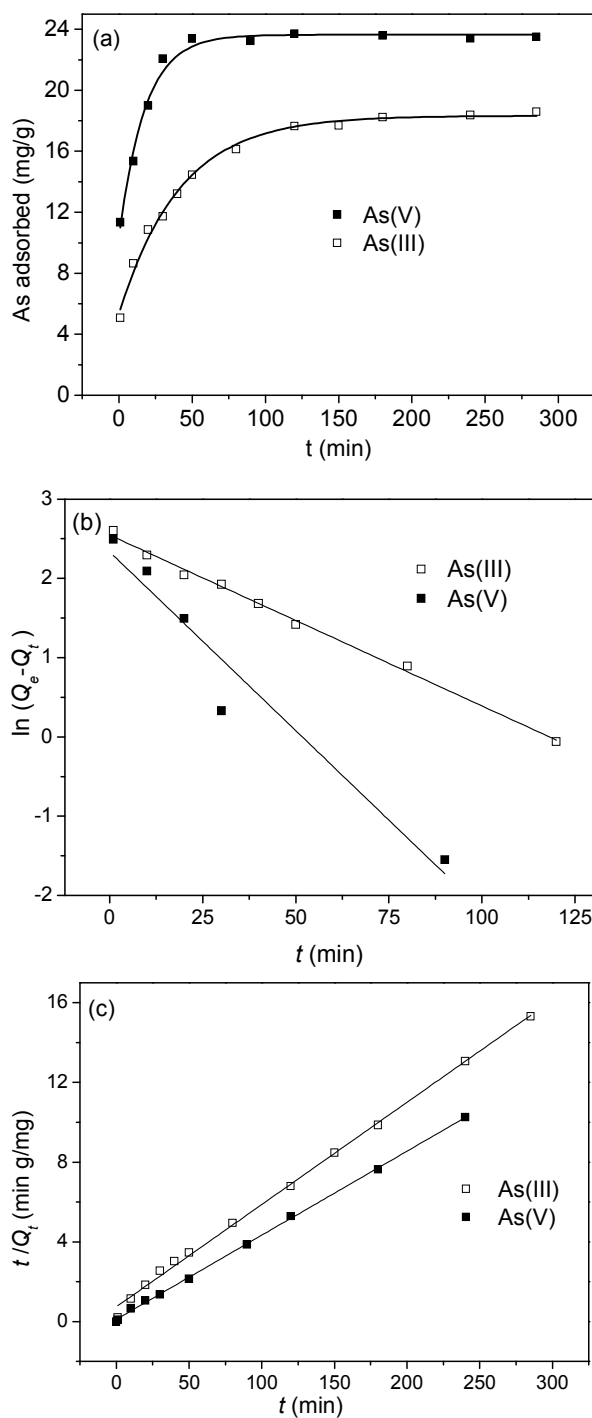


Fig. 5 Kinetics of arsenic adsorption: (a) arsenic uptake with time on stream, (b) pseudo-first-order kinetic model, and (c) pseudo-second-order kinetic model.

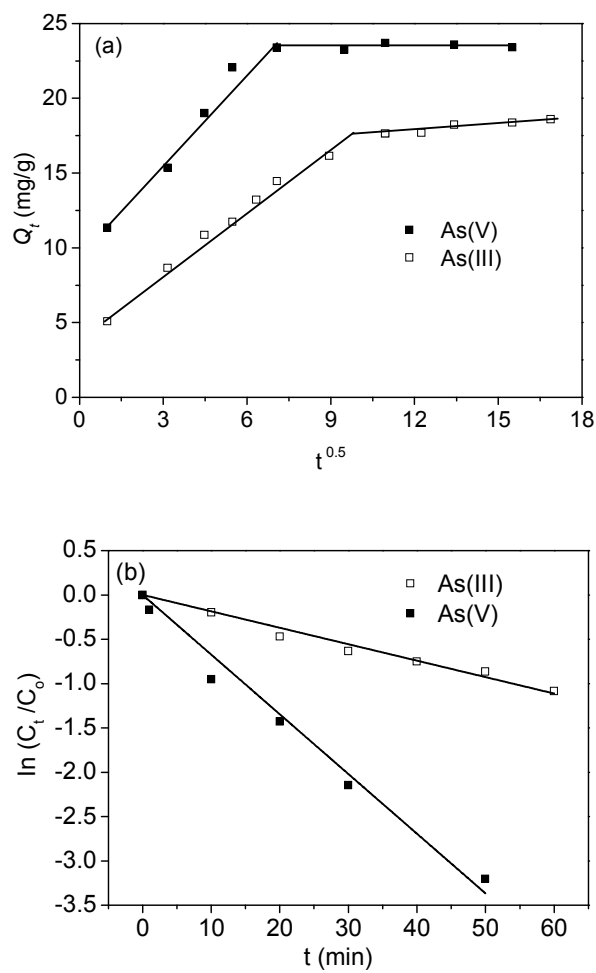
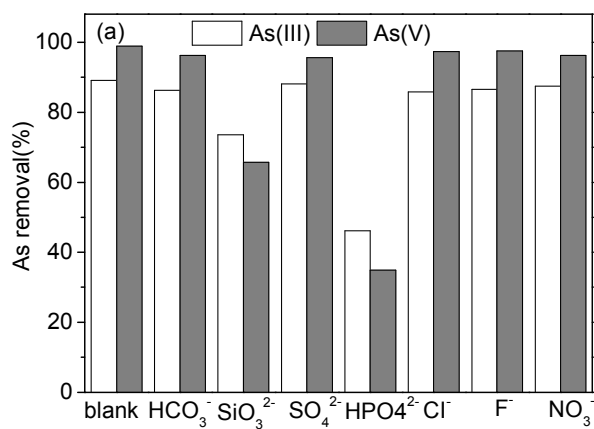


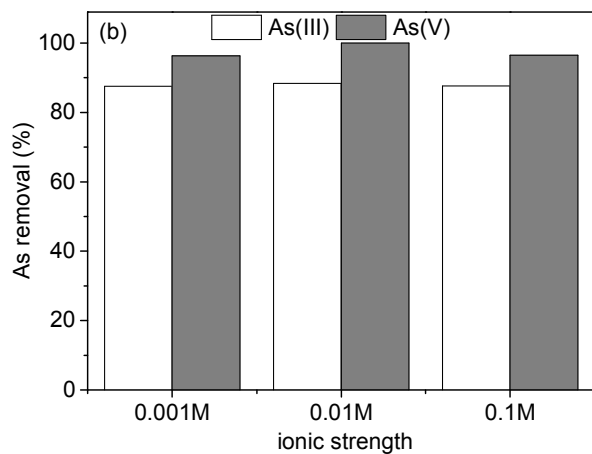
Fig. 6 (a) Intraparticle model and (b) external diffusion models.

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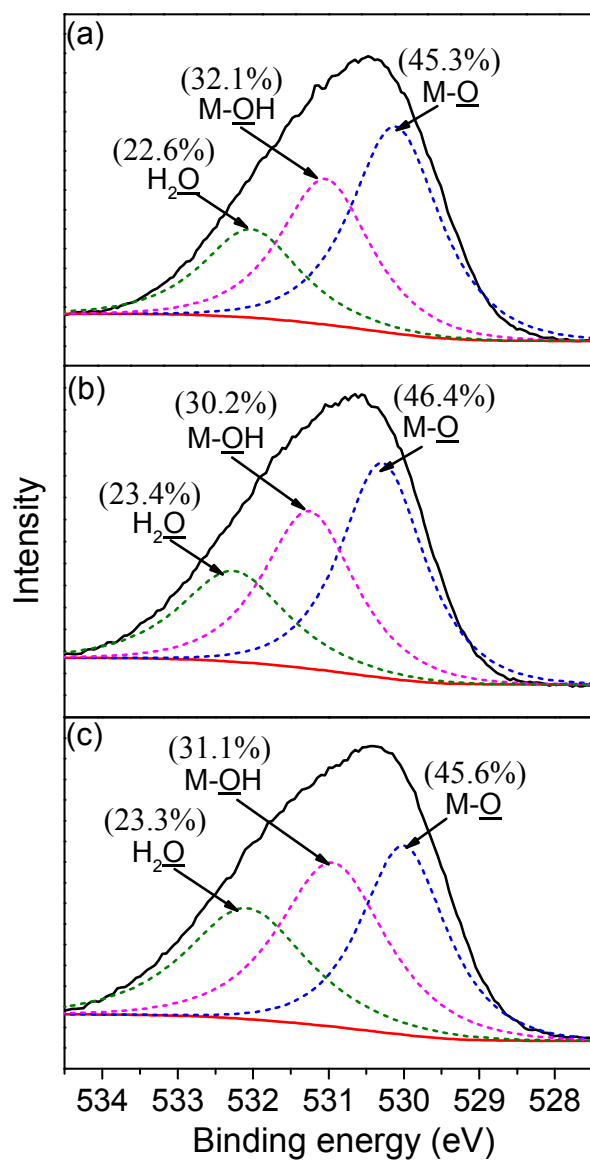
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Fig. 7 Effect of (a) coexisting ions and (b) ionic strength on As removal.

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3 **Fig. 8** Wide-scan X-ray photoelectron spectroscopy spectra of the O 1s binding energies of (a) fresh, (b)

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As(III)-adsorbed, and (c) As(V)-adsorbed adsorbent.

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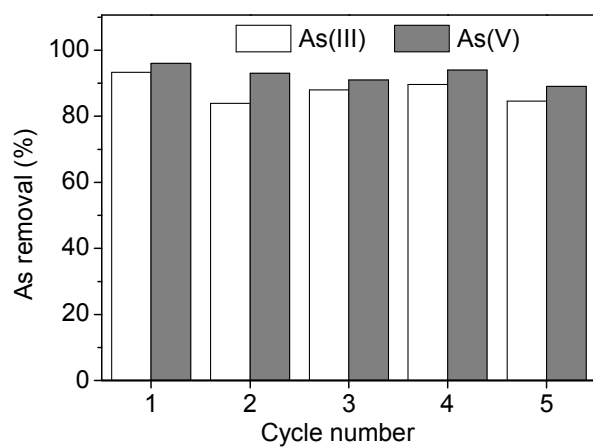
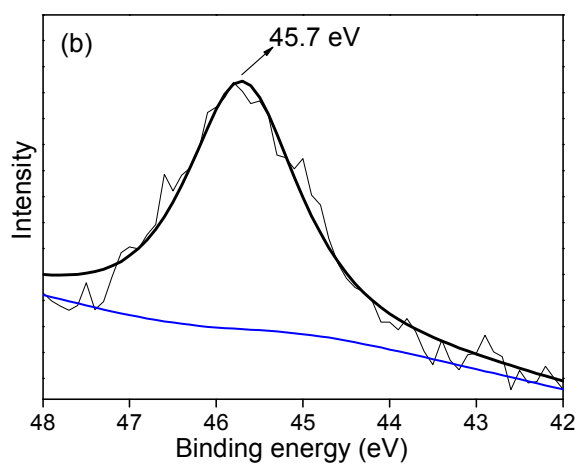
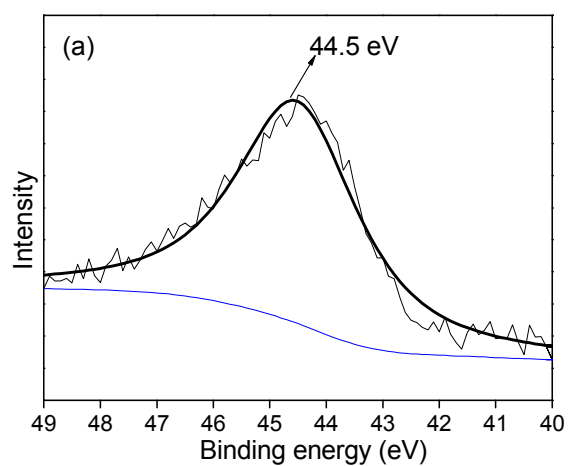


Fig. 9 As(III) and As(V) removal efficiency on regenerated nano-iron oxide.

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3 **Fig. 10** Wide-scan X-ray photoelectron spectroscopy spectra of the As 3d binding energies of the
4 adsorbent after adsorbing As(III) (a) in the presence and (b) absence of H₂O₂.

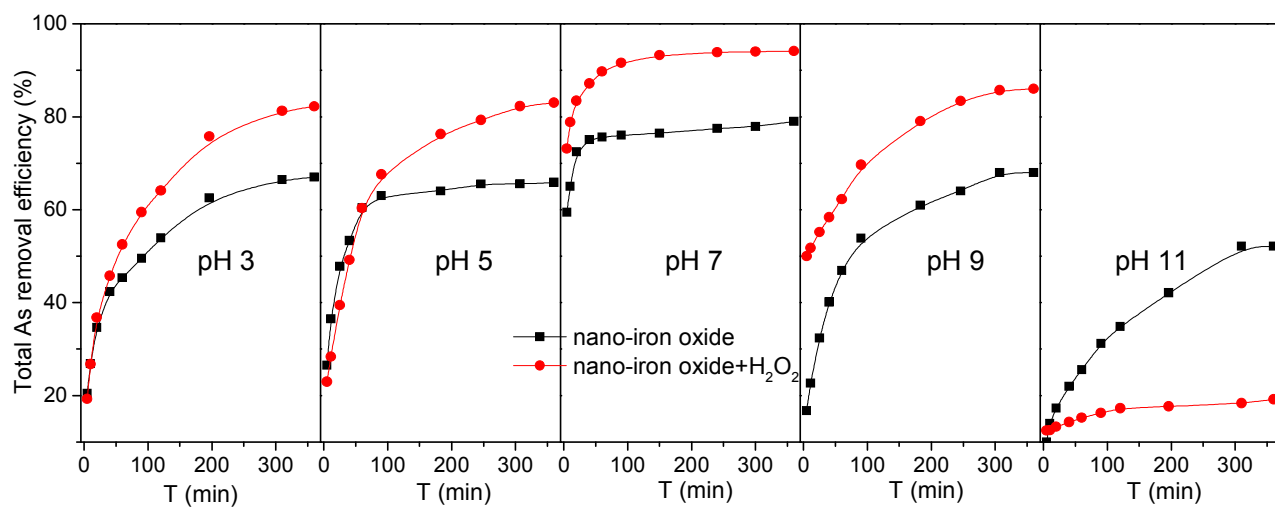


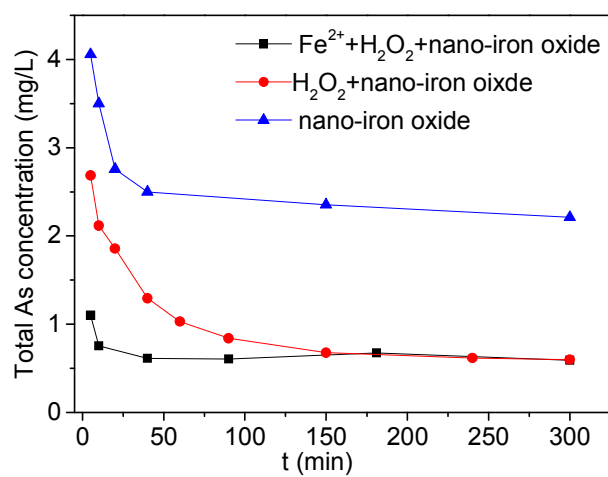
Fig. 11 Total arsenic removal with time on stream in the presence and absence of H₂O₂.

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Fig. 12 Change in total arsenic concentration with time on stream (pH 7, initial concentrations: As(III) = 10 mg/L, H₂O₂ = 300 μM, Fe²⁺ = 600 mM).

