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**Comparative study between microwave and ultrasonication**

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**aided *in situ* transesterification of microbial lipids**

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24

25 **Abstract**

26 Recent trends have focused on the development of a rapid method to convert microbial  
27 lipids to biodiesel. *In situ* transesterification allowed minimizing the requirement of  
28 solvents by combining the two steps (extraction of lipid and conversion to biodiesel) to a  
29 single step. Box–Behnken design was used for optimization of the variables to optimize  
30 the biodiesel yield and conversion. Microwave and ultrasonication assisted *in-situ*  
31 transesterification methods were compared based on the conversion efficiencies and their  
32 performance. Microwave approach revealed that around  $99\pm 0.5\%$  of conversion of  
33 FAMEs (w lipid conversion/w total lipids) was obtained in the presence of methanol to  
34 lipid molar ratio above 183:1 and NaOH addition of 2% (w/w) lipid in 20 min at 100 °C.  
35 Meanwhile, the ultrasonication yielded around  $95.1\pm 0.2\%$  (w/w total lipids) in the  
36 presence of methanol to lipid molar ratio 183:1 and NaOH addition 3% (w/w) lipid in  
37 20 min at 25 °C. The final profile of FAMEs was fully compatible with that of the  
38 conventional process based on chloroform and methanol extraction and required 12 hours  
39 for extraction.

40 **Keywords**

41 *In situ* transesterification; Ultrasonication; Microwave; Fatty acids methyl esters  
42 (FAMEs)

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## 45 **1 Introduction**

46 The gradual depletion of fossil fuel reserves and the continued use of petroleum-based  
47 fuels have encouraged researchers to seek viable, sustainable, and environmental friendly  
48 alternative sources of energy.<sup>1-3</sup> The exploitation of vegetable oils for biodiesel  
49 production had created numerous problems of food supplies and arable lands. Therefore,  
50 microbial oils called single cells oils (SCO) are considered to be a viable alternative since  
51 they do not have an impact on food supply and they do not require arable lands and could  
52 replace fossil fuels.<sup>4</sup> Many technical hurdles limit the use of these renewable source on  
53 large scale, especially, harvesting and extraction processes. Lipid extraction from  
54 oleaginous microorganisms required large amounts of organic solvents. Commonly,  
55 Folch method or its variant, the Bligh and Dyer method, have been used extensively for  
56 lipid extraction and quantitation.<sup>5</sup> However, owing to the hazardous nature of extraction  
57 using flammable organic solvents, and the adverse impact of solvent on the environment,  
58 it is strongly recommended to reduce the organic solvents and time of the extraction  
59 process. Terpenes, green solvents obtained from plants have been investigated as a  
60 replacement of organic solvents, although their efficiency and high costs limit their  
61 potential uses.<sup>6</sup> An ideal solution was to perform both extraction and transesterification  
62 processes simultaneously in one step thereby eliminating the solvent extraction step  
63 required to obtain the oil feedstock. In-situ transesterification refers to the direct  
64 transesterification of lipids in a biomass matrix without prior lipid extraction and offers  
65 the advantage of reducing processing units, lowering the fuel product costs and later  
66 quantifying fatty acids. Besides, process wastes and eventual pollution could also be  
67 reduced by this method.<sup>7</sup> Moreover, several methods are listed in literature (e.g. solvent,

68 enzymatic, mechanical, alkali, acid); however, not all were applicable due to their  
69 relatively high cost and equipment corrosion. Besides, there is no definitive standard  
70 method for neither lipid extraction nor quantification, nor for process development.<sup>8</sup>

71 Current works were based essentially on lipid extraction from algal species.<sup>9-11</sup>

72 Consequently, choosing a relevant method and optimizing its parameters was the main  
73 challenge. Microwave-assisted *in situ* transesterification could be an alternative to  
74 address the above concerns. This method allowed cell disruption and enhanced mass  
75 transfer rates<sup>12</sup>, which may result in high oils and lipids recovery.

76 Microwave irradiation has been reported to extract oil derived biomass, soils and  
77 vegetable feedstock.<sup>13-17</sup> Besides, this method allowed good quality of extracts with  
78 better target compound recovery.

79 A process that enables simultaneous oil extraction and transesterification is thus  
80 worthwhile to develop. Response surface methodology (RSM), a multivariate technique,  
81 was used in this work to optimize the levels of different variables (e.g. temperature,  
82 reaction time, catalyst concentration, and different methanol to lipid molar ratios.)  
83 reported highly critical in the *in situ* transesterification process. An optimum yield of  
84 FAMEs was envisaged. The analyses were performed on lyophilized biomass. Several  
85 trials were conducted to optimize the parameters related to this study. Besides, the impact  
86 of ultra-sonication aided in-situ transesterification on FAMEs composition was also  
87 investigated.

88

## 89 2 Material and Methods

### 90 2.1 Biological method

#### 91 2.1.1 Crude glycerol, reagents and analyses

92 All the reagents were of analytical grade and used without further purification. Methanol,  
93 hexane and NaOH were purchased from Fisher Scientific, Canada. Crude glycerol was  
94 obtained from Rothsay in Canada. Ultra-sonication experiments were conducted with  
95 ultrasonic processor CPX 750 (Cole-Parmer Instrument, IL) at 24 kHz. Microwave trials  
96 were carried out with MARS microwave extractor, CEM Corporation, North, 155  
97 Carolina, USA) equipped with Teflon tubes irradiated simultaneously. FAMES were  
98 analyzed using a Gas Chromatograph linked with Mass Spectroscopy (GC–MS) (Perkin  
99 Elmer, Clarus 500). The dimensions of the column used are 30 m, 0.25 mm, with a phase  
100 thickness of 0.2 l/m. The calibration curve was prepared with a mixture comprising 37  
101 FAMES (47885-U, 37 Component FAME Mix; Supelco, Bellefonte, PA, USA). 1,3-  
102 dichlorobenzene was used as internal standard at 50 ppm.

#### 103 2.1.2 Strain, culture and harvesting conditions

104 The strain, *Trichosporon oleaginosus* (ATCC20509) was grown in a glycerol based  
105 medium containing (per liter): 1 g (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub>, 1 g KH<sub>2</sub>PO<sub>4</sub>, 0.5 g MgSO<sub>4</sub>·7H<sub>2</sub>O, 0.2 g  
106 yeast extract, 50 g glycerol, and minerals 0.04 g CaCl<sub>2</sub>·2H<sub>2</sub>O, 0.0055 g FeSO<sub>4</sub>·7H<sub>2</sub>O,  
107 0.0052 g citric acid·H<sub>2</sub>O, 0.001 g ZnSO<sub>4</sub>·7H<sub>2</sub>O, and 0.00076 g MnSO<sub>4</sub>·H<sub>2</sub>O were added.

108 <sup>18</sup> Experiment was performed in 5 L fermenter at pH 6.5 and 28°C. pH was controlled by  
109 the addition of 4 N (NaOH and H<sub>2</sub>SO<sub>4</sub>). After 70 h, the biomass was harvested by

110 centrifugation at 5000  $x$  g for 15 min. Biomass was washed twice with distilled water to  
111 remove the residual nutrients and glycerol. The experimental method is shown in Fig. 1.

## 112 2.2 Chemical method

### 113 2.2.1 Conventional extraction and transesterification method

114 Extraction was carried out at room temperature using the standard chloroform and  
115 methanol extraction procedure.<sup>19-20</sup> About 0.2 g dry biomass resulting from the  
116 fermentation of *T. oleaginosus* after 72 hours was mixed with 4 mL solvent mixture of  
117 chloroform and methanol (2:1 (v/v)), and then subjected to 60 °C for 4 hours. The  
118 mixture was then centrifuged at 5000  $x$  g for 15 min and the solvent phase was withdrawn  
119 and transferred into a pre-weighed glass vial (W1). The extraction procedure was  
120 repeated two times. Afterwards, the vial containing the total volume of the supernatant  
121 collected from each extraction was subjected to 60°C in an oven to evaporate the solvents  
122 and was then weighed (W2). The lipid amount was calculated by the difference of W2  
123 and W1. The lipid content in the biomass is calculated as  $(W2-W1)/200 \text{ mg} \times 100\%$ . The  
124 obtained lipid was first dissolved in hexane (25 mL hexane per gram lipid), then mixed  
125 with methanol. Lipid to methanol molar ratio is 1:6 (0.3 mL methanol for per gram lipid).  
126 Sodium hydroxide was used as catalyst with addition of 1% (w/w) (NaOH/oil). The  
127 mixture was then subjected to 55 °C for 2 hours. After reaction, 5% (w/v) NaCl solution  
128 was added (100 mL NaCl solution per gram lipid), and then FAMES was extracted by  
129 two times washing with hexane (100 mL per gram lipid). After phase separation by  
130 settling, the hexane phase (upper layer) was collected. The FAMES in hexane was  
131 washed with 2% sodium bicarbonate solution (20 mL per gram lipid) and the mixture was

132 allowed to stand for 15 min for phase separation, and the top layer was collected and  
133 dried at  $60 \pm 1$  °C in an oven.<sup>21</sup>

### 134 2.2.2 *Ultrasonication aided transesterification*

135 Amounts of methanol and NaOH catalysts corresponding to ml equivalent of  
136 methanol/oil ratio (6:1, 183:1, 360:1) relating to 0.08, 2.45, 6.4 mL were added to 0.2 g  
137 of dry biomass and then reacted with a sonication probe immersed directly in the solution  
138 in a beaker placed in a water bath to control temperature at around 25°C for 20 min.  
139 Thermal meter was inserted to the bath to check the temperature. The sonication time was  
140 fixed at 20 min with one pause (2 min) at every 5 min sonication, and methanol to oil  
141 ratio was set at 60:1 - 360:1 (v/w). Amount of catalyst was varied from NaOH catalyst at  
142 1 to 5% (w/w).

### 143 2.2.3 **Transesterification aided by microwave heating**

144 Transesterification reactions were carried out in the presence of NaOH catalyst (1 to 5%  
145 (w/w) at various reaction temperatures (40 -100 °C). The catalyst was dissolved in  
146 methanol (6:1 – 360:1) (v/w) and the resulting solution was added to the oil. This reaction  
147 was then irradiated by microwave field under reflux and heated to the desired  
148 transesterification temperature in desired time. Power output of microwave was 400 W.  
149 An aliquot of 25 mL of the hexane was added to each vessel. This reaction was then  
150 irradiated by microwave field under reflux and heated to the desired transesterification  
151 temperature.



### 152 **2.3 *In situ* transesterification with microwave**

153 A pre-determined mass of 0.2 g of biomass was weighed accurately into each teflon  
154 vessels. Corresponding percent of methanol and NaOH was added separately to each  
155 vessel. The microwave power was set to 400 W. The temperature was kept at ambient  
156 ( $\pm 25^{\circ}\text{C}$  and the time was set to an initial 15 min ramp with 15 min hold time and a final  
157 15 min cooling time). After the transesterification, vessels were removed, 5% w/v NaCl  
158 solution was added (1 mL per gram biomass) and all samples filtered using Whatman  
159 filter paper to remove the residual biomass and the solvent was evaporated. The collected  
160 samples were allowed to stand overnight or (centrifugation ( $5000 \times g$ , 20 min). A small  
161 aliquot of the supernatant was siphoned off and transferred to a vial for gas  
162 chromatographic analysis.

### 163 **2.4 Two-stage process**

164 The extractive-transesterification experiments were conducted using microwave  
165 radiation. In the two-step production, transesterification was carried out on the lipid  
166 previously extracted from dry biomass with chloroform/methanol (e.c. conventional  
167 method), then using microwave and ultrasonicator, following the transesterification  
168 (described in section 2.2.2 and 2.2.3 and presented in Fig. 1).

### 169 **2.5 Optimization of *in situ* transesterification by Box–Behnken design (BBD)**

170 A 4-level 4-factor Box–Behnken design was adopted to evaluate the effects of  
171 temperature (X1), reaction time (X2), methanol to lipid molar ratios (X3), catalyst  
172 concentration (X4), and lipid conversion efficiency of *T. oleaginosus* on crude glycerol  
173 based medium. In this regard, the experimental plan contained 29 trials and the

174 independent variables were studied at three different levels, namely low (-1), medium (0)  
175 and high (+1), whose values are shown in [Table 1](#).

176 The effect of the three factors and their interactions were studied using the response  
177 surface methodology.<sup>22</sup> Based on experience and economic feasibility, a three factorial  
178 subset design was employed.<sup>23</sup> The total number of experimental runs was 29 with  
179 replications as shown in [Table 2](#). The temperature, time, methanol to oil ratio and catalyst  
180 were varied in the ranges of 40 - 100°C, 20-60 min, 6:1 - 360:1 (v/w), 1 - 5% (w/w)  
181 respectively. The lipid conversion efficiency was taken as the response variable (Y). The  
182 experimental design used in this work is shown in [Table 2](#). The response variable was  
183 fitted by a second order model to correlate the response variables to the independent  
184 variables. The second order polynomial coefficients were calculated and analyzed using  
185 the 'Design Expert' software (Version 7.0, Stat-Ease Inc., Minneapolis, USA). The  
186 general form of the second degree polynomial equation is:

$$187 \quad Y = \beta_0 + \sum \beta_i X_i + \sum \beta_{ij} X_i X_j + \sum \beta_{ii} X_i^2 \quad (1)$$

188

189 **Y:** the predicted lipid conversion efficiency (% w/w lipid)

190  **$\beta_0$ :** the intercept

191  **$\beta_i$ :** the linear coefficient

192  **$\beta_{ij}$ :** the quadratic coefficient

193  **$\beta_{ii}$ :** the linear-by-linear interaction between  $X_i$  and  $X_j$  regression coefficients

194  **$X_i, X_j$ :** input variables

195

196 Statistical analysis of the model was utilized to evaluate the analysis of variance  
197 (ANOVA). This analysis englobed Fisher's F test (overall model significance), associated  
198 probability  $p$  ( $F$ ), correlation coefficient  $R$  and determination coefficient  $R^2$ . All  
199 parameters play role in measuring the goodness of fit of regression model. Quadratic  
200 models were used for each variable and were represented as contour plots (3D). Response  
201 surface curves were generated using Design Expert software.

## 202 3 Results and discussion

### 203 3.1 Statistical analysis of experimental design

204 The conventional extraction method which consisted of a mixture of  
205 chloroform/methanol (2:1 (v/v)) provided lipid content of  $47.3 \pm 0.9$  % (w/w) of dry  
206 biomass. This percentage is considered as 100% of conversion of biomass to lipid. The  
207 lipid conversion efficiency to fatty acids methyl esters (FAMEs) is calculated by  
208 determining amount of FAMEs by GC-MS and dividing this value by total lipids (g  
209 FAMEs/g total lipids). Many parameters have been reported to control the lipid  
210 efficiency including (e.g. the amount of catalyst added, reaction time, temperature and  
211 molar methanol to lipid ratio).

212 The statistical significance of the designs was determined by F-test for ANOVA (Table  
213 3). As seen from this table, operating parameters had a significant effect on the fatty acid  
214 methyl ester content which is confirmed by the p-values of the analysis. Values of  
215 "Prob > F" are less than 0.05 which indicated that the model is significant with 98.54%  
216 confidence level. Therefore, the P-value of the lack of fit analysis was ( $< 0.0001$ ) which  
217 confirmed that the model was significant and reliable for lipid production in this study.  
218 Besides, correlation coefficient,  $R^2$  (0.989) supported the correlation between the *in situ*  
219 transesterification process parameters.

220 The value of  $\text{adj-}R^2$  (0.979) suggested that the total variation of 97.99% for the lipid  
221 concentration was attributed to the independent variables and only about 3.01% of the  
222 total variation could not be explained by the model. Besides, model coefficients for each  
223 variable are also shown in Table 3. The larger F-value and smaller P-value suggested  
224 higher significance of the corresponding coefficient. Among the model terms, X1

225 (temperature), X3 (methanol/oil ratio), X1<sup>2</sup>, X3<sup>2</sup> were significant. By contrast, other  
226 terms were not significant. The relationship between the response and experimental levels  
227 of each variable can be demonstrated by three-dimensional response surface plots which  
228 represented the regression equation mentioned below:

$$\begin{aligned} 229 \quad Y = & 82.5 + 17.08333 X1 + 0.066666 X2 + 28.316666 X3 + 0 X4 - 1.625 X1X2 + 6.4 \\ 230 \quad & X1X3 - 2.025 X1X4 - 0.475 X2X3 + 0.65 X2X4 - 1.525 X3X4 - 9 X1^2 - 0.05 X2^2 - \\ 231 \quad & 27.675 X3^2 - 0.175 X4^2 \end{aligned} \quad (2)$$

232 where Y is the observed response (lipid conversion efficiency) for the microwave in-situ  
233 transesterification. X1, X2, X3 and X4 are the coded values of independent factors  
234 temperature, reaction time, methanol to oil molar ratio and catalyst amount, respectively.

### 235 3.2 Optimization of microwave process parameters with RSM

236 In conventional method of biodiesel synthesis, the reaction time and temperature are 30  
237 min–12 hours and 55–65 °C, respectively.<sup>24-26</sup> Besides, Melo-Junior et al. (2009) have  
238 studied in detail the esterification of oleic acid (C18) under microwave irradiation while  
239 varying alcohol type (methanol or ethanol), temperature (150-225°C) and molar ratio of  
240 alcohol/fatty acid (3.5-20) , a conversion rate up to 60% was obtained in 60 min of  
241 reaction<sup>27</sup>. In this regard, present study was carried out to optimize different parameters  
242 in the microwave assisted direct transesterification; reaction temperature, time, methanol  
243 to oil molar ratio and catalyst amount were chosen as variables. To compare the  
244 temperature effect on the conversion yield, in-situ transesterification was conducted at  
245 40, 80 and 100 °C. Thus, according to literature, when using a homogeneous catalyst  
246 (herein NaOH), harsher condition including high temperature<sup>28</sup> is required to achieve

247 high FAMES yields. Besides, preliminary study has showed that only  $14.5 \pm 1.2\%$  of  
248 FAMES were obtained under low temperature at  $25\text{ }^{\circ}\text{C}$ . Conversely, higher conversion  
249 efficiency above ( $> 90\% \pm 1.2$  (w/w) was obtained in a lower reaction time 20 min at 100  
250  $^{\circ}\text{C}$ . Microwave effect at  $100\text{ }^{\circ}\text{C}$  was four fold compared to  $40\text{ }^{\circ}\text{C}$  which confirmed the  
251 positive role of temperature (low p value  $< 0.0001$ ). At  $70\text{ }^{\circ}\text{C}$ , around  $83 \pm 0.6\%$  of  
252 FAMES (w/w) was obtained. Therefore, higher the reaction temperature, the more the  
253 reaction can be driven. This is in accordance with Im et al. (2014) who proved the  
254 positive effect of temperature on FAMES yield, around  $91.1\%$  was obtained at  $95\text{ }^{\circ}\text{C}$  for  
255 90 min.<sup>29</sup> Moreover, Sunita et al. (2008) have observed that the conversion rate of oil to  
256 biodiesel increased significantly with the rise in temperature and was reported to be  $73\%$   
257 and  $97\%$  at  $180$  and  $200\text{ }^{\circ}\text{C}$ , respectively.<sup>30</sup> Moreover, a complete conversion ( $100\%$ ) of  
258 caprylic acid for the esterification was achieved at a higher temperature,  $175\text{--}200\text{ }^{\circ}\text{C}$ .<sup>31-32</sup>  
259 High temperature may lead to the formation of microzones called “hot spots”, which lead  
260 to an increase in the escalation of chemical reaction rate.<sup>33</sup> The loss of methanol was not  
261 seen in this study compared to current studies<sup>25, 34-35</sup>, this is mainly due to nature of the  
262 closed system that resists higher temperatures. Both high temperature and thermal effect  
263 caused by the microwaves enhanced the extractive properties of methanol to extract more  
264 lipids in the biomass via diffusive extraction and extended microwave effect caused the  
265 penetration through the cell walls and forces out the oils into the solvent mixture through  
266 disruptive extraction. Another observation to be taken in advantage from this work is the  
267 absence of emulsions and soap formation which is primarily related to the high  
268 temperature effect, thus, free fatty acids (FFA) are converted efficiently into FAMES,  
269 which has been proven in previous studies that noted the role of microwave irradiation in

270 the reduction of FFA content within the first 15 min.<sup>36</sup> Furthermore, Kamath et al. (2011)  
271 reported around 87.39% of FFA reduction during the transesterification of crude karanjia  
272 oil through microwave irradiation.<sup>37</sup> No soap formation is principally due to absence of  
273 the catalytic poisoning by water formed as a result of esterification, so that microwaves  
274 and high temperature reduced the free fatty acid content and made it easier to separate  
275 biodiesel and alcohol layers. As seen in Fig. 2, catalyst more than 3% (w/w) showed a  
276 positive effect on the *in situ* transesterification reaction. Herein, NaOH is used as a  
277 homogeneous, solvent-catalyst; the choice of this catalyst rather than others is related to  
278 its higher yield of biodiesel conversion rates,<sup>38</sup> and its ability to break chemically the  
279 molecule of the raw renewable oil into methyl or ethyl esters. Highest biodiesel  
280 conversion of  $93.94 \pm 0.3$  % was observed using 3 % (w/w) of NaOH catalyst with  
281 methanol to oil ratio of 183:1. Conversely, the lower amount of catalyst (proportional to  
282 methanol ratio 6:1) may not efficiently advance the reaction and gave a yield of  $24.5 \pm$   
283  $0.1$  % (w/w) of conversion rate.

284 Methanol to lipid ratio had a significant effect on the *in situ* transesterification, and this  
285 was confirmed with a low P value  $< 0.0001$ . Herein, methanol exhibited binary action  
286 and acted as a solvent for extraction of the microbial oils/lipids and a reactant for  
287 transesterification of esters.<sup>39</sup> Thus, applying microwave irradiation during *in situ*  
288 transesterification will serve for dual purpose (e.c. rendering lipids available for reaction  
289 as well as intensification of process).

290 Methanol to oil molar ratio was varied from 6:1 to 360:1 in the microwave direct  
291 transesterification reaction. A lower ratio than 6:1 (v/w) does not favor the *in situ*  
292 transesterification process and a lower yield is observed. When the methanol to oil molar

293 ratio was increased to 183:1, the maximum biodiesel conversion observed was  
294  $92.3 \pm 1.0\%$  because of the increased contact area between methanol and oil/lipid. This is  
295 in accordance with Sunita et al. (2008) who found that increasing methanol to oil ration  
296 from 10:1 to 20:1 enhance the conversion of sunflower oil to biodiesel from 30% to 90%  
297 respectively.<sup>30</sup>

298 Further increase of molar ratio up to 360:1 did not give significant difference. Generally,  
299 a higher amount of methanol may reduce the concentration of the catalyst in the reactant  
300 mixture and does not give higher yield during the transesterification reaction.<sup>40</sup>  
301 Moreover, with a lower methanol ratio, the downstream cost can be controlled.<sup>41</sup>

302 The reaction time of around 20 min seemed to be adequate for the complete process. The  
303 reaction time had no significant effect ( $p$ -value = 0.9510) on the FAMES content at  
304 higher temperature and even time can be further reduced. Generally, extended reaction  
305 times allowed higher exposure of microwave irradiations to the reaction mixture which  
306 resulted in higher efficiency of extraction and biodiesel conversion.

307 From the above analysis, the optimum given by the model to achieve a maximum of lipid  
308 conversion efficiency was 183:1 of methanol ratio with 2% of catalyst amount (w/w) and  
309 at temperature higher than  $80^{\circ}\text{C}$ , around ( $99\% \pm 0.5\%$  w/w total lipids) in minimum time  
310 required 20 min.

### 311 **3.3 Comparison of microwave vs. ultrasonication for *in situ* transesterification**

312 As discussed earlier, the biggest issue during *in-situ* transesterification is the requirement  
313 of large volumes of solvent and longer reaction time. During microwave process, 183:1  
314 (w/w) and 20 min was the optimum condition for lipid extraction and high biodiesel



315 recovery. For this purpose, ultrasonification has been also tested for its efficiency  
316 regarding biodiesel conversion. Accordingly, ultrasonification has been carried out to  
317 achieve higher yields of conversion during esterification and transesterification. High  
318 conversions yields were reported for converting algal oils and vegetable oils which  
319 allowed reduction in the reaction time.<sup>42</sup> This approach was highly dependent on  
320 temperature and other operating parameters. Around 97.3% was obtained during  
321 conversion of palm oil in 45 min at 60°C with 0.3 % KOH<sup>43</sup> and higher temperature  
322 (>60°C) was less effective during the conversion step. In the present study,  
323 ultrasonification is carried out in an open system which results in methanol evaporation.  
324 Besides, higher temperatures during ultrasonification were reported to lower FAMES  
325 content<sup>34-35</sup>. Although, higher temperatures are required for harsh extraction in the  
326 microwave as reported in the previous section (Section 3.2), Parkar et al. (2012) reported  
327 that physical effects of cavitation bubble dynamics in ultrasound assisted  
328 transesterification are more pronounced at lower temperature of 15 °C, albeit the low  
329 conversion yield of 13.45%.<sup>44</sup> Hence, the temperature was fixed to 25 °C (neither high  
330 nor low). Herein, *in situ* transesterification using ultrasound was optimized considering  
331 catalyst amount, methanol to oil molar ratio, and reaction time as reaction parameters.  
332 The optimisation of different variables is given in Table 4. The model was highly  
333 significant ( $R^2 = 0.998$ ). This indicates that model cannot explain only 0.01 % of the total  
334 variations which shows that the model fits quite well. Moreover, *p* value for the model  
335 was lower than 0.05, which confirms the statistical relation between the response and  
336 selected factors. This shows that regression analysis is statistically significant. Therefore

337 in this model, most significant factors are methanol to oil molar ratio, ( $p < 0.0001$ )  
338 followed by catalyst amount ( $p = 0.114$ ) and reaction time ( $p=0.680$ )

339 Akin to microwave approach, catalyst amount of 1, 3 and 5 % (w/w) were considered.  
340 Besides, beyond 5 % (w/w) catalyst, no further increase in the conversion of the oil to  
341 biodiesel could be achieved as the reaction was limited by mass transfer. Maximum  
342 biodiesel conversion of  $95 \pm 0.5$  % (w/w) was observed using 5 % (w/w), the catalyst in  
343 the presence of high methanol ratio 183:1. As seen in [Table 4](#), it can be found that the  
344 efficiency of lipid conversion via ultrasonicator equipment (20 kHz, 700 W) increased  
345 with the increase of methanol to oil ratio and catalyst amount (%). P values were around  
346 ( $< 0.0001$ ) and (0.1140) for methanol to oil ratio and catalyst amount which justified their  
347 positive influence on the lipid conversion. Around  $90.1 \pm 2.2\%$  (w/w total lipids) was  
348 attained in 20 min with 183:1 methanol to oil ratio (w/w). Higher conversion efficiency  
349 shown by ultrasound could be attributed to increased mass and heat transfer provided by  
350 the physical and chemical effects during intensification of reaction <sup>45</sup> Another  
351 observation to be pointed out by the present study is the formation of emulsions due to  
352 the reaction of catalyst with methanol. NaOH leads to water formation which slows the  
353 reaction rate and causes soap formation.<sup>46</sup> Thus, the FAMES mixture remains in emulsion  
354 for more than 12 hours. For that purpose, hexane was added and the mixture was filtrated  
355 and then allowed to stand for 15 min. Thereafter, the top layer of FAMES in hexane was  
356 collected for quantification. However, at  $100^\circ\text{C}$  with microwave irradiation, this problem  
357 was resolved since with closed vessels (under controlled pressure and temperature), the  
358 solvent can be heated above its normal boiling point, the fact that enhanced extraction

359 efficiency and speed.<sup>47</sup> Therefore, short reaction time, cleaner reaction product, and  
360 reduced separation-purification times are the key observations in this the present study.

361 For a conventional method, reaction time for the transesterification was assumed to be  
362 12 hours. In contrast, with the microwave and ultrasounds, the time was reduced to  
363 20 min. Herein, microwave-assisted reactions may reduce not only the time but also  
364 eliminate the need for the catalyst, however, higher reaction temperatures are required.<sup>48-</sup>

365 <sup>49</sup> During this process, microwaves interacted with triglycerides and methanol present in  
366 the mixture which resulted in increased of interfacial polarization (a combination of ionic  
367 conduction and dipolar momentum) and ionic conduction.<sup>12, 50-51</sup> These two reactions are  
368 the major causes of superheating phenomenon which is observed at elevated temperatures  
369 and led to a large reduction of activation energy with a high diffusivity of the solvent into  
370 the internal parts of biomass. Thus, methanol is defined to be a strong microwave  
371 absorber and the presence of an -OH group attached to biomass matrix behaves as though  
372 it was anchored to an immobile raft, so localized rotations result in localized superheating  
373 and the reaction may occur rapidly.<sup>52</sup> Consequently, desorption of intracellular  
374 components (lipids droplets) from the active sites of the biomass matrix was enhanced.

375 When compared to microwave method, ultrasonic-assisted extraction uses cavitation  
376 process to recover oils from microbial cells. Resulting bubbles during this process  
377 collapse near cell walls so that the cell contents are released.<sup>53,49-50</sup> The ultrasonic waves  
378 had a significant effect on cell disruption. A cavitation process is resulted due to the  
379 higher pressure and shear on the cell walls which contributes to the formation of free  
380 radicals of reacting species.<sup>54</sup> Accordingly, ultrasound permits the formation of highly  
381 reactive radicals through dissociation of entrapped vapor molecules in the bubble, which

382 are subjected to extreme conditions generated at the collapse of the bubble. In ultrasound  
383 assisted direct transesterification, cavitation effect caused by turbulence in reaction  
384 medium and free radicals are responsible for process intensification.<sup>55</sup>

385 During two-stage of conventional transesterification, around  $93.8 \pm 1.3$  % (w lipid/w total  
386 lipids) was achieved with methanol to lipid molar ratio 6:1 in the presence of NaOH  
387 amount 1% (w/w) lipid during 2 h, however, under similar conditions, only  $3.0 \pm 0.2$ % (w  
388 lipid/w total lipids) was obtained in *in-situ* transesterification (one stage). To obtain  
389 higher efficiency, the increase of methanol to oil ratio above 360:1 and NaOH above 5%  
390 (w/w) were required, thus, more than  $90.4 \pm 1.5$  was achieved during 12 hours. It is clear  
391 that *in-situ* transesterification required much larger amount of methanol and NaOH  
392 catalyst and far longer time to achieve similar lipid conversion yield than two stage  
393 transesterification process. These higher requirements during transesterification are due  
394 to the nature of cell wall that make barrier to solvent to access and extract lipid droplets  
395 from intracellular compartment. So more solvent is required to weaken, disrupt and  
396 penetrate into cell walls. In this regard, *in-situ* transesterification is preferable to  
397 overcome these hurdles.

398 In the presence of microwave irradiation, transesterification was carried out in two stage  
399 and around  $98.5 \pm 0.5$  % (w/w) was obtained at 100°C in the presence of 1% (w/w)  
400 catalyst and 183:1 % (v/w) of methanol ratio. With ultrasonication method, a higher  
401 conversion efficiency of  $94.1 \pm 0.1$  % was achieved under same conditions at 25 °C.  
402 Therefore, transesterification carried in two stages with microwave irradiation or  
403 ultrasonication bubbles have the advantage to reduce the longer time and the large  
404 amount of catalyst.

405 In the present study, microwave assisted direct transesterification showed higher  
406 efficiency than ultrasound assisted *in-situ* transesterification. Taken together, both  
407 approaches reduce the time, catalyst amount and energy requirements (Table 5).  
408 However, main obstacle for commercial application of these intensification methods is  
409 their scale up challenges. More research is required for successful implementation of  
410 these methods for direct conversion of microbial biomass to biodiesel at commercial  
411 scale. Besides, possible recovery of the catalyst from the residual biomass and its reuse  
412 needs more attention from the researchers. In this regard, future direction of research  
413 ought to focus on the process improvisation, catalyst recovery and reuse.

#### 414 **3.4 Comparison of composition of FAMEs from different transesterification** 415 **processes**

416 The analysis of the FAMEs composition is presented in Table 6. Microwave *in situ*  
417 transesterification process with a molar ratio of 183:1 at 100 °C favored a higher content  
418 of C18:2. Similar results were observed during ultrasonication aided *in-situ*  
419 transesterification at 25 °C, in 20 min and with a methanol to oil ratio of 183:1.  
420 Meanwhile, a lower C16:0 and C18:1 was observed. In fact, a lower molar ratio favored  
421 the production of phospholipids present in cell membrane<sup>53</sup>. On the other hand, higher  
422 methanol: oil ratio disrupted cells and allowed more contact with lipid droplets and major  
423 FAMEs belonged to intracellular lipids. The composition of FAMEs from two stage  
424 transesterification, conventional *in-situ* transesterification, microwave *in-situ*  
425 transesterification and ultrasonication *in-situ* transesterification were almost similar.

#### 426 **4 Conclusion**

427 The production of single cell oils and their conversion process to biodiesel are of wide  
428 interest in fuel market. Lyophilized biomass of *T. oleaginosus* was utilized for the  
429 production of biodiesel using two means of in-situ transesterification: microwave  
430 technique and ultrasonication. Among the two methods, microwave was found to give  
431 higher conversion efficiency to biodiesel amounting to  $99 \pm 0.5\%$  w/w total lipids as  
432 compared to  $95 \pm 0.2\%$  w/w total lipids with ultrasonication assisted technique.  
433 Another advantage of microwave assisted transesterification is the absence of emulsions  
434 during the whole process, the fact that reduce the separation time obtained ( $> 99\%$   
435 reduction in separation time), and all with a reduced energy consumption, meanwhile, a  
436 low reaction temperature ( $25\text{ }^{\circ}\text{C}$ ) was required for transesterification during  
437 ultrasonication method that will reduce the cost of production of biodiesel. Taken  
438 together, both approaches revealed that methanol: hexane efficiently converted FAMES  
439 compared to conventional process which relied on chloroform: methanol 2:1 (v/v) and  
440 hexane mixtures and required more catalyst and more time to obtain the desired  
441 conversion efficiency. The *in-situ* transesterification process proved to be faster and  
442 easier method to produce biodiesel with lower catalyst 1% (w/w) and in short time of  
443 20 min. Overall, microwave *in-situ* transesterification would be a promising alternative of  
444 the current two-stage transesterification process and combining the effects of the  
445 microwave and ultrasonic energy via hybrid reactor can be innovative and beneficial at  
446 large scale.

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452

### 453 **Figure Captions List**

454 **Fig. 1. Schematic representation of different transesterification methods.**

455 **Fig. 2. Response surface plots showing binary interaction of different variables. The**  
456 **interaction between: (A) methanol/oil ratio (% v/w) and temperature (°C);**  
457 **(B) temperature (°C) and time (min); (C) catalyst amount (%) and**  
458 **temperature (°C); (D) methanol/oil ratio (%) and time (min); (E) catalyst**  
459 **amount (%) and time (min); (F) catalyst amount (%) and methanol/oil ratio**  
460 **(% v/w).**

461

462 **References**

- 463 1 A. C. Pinto, L. L. N. Guarieiro, M. J. C. Rezende, N. M. Ribeiro, W. A. Lopes, P.  
464 A. P. Pereira and J. B. De Andrade, *J. Brazil. Chem. Soc.*, 2005, **16**, 1313-1330.
- 465 2 Y. Chisti, *Biotechnol. Adv.*, 2007, **25**, 294-306.
- 466 3 P. T. Vasudevan and M. Birggs, *J. Ind. Microbiol. Biotechnol.*, 2008, **35**, 421-  
467 430.
- 468 4 Y. Shen, Z. Pei, W. Yuan and E. Mao, *Int. J. Agric. Biol. Eng.*, 2009, **2**, 51.
- 469 5 W. W. Christie, James Hutton Institute and Mylnefield Lipid Analysis. (2013).
- 470 6 C. D. Tanzi, M. A. Vian and F. Chemat, *Bioresour. Technol.*, 2013, **134**, 271-275.
- 471 7 E. A. Ehimen, Z. F. Sun and C. G. Carrington, *Fuel. Process. Technol.*, 2010, **89**,  
472 677-684.
- 473 8 Z. Jacob, *Crit. Rev. Biotechnol.*, 1992, **12**, 463-491.
- 474 9 T. Suzuki, A. Takigawa and K. Hasegawa, *Agric. Biol. Chem.*, 1973, **37**, 2653-  
475 2656.
- 476 10 G. Jin, F. Yang, C. Hu, H. Shen and Z. K. Zhao, *Bioresour. Technol.*, 2012, **111**,  
477 378-382.
- 478 11 T. A. Pedersen, *Acta Chem Scand*, 1962, **16**, 374-382.
- 479 12 A.V. Kanitkar, Master's Thesis, Louisiana State University, Baton Rouge, L A.,  
480 USA, (2010), 129 p.
- 481 13 I. J. Barnabas, J. R. Dean, L. A. Fowles and S. P. Owen, *Analyst*, 1995, **120**, 1897-  
482 1904.



- 483 14 G. A. C. Kiss, E. Forgacs, T. Cserhati, T. Mota, H. Morais and A. Ramos, *J.*  
484 *Chromatogr. A*, 2000, **889**, 41-49.
- 485 15 H. Li, L. O. Pordesimo, J. Weiss and L. R. Wilhelm, *Trans. ASAE.*, 2004, **47**,  
486 1187-1194.
- 487 16 M. E. Lucchesi, F. Chemat and J. Smadja, *J. Chromatogr. A*, 2004, **1043**, 323-  
488 327.
- 489 17 J. Hernando, P. Leton, M. P. Matia, J. L. NovellaL and J. Builla-Alvarez-Builla,  
490 *Fuel. Process. Technol.*, 2007, **86**, 1641-1644.
- 491 18 Y. Zheng, Z. Chi, B. K. Ahring, S. Chen, *Biomass. Bioenerg.*, 2012, **37**, 114-121.
- 492 19 J. Folch, M. Lees and S. G. H. Sloane, *J. Biol. Chem.*, 1957, **226**, 497-509.
- 493 20 G. Vicente, L. F. Bautista, R. Rodríguez, F. J. Gutiérrez, I., Sádaba, R. M., Ruiz-  
494 Vázquez, S. Torres-Martinez and V. Garre, *Biochem. Eng. J.*, 2009, **48**, 22-27.
- 495 21 R. Halim, B. Gladman, M. K. Danquah and P. A. Webley, *Bioresour. Technol.*,  
496 2011, **102**, 178-185.
- 497 22 R. H. Myers and D. C. Montgomery, New York, Wiley (2002).
- 498 23 S. G. Gilmour, *Biometrics*, 2006, **62**, 323-331.
- 499 24 L. C. Meher, D. S. S. Vidya, S. N. Naik, *Bioresour. Technol.* 2006, **97**, 1392-  
500 1397.
- 501 25 X. Zhang, S. Yan, R. D. Tyagi, P. Drogui, and R Y. Surampalli, *Bioresour.*  
502 *Technol.*, 2014, **158**, 253-261.

- 503 26 U. Rashid, F. Anwar, T. M. Ansari, M. Arif and M. Ahmad, *J. Chem. Technol.*  
504 *Biotechnol.*, 2009, **84**, 1364-1370.
- 505 27 C. A. R. Melo-Junior, C. E. R Albuquerque, M. Fotuny, C. Dariva, S. Egues, A.  
506 F. Sastos and A. L. D. Ramos, *Energy. Fuels*, 2009, **23**, 580-585.
- 507 28 E. Lotero, Y. Liu, D. E. Lopez, K. Suwannakarn, D. A. Bruce and J. Goodwin,  
508 *Ind. Eng. Chem. Res.*, 2005, **44**, 5353.
- 509 29 H. J. Im, H. S. Lee, M. S. Park, J. W. Yang and J. W. Lee, *Bioresour. Technol.*,  
510 2014, **152**, 534-537.
- 511 30 G. Sunita, B. M., Devassy, A. Vinu, D. P. Sawant, V. V. Balasubramanian and S.  
512 B. Halligudi, *Catal. Commun.* 2008, **9**, 696-702.
- 513 31 S. Furuta, H. Matsushashi and K. Arata, *Catal. Commun.*, 2004, **5**, 721-723.
- 514 32 D. E. López, J. G. Goodwin, D. A. Bruce and S. Furuta, *Appl. Catal. A: Gen.*,  
515 2008, **339**, 76-83.
- 516 33 I. Manco, L. Giordani, V. Vaccari and M. Oddone, *Fuel*, 2012, **95**, 108-112.
- 517 34 T. Eevera, K. Rajendran and S. Saradha, *Renew. Energ.*, 2009, **34**, 762-765.
- 518 35 D. Y. C. Leung and Y. Guo, *Fuel. Process. Techno.*, 2006, **87**, 883-890.
- 519 36 K. Suppalakpanya, S. B. Ratanawilai and C. Tongurai, *Fuel*, 2010, **89**, 2140-2144.
- 520 37 H. V. Kamath, I. Regupathi and M. B. Saidutta, *Fuel Process. Technol.*, 2011, **92**,  
521 100-105.
- 522 38 A. A. Refaat, S. T. El Sheltawy and K. U. Sadek, *Int. J. Environ. Sci. Technol.*,  
523 2008, **5**, 315-322.

- 524 39 W. Mulbry, S. Kondrad, J. Buyer and D. Luthria, *J. Am. Oil Chem. Soc.*, 2009, **86**,  
525 909-915.
- 526 40 S. Zhang, Y. G. Zu, Y. J. Fu, M. Luo, D. Y. Zhang and T. Efferth, *Bioresour.*  
527 *Technol.*, 2010, **101**, 931-936.
- 528 41 S. Stiefel and G. Dassori, *Ind. Eng. Chem. Res.*, 2009, **48**, 1068-1071.
- 529 42 C. B. Hobuss, D. Venzke, B. S. Pacheco, A. O. Souza, M. A. Santos, S. Moura, F.  
530 H. Quina, K. G. Fiametti, J. Vladimir Oliveira and C. M. Pereira, *Ultrason.*  
531 *Sonochem.*, 2012, **19**, 387-389.
- 532 43 L. P. Lima, F. F. P. Santos, E. Costa and F. A. N. Fernandes, *Biomass Convers.*  
533 *Biorefin.*, **2012**, *2*, 309-315.
- 534 44 P. A. Parkar, H. A. Choudhary and V. S. Moholkar, *Chem. Eng. J.*, 2012, **187**,  
535 248-260.
- 536 45 V. L. Gole and P. R. Gogate, *Ind. Eng. Chem. Res.*, 2012, **51**, 11866-11874.
- 537 46 N. Saifuddin, A. Samiuddin and P. Kumaran, *Trends. Appl. Sci. Res.*, 2015, *10*, 1-  
538 37.
- 539 47 P. C. Veggi, J. Martinez and M. A. A. Meireles, In: Food Engineering Series 4,  
540 CFaCG, editor, Springer, New York, USA, (2013), 15 p.
- 541 48 J. Geuens, J. M. Kremsner, B. A. Nebel, S. Schober, R. A. Dommissie, M.  
542 Mittelbach, S. Tavernier, C. O. Kappe and B. U. W. Maes, *Energy. Fuels*, 2008,  
543 **22**, 643-645.

- 544 49 R. Harun, M. Singh, G. M. Forde and M. K. Danquah, *Renew. Sust. Energ. Rev.*,  
545 2010, **14**, 1037-1047
- 546 50 F. Wei, G. Z. Gao, X. F. Wang and X .Y. Dong, *Ultrason. Sonochem.*, 2008, **15**,  
547 938-942.
- 548 51 V. G. Gude, P. D. Patil, E. Martinez-Guerra, S. Deng and N. Nirmalakhandan,  
549 *Sustain. Chem. Process.*, 2013, **1**, 1-31.
- 550 52 J. P. Tierney and P. Lidstrom, Oxford, UK: CRC Press, 2005.
- 551 53 S. Giroud, C. Frare, A. Strijkstra, A. Boerema, W. Arnold and T. Ruf, PLoS One,  
552 2013, **8**, 1-9.
- 553 54 E. V. Rokhina, P. Lens and J. Virkutyte, *Trends Biotechnol.*, 2009, **27**, 298-306.
- 554 55 P. R Gogate, V. S. Sutkar andA. B. Pandit, *Chem. Eng. J.*, 2011, **166**, 1066-1082.  
555

**Table 1** Coding and levels of experiment factors

Factor	Parameter	Code level		
		-1	0	+1
Temperature (°C)	X1	40	70	100
Time (min)	X2	20	40	60
Methanol to oil ratio (v/w)	X3	6:1	183:1	360:1
Catalyst (% w/w)	X4	1	3	5

**Table 2** Box–Behnken design arrangement

Run	Parameter			
	X1	X2	X3	X4
1	0	-1	1	0
2	-1	1	0	0
3	1	0	0	1
4	1	0	-1	0
5	0	0	0	0
6	1	-1	0	0
7	0	1	0	1
8	0	1	0	-1
9	-1	-1	0	0
10	0	0	0	0
11	0	0	1	-1
12	0	0	1	1
13	0	0	0	0
14	-1	0	-1	0
15	0	-1	0	-1
16	1	1	0	0
17	-1	0	0	-1
18	0	1	1	0
19	0	0	0	0
20	-1	0	1	0
21	0	0	-1	-1
22	0	-1	0	1
23	1	0	1	0
24	1	0	0	-1
25	0	0	0	0
26	-1	0	0	1
27	0	1	-1	0
28	0	-1	-1	0
29	0	0	-1	1

**Table 3** Analysis of variance (ANOVA) for response surface quadratic model for the FAME content

Source	Sum squares	of df*	Mean square	F value	p-value (Prob > F)
Model	18788	14	1342	98.545	< 0.0001
X1	3502	1	3502	257.17	< 0.0001
X2	0.05333	1	0.05333	0.00391	0.9510
X3	9622	1	9622	706.57	< 0.0001
X4	0	1	0	0	1.0000
X1X2	10.563	1	10.563	0.77563	0.3933
X1X3	163.84	1	163.84	12.031	0.0038
X1X4	16.403	1	16.403	1.2045	0.2909
X2X3	0.9025	1	0.9025	0.06627	0.8006
X2X4	1.69	1	1.69	0.12410	0.7299
X3X4	9.3025	1	9.3025	0.68311	0.4224
X1 <sup>2</sup>	525.41	1	525.41	38.582	< 0.0001
X2 <sup>2</sup>	0.01622	1	0.01622	0.00119	0.9730
X3 <sup>2</sup>	4968	1	4968	364.82	< 0.0001
X4 <sup>2</sup>	0.19865	1	0.19865	0.01459	0.9056
Residual	190.65	14	13.618		
Lack of Fit	190.21	10	19.021	172.92	< 0.0001
Pure Error	0.44	4	0.11		
Cor Total	18978	28			

\* *df* : degree of freedom

**Table 4** Box–Behnken model results for ultrasonication assisted direct transesterification.

Run	Time (min)	Catalyst (%)	Methanol/oil ratio (w/w)	Lipid conversion efficiency (%)
1	60	3	6	25.1
2	40	3	183	92.3
3	40	3	183	93.0
4	40	5	6	25.8
5	20	3	6	28.9
6	40	5	360	95.9
7	40	1	6	25.9
8	40	3	183	93.9
9	60	5	183	94.1
10	40	1	360	93.9
11	20	1	183	90.1
12	40	3	183	92.1
13	60	1	183	93.4
14	20	3	360	92.2
15	20	5	183	95.5
16	60	3	360	92.2
17	40	3	183	94.2

*R-Squared = 0.998. Adj R-Squared = 0.997. Pred R-Squared = 0.983.*



**Table 5** Comparative study of *in situ* transesterification methods

	<b>Conventional</b>	<b>Ultrasonication</b>	<b>Microwave</b>
Time	12 h	20 min	20 min
Temperature (°C)	60	25	100
Power requirements	-	700 W	400 W
Differences	<ul style="list-style-type: none"> <li>- Easy separation</li> <li>- Longer time</li> <li>- Higher methanol content</li> </ul>	<ul style="list-style-type: none"> <li>- Difficulty of separation (12 h)</li> <li>- Emulsification and saponification</li> <li>- Reduced time</li> </ul>	<ul style="list-style-type: none"> <li>- Separation and purification steps not required (5 min)</li> <li>- No emulsification</li> <li>- Reduced time</li> <li>- Lower catalyst and methanol amount</li> </ul>

**Table 6** Comparison of fatty acid profiles of biodiesel produced using transesterification methods.

Fatty acids	Conventional transesterification			Microwave transesterification			<i>in-situ</i> Ultrasonication transesterification		
	6:1	183:1	360:1	6:1	183:1	360:1	6:1	183:1	360:1
C14:0	ND	0.5	ND	ND	0.5	0.5	ND	0.5	0.5
C15:0	ND	0.5	0.5	0.5	0.5	0.5	0.4	0.5	0.5
C16:0	22.1	26.5	28.4	25.9	28.2	28.5	25.7	28.5	28.7
C16:1	0.4	0.9	0.7	1.1	1.0	1.1	1.1	1.0	1.0
C18:0	9.0	9.9	10.5	9.2	9.9	10.1	9.3	10.1	10.2
C18:1	39.4	48.0	48.5	44.4	49.3	46.7	44.1	49.2	49.3
C18:2	28.5	11.8	10.3	19.0	8.9	9.0	18.1	8.1	8.9
C20:0	0.6	1.0	1.1	1.2	1.2	0.9	1.3	1.0	1.1
C22:0	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27	0.27
C24:0	0.29	0.30	0.31	0.30	0.31	0.30	0.29	0.30	0.30

*The fatty acid content is less than 0.5% was not given.*

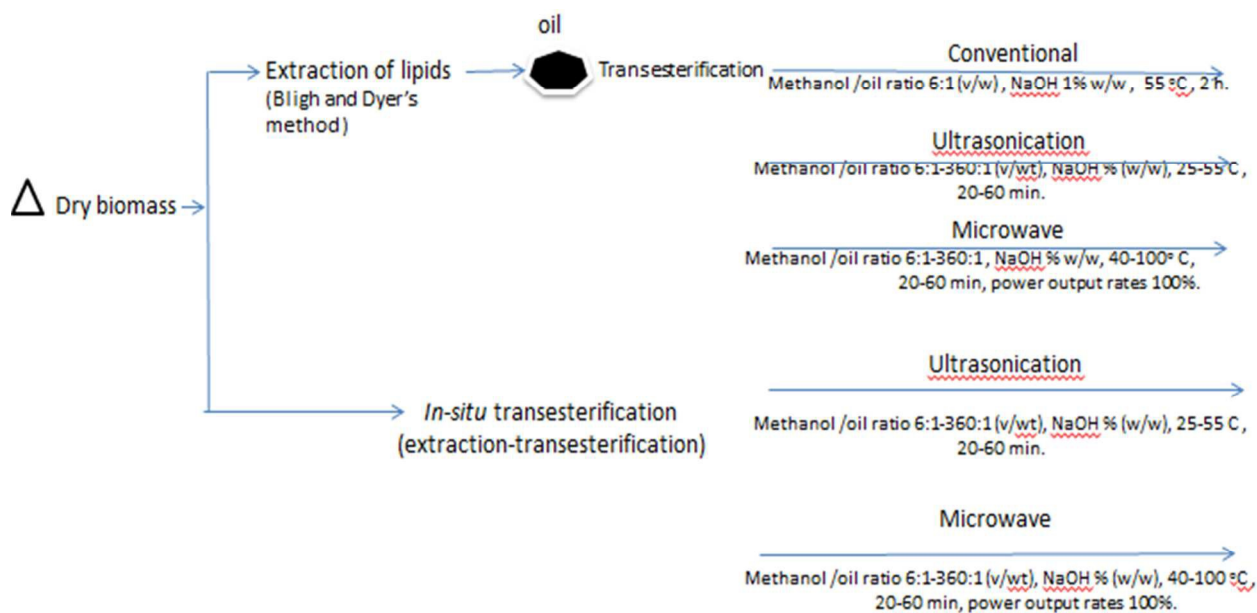
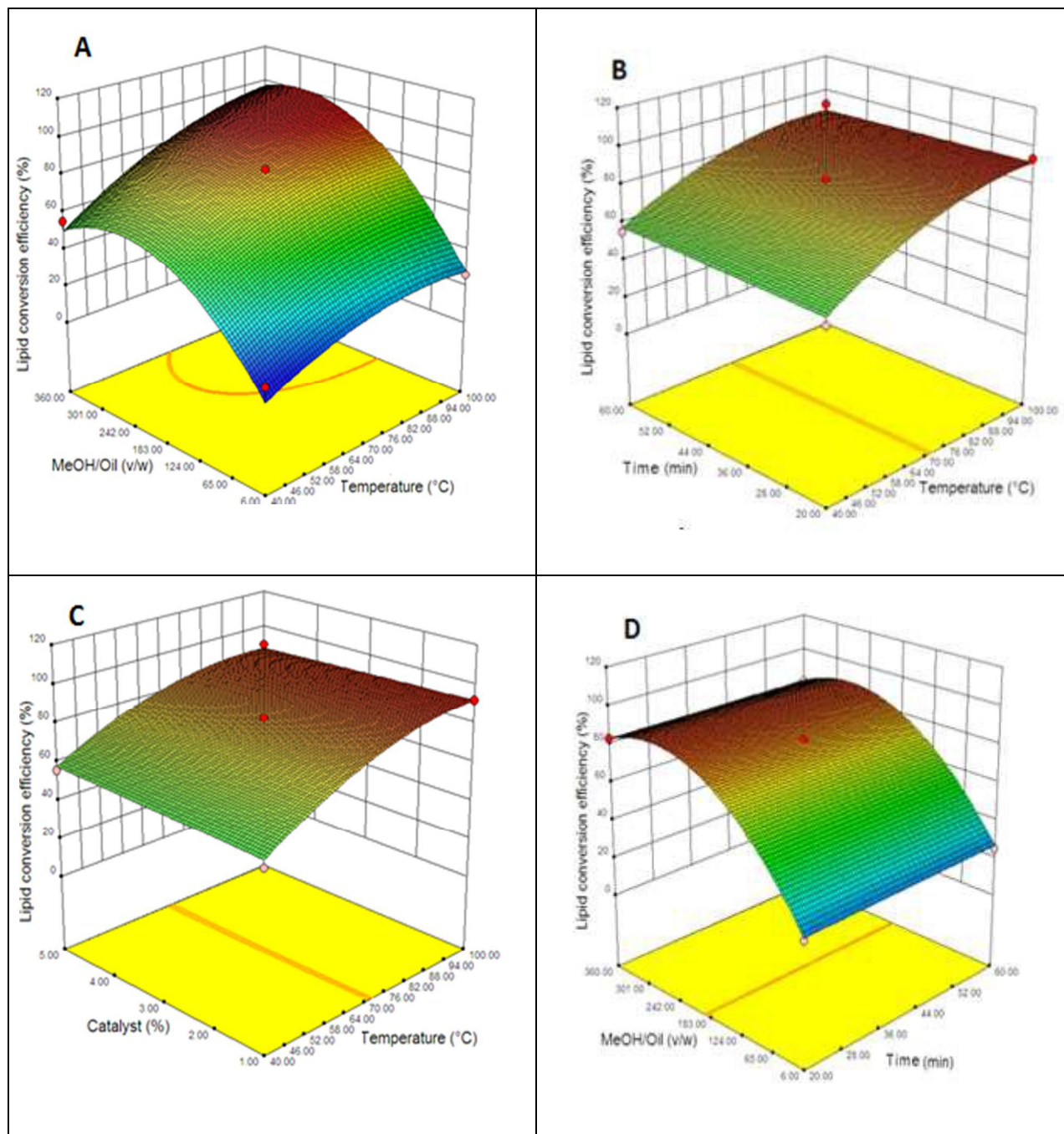


Fig. 1.



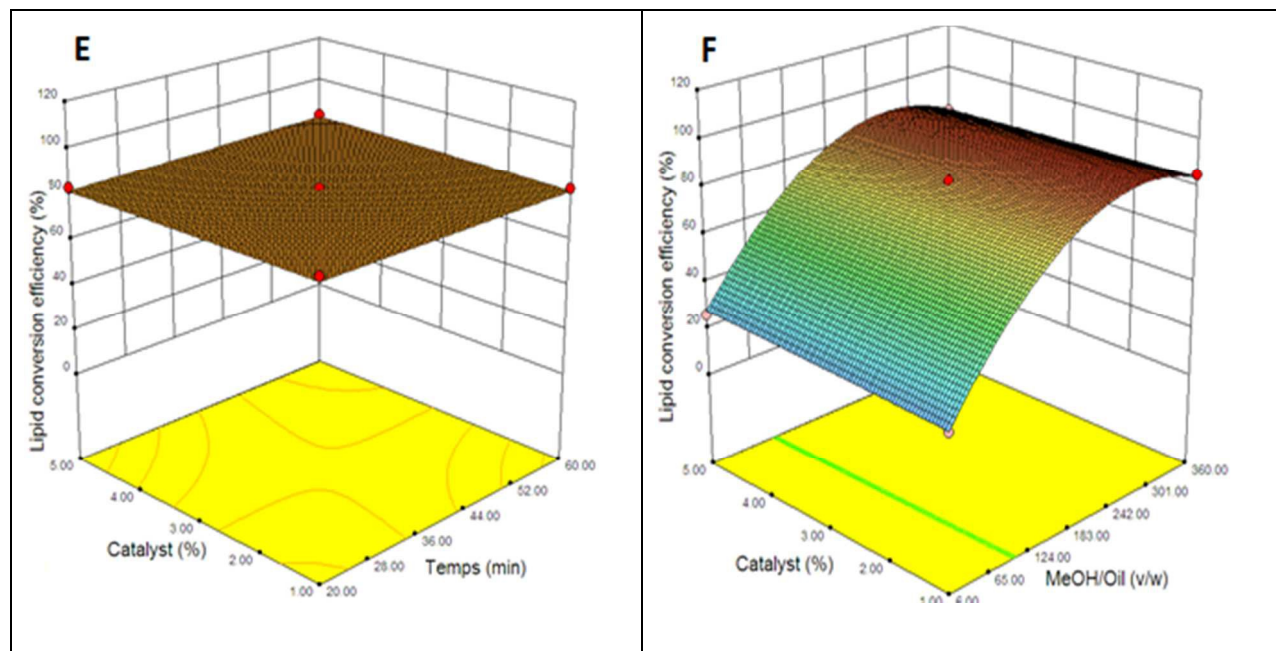


Fig. 2.

**Graphical Abstract**

