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## ARTICLE

## First-principles microkinetic modeling of partial methane oxidation over graphene-stabilized single-atom Fe-catalysts

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Catalytic conversion of CH<sub>4</sub> to transportable liquid hydrocarbons via partial oxidation is a promising avenue towards efficient utilization of natural gas. Single Fe atoms on N-functionalized graphene (FeN<sub>4</sub>/GN) have recently been shown to be active for partial CH<sub>4</sub> oxidation with H<sub>2</sub>O<sub>2</sub> at room temperature. Here, density functional theory (DFT) calculations combined with mean-field microkinetic modeling (MKM) have been applied to obtain kinetic understanding of partial CH<sub>4</sub> oxidation with H<sub>2</sub>O<sub>2</sub> to CH<sub>3</sub>OH and CH<sub>3</sub>OOH over FeN<sub>4</sub>/GN. CH<sub>3</sub>OH and CH<sub>3</sub>OOH are found to be minor and major reaction products, respectively, with a selectivity in agreement with reported experimental data. The kinetic modeling reveals two pathways for CH<sub>3</sub>OH production together with a dominant catalytic cycle for CH<sub>3</sub>OOH formation. The selectivity is found to be sensitive to the temperature and H<sub>2</sub>O<sub>2</sub> concentration, with the CH<sub>3</sub>OH selectivity increasing with increasing temperature and decreasing H<sub>2</sub>O<sub>2</sub> concentration. Turnover frequencies of both CH<sub>3</sub>OH and CH<sub>3</sub>OOH are found to decrease over time, due to a change in the Fe formal oxidation state from +6 to +4; Fe(+6) is more active, but less stable than Fe(+4). The present work unravels the detailed reaction mechanism for partial oxidation of methane by FeN<sub>4</sub>/GN, rationalizes experimental observations and provides guidance for efficient room-temperature methane conversion by single-atom Fe-catalysts.

### Introduction

Natural gas is still one of the most important energy sources.<sup>1</sup> The share of natural gas in global energy production has gradually increased over the last decade due to its vast reserves and less CO<sub>2</sub> released per produced energy unit compared to other fossil fuels.<sup>1,2</sup> Nevertheless, natural gas associated with petroleum extraction has been flared since its utilization is not profitable and CH<sub>4</sub> (the largest component of natural gas) has a much higher global warming potential than CO<sub>2</sub>.<sup>3</sup> The amount of natural gas flared worldwide is as much as 17% of the total natural gas consumption in the United States.<sup>1,4</sup> CH<sub>4</sub> is flared because of challenges handling gaseous products at the sites of petroleum extraction and the lack of processes for small scale on-site catalytic conversion to liquid products. The commercial CH<sub>4</sub>-to-CH<sub>3</sub>OH conversion process is presently syngas production followed by Fischer-Tropsch synthesis, which are highly centralized and energy intensive processes.<sup>5-7</sup>

Small-scale on-site catalytic conversion of CH<sub>4</sub> to liquid hydrocarbon could be a promising avenue toward valorizing natural gas that presently is being wasted. The liquid derivatives of CH<sub>4</sub> can replace natural gas as a primary energy source since the storage and transportation of liquid products are safer and less costly than those of gaseous products. Further, the possible

products, e.g., alcohols and olefins, are value-added chemicals with high industrial demand. Especially, methanol (CH<sub>3</sub>OH) is a valuable target chemical, since it can be used as both a fuel for combustion engines<sup>8</sup> or fuel cells,<sup>9,10</sup> and chemical feedstock for a range of chemicals, such as methyl tertiary-butyl ether,<sup>11</sup> dimethyl ether,<sup>12</sup> and formaldehyde<sup>13</sup>. Hence, significant research has been recently devoted to study catalysts for direct partial CH<sub>4</sub> oxidation at low temperatures. Direct partial oxidation of CH<sub>4</sub> is challenging due to the chemical inertness of CH<sub>4</sub>.<sup>14</sup> High temperatures facilitate C–H bond activation, but with the risk of over-oxidation of CH<sub>3</sub>OH to CO<sub>2</sub>, as the C–H bond of CH<sub>3</sub>OH is weaker than that of CH<sub>4</sub>.<sup>14,15</sup> Thus, CH<sub>4</sub>-to-CH<sub>3</sub>OH conversion should be performed at low temperatures. Over-oxidation could be suppressed by having well-defined catalytic sites with single metal centers embedded in an inert matrix. However, single metal centers may not be multifunctional and active for O<sub>2</sub> activation (in addition to CH<sub>4</sub> activation), requiring oxidants such as N<sub>2</sub>O and H<sub>2</sub>O<sub>2</sub>.<sup>16</sup>

Metal- and metal oxide-based homogeneous catalysis for CH<sub>4</sub> activation has been widely studied since the 1980s.<sup>17-23</sup> Among many catalysts, CoO<sup>+</sup> and FeO<sup>+</sup> showed activity toward CH<sub>4</sub>-to-CH<sub>3</sub>OH conversion.<sup>18,19</sup> Periana and coworkers demonstrated high activity of Hg(II) and Pt(II) salts in a concentrated H<sub>2</sub>SO<sub>4</sub> solution.<sup>24,25</sup> Moreover, partial oxidation of CH<sub>4</sub> can be performed over methane monooxygenases (MMOs) at room-temperature.<sup>26-29</sup> Despite the partial successes, homogeneous catalysis has intrinsic constraints for commercialization as it requires additional product separation processes, which has motivated research efforts in developing heterogeneous catalysts for CH<sub>4</sub> conversion. Especially, biomimetic partial oxidation of CH<sub>4</sub> using Fe- and Cu-based

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zeolite catalysts has attracted interest. The Fe sites of Fe-ZSM-5 obtain active oxygen species ( $\alpha$ -oxygen) from nitrous oxide ( $\text{N}_2\text{O}$ ), which can convert  $\text{CH}_4$  to  $\text{CH}_3\text{OH}$ .<sup>30-32</sup> The active binuclear Fe center of Fe-ZSM-5 resembles the di-iron center of soluble-MMO enzymes.<sup>30-32</sup> Likewise, Cu-ZSM-5 catalysts have shown activity towards  $\text{CH}_4$ -to- $\text{CH}_3\text{OH}$  conversion, mimicking particulate-MMO enzymatic systems, although the nature of the active centers has not been completely understood.<sup>33-35</sup> One severe drawback of the zeolite-based catalysts is that they require elevated temperatures ( $\geq 200$  °C) for the extraction of  $\text{CH}_3\text{OH}$  due to the hydrophilic nature of the zeolite framework.<sup>33,36</sup>

In 2018, Cui and coworkers reported room-temperature activity for partial  $\text{CH}_4$  oxidation over N-functionalized single Fe atom catalyst stabilized on graphene ( $\text{FeN}_4/\text{GN}$ ) with  $\text{H}_2\text{O}_2$  as oxidant.<sup>37</sup> The measured reaction products included  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{OOH}$ ,  $\text{HOCH}_2\text{OOH}$ , and  $\text{HCOOH}$ , where the two last species were suggested to originate from  $\text{CH}_3\text{OH}$  oxidation.<sup>37</sup> Over-oxidation of the reaction product to  $\text{CO}_2$  was significantly suppressed probably owing to the low operating temperature (25 °C) and the isolated nature of the active center (6.3% selectivity for  $\text{CO}_2$ ).<sup>37</sup> The  $\text{CH}_4$  conversion is comparable to, or higher than, that of zeolite-based catalysts operated at higher temperatures.<sup>38,39</sup>

We have previously performed Density Functional Theory (DFT) calculations to elucidate the reaction paths for partial  $\text{CH}_4$  oxidation over  $\text{FeN}_4/\text{GN}$ .<sup>40</sup> Plausible reaction mechanisms were identified that demonstrated the role of  $\text{H}_2\text{O}_2$  as a key reacting species to produce  $\text{CH}_3\text{OH}$ .<sup>40</sup> Moreover, the Energetic span model proposed by Kozuch and Shaik<sup>41</sup> was applied to estimate the turnover frequencies (TOFs) of different reaction pathways and get activity trends from individual reaction mechanisms. However, the Energetic span model is an over-simplification in this case as it does not account for nested reaction paths and, moreover, does not properly account for the operating conditions, e.g., the reactant concentrations. In addition, our previous work focused primarily on mechanisms producing  $\text{CH}_3\text{OH}$  without considering other products.<sup>40</sup>

Herein, we develop a first-principles-based mean-field microkinetic model (MKM) for  $\text{CH}_4$  conversion on  $\text{FeN}_4/\text{GN}$  catalyst. First-principles-based MKM is a powerful tool to provide unbiased kinetic information on TOF, selectivity, apparent activation energy, reaction-orders, surface coverages and rate-controlling reaction steps over a variety of complicated heterogeneous catalytic systems.<sup>42-49</sup> The multiple reaction mechanisms determined using the DFT calculations are coupled in the MKM to examine the kinetic properties of nested catalytic cycles with a dynamic change in the Fe oxidation state.<sup>40</sup> Moreover, to compare with experiments, additional reaction mechanisms for the conversion of  $\text{CH}_4$  to methyl hydroperoxide ( $\text{CH}_3\text{OOH}$ ), which is another major reaction product<sup>37</sup>, have been investigated with DFT and included in the kinetic modeling. The present first-principles-based MKM rationalizes experimental observations, demonstrating the capability of MKM to model a highly complex reaction network and provide a fundamental understanding of the active nature of  $\text{FeN}_4/\text{GN}$  catalyst. This work can guide further efforts on designing

efficient catalysts for  $\text{CH}_4$  conversion to value-added fuels and chemicals.

## Computational details

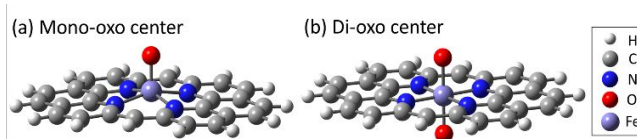
### Density functional theory calculations

Density functional theory (DFT) calculations were performed with the Gaussian 09 software package at the B3LYP/6-31G(d) level of theory.<sup>50-52</sup> Comparative computations with the M06-2X functional yields similar results.<sup>40</sup> Vibrational frequency calculations were performed to confirm that the stationary points are either minima or saddle points. The optimized transition state (TS) structures were confirmed to connect the corresponding reactants and products by Intrinsic Reaction Coordinate calculations.<sup>53</sup>  $\text{FeN}_4/\text{GN}$  is modeled having a central single Fe atom, which is anchored by 4 N atoms to a graphene flake (represented by 26 C atoms terminated by H atoms on the edges). The reaction energetics depend very weakly on the size of the graphene flake (Figure S1). Two different types of active centers were considered<sup>40</sup>: singly oxygenated (mono-oxo) and doubly oxygenated (di-oxo) centers (Figure 1). As the reaction takes place in water experimentally,<sup>37</sup> solvent effects were considered in all calculations by applying the conductor-like polarizable continuum model (CPCM)<sup>54</sup> with water as the solvent. The reaction energetics were described in terms of Gibbs free energy at 298.15 K and 1 atm, unless otherwise specified in the results. The enthalpic and entropic contributions to Gibbs free energy of reaction are assumed to be constant within the small temperature range considered (278.15 - 318.15 K). Hence, Gibbs free energy of reaction at temperature T was calculated as:

$$\Delta G_{rxn, T} = \Delta H_{rxn, 298.15 K} - T * \Delta S_{rxn, 298.15 K} \#(1)$$

Entropy values reported in ref.<sup>55</sup> (at 298.15 K in water) were used for all the molecules except  $\text{CH}_3\text{OOH}$ , which is unavailable in the literature. The entropy of  $\text{CH}_3\text{OOH}$  was therefore determined by multiplying a factor of 0.62 to the gas-phase DFT-determined entropy, based on the simple scaling relation reported in Ref.<sup>56</sup> This scaling factor is very similar to how the experimental and gas-phase calculated entropies of  $\text{H}_2\text{O}_2$  scale (Table S1), demonstrating the validity of this selection considering the structural similarity between the  $\text{CH}_3\text{OOH}$  and  $\text{H}_2\text{O}_2$  molecules. For the structures involving the catalyst surfaces, real vibrational frequencies lower than  $100 \text{ cm}^{-1}$  were replaced by  $100 \text{ cm}^{-1}$  when determining entropies and free energies to reduce errors that can emerge from calculations of low-frequency modes.<sup>57</sup> The studied mechanisms are presented in Figure 2 (*vide infra*) and in Section 2 of the Supplementary Information file.

### Microkinetic model



**Figure 1** Catalyst structures with (a) mono-oxo and (b) di-oxo  $\text{FeN}_4/\text{GN}$  centers.

The microkinetic model consists of a system of coupled ordinary differential equations, which describe the time-evolution of the concentration of species. The differential equations have the form:

$$\frac{dc_i}{dt} = \sum_j v_{ij} r_j(\vec{c}) \quad \#(2)$$

where  $c_i$  is the concentration of species  $i$ ,  $r_j$  is the rate of reaction  $j$ , which is a function of concentrations  $\vec{c}$ , and  $v_{ij}$  is the stoichiometric number of species  $i$  in reaction  $j$ . For the FeN<sub>4</sub>/GN system, 'species' are unique complexes between the Fe-center and some (or none) ligands, which include a single oxygen (mono-oxo center), two oxygens (di-oxo center) and other ligands that appear as intermediates in catalytic cycles. The di-oxo center has an initial concentration of unity as it has been suggested to be an active center.<sup>37</sup> The fraction (coverage) of species  $i$  ( $x_i$ ) is defined as the ratio of the number of species  $i$  ( $n_i$ ) to the total number of all the possible species:

$$x_i = \frac{n_i}{\sum_i n_i} \quad \#(3)$$

The mole fractions of all species obey the summation:

$$\sum_i x_i = 1 \quad \#(4)$$

In the case of FeN<sub>4</sub>/GN, the entire catalytic cycle is assumed to take place at single Fe-centers, with no interaction or cross-reactions between adjacent Fe-centers. Thus, each elementary reaction is first order, with the forward (backward) reaction rate depending only on the concentration of the reactant (product) species multiplied by the rate constant. The rate constants of reactions are calculated according to transition-state theory as:

$$k = \frac{k_B T}{h} \exp \left[ -\frac{\Delta G^\ddagger}{k_B T} \right] \quad \#(5)$$

where  $k_B$  is the Boltzmann constant,  $T$  is the temperature, and  $\Delta G^\ddagger$  is the standard Gibbs free energy barrier determined using DFT calculations as previously described.

Adsorption of a free species (e.g., CH<sub>4</sub> and H<sub>2</sub>O<sub>2</sub>) from the solution to the catalyst surface is taken to be purely diffusion-controlled, where the catalyst is assumed to be a stationary 2-D flake, giving the following expression for the adsorption rate constant  $k_a$ .<sup>58</sup>

$$k_a = 4r_a D_i c_i \quad \#(6)$$

where  $r_a$  is the radius of the active site, and  $D_i$  and  $c_i$  are the diffusivity and the bulk concentration of the adsorbing species  $i$ , respectively. The diffusivity of a free species is obtained by the Stokes-Einstein equation:

$$D_i = \frac{k_B T}{6\pi\eta r_i} \quad \#(7)$$

where  $\eta$  is the viscosity of the fluid and  $r_i$  is the radius of the species. The viscosity of the fluid is approximated by the dynamic viscosity of water at room temperature. The relative radius of the adsorption center of the catalyst to free species is approximated to be 4 (i.e.,  $r_a = 4r_i$ ), considering the larger size of the FeN<sub>4</sub> center compared to free molecules. This leads to the adsorption rate constant given by:

$$k_a = \frac{8 k_B T}{3\pi \eta} c_i \quad \#(8)$$

Note that the unit of  $k_a$  is s<sup>-1</sup>. The desorption rate constants  $k_d$  are calculated from the adsorption rate constant via the equilibrium constant  $K_{eq}$ :

$$K_{eq} = \frac{k_a}{k_d} = \exp \left[ -\frac{\Delta G}{k_B T} \right] \quad \#(9)$$

$\Delta G$  is the free energy change of adsorption. Solving eqn. 9 for  $k_d$  gives:

$$k_d = k_a \exp \left[ \frac{\Delta G}{k_B T} \right] \quad \#(10)$$

Note that  $k_d$  (unit s<sup>-1</sup>) is independent of the bulk concentration of the desorbing species.

The coupled ODEs were solved using a Python 3-based code with the `solve_ivp` function from the Scipy package<sup>59</sup> `scipy.integrate`. The integration intervals were chosen to be long enough (10<sup>4</sup> seconds in general) to ensure that a steady state is reached.

Degree of rate control (DRC) and degree of selectivity control (DSC) analyses<sup>60</sup> were performed to identify elementary steps with rate control of the CH<sub>3</sub>OH and CH<sub>3</sub>OOH formation and the CH<sub>3</sub>OH selectivity. DRC of elementary step  $i$  ( $X_{RC,i}$ ) is defined as:

$$X_{RC,i} = \frac{k_i}{r} \left( \frac{\partial r}{\partial k_i} \right)_{k_{j \neq i}, K_i} \quad \#(11)$$

where  $k_i$  is the forward rate constant of step  $i$  and  $r$  is the overall reaction rate. The  $X_{RC,i}$  is approximated with a finite difference method, performed by lowering the forward and backward rate constant of a single elementary step by 1%, while all the other rate constants  $k_i$  are unvaried, and observing the change in the overall reaction rate at steady state. A positive  $X_{RC,i}$  value indicates a rate-limiting step, whereas a negative value indicates an inhibition step.<sup>60</sup> The degree of selectivity control  $X_{SC,i}$  of an elementary step  $i$  is defined as:

**Table 1** Reaction conditions and parameters for microkinetic modeling.

Parameter	Symbol	Value	Units
Standard molarity	$c^\circ$	1	mol·dm <sup>-3</sup>
H <sub>2</sub> O <sub>2</sub> concentration†	[H <sub>2</sub> O <sub>2</sub> ]	5	mol·dm <sup>-3</sup>
H <sub>2</sub> O concentration	[H <sub>2</sub> O]	50	mol·dm <sup>-3</sup>
CH <sub>4</sub> concentration†	[CH <sub>4</sub> ]	0.03	mol·dm <sup>-3</sup>
CH <sub>3</sub> OH concentration	[CH <sub>3</sub> OH]	1e-5	mol·dm <sup>-3</sup>
CH <sub>3</sub> OOH concentration	[CH <sub>3</sub> OOH]	1e-5	mol·dm <sup>-3</sup>
Dynamic viscosity of water	$\eta$	890.2 <sup>61</sup>	μPa·s
Henry's constant of CH <sub>4</sub> in water	$H_{CH_4}$	38741 <sup>62</sup>	bar

†Based on the experimental condition<sup>37</sup>

$$X_{SC,i} = \frac{1}{S} \left( \frac{\partial S}{\partial k_i} \right)_{k_j \neq i, K_i} \quad \#(12)$$

where  $S$  is the CH<sub>3</sub>OH selectivity, which is defined as the ratio of the catalyst's TOF to CH<sub>3</sub>OH to the sum of the TOFs to both products.

The reaction orders of CH<sub>3</sub>OH and CH<sub>3</sub>OOH formation were determined with respect to each reactant (CH<sub>4</sub> and H<sub>2</sub>O<sub>2</sub>) as calculated from:

$$n_i = \frac{\partial \ln r}{\partial \ln c_i} \quad \#(13)$$

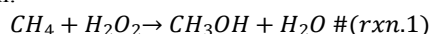
where  $r$  is the net reaction rate and  $c_i$  is the concentration of the reactant  $i$ . The partial derivatives were approximated by finite differences by increasing  $c_i$  by 1%, while all the other parameters were kept constant. Apparent activation energies for CH<sub>3</sub>OH and CH<sub>3</sub>OOH formation were calculated from the slopes of their respective Arrhenius plots in the temperature range from 278.15 to 318.15 K. This approach is valid as the plots were found to be linear in the tested temperature range. Reaction conditions and parameters used in the MKM are listed in Table 1.

Further details on MKM can be found in the Supplementary Information Section 3 and the assumptions made in the diffusion model are discussed in the Supplementary Information Section 4.

## Results and discussion

### Methane conversion mechanisms

**CH<sub>3</sub>OH formation.** Prior work<sup>40</sup> identified 11 different mechanisms of CH<sub>4</sub>-to-CH<sub>3</sub>OH conversion over FeN<sub>4</sub>/GN. Gibbs free energy profiles of some relevant pathways are reproduced here (Figures 2, S1, and S2) for completeness and as additional corrections have been made to the Gibbs free energies for higher accuracy (see Computational details). Figure 2a and b shows two important mechanisms for CH<sub>4</sub>-to-CH<sub>3</sub>OH conversion with the net reaction:

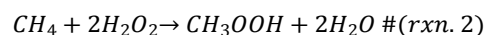


Path 1 proceeds over the di-oxo species and is an H<sub>2</sub>O<sub>2</sub>-mediated radical mechanism (Figure 2a). The di-oxo center breaks a primary C–H bond of CH<sub>4</sub> to generate a methyl radical

(CH<sub>3</sub>·), which reacts with H<sub>2</sub>O<sub>2</sub> to give CH<sub>3</sub>OH and a hydroxyl radical (OH·). Thereafter, the hydroxyl radical abstracts H from the hydroxyl center to regenerate the di-oxo-center. Path 2 proceeds over the mono-oxo species and is a Fenton-type reaction mechanism (Figure 2b). The O=O bond of H<sub>2</sub>O<sub>2</sub> is in this case homolytically dissociated at the bare Fe side of the mono-oxo center (bottom of the structure shown in Figure 1(a)), producing a hydroxyl radical and hydroxylating the Fe site. The hydroxyl radical activates CH<sub>4</sub> to CH<sub>3</sub>·, which is converted to CH<sub>3</sub>OH by abstracting the hydroxyl surface ligand.

Additional mechanisms include one on a di-oxo center (direct radical mechanism as path 4; Figure S2) and two on a mono-oxo center (direct and H<sub>2</sub>O<sub>2</sub>-mediated radical mechanisms as path 5 and 6, respectively; Figure S3). These pathways are associated with higher barriers either for the recovery of the active center (path 4) or homolytic C–H dissociation of CH<sub>4</sub> (paths 5 and 6). Importantly, the different reaction mechanisms share some common states. For example, Paths 1 and 2 have common state 3 (Figure 2), which suggests a possibility of a larger reaction network with a dynamic oxidation state of Fe along the reaction coordinate.

**CH<sub>3</sub>OOH formation.** CH<sub>3</sub>OOH is another major, experimentally observed, reaction product.<sup>37</sup> Thus, we examine reaction mechanisms for CH<sub>4</sub> conversion to CH<sub>3</sub>OOH on both the di-oxo (Path 3 in Figure 2) and mono-oxo (Path 7 in Figure S3) centers. The four first elementary steps of path 3 are identical to those in Path 1; the di-oxo center homolytically dissociates the primary C–H bond of CH<sub>4</sub>, and one H<sub>2</sub>O<sub>2</sub> is adsorbed on the surface. Thereafter, one H from H<sub>2</sub>O<sub>2</sub> is abstracted by the hydroxylated center, and CH<sub>3</sub>· species is combined with the remaining ·OOH simultaneously, producing surface water and CH<sub>3</sub>OOH (TS7). This radical mechanism resembles the CH<sub>4</sub> conversion by Pd/MoO<sub>3</sub> photocatalyst reported in Ref.<sup>63</sup> Next the surface water is dehydrogenated (to OH) by a second H<sub>2</sub>O<sub>2</sub>, producing one water molecule and a hydroxyl radical (OH·) as the O=O bond of H<sub>2</sub>O<sub>2</sub> is dissociated (TS8). This step involves the highest activation energy in the pathway ( $\Delta G^\ddagger = 1.00$  eV). The remaining hydroxyl center is further dehydrogenated by OH·, regenerating the di-oxo active center and closing the catalytic cycle. The mono-oxo counterpart of path 3 is path 7 in Figure S3, which involves a high activation energy for the C–H bond cleavage (TS10,  $\Delta G^\ddagger = 1.52$  eV). Hence, substantial formation of CH<sub>3</sub>OOH is only possible via path 3. The net reaction of the mechanism for this reaction is:



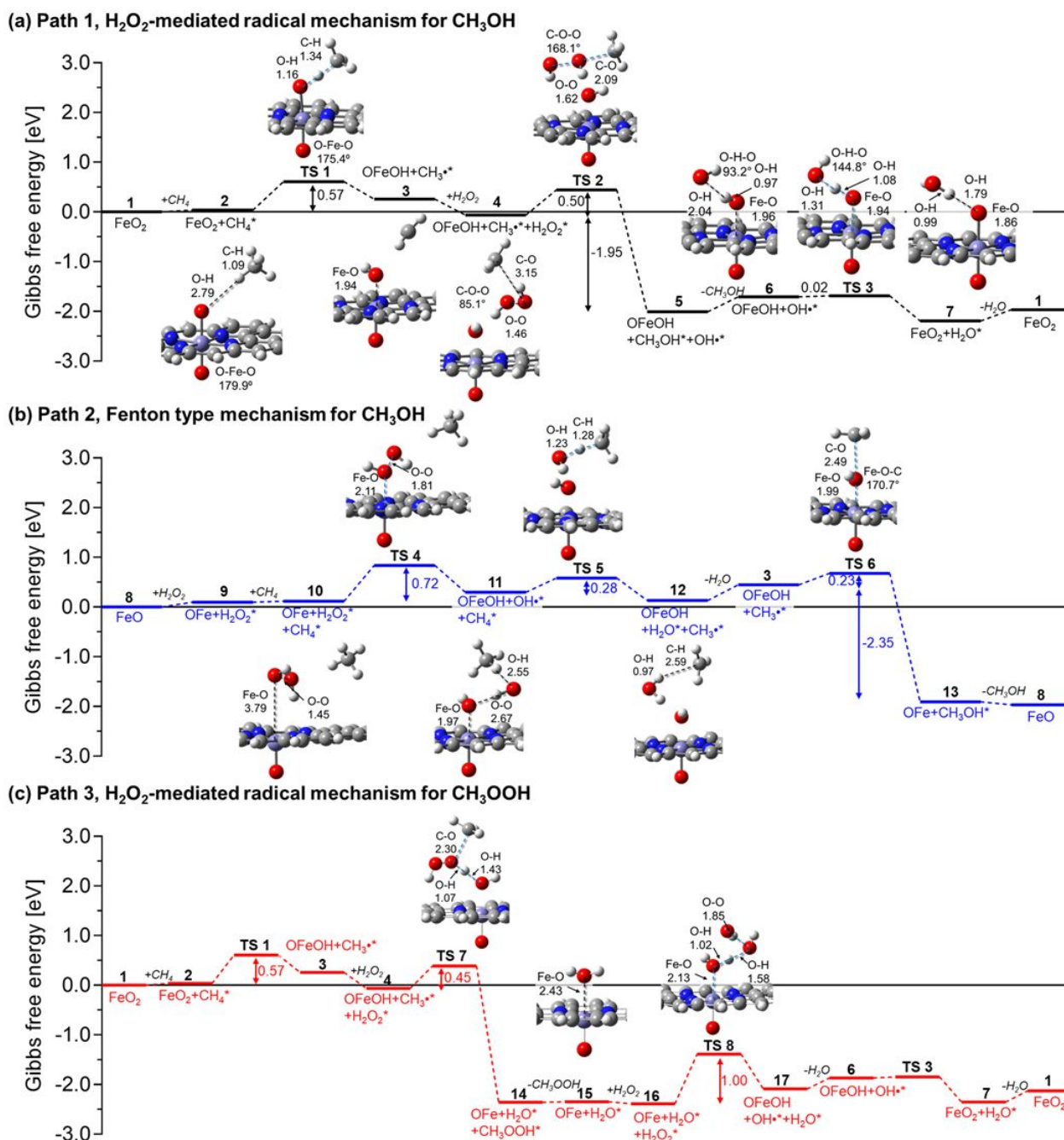
There are two important observations on Path 3: First, TS7 (producing CH<sub>3</sub>OOH) competes with TS2 of path 1 (producing CH<sub>3</sub>OH) since they share the reactant state (state 4), where the barrier for CH<sub>3</sub>OOH formation is lower than that of CH<sub>3</sub>OH formation, which indicates a preference for CH<sub>3</sub>OOH formation over the di-oxo center. Second, state 15 (after CH<sub>3</sub>OOH has desorbed) is essentially a mono-oxo center with a water molecule on the bare Fe side. If the water desorbs (instead of going through the remaining steps in path 3), then the system is converted to the bare mono-oxo state (state 8). Conversely, if one water molecule adsorbs on the bare Fe site of the



mono-oxo catalyst and reacts with  $\text{H}_2\text{O}_2$  (through TS8), it forms the di-oxo center. These scenarios provide routes to connect different reaction mechanisms on two different active centers. To investigate the possibility of dynamic behavior of the active center, the additional elementary step of water adsorption on the bare Fe site of the mono-oxo center is considered in the MKM.

### Microkinetic modeling

**Reaction network.** We carried out MKM calculations with the parameters in Table 1 using either the full reaction mechanism or a reduced set of the reaction mechanisms. For the full reaction mechanism, all the reaction pathways on both the di- and mono-oxo centers (i.e., paths 1-7) are considered. For the reduced set of reaction mechanisms, only three energetically feasible mechanisms (i.e., paths 1-3) were included. The differences of the total TOFs between the full reaction mechanisms and the reduced set of the reaction mechanisms are negligible owing to the high barriers in paths 4-7 (see



**Figure 2** Detailed Gibbs free energy profiles of  $\text{CH}_4$ -to- $\text{CH}_3\text{OH}$  conversion at 25 °C following (a) Path 1 -  $\text{H}_2\text{O}_2$ -mediated radical mechanism on the di-oxo center, (b) Path 2 - Fenton type mechanism on the mono-oxo center, and (c) Path 3 -  $\text{CH}_4$ -to- $\text{CH}_3\text{OOH}$  conversion following  $\text{H}_2\text{O}_2$ -mediated radical mechanism on the di-oxo center. “Fe” on the profiles stands for the  $\text{FeN}_4/\text{GN}$  catalyst structure, and “TS” represents the transition state. Asterisk (\*) denotes the adsorbed species on the catalyst surface. Selected interatomic distances (in Å) are shown on the molecular structures.

**Table 2** Steady-state net reaction rates of all elementary steps in the reduced set of the reaction mechanisms calculated by MKM at 25 °C and reaction conditions tabulated in Table 1.

Elementary step†	Step††	Rate (s <sup>-1</sup> )‡	Starting state	Ending state	Pathway
R1 FeO <sub>2</sub> + CH <sub>4</sub> → FeO <sub>2</sub> + CH <sub>4</sub> *	Ads	1.70E-07	1	2	1, 3
R2 FeO <sub>2</sub> + CH <sub>4</sub> * → OFeOH + CH <sub>3</sub> *	TS1	1.70E-07	2	3	1, 3
R3 OFeOH + CH <sub>3</sub> * + H <sub>2</sub> O <sub>2</sub> → OFeOH + CH <sub>3</sub> * + H <sub>2</sub> O <sub>2</sub> *	Ads	1.47E-06	3	4	1, 3
R4 OFeOH + CH <sub>3</sub> * + H <sub>2</sub> O <sub>2</sub> * → OFeOH + CH <sub>3</sub> OH* + OH*	TS2	1.75E-07	4	5	1
R5 OFeOH + CH <sub>3</sub> OH* + OH* → OFeOH + CH <sub>3</sub> OH + OH*	Des	1.75E-07	5	6	1
R6 OFeOH + OH* → FeO <sub>2</sub> + H <sub>2</sub> O*	TS3	1.70E-07	6	7	1, 3
R7 FeO <sub>2</sub> + H <sub>2</sub> O* → FeO <sub>2</sub> + H <sub>2</sub> O	Des	1.70E-07	7	1	1, 3
R8 FeO + H <sub>2</sub> O <sub>2</sub> → OFe + H <sub>2</sub> O <sub>2</sub> *	Ads	1.39E-06	8	9	2
R9 OFe + H <sub>2</sub> O <sub>2</sub> * + CH <sub>4</sub> → OFe + H <sub>2</sub> O <sub>2</sub> * + CH <sub>4</sub> *	Ads	1.39E-06	9	10	2
R10 OFe + H <sub>2</sub> O <sub>2</sub> * + CH <sub>4</sub> * → OFeOH + OH* + CH <sub>4</sub> *	TS4	1.39E-06	10	11	2
R11 OFeOH + OH* + CH <sub>4</sub> * → OFeOH + H <sub>2</sub> O* + CH <sub>3</sub> *	TS5	1.39E-06	11	12	2
R12 OFeOH + H <sub>2</sub> O* + CH <sub>3</sub> * → OFeOH + H <sub>2</sub> O + CH <sub>3</sub> *	Des	1.39E-06	12	3	2
R13 OFeOH + CH <sub>3</sub> * → OFe + CH <sub>3</sub> OH*	TS6	9.37E-08	3	13	2
R14 OFe + CH <sub>3</sub> OH* → FeO + CH <sub>3</sub> OH	Des	9.37E-08	13	8	2
R15 OFeOH + CH <sub>3</sub> * + H <sub>2</sub> O <sub>2</sub> * → OFe + H <sub>2</sub> O* + CH <sub>3</sub> OOH*	TS7	1.30E-06	4	14	3
R16 OFe + H <sub>2</sub> O* + CH <sub>3</sub> OOH* → OFe + H <sub>2</sub> O* + CH <sub>3</sub> OOH	Des	1.30E-06	14	15	3
R17 OFe + H <sub>2</sub> O* + H <sub>2</sub> O <sub>2</sub> → OFe + H <sub>2</sub> O* + H <sub>2</sub> O <sub>2</sub> *	Ads	-5.96E-08	15	16	3
R18 OFe + H <sub>2</sub> O* + H <sub>2</sub> O <sub>2</sub> * → OFeOH + OH* + H <sub>2</sub> O*	TS8	-4.96E-09	16	17	3
R19 OFeOH + OH* + H <sub>2</sub> O* → OFeOH + OH* + H <sub>2</sub> O	Des	-4.96E-09	17	6	3
R20 OFe + H <sub>2</sub> O* → FeO	Des	1.30E-06	15	8	2, 3

† Given as forward reactions. Asterisk (\*) denotes the adsorbed species on the Fe-center.

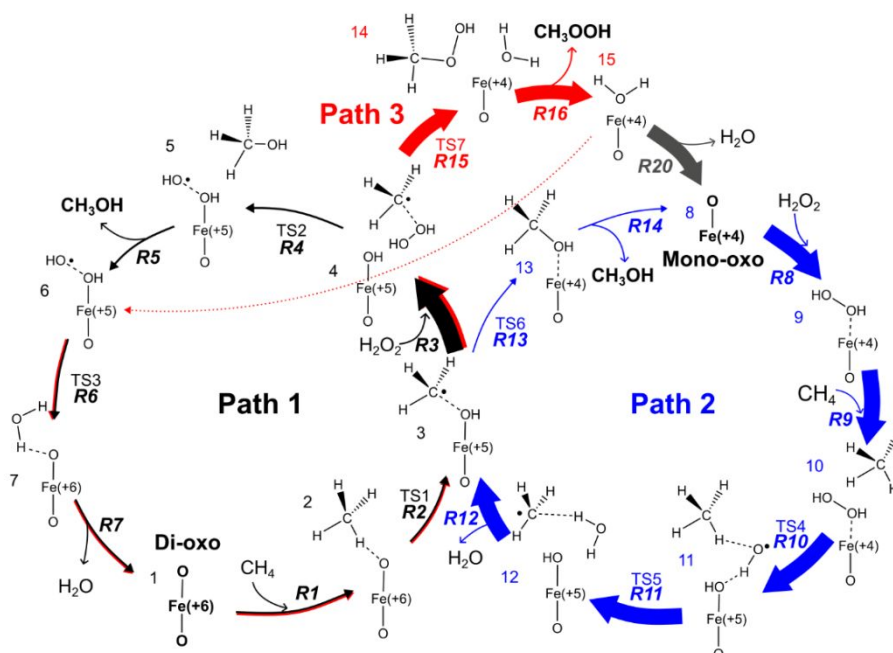
†† "Ads" and "Des" represent adsorption and desorption steps, respectively, and "TS#" stands for the transition state involved in the reaction step.

‡ A negative reaction rate indicates that the backward reaction is faster than the forward reaction.

Supplementary Information Section 3). Hence, the reduced model is used in the present work for convenience to analyze the kinetic behaviour. The elementary reactions included in the reduced model are tabulated in Table 2.

Table 2 shows the states and elementary steps that are shared by different reaction pathways. The elementary steps that include different pathways allow for the construction of a nested reaction network, as visualized in Figure 3. The reaction network is composed of the full pathways of paths 1 and 2 and a part of path

3. The rest steps of path 3 (from state 15 to 6) are presented as a dotted line in Figure 3 with the details being omitted due to the net small negative steady-state reaction rates (R17-19 in Table 2). The arrow width indicates magnitude of elementary reaction rates at steady state (Table 2). Figure 3 shows a catalytic cycle with a high TOF that emerges from the construction of the nested network: starting from a mono-oxo center (state 8; upper right), (1) methyl radical is formed following path 2 (from state 8 to 3; blue arrows), (2) CH<sub>3</sub>OOH is formed following the steps



**Figure 3** Reaction network of CH<sub>4</sub> conversion to CH<sub>3</sub>OH and CH<sub>3</sub>OOH. The arrow width indicates the relative steady-state reaction rate of each elementary step estimated by MKM. "Fe" on each structure stands for the FeN<sub>4</sub>/GN catalyst with the corresponding formal oxidation state of Fe in parenthesis. The reaction labels correspond to the reactions in Table 2 and the color scheme for each pathway is consistent with Figure 2. Mono-oxo and Di-oxo denote the two different states of the catalyst involved in the catalytic cycles and serve as starting points on the nested reaction network.

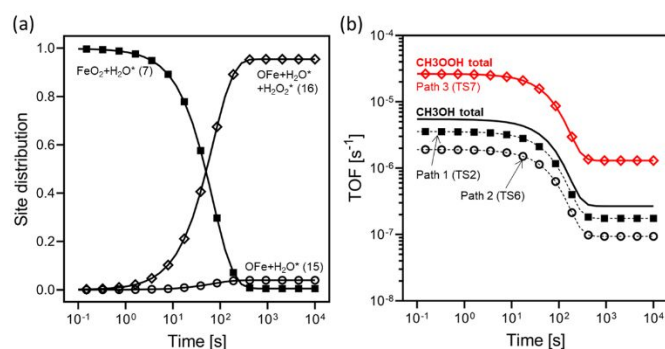
identified in path 3 (from state 3 to 15; red arrows), and (3) the mono-oxo center is regenerated as a surface water molecule desorbs (R20). The product of this catalytic cycle is  $\text{CH}_3\text{OOH}$ , with the net reaction being that of rxn.2. In the cycle, the oxidation state of Fe changes between +4 and +5 (Figure 3).  $\text{CH}_3\text{OH}$  can be produced either via a reaction between methyl radical and hydroxyl center (R13 through TS6, i.e., completing path 2) or following the full path 1 from state 4. The latter involves di-oxo catalyst with the high oxidation state of Fe (+6). The Fe oxidation state changes between +4 and +6, as suggested in our previous work.<sup>37</sup>

Figure 4 shows the time evolution of the site distribution and TOFs. The initial di-oxo site (with one  $\text{H}_2\text{O}$  molecule adsorbed; state 7) is gradually converted to mono-oxo (with adsorbates on the bare Fe site: one  $\text{H}_2\text{O}$  molecule - state 15, or both  $\text{H}_2\text{O}$  and  $\text{H}_2\text{O}_2$  molecules - state 16) over time (Figure 4a). The conversion of the di-oxo state to the mono-oxo state is reasonable given the higher thermodynamic stability of mono-oxo over di-oxo<sup>37</sup> and the high barrier for di-oxo regeneration ( $\Delta G^\ddagger = 1.00$  eV; TS8 in Figure 2c). The conversion of di-oxo accelerates after  $\sim 10$  s and there is a clear switchover from a di-oxo-dominated to a mono-oxo-dominated Fe population at around 50 s. Di-oxo Fe sites have almost completely disappeared at around 400 s.

The TOFs towards both  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  production decrease with time: from  $5\text{e-}6$   $\text{s}^{-1}$  to  $3\text{e-}7$   $\text{s}^{-1}$  for  $\text{CH}_3\text{OH}$  and from  $3\text{e-}5$   $\text{s}^{-1}$  to  $1\text{e-}6$   $\text{s}^{-1}$  for  $\text{CH}_3\text{OOH}$  (Figure 4b). The time evolution of the TOFs is linked to the switchover of the site distribution from di-oxo to mono-oxo. Thus, the di-oxo center is more active than the mono-oxo center for both products but is eventually consumed due to the unfavorable thermodynamics and kinetics of its regeneration. The reaction rates of the individual pathways are shown in Figure 4b (TS2, TS6, and TS7 characterize paths 1, 2, and 3, respectively; see Figure

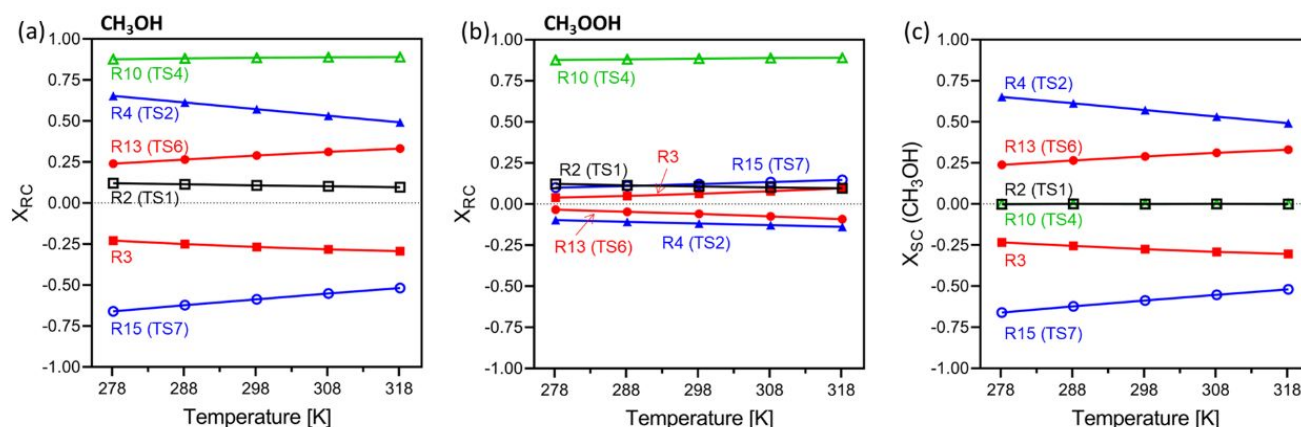
2 for details). The rate of path 3 is identical to the TOF to  $\text{CH}_3\text{OOH}$  as path 3 is the only pathway where  $\text{CH}_3\text{OOH}$  is formed. By contrast,  $\text{CH}_3\text{OH}$  is formed from both paths 1 and 2. The contribution from Path 1 is roughly 2 times of that of Path 2 (Figure 4b).

Four C1 products have been reported experimentally<sup>37</sup>:  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{OOH}$ ,  $\text{HCOOH}$ , and  $\text{HOCH}_2\text{OOH}$ . Cui et al.<sup>37</sup> proposed that the last two products are produced by oxidation of  $\text{CH}_3\text{OH}$ . However, the possibility of  $\text{CH}_3\text{OOH}$  oxidation to these products cannot be ruled out. Wang et al. demonstrated the room-temperature activity of  $\text{FeN}_4/\text{GN}$  towards  $\text{C}_2\text{H}_6$  activation, showing that the  $-\text{OOH}$  derivative ( $\text{CH}_3\text{CH}_2\text{OOH}$ ) can be further converted to a carboxylic acid ( $\text{CH}_3\text{COOH}$ ).<sup>64</sup> A direct comparison of experimental and simulated selectivities is difficult as we do not explore further oxidation of  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$ . Nevertheless, assuming identical consumption rates of  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  (to  $\text{HCOOH}$ , and  $\text{HOCH}_2\text{OOH}$ ), the experimental  $\text{CH}_3\text{OH}$  selectivity is 11% (the amount of  $\text{CH}_3\text{OH}$  divided by the amount of  $\text{CH}_3\text{OH} + \text{CH}_3\text{OOH}$  produced over 10 hours).<sup>37</sup> This is in a good agreement with the MKM-determined  $\text{CH}_3\text{OH}$  selectivity, which is 17% (Figure 4b). It should be noted that the product selectivity is sensitive to the adsorption rate constant ( $k_a$ ). To study the effect of  $k_a$ , the time evolution of the site distribution and TOF are simulated with lower and higher adsorption rate constants (Supplementary Information Section 4 and Figure S7). The active site distribution and the total TOF do not depend on  $k_a$ . However, the  $\text{CH}_3\text{OH}$  selectivity changes to 13% and 29% with 4 times higher and 4 times smaller  $k_a$  than the original  $k_a$  (eqn. 8), respectively. This result shows a possible relationship between product selectivity and diffusion (see eqn. 6) that is independent of the overall  $\text{CH}_4$  conversion by the  $\text{FeN}_4/\text{GN}$  catalyst. The  $\text{CH}_3\text{OH}$  selectivity control strategy by limiting diffusion process has also been suggested by Nørskov et al.<sup>38</sup>



**Figure 4** Change of (a) the distribution of the catalytic site and (b) turnover frequency (TOF) over time up to  $10^4$  s determined by microkinetic modeling (MKM) using a reduced reaction system (paths 1-3) at 25 °C and reaction conditions tabulated in Table 1. On panel (b), the TOF to each product (thick solid lines) is determined as a sum of the rates of the product desorption steps. The TOFs through individual pathways (dotted lines with symbols) represented by reaction rates of their characteristic elementary steps as shown in the parentheses. See Supplementary Information Section 3 for the results with a full reaction system (paths 1-7).





**Figure 5** Degree of rate control ( $X_{RC}$ ) for (a)  $\text{CH}_3\text{OH}$  and (b)  $\text{CH}_3\text{OOH}$ , and (c) degree of selectivity control ( $X_{SC}$ ) of  $\text{CH}_3\text{OH}$ . The elementary steps that compete are shown with the same color. Details of the elementary steps are found in Table 2. The elementary steps with the absolute value of  $X_{RC}$  lower than  $2.0 \times 10^{-3}$  over the studied temperature range are omitted.

**Degree of rate and selectivity control.** DRC ( $X_{RC,i}$ ) and DSC ( $X_{SC,i}$ ) analyses<sup>60</sup> are shown in Figure 5. For both products, 6 elementary steps are found to have rate control, namely R2, R3, R4, R10, R13, and R15 (Table 2). Among these steps, R10 is found to be the largest rate control with  $X_{RC} = 0.88$ - $0.89$  for both products over the temperature range (278-318 K). R10 is the dissociation of O=O bond in  $\text{H}_2\text{O}_2$  on the bare Fe side of the mono-oxo center (TS4; see Figure 2b). It has the highest activation energy (0.72 eV) in the most favorable pathway identified in Figure 3 (bold arrows). This step has equivalent influences on both products ( $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$ ), and therefore there is no net effect on the product selectivity (i.e.,  $X_{SC} = 0$ ) as seen in Figure 5c. Similarly, R2 has no effect on the selectivity since it has the same effect on both products with a smaller  $X_{RC}$  than that of R10 (0.10-0.12). R2 and R10 have no selectivity control since they are associated with the production of states that are shared by both products. As shown in the reaction network in Figure 3, starting from the mono-oxo species (state 8; upper right), the reaction proceeds through a single pathway up to state 3. Hence, all the elementary reaction steps that produce any state between states 8 and 3 have a net zero effect on the product selectivity.

For  $\text{CH}_3\text{OH}$  production, R4 and R15 are equivalently the second most influential steps with similar DRC values but opposite sign (blue lines in Figure 5a):  $X_{RC,R4} > 0$  (rate-limiting) and  $X_{RC,R15} < 0$  (inhibition). The  $\text{CH}_3\text{OH}$  formation rate is, thus, accelerated and slowed down by increasing the rates of R4 and R15, respectively. They have opposite effects as they occur in parallel at the shared state 4, leading to the production of either  $\text{CH}_3\text{OH}$  (R4) or  $\text{CH}_3\text{OOH}$  (R15) (Figure 3). Thus, the signs of  $X_{RC,R4}$  and  $X_{RC,R15}$  are exchanged for  $\text{CH}_3\text{OOH}$  compared to  $\text{CH}_3\text{OH}$  (Figure 5b). The magnitudes of  $X_{RC}$  of R4 and R15 for  $\text{CH}_3\text{OOH}$  are smaller as the overall TOF to  $\text{CH}_3\text{OOH}$  is much higher than that of  $\text{CH}_3\text{OH}$  (Figure 4b). Consequently, these steps play a significant role in product selectivity (Figure 5c). Similarly, there are two reaction steps that are the third most influential, R3 and R13 (red lines in Figure 5):  $X_{RC,R13} > 0$  (rate-limiting) and  $X_{RC,R3} < 0$  (inhibition). With increasing

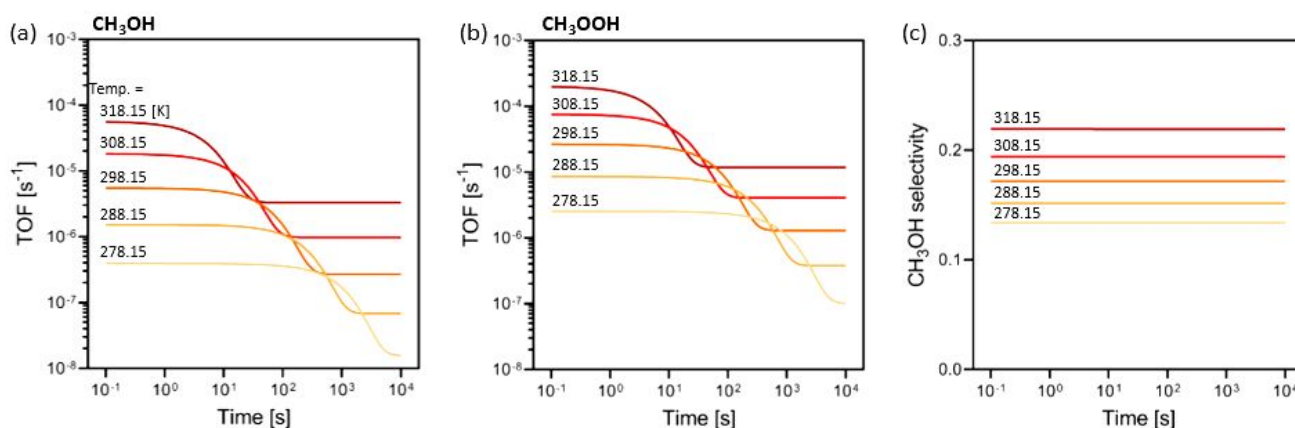
temperature (from 278.15 to 318.15 K), R4 and R15 become less influential (smaller absolute values of  $X_{RC}$ ), whereas R3 and R13 become more influential (larger absolute values of  $X_{RC}$ ). Hence, all these steps show a significant  $X_{SC}$  at a high temperature. Again, the DRC and DSC of these elementary steps (Figure S8) strongly depends on the adsorption rate constant ( $k_a$ ), primarily because it determines the rate of R3 ( $\text{H}_2\text{O}_2$  adsorption step). See Supplementary Information Section 4 for further details.

**Temperature effect.** To understand how the reaction kinetics depend on temperature, we investigate how the TOF changes over time by varying the temperature between 278.15 and 318.15 K as shown in Figure 6. As expected, TOFs to both products increase with temperature. The steady-state TOFs to  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  increase by roughly an order of magnitude as the temperature shifts from 298.15 K to 318.15 K. On the other hand, the low-temperature (278.15 K) steady-state TOFs to  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  are only 6 and 8% of those at 298.15 K. Interestingly, the TOF to  $\text{CH}_3\text{OH}$  increases more significantly compared to  $\text{CH}_3\text{OOH}$  as temperature increases. This leads to an increase in  $\text{CH}_3\text{OH}$  selectivity with temperature, from 13% (at 278.15 K) to 22% (at 318.15 K) (see Figure 5c). This clearly demonstrates that temperature not only modifies the overall reaction rate but also controls product selectivity, where a small increase in temperature leads to higher TOF to  $\text{CH}_4$  and higher selectivity toward  $\text{CH}_3\text{OH}$ . Nevertheless, it should be noted that an increase in temperature can also potentially lead to over-oxidation to  $\text{CO}_2$ , which cannot be assessed in the present model.

**Apparent activation energy and reaction order analysis.** Based on the temperature dependent steady-state TOFs to  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  (Figure 6a and b), we produce the Arrhenius plots shown in Figure 7a. In the given temperature range, the apparent activation energies ( $\Delta E_{app}^\ddagger$ ) for  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  are 1.06 and 0.94 eV, respectively. The apparent activation energy can also be calculated from the degree of rate control and relative Gibbs free energies of each step as reported by Mao and Campbell.<sup>65</sup> Considering only the 6 elementary steps

reported in Figure 5 with an ideal behavior assumption (i.e., neglecting effects of adsorbing/desorbing species and catalytic site fractions),  $\Delta E_{app}^\ddagger = 1.07$ - $1.09$  eV for  $\text{CH}_3\text{OH}$  and  $0.88$ - $0.84$  eV for  $\text{CH}_3\text{OOH}$ , which are increasing and decreasing with temperature (from 278.15 to 318.15 K), respectively. Both results agree with the higher TOF of  $\text{CH}_3\text{OOH}$  than that of  $\text{CH}_3\text{OH}$  reported in Figure 4.

effect on the overall activity (nearly constant  $\Delta E_{app}^\ddagger$ ) but significantly affects  $n_{\text{H}_2\text{O}_2}$  in such a way that the lower  $k_a$  results to higher magnitude of  $n_{\text{H}_2\text{O}_2}$ . The selectivity control by  $[\text{H}_2\text{O}_2]$  can, thus, be facilitated by slowing down the diffusion. In addition, as already mentioned, the  $\text{CH}_3\text{OH}$  selectivity increases with temperature (Figure 6c). Taken all together, we demonstrate the synergistic effects among temperature,  $[\text{H}_2\text{O}_2]$ , and diffusion



**Figure 6** TOFs to (a)  $\text{CH}_3\text{OH}$  and (b)  $\text{CH}_3\text{OOH}$ , and (c)  $\text{CH}_3\text{OH}$  selectivity under various temperatures between 278.15 and 318.15 K over time up to  $10^4$  s.

The reaction orders,  $n_i$ , of the reactants ( $\text{CH}_4$  and  $\text{H}_2\text{O}_2$ ) with respect to each product ( $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$ ) obtained by eqn. 13 are presented in Figure 7b. Reaction rates of both products depend linearly on  $[\text{CH}_4]$  over the temperature range investigated (i.e.,  $n_{\text{CH}_4} = 1$ ). On the contrary,  $n_{\text{H}_2\text{O}_2}$  is smaller for both products; around  $-0.23$  for  $\text{CH}_3\text{OH}$  and  $0.06$ - $0.19$  for  $\text{CH}_3\text{OOH}$  and increasing with temperature. Thus, increased  $[\text{H}_2\text{O}_2]$  yields slower  $\text{CH}_3\text{OH}$  formation and faster  $\text{CH}_3\text{OOH}$  formation. The reason for the different signs of the  $\text{H}_2\text{O}_2$  reaction order is that R3 ( $\text{H}_2\text{O}_2$  adsorption) outcompetes the parallel reaction, R13 (see Figure 3). Although the rate of the minor reaction stream to form  $\text{CH}_3\text{OH}$  after state 4 increases as the rate of R3 increases, the decrease in the rate of R13 counteracts this effect, leading to a net decrease in  $\text{CH}_3\text{OH}$  formation rate. Thus, the product selectivity can be controlled by modifying  $[\text{H}_2\text{O}_2]$ , where low  $[\text{H}_2\text{O}_2]$  favors high  $\text{CH}_3\text{OH}$  selectivity.

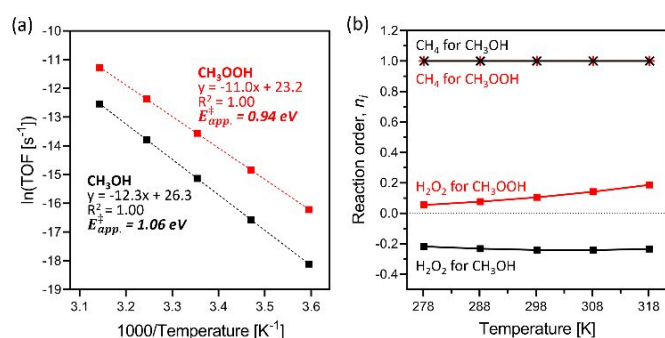
It is worth noting that the difference between  $n_{\text{H}_2\text{O}_2}$  for the two products increases with temperature. This indicates that selectivity control by  $[\text{H}_2\text{O}_2]$  is more significant at a higher temperature, as also seen in Figure 5c (red lines; R3 is adsorption of  $\text{H}_2\text{O}_2$  from bulk phase to catalyst).

The apparent activation energies and reaction orders have been also investigated with different adsorption rate constants ( $k_a$ ) (Figure S9). The analysis shows that varying  $k_a$  has a small

on controlling product selectivity, where the  $\text{CH}_3\text{OH}$  selectivity can be enhanced by reaction conditions with high temperature, low  $[\text{H}_2\text{O}_2]$ , and slow diffusion. This provides a large design space for room-temperature  $\text{CH}_4$  conversion by a  $\text{FeN}_4/\text{GN}$  catalyst towards target liquid product.

## Conclusions

We developed a first-principles-based mean-field microkinetic model (MKM) for partial  $\text{CH}_4$  conversion to  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  over  $\text{FeN}_4/\text{GN}$ . In total, 7 reaction mechanisms (5 for  $\text{CH}_3\text{OH}$  and 2 for  $\text{CH}_3\text{OOH}$ ) on two different Fe-centers (i.e., di-oxo and mono-oxo) are considered. A reaction network is constructed, which involves a dynamic change of the Fe oxidation state between +4, +5 and +6. The evolution of the site fraction shows that the di-oxo site is converted to the mono-oxo site over time. The switchover from di-oxo to mono-oxo is connected to a significant drop in turnover frequency (TOF). Thus, the di-oxo center ( $\text{Fe}^{+6}$ ) is more active but less stable compared to the mono-oxo center ( $\text{Fe}^{+4}$ ). The catalytic activity for  $\text{CH}_3\text{OH}$  formation can, therefore, be enhanced by stabilizing the metal center in the di-oxo form.  $\text{CH}_3\text{OH}$  and  $\text{CH}_3\text{OOH}$  are found to be minor and major reaction products, respectively. The  $\text{CH}_3\text{OH}$  selectivity is found to be 17%, which agrees with the experimental observations.<sup>37</sup> The degree of rate control analysis shows that scission of the  $\text{O}=\text{O}$  bond in  $\text{H}_2\text{O}_2$  is rate-controlling. Interestingly, however, this step has no net effect on product selectivity. Instead, two pairs of competing elementary reaction steps with significant influences on the product selectivity are identified by the degree of selectivity analysis. The apparent activation energies obtained from Arrhenius plots are consistent with the fact that  $\text{CH}_3\text{OOH}$  is the major product. The apparent



**Figure 7** (a) Arrhenius plots for the production of  $\text{CH}_3\text{OH}$  (black) and  $\text{CH}_3\text{OOH}$  (red) with linear fits and apparent activation energies ( $E_{app}^\ddagger$ ). (b) Reaction order of reactants ( $\text{CH}_4$  and  $\text{H}_2\text{O}_2$ ) for each product.

activation energy for CH<sub>3</sub>OOH is calculated to be 0.94 eV, whereas the value is 1.06 eV for CH<sub>3</sub>OH.

Three key factors for product selectivity control are identified: temperature, H<sub>2</sub>O<sub>2</sub> concentration, and diffusion. Increasing temperature accelerates the overall TOF as expected. As the CH<sub>3</sub>OH formation rate has a stronger temperature dependence than CH<sub>3</sub>OOH formation, the CH<sub>3</sub>OH selectivity can be enhanced by increasing the temperature. The reaction order analysis demonstrates the opposite effect of [H<sub>2</sub>O<sub>2</sub>] on the product distribution. The CH<sub>3</sub>OH production is favored by a lower [H<sub>2</sub>O<sub>2</sub>]. Furthermore, the diffusion of free species from bulk phase to a catalyst surface is found to play a significant role in the reaction kinetics by altering product selectivity without affecting the overall CH<sub>4</sub> conversion. More importantly, we reveal that there is a synergistic effect among these factors as they have a mutual dependence. This suggests a significant engineering space exists for product selectivity in CH<sub>4</sub> conversion by FeN<sub>4</sub>/GN catalyst.

Generally, we demonstrated that the DFT-based kinetic modeling is a useful tool for investigating complicated reaction systems like that of methane to methanol conversion. Our findings provide an in-depth kinetic understanding of the low-temperature CH<sub>4</sub> conversion to C1 products, which can potentially guide experimental efforts to discover efficient catalysts, as well as fine-tune catalytic performance.

### Author Contributions

The project was conceptualized and supervised by G.M. and H.G. Computational chemistry calculations were performed by S.H. Microkinetic modeling was performed by M.M.K. and S.H. in cooperation with E.V.M. The original draft of the manuscript was prepared by S.H., M.M.K., G.M. and H.G. All authors contributed to scientific discussions and editing of the manuscript.

### Conflicts of interest

There are no conflicts to declare.

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