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# Engineering asymmetric multifunctional phase change composites for improved electromagnetic interference shielding and wireless personal thermal therapy†

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Composites with long-term stability, safety, and comfort are desired as portable equipment continues to advance quickly. However, it is challenging to achieve stability, safety, and comfort in a single composite with respect to electromagnetic interference (EMI) shielding, thermal management, and antibacterial performances. In this study, we developed a series of layered asymmetric multifunctional PCCs with MXene layers and phase change layers. The asymmetric structure could adjust the EMI shielding efficiency as high as 54.5 dB, and improve light-to-thermal/magnetic-to-thermal conversion to assist PCCs in maintaining a considerable temperature. As the MXene@PDA with improved structural/chemical stability was proven to exhibit high antibacterial activity at higher temperatures, the PCCs appear to have great potential in antibacterial applications. Overall, our work provides new insights into the fabrication of advanced composites through asymmetric design, and the obtained PCCs display significant application potential in EMI shielding and wireless personal thermal therapy.

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## 1. Introduction

In light of the rapid development of portable equipment, stability, safety, and comfort have become of primary importance in practical applications.<sup>1</sup> On one hand, portable equipment often requires long-distance communication, thus effective shielding of electromagnetic waves (EMWs) is crucial in maintaining stable communication.<sup>2–4</sup> Continuous conductive networks, such as aligned, foam, or segregated structures in functional materials, could be efficient skeletons for improving the electromagnetic interference (EMI) shielding efficiency.<sup>5,6</sup> However, realization of these structures involves complex procedures such as high-pressure molding or multiple chemical reactions, which are neither environmentally friendly nor cost-effective. The layered structure, which was developed via a simple process and achieved significant EMI shielding efficiency previously, could be an ideal alternative.<sup>7,8</sup> Among various kinds of layered structures, the bilayer as the simplest



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type is easier to fabricate than the sandwich and multilayered structure. In addition, the bilayer structure is an asymmetric structure, which shows different properties in varying directions and the performances could be adjusted better *via* a direction change.<sup>9–11</sup> The bilayer asymmetric structure could be a cost- and time-efficient option for developing advanced composites.

On the other hand, the poor thermal comfort and susceptibility to bacterial growth of portable equipment are of increasing concern. Substantial efforts have been devoted to the simultaneous realization of thermal management and antibacterial ability, but the combination of both performances remains a huge challenge. Thermal management based on organic phase change materials to maintain an ideal temperature is a promising solution to improve personal thermal comfort owing to their modest temperature, low cost, nontoxicity, and low supercooling.<sup>12,13</sup> Since the growth of bacteria is closely related to temperature, the phase change process with efficient heat input to maintain a moderately high temperature could simultaneously enhance the antibacterial and thermal therapy performance. However, the traditional approach to input stable heat is mainly through heat conduction or the Joule effect, requiring direct contact with the energy source, which may lead to varying risks like an electric shock. Wireless energy supply through light-to-thermal and magnetic-to-thermal conversion offers a safer and more effective route. Besides, the heat generated by light-to-thermal and magnetic-to-thermal conversion can enhance both thermal comfort and antibacterial performance. Based on this, the development of wireless antibacterial thermal management materials has a very broad application scenario in personal thermal therapy.

MXene is an emerging two-dimensional conductive nanomaterial that has been widely used in various applications such as catalysis,<sup>14</sup> sensing,<sup>15</sup> batteries,<sup>16</sup> and EMI shielding.<sup>17–19</sup> High electrical conductivity and light absorption performances make MXene a pioneering candidate for the fabrication of thermal

comfort materials with excellent EMI shielding performances.<sup>20</sup> Furthermore, MXene exhibited higher antibacterial efficiency against various kinds of bacteria compared to graphene oxide (GO), which has been widely reported as an antibacterial agent.<sup>21</sup> Hence, MXene has significant potential as a multifunctional filler to fabricate advanced composites with simultaneous EMI shielding, thermal comfort, and antibacterial properties, which are challenging to achieve in one composite. However, MXene is prone to be oxidized on multiple occasions, which could be a threat to long-term service.<sup>22</sup>

In this regard, we fabricated a bilayer asymmetric phase change composite (PCC) with a MXene@polydopamine (MXene@PDA) layer and a phase change layer (Fig. 1). The asymmetric structure could adjust the EMI shielding efficiency of the PCC as high as 54.5 dB and the PDA could improve the structural/chemical stability of the MXene layer. In addition, the asymmetric structure endows the PCC with excellent wireless thermal therapy performance due to enhanced light-to-thermal conversion and efficient magnetic-to-thermal conversion, which could maintain a considerable temperature. As a result, the combination of the MXene@PDA layer and the phase change layer exhibited great potential to enhance the antibacterial performance, revealing great value in the application of personal thermal therapy. Overall, the work provides new insights into the fabrication of advanced composites and the obtained PCCs show great practical application potential on varying occasions.

## 2. Results and discussion

### 2.1 Fabrication of asymmetric PCCs

The fabrication of asymmetric PCCs entailed the development of a hydrophilic aerogel, followed by the absorption of PEG and coating with a MXene@PDA layer (Fig. 2).

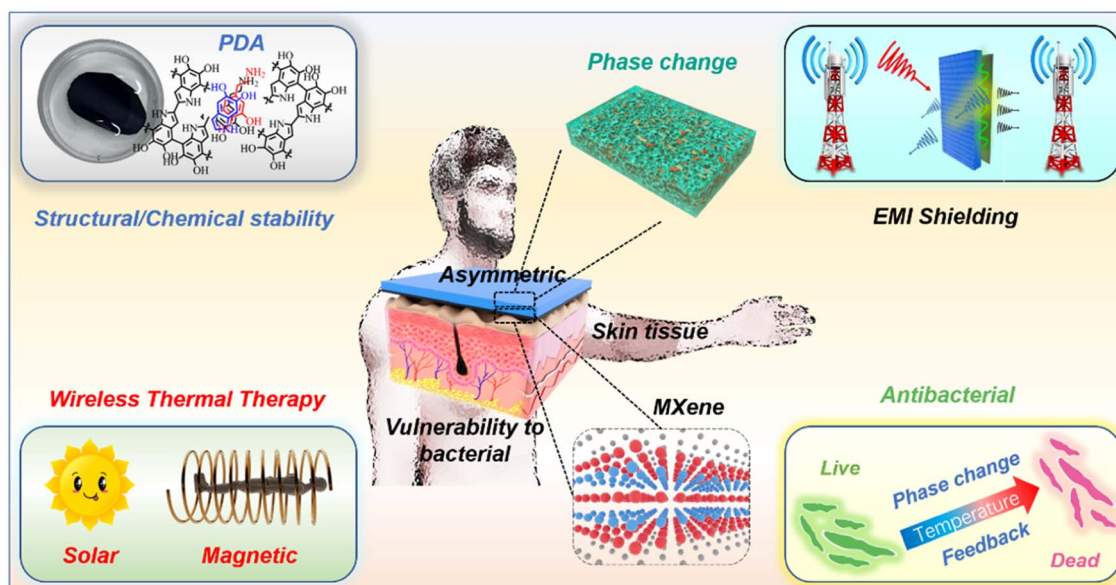


Fig. 1 The multifunctionality and performance of the composite phase change films.



Fig. 2 Schematic diagram for the preparation of the asymmetric phase change composite.

The MXene@PDA layer was fabricated by high-quality MXene@PDA dispersion *via* a vacuum filtration approach.<sup>23</sup> The successful synthesis of the high-quality MXene dispersion was verified by X-ray diffraction (XRD), AFM, and the Tyndall effect. As reported, the selective removal of Al layers from the  $\text{Ti}_3\text{AlC}_2$  MAX phase with a LiF/HCl solution yields clay-like unexfoliated MXene (Fig. 3a).<sup>24</sup> The removal of Al layers was proved by the leftward shifted (002) peak observed by XRD characterization (Fig. 3b), in which the (002) peak appeared at  $9.5^\circ$  before the exfoliation and shifted to  $6.4^\circ$  after the exfoliation.<sup>25</sup> Simultaneously, the presence of few-layer MXene nanosheets was proved by the AFM characterization and the corresponding height profiles, in which the average heights of MXene nanosheets range from 2.73 to 2.94 nm (Fig. 3c).<sup>26</sup> In addition, a bright “path” in the MXene dispersion can be observed from the direction perpendicular to the incident light (Fig. 3d), revealing that the size of nano-particles in the dispersion ranges from 1 to 100 nm.<sup>27</sup> These results demonstrate that a high-quality MXene dispersion was synthesized.

As the MXene is prone to be oxidized, the PDA was combined with MXene to enhance the structural and chemical stability of MXene.<sup>28</sup> The MXene–PDA dispersion was successfully produced and proved by FTIR characterization (Fig. S1†), then MXene@PDA was co-vacuum filtered to produce a thin film which was observed to have a continuous and smooth surface by SEM observation (Fig. 3e). Fig. 3f demonstrates the structural stability of the MXene@PDA film. Upon being immersed in

deionized water for 2 weeks, the MXene film broke into small pieces, while the MXene@PDA film remained stable. XRD analysis was conducted on the MXene (MXene-2W) and MXene@PDA (MXene@PDA-2W) films after 2 weeks of immersion (Fig. 3g and h). While the XRD curves of the MXene@PDA films hardly exhibited any changes, the characteristic peak ( $27.5^\circ$ ) of  $\text{TiO}_2$  appeared in the XRD pattern of MXene-2W, indicating that the MXene film has been oxidized and MXene@PDA has not been oxidized. It is known that MXene flakes are prone to be oxidized in either humid air or aqueous environments.<sup>29</sup> The structural and chemical stabilities of MXene@PDA play a vital part in long-term applications concerning ambient environments, and addressing the oxidation behavior of MXene has been a critical issue. In this work, the introduction of PDA was demonstrated to increase the oxidation and structural stability of  $\text{Ti}_3\text{C}_2\text{T}_x$  MXene film, revealing its great potential on varying occasions.

Obtaining a high-quality MXene@PDA film, the phase change layer was produced by the template method and vacuum impregnation method. A NaCl template was utilized to create expanded graphite (EG)/ethylene propylene diene monomer (EPDM) (EE) foams, wherein the NaCl content significantly impacted the structure of the resulting foam (Fig. 4a).<sup>30</sup> As demonstrated, when an 80.0 wt% NaCl component was introduced into the EE composites, complete etching of NaCl was not feasible, resulting in visible residues on the surface. Conversely, when the NaCl content was increased to 85%, no



Fig. 3 (a) Illustration of MXene synthesis. (b) XRD characterization of the obtained MXene. (c) AFM characterization of the obtained MXene. (d) Tyndall effect of the obtained MXene dispersion. (e) The surface of the MXene@PDA layer. (f) Digital photos and (g) XRD patterns of MXene-Fresh and MXene-2W. (h) XRD patterns of MXene@PDA-Fresh and MXene@PDA-2W films.

NaCl residue was observed, signifying the successful removal of the NaCl component by water. The results were further validated *via* weight characterization (Fig. 4b). Specifically, when an 80 wt% NaCl content was used in the EE composites, only 72.4 wt% of NaCl was removed through the process. However, as the NaCl content increased beyond 85.0 wt%, complete removal of NaCl was achievable. These disparities originate from the fact that a high NaCl weight fraction fosters the formation of a continuous phase in the EE foam, thereby enabling the complete etching of NaCl through the water. Conversely, low NaCl weight fractions result in the formation of island phases surrounded by EPDM and EG, which resist the etching process.<sup>31</sup>

As the porous EE foam was successfully developed with 85.0 wt% NaCl, the EE foam was subsequently coated with PDA to improve its hydrophilicity.<sup>32,33</sup> The presence of PDA creates numerous hydrophilic sites such as  $-OH$ ,  $-NH-$ , and  $-NH_2$  (Fig. 2), which significantly improve the hydrophilicity of EE foam. After 24 hours of dopamine (DA) polymerization in a buffer of pH = 8.5, the successful coating of PDA on the EE foam was confirmed by Fourier transform infrared (FTIR) spectroscopy, contact angle testing, and scanning electron microscopy (SEM). Compared to the FTIR spectra of EE foam before undergoing DA polymerization, the FTIR spectra of the PDA-coated EE foam (PEE) demonstrated three new signals at 1530, 1595, and 3310  $cm^{-1}$  (Fig. 4c). These signals correspond

to the shearing vibration of N–H, stretching vibration of the aromatic ring and bending vibration of N–H, and stretching vibration of phenolic O–H and N–H, respectively, all of which belong to the PDA coatings.<sup>34</sup> The result indicated the successful PDA coating on the EE foam. The contact angle tests simultaneously revealed the PDA coating on the foam as the hydrophilicity of the PEE foam has been significantly improved (Fig. 4d). Prior to the PDA coating, EE foam displayed a contact angle of 117° due to the hydrophobic nature of both EPDM and EG. After the DA polymerization, the contact angle decreased to 47°. Besides, the microstructure observation indicated the surface change caused by the PDA coating on the foam (Fig. 4e and f). There are plenty of EG particles on the surface of EE foam, whereas the surface of PEE foam becomes smoother and the EG nanoparticles could not be observed after the PDA coating. Additionally, the microstructure characterization revealed the interconnected porous structure of PEE foam. With the vulcanized EPDM constructing the skeleton and the EG dispersed in the EPDM skeleton, the obtained PDA-coated foam maintains excellent flexibility (Fig. 4g). The foam could be half-bent and rolled into a ring without brittle failures, and moreover the PEE foam could recover its initial shape without any deformation.

The above results revealed the exceptional shape stability of the foam and its great potential to act as a holding matrix for phase change materials. Coupled with the successful PDA



Fig. 4 (a) Images of water-etched foams with different NaCl content and PDA-coated foam. (b) Etched NaCl fraction by water with different NaCl content. (c) FTIR spectra of EE and PEE. (d) Contact angle tests of EE and PEE. The SEM images of (e) EE and (f) PEE. (g) The flexibility of PEE.

coating to facilitate the adhesion of hydrophilic substances, the PDA-coating foam shows an improved capacity to absorb polyethylene glycol (PEG). SEM images show that there is a visible difference in PEG absorption performance between the uncoated foam (EE) and PDA-coated foam (PEE) (Fig. 5a); there are plenty of pores existing in the EE skeleton-based PCC, while the PDA-coating PEG-based (PPEE) PCC shows a more even surface and there are no pores in the morphology after the PEG impregnation process (Fig. 5b). The PEG capacity simultaneously demonstrates the trend: the PDA-coated foam demonstrates a higher PEG absorption capacity of 68.1 wt% compared to the 64.7 wt% of the uncoated foam (Fig. 5c). This difference arises due to the hydrophilic nature of PEG, which can well interact with the hydrophilic PDA-coated foam through hydrogen bonding, capillary force, and van der Waals forces.<sup>35</sup> In contrast, the uncoated foam can only absorb PEG through capillary force and van der Waals forces, leading to numerous defects due to the hydrophobic nature of the EPDM and EG.<sup>36</sup> The capacity improvement leading to fewer defects in the PCCs is beneficial to thermal energy storage and mechanical properties, which are vital to practical applications.

To obtain the PCC with improved PEG impregnation ratio, the MXene@PDA layer was coated on the PCC (Fig. 5d). Since both the PEG and PDA-coated foam are hydrophilic, the PPEE facilitates the adhesion of the MXene@PDA layer. The MXene was successfully coated and formed a continuous layer with numerous parallel sheets on the surface of PPEE to develop MXene-based PPEE (MPPE) PCCs (Fig. 5d and S2†). In addition,

the MXene layer well adheres to the PPEE, and no defects are observed. EDS mapping was simultaneously conducted to verify the distribution of the MXene (Fig. 5e). While the C and O elements are homogeneously dispersed in the morphology, the Ti element disperses in a continuous layer, demonstrating that the MXene@PDA layer forms a continuous conductive layer and tightly adheres to the PDA-coated foam. Additionally, the obtained MPPE PCCs show high entropy which is characterized by DSC (Fig. S3 and Table S1†). All of the MPPE PCCs have latent heat above  $100 \text{ J g}^{-1}$ , which significantly contributes to personal thermal comfort.<sup>37</sup> Besides, the conductivity of the obtained composites with MXene@PDA thickness of 10, 20, and 40  $\mu\text{m}$  is 573.0, 690.5, and 826.5  $\text{cm}^{-1}$ , respectively, which are remarkable values (Fig. 5f).

## 2.2 Asymmetric EMI shielding efficiency of PCCs

Owing to the high electrical conductivity of MXene@PDA and asymmetric structure, the PCCs exhibit unique EMI shielding performance and reveal some new insights into the development of EMI shielding materials. The EMI shielding performances of MPPE-20 and MPPE-40 with the MXene thicknesses of 20 and 40  $\mu\text{m}$  were evaluated (Fig. 6a).

The scattering parameters including  $S_{11}$  and  $S_{21}$  were recorded to calculate the coefficients (reflectivity:  $R$ ; transmissivity:  $T$ ; absorptivity:  $A$ ;  $SE_R$ : reflection shielding efficiency;  $SE_A$ : absorption shielding efficiency;  $SE_T$ : total shielding efficiency) using the following equations (eqn (1)–(6)):<sup>38–40</sup>



Fig. 5 SEM images of (a) the PEG-impregnated EE foam and (b) PPEE. (c) The PEG absorption rate comparison before and after PDA coating. (d) SEM image of the MPPE. (e) EDS characterization of MPPE. (f) Electrical conductivity of the MPPE with different MXene thicknesses.

$$R = |S_{11}|^2 \quad (1)$$

$$T = |S_{21}|^2 \quad (2)$$

$$A = 1 - R - T \quad (3)$$

$$SE_R = -10 \log(1 - R) \quad (4)$$

$$SE_A = -10 \log\left(\frac{T}{1 - R}\right) \quad (5)$$

$$SE_T = SE_R + SE_A \quad (6)$$

The PPEE PCC shows an EMI shielding efficiency of 14.1 dB (Fig. 6b). For the EMWs incident from the MXene layer, the EMI shielding efficiencies of MPPE-20 and MPPE-40 are 28.1 and 48.4 dB, respectively. Interestingly, remarkable differences are observed in the EMI shielding performance as the incidence direction of the EMWs changed. Specifically, when the EMWs are incident on the PPEE side, the MPPE-20 and MPPE-40 show EMI shielding efficiencies of 32.9 dB and 54.4 dB, respectively. The EMI shielding efficiency is found to improve with increasing thickness of the MXene layer in the same direction. Moreover, the EMI shielding efficiencies for EMWs incident from the PPEE side are consistently higher than those of EMWs incident from the MXene layer.

$SE_R$  and  $SE_A$  were calculated to reveal the effect of incident EMW direction. On one hand, the  $SE_R$  slightly increases when the MXene thickness increases (Fig. 6c). For the EMWs incident from the MXene layer, the  $SE_R$  of MPPE-20 and MPPE-40 are 10.9 dB and 11.4 dB, respectively, which surpass those of EMWs

incident on the PPEE side (5.2 dB and 5.9 dB for MPPE-20 and MPPE-40, respectively). On the other hand, the  $SE_A$  increases significantly when the MXene thickness increases (Fig. 6d). It can be visually seen that higher  $SE_A$  values are achieved for the EMWs incident from the PPEE side.

As the EMW incidence direction notably influences the EMI shielding performances of the asymmetric PCCs, the EMW transmittance processes from different sides are illustrated (Fig. 6e). When the EMWs are incident from the MXene side, some of the EMWs are reflected to the air due to the electrical conductivity mismatch between the air and MXene layer.<sup>41,42</sup> The remaining EMWs would be transformed into heat in the form of microcurrent flow as they pass the MXene layer with numerous parallel MXene nanosheets (Fig. S2†), which causes numerous reflections and absorptions.<sup>43,44</sup> Then the EMWs would enter the PPEE layer with an interconnected EPDM/EG skeleton, which would result in plenty of inter-reflections and absorption, and finally the surviving EMWs transmit from the PCCs.<sup>45</sup> In contrast, the EMWs incident from the PPEE side first need to experience inter-reflection and absorption caused by the interconnected EPDM/EG skeleton. Then the EMWs undergo reflection at the interface of PPEE and MXene layers caused by the electrical conductivity mismatch.<sup>46,47</sup> The remaining EMWs are reflected multiple times between the parallel MXene nanosheets and finally transmit from the PCCs.<sup>48</sup>

As demonstrated by the  $SE_A$  and  $SE_R$  values, when the EMWs are incident from the PPEE layer, although the reflection (5.2 and 5.9 dB for MPPE-20 and MPPE-40, respectively) is weakened due to the low electrical conductivity of PPEE, the absorption

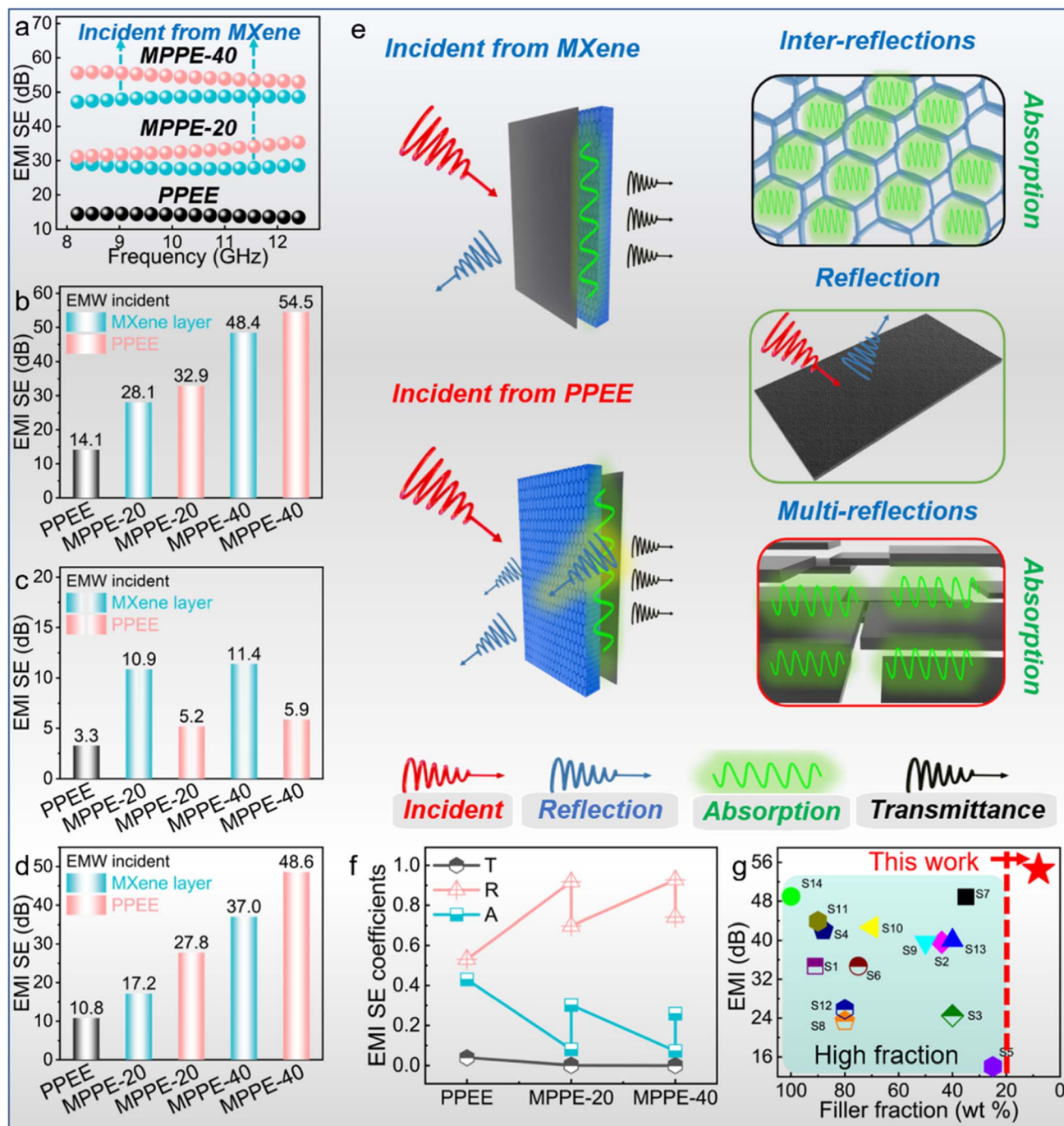


Fig. 6 (a) EMI shielding curves of PCCs with different incident EMWs and MXene thicknesses in the X-band. (b) Average  $SE_T$  of PCCs with different incident EMWs and MXene thicknesses. (c) Average  $SE_R$  of PCCs with different incident EMWs and MXene thicknesses. (d) Average  $SE_A$  of PCCs with different incident EMWs and MXene thicknesses. (e) Illustration of the EMW transmittance process through MPPE with different incident EMWs. (f)  $T$ ,  $R$ , and  $A$  parameters with different incident EMWs and MXene thicknesses. (g) Comparison of EMI shielding efficiency with varying filler fractions.

(27.8 and 48.6 dB for MPPE-20 and MPPE-40, respectively) is significantly enhanced because most reflected EMWs are absorbed by the PPEE layer. Consequently, the EMI shielding efficiency (32.9 and 54.5 dB for MPPE-20 and MPPE-40, respectively) is notably improved. Conversely, when the EMWs are incident upon the MXene layer, there is an opposite trend

with an increase in reflection (10.9 and 11.4 dB for MPPE-20 and MPPE-40, respectively) and a reduction (17.2 and 37.0 dB for MPPE-20 and MPPE-40, respectively) in absorption. Therefore, the change in EMI shielding efficiency is attributed to the differences in reflection and absorption between the PPEE and MXene layers.

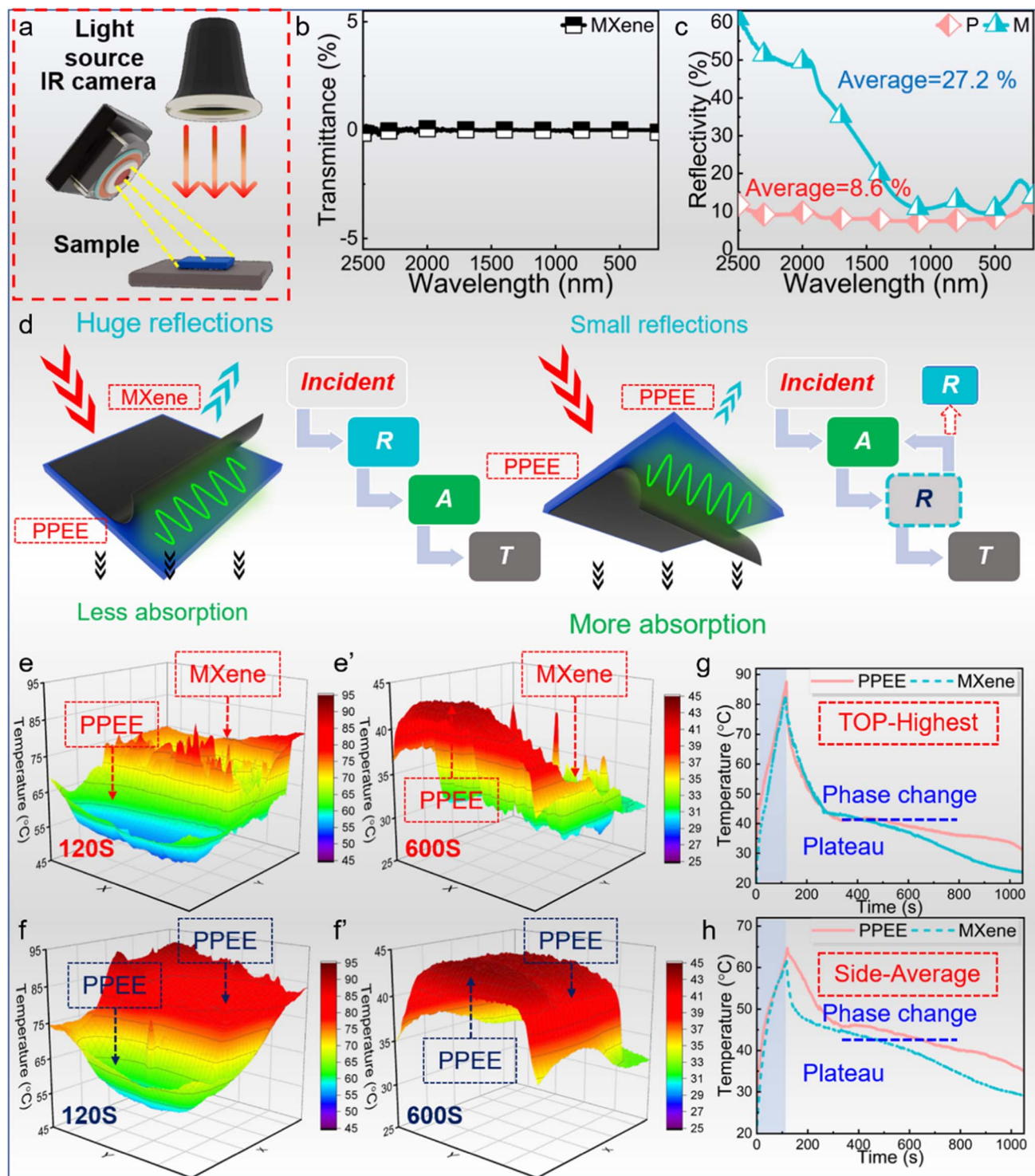


Fig. 7 (a) Setup and temperature monitoring of light-to-thermal conversion. (b) UV-vis-IR transmittance of MPPE-40. (c) UV-vis-IR reflectivity of MPPE-40. (d) Illustration of the light transmittance process through MPPE with different incident light. (e) Temperature distribution of MPPE with light incident from the MXene layer. (f) Temperature distribution of MPPE with light incident from the PPEE layer. (g) Highest temperature curves of the upper surface with different incident light. (h) Average temperature curves of the side surface with different incident light.

The reflectivity and absorptivity simultaneously support these conclusions. The obtained PCCs showed high reflectivity ( $R > 0.6$ ) and low absorptivity ( $A < 0.4$ ) (Fig. 6f), and the values of  $R$  and  $A$  change significantly in response to the change of EMW incidence

direction.<sup>49</sup> This finding reveals that the EMI shielding performances of asymmetric PCCs could be fine-tuned by adjusting the incidence direction of EMWs. Additionally, the obtained PCCs exhibit high EMI shielding efficiency with a low fraction of fillers



(Fig. 6g and Table S2†), illustrating superior effectiveness in EMI shielding. Overall, the present study unveils novel findings that differentiate it from prior research by showing that the asymmetric structure can enhance the EMI shielding performances of PCCs by direction adjustment. The development of the asymmetric structure could be a general approach for advancing composites with superior performance in areas like EMI shielding, reflecting the broad potential of asymmetric PCCs in practical applications.<sup>50</sup>

### 2.3 Wireless thermal therapy performances of PCCs

Light and magnetic input could be ideal alternative energy sources for wireless thermal therapy as the light and magnetic field do not need to be in direct contact with the skin, and thermal therapy based on wireless heat input shows great potential.<sup>51,52</sup> In our work, both the light-to-thermal and magnetic-to-thermal conversions of PCCs were characterized and the PCCs exhibit high efficiency in maintaining considerable temperature for thermal therapy and antibacterial properties.

The obtained asymmetric PCCs display different light absorption properties from traditional multilayered and sandwich composites. Specifically, the light incident from different

directions shows totally changed absorption performances. When light is incident from the MXene side, the PCC shows a higher reflectivity in the whole wavenumber range and the average value is 27.2% while the light reflectivity from the PPEE is only 8.6% (Fig. 7c). As eqn (7) shows,

$$\text{Input} = \text{reflection} + \text{absorption} + \text{transmittance} \quad (7)$$

While almost no light is transmitted from the PCCs because of the excellent light-shielding ability of the MXene layer (Fig. 7b), more light incident from the MXene layer would be reflected into the air and less light will be absorbed by the PCCs. Conversely, as the light is incident from the PPEE, less light will be reflected, leading to much light absorption. The asymmetric structure could boost light absorption performance by adjusting the light direction, showing more potential compared with the traditional sandwich and multilayered structured composites.

The light-to-thermal conversion was simulated further (Fig. 7a). Initially, the PCC first experiences a rapid temperature increase. This is followed by a rapid temperature decrease, and the temperature remains stable for a considerable period due to the phase change process.<sup>53</sup> Then the temperature gradually

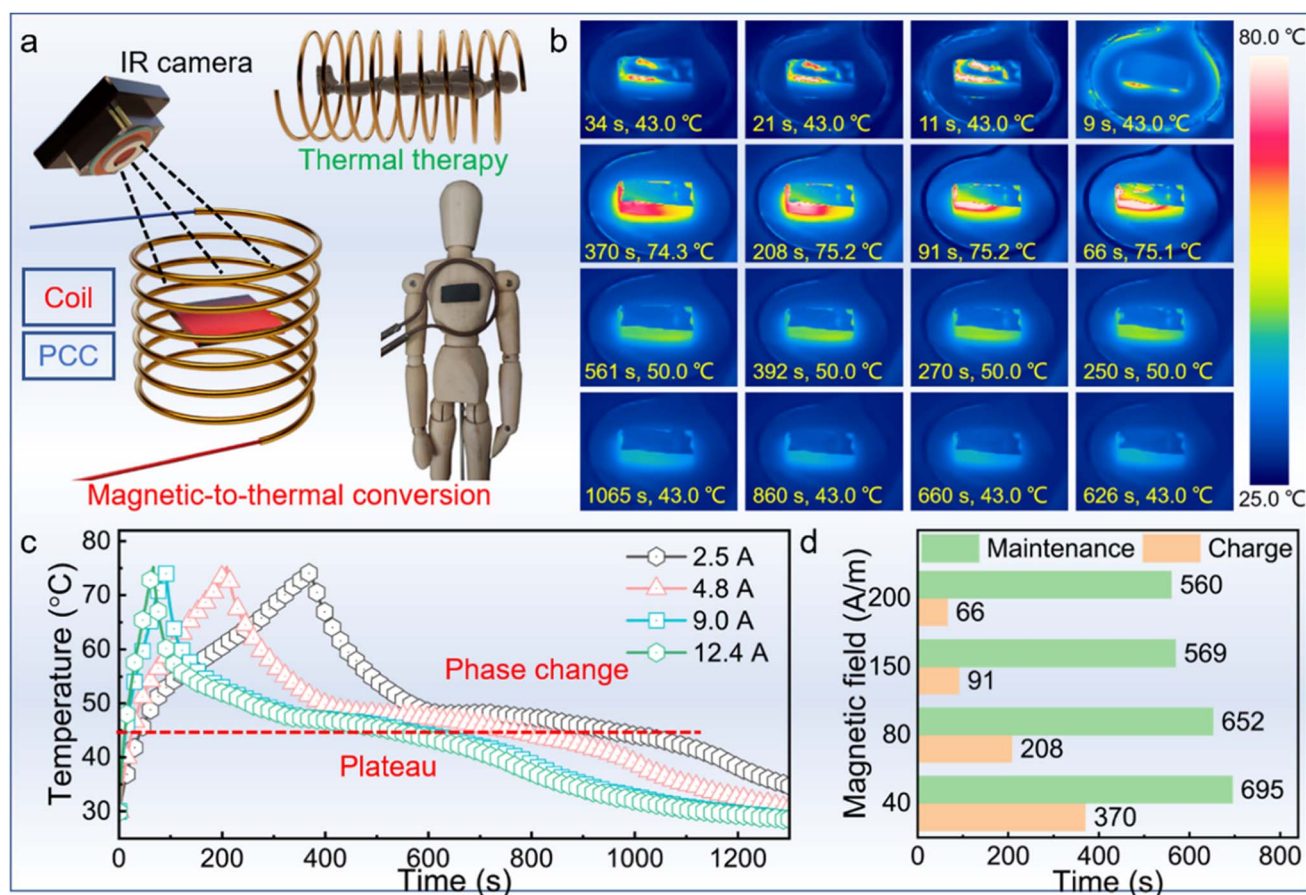


Fig. 8 (a) The illustration of magnetic-to-thermal conversion in thermal therapy application. (b) In-time images of the PCC with a current of 2.5, 4.8, 9.0, and 12.4 A. (c) Temperature curves of the PCC with a current of 2.5, 4.8, 9.0, and 12.4 A. (d) Charge and temperature maintenance performances of the PCC.

decreases to the ambient temperature. The temperature increase curve hardly shows any decay because the PCC is charged rapidly, revealing the excellent light absorption ability of PCCs. The in-time images of temperature distribution concurrently demonstrate the better light absorption ability adjusted by the asymmetric structure. When the light is incident from the MXene layer, the upper surface is the MXene layer and the side face is the PPEE layer (Fig. 7e). At 120 seconds, the temperature of the MXene layer surpasses that of the PPEE layer because the light is transformed into heat in the MXene layer and the heat transfers to the PPEE layer. At 600 seconds, the temperature of the PPEE layer is higher than that of the MXene layer, triggered by the release of heat stored in the PPEE layer during cooling. After the light direction changes to incident from the PPEE layer, both the upper surface and side face are PPEE, whose temperatures are always higher than those of PCCs with light incident from the PPEE side at 120 and 600 seconds (Fig. 7f). The divergence is caused by the diverse light absorption performances between MXene and PPEE. The corresponding light absorption processes are depicted in Fig. 7d. Given that the light contacts the MXene layer directly, it reflects off into the air, leading to serious energy loss. However, when the light initially exposes the PPEE layer, only a fraction of it is reflected to the air, and most of the reflected light by MXene is consequently absorbed by the PPEE layer, thereby yielding an optimized light absorption efficiency.

The temperature curves provide evidence supporting our conclusion (Fig. 7g and h). The maximum and average temperatures of MPPE simultaneously demonstrate the trend.

When the light is incident from the PPEE layer, both the upper and side surfaces of the MPPE exhibit elevated temperatures throughout the process. Besides, the PCCs display exceptional temperature maintenance performance, as evident from the presence of notable plateaus in the curves. Impressively, after only 120 seconds of heating, the PCC maintained a temperature above 43 °C for over 600 seconds, highlighting the outstanding performance and efficiency of the phase change process in maintaining the desired temperature.

In addition to its notable light-to-thermal conversion, the PCC exhibits remarkable magnetic-to-thermal conversion despite its lack of magnetic composition (Fig. 8a). When subjected to a magnetic field, the PCC generates considerable heat through periodic electron motion stemming from either Néel relaxation or Brownian relaxation,<sup>54</sup> facilitated by its highly conductive MXene layer. By reaching an average temperature of 75 °C, the magnetic field was cut off. At a magnetic field of 2.5/4.8/9.0/12.4 A, the PCCs were fast heated to about 75 °C in 370, 208, 91, and 66 seconds, respectively (Fig. 8b). The charging time reduces with the increase of magnetic field strength. Then the temperature rapidly decreases until the PCCs begin to experience phase change processes. The PCCs were found to exhibit excellent temperature maintenance performances. From 50 °C to 43 °C, the PCC spends 504, 468, 390, and 376 seconds, respectively. The temperature curves could more clearly show the trend (Fig. 8c). When the magnetic field increases, the temperature-increase rate is boosted. Besides, all of the curves exhibit obvious plateaus of more than 300 seconds, which is



Fig. 9 The images of antibacterial tests of control (left) and MXene (right) groups on *S. aureus* at various temperatures: (a) 43 °C, (b) 37 °C, and (c) 25 °C. OD regrowth data of *S. aureus* at various temperatures: (d) 43 °C, (e) 37 °C, and (f) 25 °C. (g) Comparison of OD regrowth curves of *S. aureus* at various temperatures. (h) Illustration of the antibacterial effect of temperature and MXene.

caused by the phase change process. The PCCs last 595, 652, 569, and 560 seconds from 75 °C to 43 °C in the magnetic field of 2.5/4.8/9.0/12.4 A, respectively (Fig. 8d). For a charge of 66 seconds, the temperature could remain above 43 °C for more than 560 seconds, showing excellent thermal therapy potential in practical applications.

#### 2.4 Temperature-dependent antibacterial performance

Temperature plays a critical role in the growth and survival of bacteria.<sup>55</sup> Given the excellent temperature maintenance abilities of PCCs (effective above 43 °C) under light and magnetic fields, the PCCs possess substantial potential for wireless thermal management and antibacterial activity. The antibacterial effectiveness of MXene against *S. aureus* at varying temperatures (25, 37, and 43 °C) was assessed by evaluating the growth curve and cell viability. Following co-incubation of *S. aureus* ( $10^7$  CFU mL<sup>-1</sup>) with MXene (0.5 mg mL<sup>-1</sup>) for 60 minutes, laser irradiation was employed to raise the mixture's temperature to 25, 37, and 43 °C, respectively, and kept for 5 minutes. Subsequently, the mixture was reincubated on agar plates at 37 °C for 18 hours, and typical photographs of bacterial colonies treated with PBS and MXene are shown in Fig. 9a.

At 25 °C and 37 °C, the *S. aureus* in control groups display high activity as numerous colonies are surviving, while the *S. aureus* at 43 °C exhibit low activity with a significantly reduced number of *S. aureus*. The number of colonies shows a reducing trend with increasing temperature, implying that the temperature increase could hinder the growth of *S. aureus*.<sup>56</sup> Besides, at each temperature, the number of colonies in the MXene-treated groups was significantly reduced compared to the control groups, indicating that MXene has good antibacterial activity on *S. aureus*. Meanwhile, the number of colonies in the MXene-treated group reduced obviously as the temperature increased. These results suggest that the temperature increase could further improve the antibacterial activity of MXene to achieve a better bactericidal effect.<sup>57</sup> The proliferation of *S. aureus* was simultaneously assessed by OD<sub>600</sub> values (Fig. 9b). At all the assessed temperatures (25, 37, and 43 °C), the MXene-treated groups always yielded lower OD<sub>600</sub> values than the control groups. In addition, the OD<sub>600</sub> value reduced significantly from 37 °C to 43 °C (Fig. 9c). The results suggest that MXene has excellent antibacterial activity and the considerable temperature could further enhance the antibacterial performance of MXene. Coupled with the excellent light-to-thermal and magnetic-to-thermal conversion to keep PCCs at a considerable temperature, the obtained PCCs show tremendous potential in thermal therapy applications (Fig. 9d).

### 3. Conclusion

A series of layered asymmetric PCCs with anti-oxidation MXene@PDA and phase change layers were fabricated. The asymmetric structure could adjust the EMI shielding efficiency as high as 54.5 dB. Simultaneously, the PCCs exhibited improved light-to-thermal conversion and excellent magnetic-to-thermal conversion, which reveal high efficiencies in maintaining a considerable

temperature. As the experimental results show that considerable temperature could assist the antibacterial performances and the MXene has excellent antibacterial activity, the obtained PCCs demonstrated great potential in the application of thermal comfort and antibacterial applications. Overall, the work gives new insights into the fabrication of advanced composites with improved EMI shielding efficiency and light-to-thermal conversion by asymmetric design, and the obtained PCCs display great practical application prospects in terms of varying demanding occasions.

## 4. Experimental

#### 4.1 Materials

The EPDM (4820P) was obtained from Dow Chemical Company (USA). Stearic acid (SA), zinc oxide (ZnO), PEG ( $M_n = 4000$ ), dopamine hydrochloride (DA), hydrogen chloride (HCl), lithium chloride (LiCl), lithium fluoride (LiF), and tris(hydroxymethyl) aminomethane (Tris) were purchased from Aladdin Reagent (Shanghai, China). MAX powder (Ti<sub>3</sub>AlC<sub>2</sub>, 200 mesh) was supplied by Jilin 11 Technology Co., Ltd. *N*-Cyclohexyl-2-benzothiazole sulfonamide (CBS) was purchased from Shanghai Chengjin Chemical Co., Ltd (China). Sulfur was purchased from Lianyungang Lanxing Industrial Technology Co., Ltd (China). Phosphate buffered saline (PBS) and Luria-Bertani broth (LB) were purchased from Sigma-Aldrich.

#### 4.2 Fabrication of EPDM/EG (EE) foam

EPDM/EG foams were obtained by two-step melt blending and water-soluble etching. The EPDM/EG composite was obtained by melt blending in a self-developed biaxial eccentric rotor extruder (BERE) based on elongational rheology as reported in our previous work.<sup>58</sup> And the ratios of curing agents are the same as reported in our previous work. This was followed by melt blending with NaCl, whose weight fractions are 80/85/90%. The composites denoted as F80, F85, and F90 were vulcanized at 180 °C and at a pressure of 10 MPa for 30 minutes. The obtained composites were sonicated in water for 24 hours to remove water-soluble NaCl and to acquire the corresponding EE foam.

#### 4.3 Fabrication of PDA-coated foam (PEE), PEG-based (PPEE) PCCs, and MXene-based (MPPE) PCCs

Ti<sub>3</sub>C<sub>2</sub>T<sub>x</sub> MXene was synthesized through the selective chemical etching method.<sup>59</sup> The typical preparation process is to mix 40 mL concentrated 9 M HCl and 3.1128 g LiF in a polytetrafluoroethylene beaker, which was stirred to generate an ionic solution. Then, 2.0 g MAX Ti<sub>3</sub>AlC<sub>2</sub> powder was slowly added in and reacted at 38 °C for 48 hours. Afterward, the resultant slurry was washed with 1 M HCl, 1 M LiCl, and deionized water until its pH reached 7.0. Deionized water (50 mL) was added to the sediment and then the mixture was ultrasonicated for 60 min under a N<sub>2</sub> flow in an ice bath for exfoliation of the MXene sheets. The supernatant, a uniform Ti<sub>3</sub>C<sub>2</sub>T<sub>x</sub> MXene colloidal dispersion, was collected by centrifugation at 3500 rpm. Then the MXene and dopamine at a weight ratio of 1 : 1 were added into a Tris buffer solution (pH = 8.5) and then stirred for 24 hours to synthesize MXene@PDA,

which was extracted by centrifugation (12 000 rpm, 10 min) and washed with deionized water 3 times. The MXene film and MXene@PDA film were obtained *via* vacuum filtration.

The EE foam was immersed into a Tris buffer solution (pH = 8.5), in which 5.0 mg per mL DA was added and self-polymerized for 24 hours under stirring. After the reaction, the samples were washed with deionized water under sonication twice and then freeze-dried to remove all the deionized water.

The PPEE PCC was prepared *via* the vacuum impregnation method. The PEE films were dipped in the melted PEG ( $M_n = 4000$ ), and then put into a vacuum oven for impregnation, and the process was left to occur at 80 °C for 24 hours. Afterward, the films were put on filter paper and then placed in the oven (80 °C) for another 4 hours to remove the excess PEG on the surface. The same impregnation process was carried out on the EE foam for comparison.

Different thicknesses (10/20/40  $\mu\text{m}$ ) of MXene films were prepared *via* a vacuum filtration process. Then the MXene layers with 20 and 40  $\mu\text{m}$  thicknesses were coated on the PPEE films at 80 °C to obtain MPPE-20 and MPPE-40.

#### 4.4 Antibacterial test of MXene

The *S. aureus* ATCC 6538 strain was cultured in an LB medium and harvested during the exponential growth phase through centrifugation for subsequent experiments. Bacterial concentration was monitored at 600 nm through optical density (OD) measurement using a spectrophotometer. The initial bacterial concentration was adjusted to  $2 \times 10^8$  CFU  $\text{mL}^{-1}$  before experimentation. To investigate the antibacterial effect of the MXene on *S. aureus*, the MXene dispersion (concentration of 0.5 mg  $\text{mL}^{-1}$ ) was mixed with bacterial cultures ( $10^7$  CFU  $\text{mL}^{-1}$ ) and maintained at 25, 37, and 43 °C for 5 minutes, followed by incubation for 30 minutes. Then, 100  $\mu\text{L}$  of each bacterial suspension was plated on LB agar plates and incubated at 37 °C for 18 hours. Additionally, bacterial cultures in the logarithmic growth phase were diluted to a concentration of  $10^5$  CFU  $\text{mL}^{-1}$  and treated with 10  $\mu\text{L}$  of the MXene (final concentration of 0.1 mg  $\text{mL}^{-1}$ ) for cocultivation. The PBS group was used as the control group ( $n = 5$ ). Bacterial growth was continuously monitored at 600 nm for 12 hours, and the growth of each bacterial group was analyzed and evaluated.

## Author contributions

X. Hu, X. L., and J. Q. conceived the project. X. Hu, B. Q., and B. A. performed the experiments. X. Hu and B. Q. analyzed the results. B. Q., M. S., L. S., X. Huang, and H. W. provided useful suggestions for this work. X. Hu wrote the manuscript. X. Hu, X. L., and J. Q. critically discussed the results and reviewed the manuscript.

## Conflicts of interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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