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Towards Flexible Large-Scale Environmentally Sustainable Methanol and Ammonia Production using Industrial Symbiosis

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Sustainability Spotlight Statement

Methanol and Ammonia are critically important building blocks for several commodities from solvents and fuels to fertilizers. Thus, defossilization at large scale is essential for cleaner production. While presently the two systems are treated independently, our study seeks to investigate industrial symbiosis as a pathway to sustainable co-production schemes utilizing cleaner, advanced technologies and greener supply chains. Here, we modeled and examined the life cycle impacts of independent production versus integrated processing, highlighting the impact of increased process efficiency and reduced resource intensity in decreasing carbon footprint while acknowledging burden-shifting. Our results align directly to the UN sustainable development goals of industry, innovation and infrastructure (SDG 9), responsible consumption and production (SDG 12) and climate action (SDG 13).



1 **Towards Flexible Large-Scale, Environmentally Sustainable Methanol**
2 **and Ammonia Co-Production using Industrial Symbiosis.**

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24

25 **Abstract**

26 As industries face increasing societal and governmental pressures to adopt sustainable
27 practices, the methanol (MeOH) and ammonia (NH₃) sectors, significant contributors to
28 greenhouse gas (GHG) emissions, are seeking innovative solutions to transition toward
29 net-zero emissions. Here, we report on the use of industrial symbiosis (IS) as a
30 transformative strategy to facilitate the cleaner co-production of MeOH and NH₃ by
31 integrating green hydrogen (H₂) within a carbon capture and utilisation (CCUS) flowsheet.
32 We examined the environmental assessment of various co-production pathways across
33 a system boundary, which includes three (3) leading technologies -Steam Methane
34 Reforming (SMR), Autothermal Reforming (ATR) and Gas Heated Reforming (GHR),
35 considering both business-as-usual (BAU) and hybrid IS integration (*Hyd*). MeOH
36 flowsheets utilised all three technologies, while NH₃ production employed SMR and ATR
37 systems. This comprised of six (6) BAU MeOH and NH₃ co-production schemes (GHR-
38 SMR_{BAU}, SMR-SMR_{BAU}, ATR-SMR_{BAU}, GHR-ATR_{BAU}, SMR-ATR_{BAU}, ATR-ATR_{BAU}) and
39 six (6) *Hyd* (GHR-SMR_{Hyd}, SMR-SMR_{Hyd}, ATR-SMR_{Hyd}, GHR-ATR_{Hyd}, SMR-ATR_{Hyd},
40 ATR-ATR_{Hyd}) cases, utilising cradle-to-gate life cycle assessments (LCA). Results show
41 that IS-integrated flowsheets reduced GHG emissions by 12-28% compared to BAU
42 operations, with GHG impacts improving in the order GHR-ATR_{Hyd} > ATR-ATR_{Hyd} > SMR-
43 ATR_{Hyd} > GHR-SMR_{BAU} > ATR-SMR_{BAU} > SMR-SMR_{BAU}, in agreement with energy and
44 resource efficiency results. Notably, the GHR-ATR_{Hyd} configuration outperformed all other
45 cases, reducing natural gas consumption by 11% and heating requirements by 8.3%.
46 Furthermore, sustainability results support IS as a pathway to environmental benefits-
47 with ATR-based NH₃ operations achieving up to 31% improved impacts linked to both
48 ecosystem quality and human health. Ultimately, our study underscores the critical role
49 of IS in advancing resilient, low-carbon practices, promoting sustainable technologies for
50 net-zero emissions and defossilisation, thereby supporting a transformative shift towards
51 sustainable industrial operations.

52



53 **Keywords:** Life Cycle Assessment; Industrial symbiosis, CCUS, Sustainable Industries,
54 Energy efficiency.

55

56 1. Introduction

57 On a global scale, GHG emissions have increased by 50% over the last 30 years,¹ in
58 which CO₂ emissions have increased from 22.75 billion tonnes per annum to 37.15 billion
59 as of 2022 (63.3% increase). The Paris Agreement in 2015, amongst other legislations,
60 set out the ambitious target to limit global temperature rises to 1.5°C and decrease global
61 GHG emissions by 43% by 2030.² However, current trends in emissions and
62 infrastructure put these commitments in jeopardy,³ concluding that overall emissions
63 within the chemical industry must be reduced by 60% to meet these targets.⁴ As an
64 initiative to reduce GHG emissions, chemical manufacturing companies have also agreed
65 to cut emissions via more renewable chemical production routes, particularly weaning off
66 the use of fossil fuel feedstocks. This is particularly apparent in the production of both
67 MeOH and NH₃, which are predominantly produced from natural gas.

68 MeOH is considered to be one of the most important chemical raw materials and is even
69 identified as playing an essential role in the transition from fossil fuels to renewable energy
70 since it can be easily transported and has the potential to be an energy carrier for
71 hydrogen storage.⁵ Based on the current MeOH capacities, 90% is derived from natural
72 gas feedstocks, predominantly via steam methane reforming (SMR), autothermal
73 reforming (ATR) and gas-heated reforming (GHR) technology routes.⁶ Globally, MeOH
74 production has increased at a compound annual growth rate (CAGR) of 5.2%, resulting
75 in the production rate exceeding 110 million MTPA in 2021.¹ This increasing MeOH
76 demand has been driven by its versatility in its use as a feedstock in further chemical
77 generation, including processing formaldehyde, acetic acid, dimethyl ether, gasoline
78 blending and fuel cells.⁷ On top of this, 40% of methanol consumption worldwide
79 comprises energy-related uses.⁸

80 NH₃, like MeOH, is a necessary commodity chemical, and it is especially important in the
81 fertiliser industry. It has also been identified as a liquid energy carrier, and therefore, it



82 makes it a powerful option for fuel.⁹ NH₃ is typically produced by steam methane
83 reforming (SMR) of natural gas to produce hydrogen, which is then combined with
84 nitrogen in the Haber-Bosch process. Like MeOH, the global consumption of NH₃ is
85 expected to increase. In 2022, the global NH₃ market size was upwards of USD 202 billion
86 and is projected to surpass USD 353.3 billion by 2032 (5.8% CAGR).¹⁰ A worldwide
87 intensification of agriculture primarily drives this expected growth to meet higher food
88 demands for a rapidly increasing population, which is expected to double by 2050.¹¹ Due
89 to this excessive use, NH₃ production releases more CO₂ into the atmosphere than any
90 other large-scale chemical process and accounts for 1.8% of global GHG emissions.

91 It is evident that there is a high demand for both MeOH and NH₃, but since both are
92 predominantly produced from natural gas, this leads to high GHG emissions, which is a
93 significant downfall. MeOH and NH₃ production from natural gas via SMR emits 0.62 t
94 CO₂e/t MeOH and 2.16 - 2.51 t CO₂e./t NH₃ respectively.^{12, 13} Without changing the BAU
95 operations, which have been mostly reliant on fossil fuels, it is expected that CO₂
96 emissions from MeOH production will rise to 1.5 Gt CO₂/y by 2050.¹⁴

97 Co-production of MeOH and NH₃ allows for flexibility in plant operations and a decrease
98 in natural gas usage. High-purity CO₂ from the NH₃ plants can be used as a feedstock for
99 MeOH production via the CO₂ hydrogenation route, which has a lower thermal efficiency
100 compared to conventional methods.¹⁵ The co-production scheme not only enables
101 production with overall decreased GHG emissions but creates industrial symbiotic
102 linkages between the plants since the waste CO₂ from the NH₃ plant is used as a
103 feedstock in the MeOH plant. The concept of industrial symbiosis (IS) is not new and has
104 existed for more than three decades.¹⁶ It is a concept where resource exchanges and the
105 transactions amongst entities are mutually beneficial for all involved and has the potential
106 to create a cyclic approach to production compared to a linear transformation from raw
107 materials to production, thereby supporting a circular economy approach. Previous
108 studies have shown that IS can reduce GHG emissions and CO₂ emissions and create
109 an overall positive environmental impact.¹⁷⁻²⁰



110 The waste emissions in the co-production scheme can be further reduced by considering
111 alternative energy sources. For sustainable NH₃ production, biochemical pathways and
112 water electrolysis using renewable sources have been investigated.²¹ Similarly, multiple
113 routes for sustainable MeOH production have been investigated, which also includes
114 thermo-catalytic hydrogenation and biocatalysis.²² However, the major challenge
115 encountered is the technology readiness level (TRL) and economics associated with the
116 alternative pathways compared to the BAU scenarios.²³ Green hydrogen (H₂) has shown
117 promise and is deemed a suitable alternative to fossil-based fuels.²⁴ There are various
118 pathways for green H₂ production which includes thermal, electrochemical and biological
119 primary methods.²⁵ Thermal and electrolysis conversion pathways for H₂ production have
120 been identified as the focal areas for research to achieve the targets of the production of
121 10 Mt of clean H₂ by 2030 and 50 Mt by 2050 based on the U.S. National Clean Hydrogen
122 Strategy and Roadmap.²⁶ In 2022, the global H₂ demand was 95 Mt and was deemed as
123 a historical high and it is estimated that this production accounted for greater than 900 Mt
124 of CO₂ emissions since H₂ was produced mainly by traditional methods. Out of this
125 demand, 50% was required for NH₃ and MeOH production and hence was responsible
126 for 450 Mt of CO₂ emissions. In the United States, SMR currently accounts for the majority
127 of the commercially produced H₂²⁷ but the country has begun putting policies in place for
128 cleaner H₂ production. In 2021, \$9.5 billion was allocated for clean H₂ production and in
129 2022, additional policies and incentives were put in place to boost the country's market
130 for H₂ production. However, it is not expected that clean H₂ production methods will
131 completely replace the traditional approaches. Reasons for this include technological
132 issues with H₂ production, distribution and storage,²⁸ high cost,²⁹ scarcity of resources for
133 infrastructure development,³⁰ and the unreliability of renewable energy sources.³¹

134 Nevertheless, due to the high usage of H₂ in the NH₃ and MeOH sectors, it is anticipated
135 that a fraction of the clean H₂ will be integrated into these sectors and would significantly
136 reduce emissions for both production schemes. Based on the target clean H₂ production
137 in the United States, it is expected that there will be a hybrid system using both clean H₂
138 and fossil-based H₂. Despite the continuous effort towards a low-carbon economy, little
139 work has been done in investigating co-production schemes for commodities such as



140 MeOH and NH₃ and the transition to a hybrid system using both fossil-based and green
141 H₂. In this study, we examine the co-production of MeOH and NH₃ using various
142 technologies and the integration of green H₂ through LCAs. These results will assist in
143 charting the way forward to lower GHG emissions and more sustainable operations.

144 **2. Methodology**

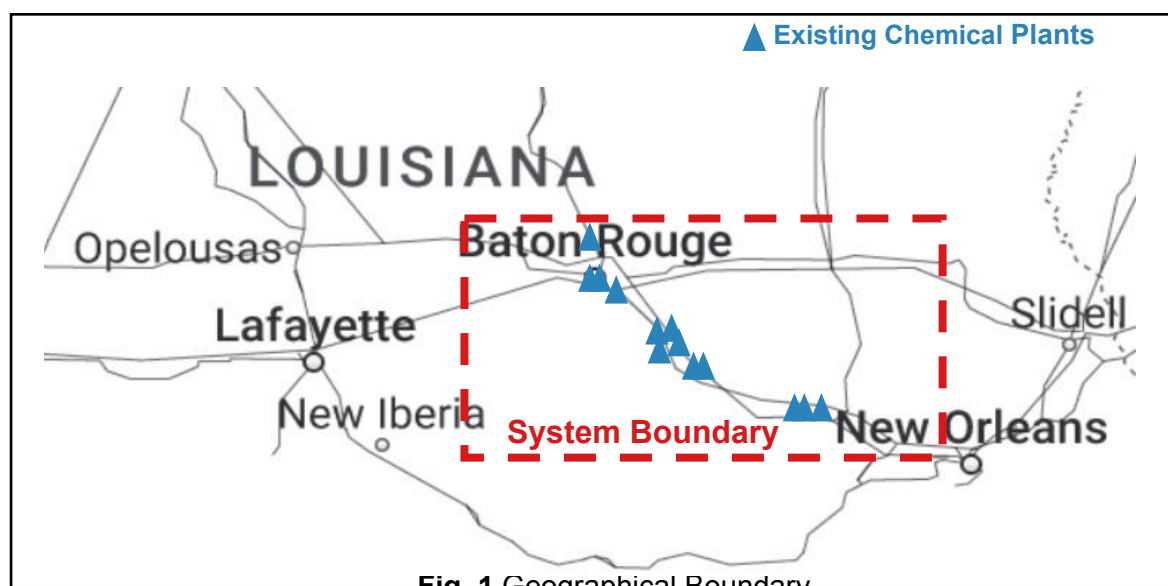
145 This section provides a detailed overview of the modelling framework, and scenario-
146 specific descriptions applied to the integrated co-production of MeOH and NH₃, utilising
147 IS. Our analysis considers validated process design, for which mass and energy balances
148 were derived and used to inform life cycle assessments and energy and resource
149 efficiencies.

150 **2.1 Geographical Process Boundary**

151 In the United States, the chemical and petrochemical industries which are mainly
152 concentrated in the Gulf Coast, particularly in Texas and Louisiana, account for
153 approximately 40% of industrial energy consumption and emissions.³² Louisiana is
154 renowned for its booming oil and gas and petrochemical sectors. The petrochemical
155 sector houses more than 150 petrochemical plants and 15 refineries and is therefore a
156 strategic location for process industries.³³ The majority of the plants are located in the St.
157 James Parish along the lower Mississippi River corridor between Baton Rouge and New
158 Orleans and is known as the Louisiana Chemical Corridor.^{34, 35} The state possesses the
159 third highest energy consumption and the second highest energy consumption per capita
160 in the United States. In 2022, approximately 4,230 GWh of energy was generated with
161 the leading sources being natural gas and nuclear power. Renewable energy from
162 biomass, hydropower and solar energy accounted for 3.5% of the net electricity
163 generation. Approximately 70% of the available energy is consumed by the industrial
164 sector.³⁶ Although most of the energy is produced via natural gas, Louisiana is
165 considering alternative energy sources such as solar and offshore wind. The climate in
166 Louisiana is conducive to solar energy production since it has a high average of warm
167 and sunny days compared to other states and flat, land space is available to install solar
168 panels. Louisiana has the potential to generate up to 13,000 MW of solar power.³⁷ This



169 amount of solar power is more than sufficient to provide green hydrogen for this project
170 in Louisiana. **Fig. 1** shows the approximate location of the existing chemical plants,
171 the system boundary used in this study.



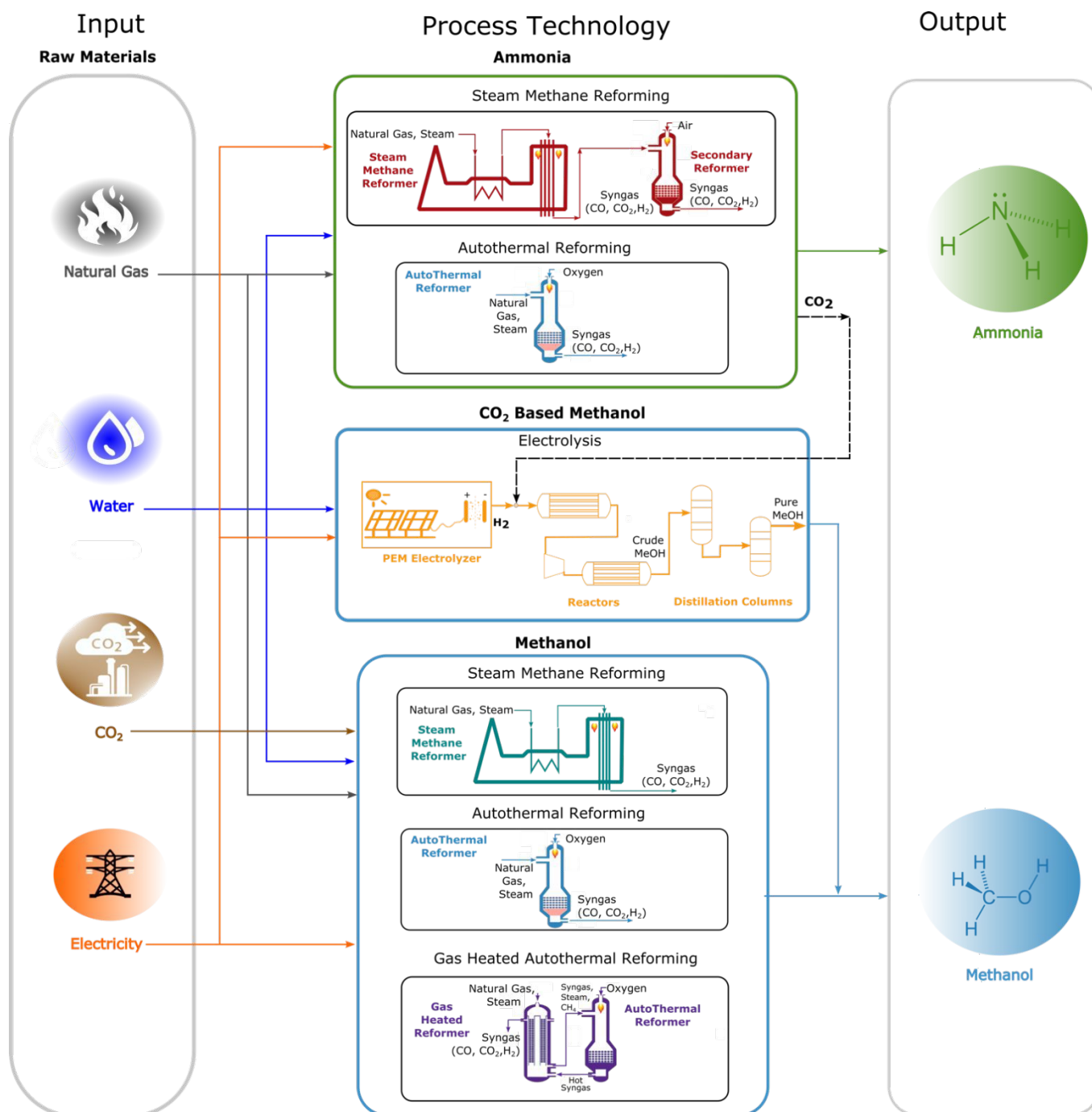
2.2. Process System Overview

189 The overall process system boundary is given in **Fig. 2**. Technologies investigated
190 considered validated large-scale SMR_{MeOH} , ATR_{MeOH} and GHR_{MeOH} reforming operations
191 for MeOH production coupled with conventional SMR_{NH_3} and ATR_{NH_3} flowsheets for NH_3
192 manufacturing. Process inventories for all MeOH technologies and SMR_{NH_3} production
193 were taken from our previous work,^{1, 38} which were validated against industrial data, while
194 ATR_{NH_3} flowsheets were modelled using Aspen Plus (V10) process simulation software,
195 utilising the RK-Aspen property package. ATR_{NH_3} was considered in this study since Air
196 Liquide and KBR are partnering to develop NH_3 plants using this process.³⁹ Thus, our
197 analysis compares six (6) business-as-usual (BAU) MeOH and NH_3 co-production
198 schemes ($\text{GHR-SMR}_{\text{BAU}}$, $\text{SMR-SMR}_{\text{BAU}}$, $\text{ATR-SMR}_{\text{BAU}}$, $\text{GHR-ATR}_{\text{BAU}}$, $\text{SMR-ATR}_{\text{BAU}}$,
199 $\text{ATR-ATR}_{\text{BAU}}$) and six (6) hybridised (*Hyd*) IS flowsheets ($\text{GHR-SMR}_{\text{Hyd}}$, $\text{SMR-SMR}_{\text{Hyd}}$,



200 ATR-SMR_{Hyd}, GHR-ATR_{Hyd}, SMR-ATR_{Hyd}, ATR-ATR_{Hyd}). For BAU co-production
201 schemes, conventional mega-methanol and NH₃ flowsheets operating at 5000 MTPD and
202 1850 MTPD, respectively, were considered as these scales were consistent with large-
203 scale MeOH and NH₃ production. Several industry leaders, including Johnson Matthey,
204 in conjunction with KBR, have already begun to examine the potential co-production of
205 MeOH and NH₃. The proposed method of integration can produce up to approximately
206 6800 MTPD of MeOH and NH₃ combined, and it has been shown that this co-production
207 is competitive with current industrial scales.⁴⁰
208





209
210 **Fig. 2** Overall process system boundary. The system includes inputs in the form natural gas,
211 water, CO₂, electricity, for cleaner co-production of MeOH and NH₃ by integrating green H₂
212 produced via solar powered electrolysis and captured CO₂ from NH₃ synthesis.
213 Within the BAU co-production flowsheet, each technology was operated independently to
214 produce both MeOH and NH₃ without IS. For integrated IS flowsheets, CO₂ flows from
215 both SMR and ATR NH₃ operations were used to produce E-methanol embedded within



216 MeOH process designs. The IS flows for each process are shown in **Table 1**. To promote
 217 flexible BAU MeOH operations, fossil-based production was ramped down to support E-
 218 methanol operations while maintaining large-scale capacity. Green H₂ feedstocks
 219 required for E-methanol production were derived from solar-powered PEM electrolysis,
 220 operating at an efficiency of 70.5%, a capacity factor of 0.241 and a standard enthalpy of
 221 electrolysis of 39 kWh/kgH₂.⁴¹ The scale of E-methanol operations was constrained to
 222 270,000 tonnes/year (Total capacity =300,000 tonnes/year, on-stream factor assumed at
 223 90%) in accordance with typical global E-methanol operations.⁴² and the solar power
 224 resource capacities of the Louisiana region. As SMR MeOH technologies utilised CO₂ for
 225 combined steam and dry methane reforming, IS-integrated SMR-SMR_{Hyd} cases required
 226 external CO₂ feedstocks for co-production and, thus, captured CO₂ from natural gas
 227 power plant operations were utilised. Process inventories for E-methanol production and
 228 captured CO₂ were taken from the work by González-Garay *et al.*⁴¹

230 **Table 1** IS Flows associated with each process

Process/ Technology	Capacity [MTPD]	IS Flows Entering	IS Flows Exiting
SMR _{MeOH}	5000	CO ₂	None
ATR _{MeOH}	5000	None	None
GHR _{MeOH}	5000	None	None
E-Methanol	822	H ₂ , CO ₂	None
SMR _{NH3}	1850	None	CO ₂
ATR _{NH3}	1850	None	CO ₂

231



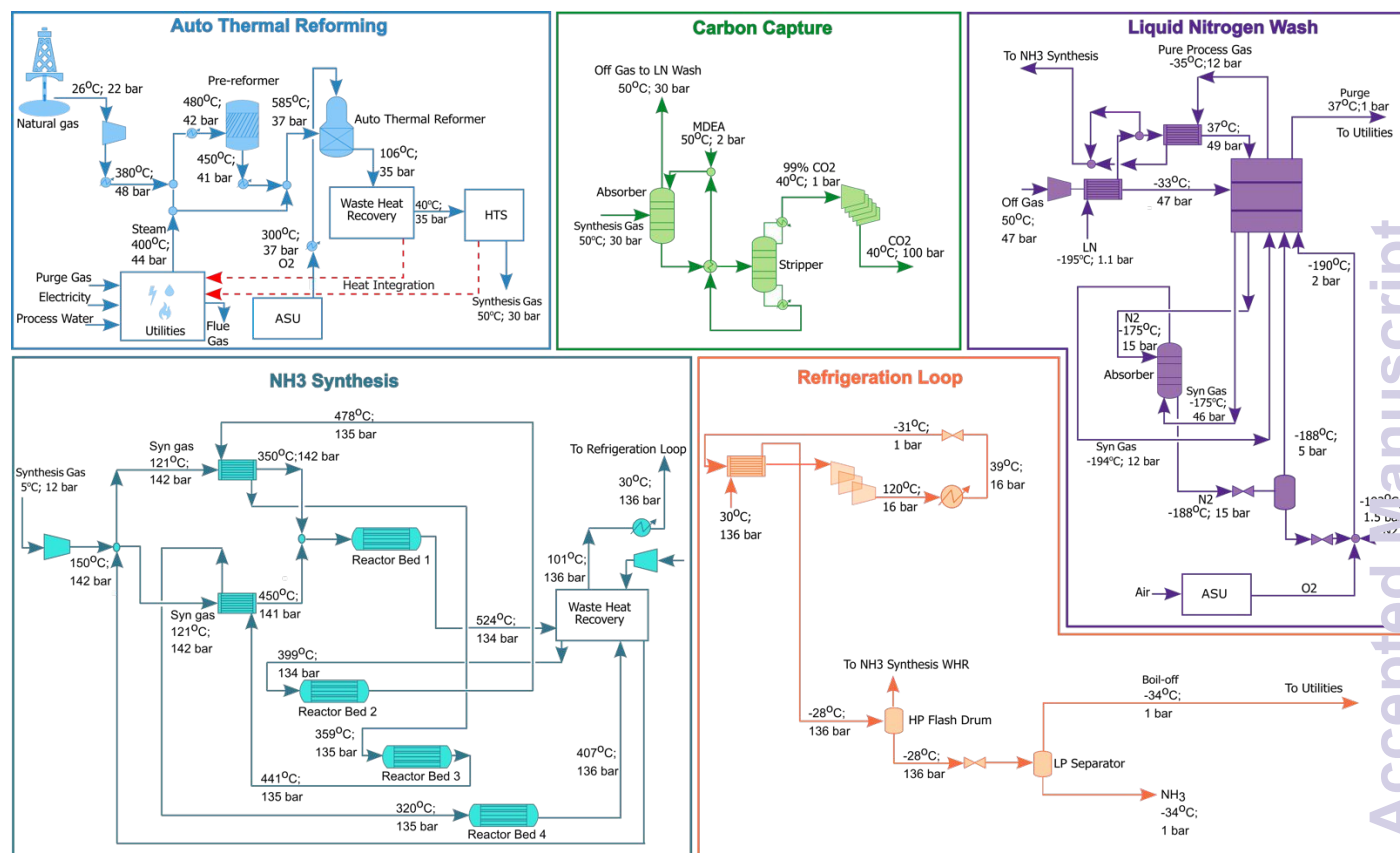
232 **2.2.1 ATR_{NH3} Process Development**

Fig. 3 Overall ATR_{NH3} flowsheet consisting of five (5) unit operations, including auto-thermal reforming, carbon capture, liquid nitrogen wash, ammonia synthesis and product removal using refrigeration. Process integration is linked throughout, illustrating the transfer of purge gases and boil-off for energy recovery as well as heat recovery across synthesis and reforming sections.

The overall ATR_{NH3} flowsheet is given in **Fig. 3**. The front-end plant model followed standard ATR-based H₂ production according to available literature.^{43, 44} Desulphurised natural gas was compressed to 49 bar and mixed with medium-pressure (MP) steam at a steam-to-carbon ratio of 0.6. This mixed feed gas was preheated to pre-reforming conditions (480°C), allowing for the methanation of higher hydrocarbons (eqns (1-4)), creating a lean methane-rich feed gas for autothermal reforming. The lean feed gas was mixed with preheated oxygen (99.5% mol, 300°C) and reacted in an adiabatic ATR unit. Methane partial oxidation (eqns (6-7)) occurs simultaneously with reforming reactions (eqns (4-5)), providing the thermal energy required for steam reforming. The hot reformed



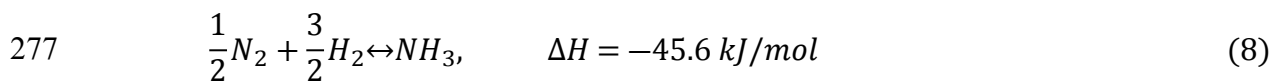
249 gas was then cooled through waste heat recovery, mixed with auxiliary MP steam and
250 reacted across two high-temperature water-gas shift converters, where CO is converted
251 into CO₂ (eqn (4)). The resulting H₂-rich gas was further cooled and sent to CO₂ removal.
252



260 The CO₂ removal unit was modelled based on our past work,⁷ assuming a rate-based
261 methyl-diethanolamine (MDEA) capture system with a 90% capture efficiency and
262 normalised heating and cooling demands of 5.7 and 6.2 kJ/kg CO₂. The sweet synthesis
263 gas leaving the CO₂ removal unit was sent to an adsorber where residual CO₂ and
264 moisture were removed. The dried synthesis gas is chilled to -175°C through a triple
265 cascade counter-current heat exchange system and washed with liquid nitrogen, where
266 inerts are completely removed. The final purified gas was mixed with gaseous nitrogen,
267 ensuring a 3:1 ratio of H₂:N₂ required for NH₃ synthesis. The liquid nitrogen system was
268 modelled using the conditions described by Haonan *et al.*⁴⁵
269

270 The back end section of the ATR NH₃ flowsheet considered a traditional Haber-Bosch
271 process,⁴⁶ whereby N₂ and H₂ react to produce NH₃ over an iron catalyst at 141 bar and
272 450°C (eqn (8)). The NH₃ synthesis unit consists of 4 adiabatic-packed bed reactors,
273 integrated with heat recovery and MP steam generation which effectively removes the
274 heat of reaction. The reactor model followed Temkin and Pyzhev kinetics,⁴⁷ imported into
275 Aspen Plus. The cooled effluent from the synthesis section was chilled to -33°C using an
276 NH₃ refrigeration cycle and flash separated at 1 bar to yield 100% pure product NH₃.





279 The utilities section of the ATR process included heat recovery through steam generation,
280 power generation, heating and cooling. Steam generated within the front and back end
281 was used as feedstock for steam reforming and heating within CO₂ removal and liquid
282 nitrogen wash units. Purge gas arising from the liquid nitrogen wash and low-pressure
283 NH₃ boil-off was combusted, providing heating duties within the front end and power
284 generation for process operations, considering a standard Rankine cycle with an
285 efficiency of 30%.

286

287 **2.3 Life Cycle Assessment (LCA)**

288 To investigate the environmental impacts associated with each scenario-specific co-
289 production scheme, a cradle-to-gate LCA methodology was applied, utilising the ISO
290 14040:2006 framework. In accordance with the ISO framework, the assessment
291 methodology is conducted across four (4) levels. *Level 1: Goal and Scope*. The goal and
292 scope of our study considers twelve (12) MeOH-NH₃ co-production system boundaries
293 (**Fig. 3**), considering independent BAU MeOH and NH₃ co-production pathways as well
294 as IS integrated schemes. As illustrated, CO₂ is the main IS flow, and it is combined with
295 green H₂ to produce E-methanol, allowing for integrated waste-to-resource value chains.
296 As the aim of our study is to examine climate-friendly NH₃ manufacturing, the functional
297 unit was set as 1 kg NH₃ produced from each co-production scheme. *Level 2: Life Cycle*
298 *Inventory Analysis (LCI)*. Scenario-specific inventories were defined from the integration
299 of both technologies as described previously in **Section 2.2**, with foreground system
300 inventories derived from literature data^{1, 38, 41} and process simulations. In contrast,
301 background supply chain inventories were taken from Ecoinvent databases. Economic
302 allocation was used to distribute burdens between co-products, as neither system
303 boundary expansion nor substitution were deemed favourable allocation approaches due
304 to the complexity of the integrated flowsheets. The input-output structure is defined in **Fig.**
305 **2**, which illustrates the mass and energy flows for each technology. The inputs consisted
306 of natural gas (both as a feedstock and utility), water, electricity, captured CO₂ and green



307 H₂. Outputs were co-products of MeOH and NH₃, process-based (CO₂ removal in NH₃
308 technologies), and other CO₂ emissions arising from fuel combustion for heating and
309 power generation within technologies. Detailed normalised inventories are given in **Table**
310 **2** in the **Results and Discussion Section**.

311
312 Level 3: Life Cycle Impact Assessment (LCIA). In the LCIA stage of our study, both
313 midpoint and endpoint characterisation methods were used, following the ReCiPe 2016
314 Hierarchist-H method, using SimaPRO LCA software. The Hierarchist (H) perspective
315 method was deemed the most appropriate for our research, allowing for easier, quantitative
316 comparison of the environmental burdens associated with each of our cases.⁴⁸ While the
317 ReCiPe (H) midpoint characterisation considers 18 impact categories, only GHG missions
318 (Global Warming Potential) were investigated for our study. However, to analyse the
319 impact of potential burden-shifting within impact categories, endpoint characterisation
320 was examined across three main areas- human health, ecosystem quality and resource
321 depletion. The full LCIA results of all cases are given in **Supplementary Data, Section**
322 **2. Level 4: Interpretation**. By comprehensively analysing the LCIA at both the midpoint
323 and endpoint, decision variables can be used to compare BAU co-production schemes
324 with IS-integrated flowsheets through multiple decision-making criteria (**see Results and**
325 **Discussion Section 3.4**), guiding achieving cleaner large-scale NH₃ manufacturing.

326

327 **3. Results and Discussion**

328 This section presents the results summary and analysis over five (5) main sections: LCI
329 overview and Analysis, Energy and Resource Performance, LCIA, and Multiple Decision-
330 Making Criteria. Twelve (12) MeOH and NH₃ co-production schemes were modelled and
331 defined by mass and energy balances, correlated by key performance indicators and
332 characterised by thermodynamic profiles and environmental burden quantification. By
333 analysing hotspots and trade-offs within each case-specific model, multiple decision-
334 making criteria were applied, revealing the most environmentally sustainable route to eco-
335 friendly NH₃ production at scale.

336



3.1 LCI Overview and Analysis

337
338 Considering the overall performance of each technology, **Table 2** gives an overview of
339 the normalised mass and energy balance profiles for both BAU and IS-integrated (*Hyd*)
340 co-production flowsheets. Focusing on BAU processes across all cases, SMR_{NH_3}
341 technologies utilise, on average, approximately 17% more natural gas input and three
342 times as much heat than ATR_{NH_3} cases. This is mainly attributed to the heating needs of
343 SMR operations, both for primary and secondary reforming and steam production within
344 both MeOH and NH_3 production. Looking closely at individual operations, ATR_{NH_3} utilise
345 40% more water than SMR_{NH_3} cases due to the increase in CO shift conversion arising
346 from autothermal reforming and partial oxidation but requires 41% less cooling needs due
347 to efficient heat recovery. Although ATR_{NH_3} flowsheets produce 20% more process CO_2
348 than SMR_{NH_3} operations, they require no additional heating needs, and thus, this increase
349 in energy efficiency accompanies a 33% reduction in total CO_2 produced. Overall, NH_3
350 technologies consume less electricity than MeOH technologies, such as GHR units,
351 where trade-offs between heating and electrification are required for pumping and
352 compression. For IS integrated flowsheets, the inherent flexibility of MeOH operations
353 accompanied reductions in natural gas utilisation (11%) and heating (8.3%) but an 8%
354 increase in electricity consumption due to E-methanol operations. This decrease in the
355 use of resources coupled with CO_2 utilisation saw an average 28% reduction in total CO_2
356 emissions across all IS cases compared to BAU operations. Ultimately, trade-offs
357 between electrification and heating pose the greatest benefits in contributing to low-
358 carbon NH_3 production, with the GHR- ATR_{Hyd} boasting net zero heating and the lowest
359 recorded natural gas usage, cooling duties and total CO_2 emissions across all co-
360 production cases.

361

3.2 Energy and Resource Efficiencies

362
363 The process performance of all co-production cases was analysed using energy
364 efficiency (EE) and resource intensity (RI) KPIs, given in eqns (9-10) below:

$$365 \quad EE = \frac{\sum_p^n F_p \cdot NHV_p}{\sum_i^n F_i \cdot NHV_i + E_{Grid}} \quad (9)$$



$$RI = \frac{F_{Natgas} \cdot NHV_{Natgas}}{\sum_p^n F_p} \quad (10)$$

where, $F_{i,p,Natgas}$ is the mass flow (kg/s) of raw materials, products, natural gas, $NHV_{i,p,natgas}$ is the heating value of raw materials, products, natural gas, E_{Grid} is the electricity consumption from the Louisiana power grid.

EE of a given process outlines the energy conversion rate from inputs to outputs, while RI shows the use of fossil fuel resources in producing both MeOH and NH₃. Thus, an increase in EE and a decrease in RI give a more energetically and resource-efficient process flowsheet, favouring greater sustainable operations. The results of EE and RI across all cases are presented in **Fig. 4**. In alignment with the process systems overviews provided in **Section 3.1**, general trends show EE increases and RI decreases in the order GHR>ATR>SMR, with ATR_{NH₃} technologies outperforming SMR_{NH₃} cases. Focusing on BAU flowsheets, SMR-SMR_{BAU} gives the highest RI and lowest EE at 35 MJ/kg_{Product} and 61.5%, respectively. In contrast, GHR-ATR_{BAU} was the most energetically favourable at an RI of 25.89 MJ/kg_{Product} and EE at 79.6%. Comparing like-for-like MeOH technologies across NH₃ flowsheets, EE improves between 17.1 -19%, and RI decreases between 15.3-17.2% with the adoption of ATR_{NH₃} production. Similar results are observed considering hybrid operations, with GHR-ATR_{Hyd} operations outperforming all other cases at an EE of 80.1% and RI at 25.74 MJ/kg_{Product}. Notably, hybrid flowsheets do not suffer much energy penalties, with EE increasing within the range of 0.58-1.9% compared to BAU processes. This indicates the synergy between both flowsheets to support co-production. Although IS provides pathways towards efficient energy utilisation, it is important to note that GHR-ATR_{BAU} systems outperform all other cases except its own hybrid flowsheet GHR-ATR_{Hyd} - at most a 30% increase in EE and a 27% decrease in RI, promoting the need for greater energy analysis and trade-off assessment in co-production schemes.



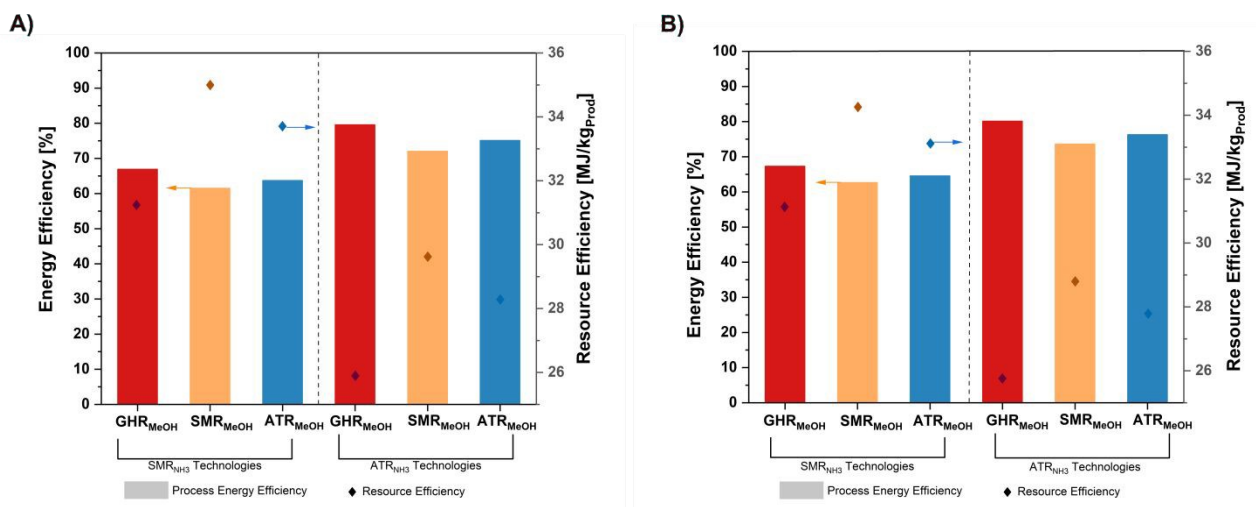


Fig. 4 Energy and resource efficiencies. A) BAU cases, B) IS integrated (*Hyd*) cases.

3.3 LCIA

3.3.1 GHG Impact

The LCIA results are given for different IS-integrated MeOH-NH₃ co-production flowsheets and BAU processes as outlined in **Fig. 5**. For BAU co-production schemes, the main hotspots identified were linked to natural gas consumption (22-26%) and direct CO₂ emissions (process + other) arising from co-production operations (53-75%). Minor GHG contributions cumulating 3-27% were attributed to electricity and water consumption. For all inventories, environmental burdens arise from releasing CO₂, CH₄ and N₂O across raw material supply chains, consistent with raw material extraction and processing, fossil fuel consumption and fugitive emissions. Across BAU cases, SMR_{NH3} technologies performed worse than ATR_{NH3}, with the highest GHG burdens of 1.23 kgCO₂e/kg_{NH3} assigned to SMR-SMR_{BAU} co-production. At the same time, the most significant reduction in GHG (28%) was observed for GHR-SMR_{BAU}, mainly due to lower direct CO₂ emissions associated with GHR operations.

Similar results were observed across hybrid co-production cases, with the main hotspots, natural gas consumption (22-26%) and direct CO₂ contributions (38-65%), being marginally lower. Furthermore, the addition of green H₂ and captured CO₂ added little to the overall GHG impact (1.1-11%), as consolidated impacts were heavily outweighed by reduced GHG burdens due to decreased natural gas utilisation and minimised process-



413 based CO₂ emissions. Although overall performance followed similar trends at the BAU
414 level, hybrid cases produced 12% less GHG emissions on average than BAU cases - with
415 GHR-ATR_{Hyd} performing the best (0.76 kgCO₂e/kg_{NH3}). Notably, despite the apparent
416 benefits of IS, hybrid SMR_{NH3} technologies' GHG burdens exceeded ATR_{NH3} BAU cases,
417 illustrating the need to move towards ATR-based ammonia operations. Ultimately, GHG
418 impacts improve in the order GHR-ATR_{Hyd} > ATR-ATR_{Hyd} > SMR-ATR_{Hyd} > GHR-SMR_{BAU}
419 > ATR-SMR_{BAU} > SMR-SMR_{BAU}, in agreement with energy and resource efficiency
420 results. While IS benefits are only realised through the integration of green H₂, the
421 flexibility of IS-integrated co-production flowsheets will likely support larger E-methanol
422 integration as renewable electricity is scaled up, allowing for greater sustainable
423 operations of MeOH and NH₃ manufacturing.

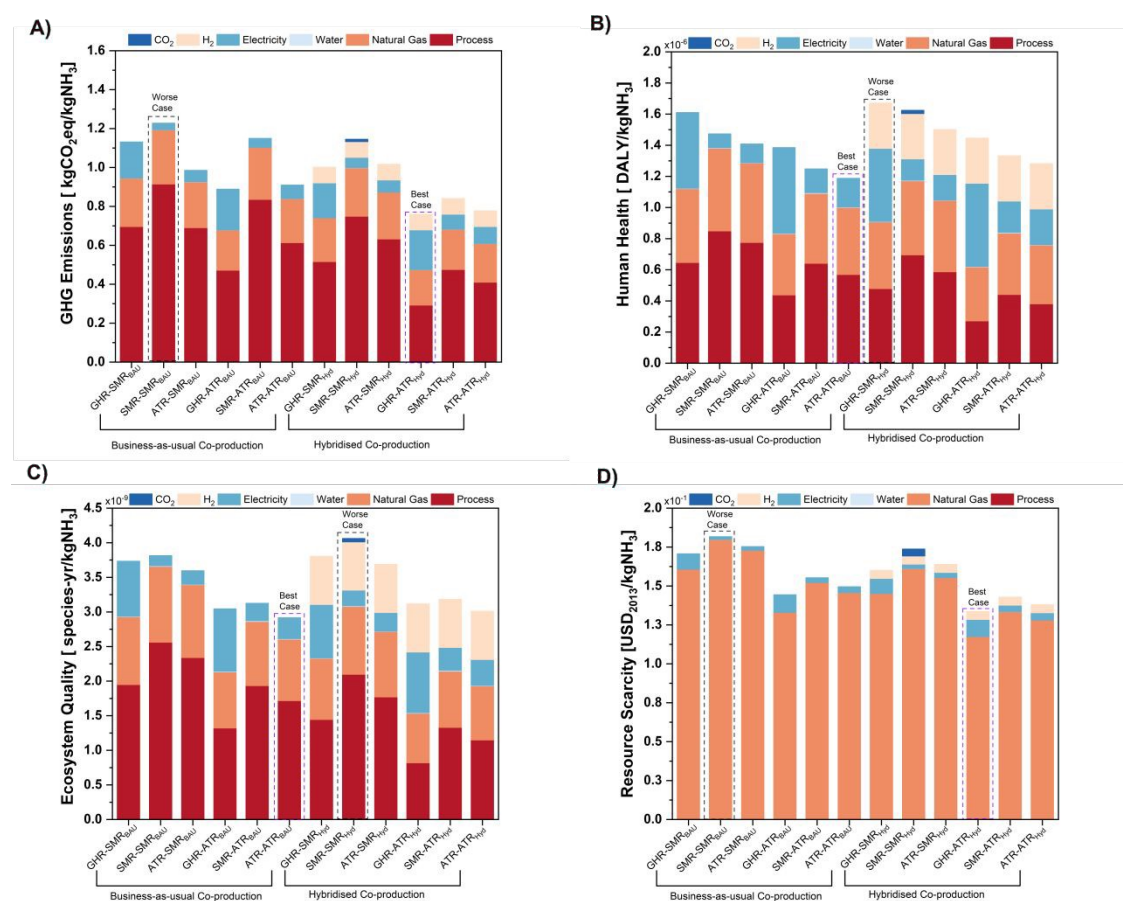
424

425 3.3.2 Burden-Shifting Analysis

426 As IS supports decreased GHG impacts and resource intensities at the co-production
427 level, it may accompany burden-shifting to other impact categories compared to BAU
428 operations due to the integration of new feedstocks. Considering all midpoint categories
429 (see **Supplementary Data, Section 2**), burden-shifting is apparent across most impact
430 categories, including ionising radiation, ozone formation, particulate matter, ecotoxicities,
431 acidification, eutrophication, fossil resource scarcity and water consumption. At the
432 endpoint, impacts were consolidated with human health burdens linked to particulate
433 matter, ecotoxicities, ozone depletion, eutrophication, and acidification attributed to
434 ecosystem quality. In contrast, global warming, ionising radiation and particulate matter
435 are shared. Burdens affiliated with water consumption, fossil and mineral depletion and
436 land usage are linked to resource scarcity. These burdens were mainly attributed to
437 mining and mineral extraction, as well as materials production and fabrication, which
438 released harmful compounds such as copper, zinc, antimony, lead, and arsenic, as well
439 as radioactive sources, nitrogen oxides, phosphates and SO₂ into the environment.
440 Focusing on endpoint impacts (**Fig. 5(B-C)**), burdens associated with natural gas
441 consumption were reduced by 11%, moving away from BAU operations – with improved
442 IS contributions to human health and ecosystem quality ranging from 26-31% and 23-



443 26%, respectively. These results were particularly noticeable in resource scarcity, where
 444 natural gas consumption dominated the burden contribution, ranging from 88-99%. Unlike
 445 the other endpoint impact categories, burden-shifting was not observed in resource
 446 scarcity– with technological performance following the same trends as described for GHG
 447 impact (Best case, GHR-ATR_{Hyd} = 0.133 USD₂₀₁₃/kgNH₃; Worse case, SMR-SMR_{BAU} =
 448 0.182 USD₂₀₁₃/kgNH₃). However, additional E-methanol operations worsen human health
 449 and ecosystem quality burdens, with green H₂ and increased electricity consumption
 450 leading to an increase in human health and ecosystem quality by 7% and 3%,
 451 respectively. Overall, ATR flowsheets performed the best across both human health
 452 (ATR-ATR_{BAU} = 1.19x10⁻⁶ DALY/kgNH₃) and ecosystem quality (ATR-ATR_{BAU} = 2.91x10⁻⁹
 453 species-yr/kgNH₃) and while GHR and SMR technologies performed the worse (GHR-
 454 SMR_{Hyd} = 1.67x10⁻⁶ DALY/kgNH₃; SMR-SMR_{Hyd} = 4.06x10⁻⁹ species-yr/kgNH₃).



455
 456 **Fig. 5** LCIA results for all co-production cases across four (4) main categories including, A)
 457 GHG emissions, B) Human health, C) Ecosystem quality and D) Resource scarcity.



458 3.4 Multiple Decision-Making Criteria

459 Normalised spider plots, as shown in **Fig. 6**, were developed to assist in a multi-criteria
 460 decision-making approach for evaluating the sustainability of the co-production systems.
 461 The indicators, which consisted equal weights of both environmental and process, were
 462 resource scarcity, ecosystem quality, human health, GHG emissions and process
 463 efficiency. The reverse score was used for process efficiency since this indicator should
 464 be maximised, compared to all the other indicators, which should be minimised.
 465 Therefore, the largest area in the normalised spider plots will represent the most inferior
 466 co-production system.



468
 469
 470 **Fig. 6** Sustainability Analysis of A) BAU and B) IS integrated MeOH-NH₃ co-production
 471 flowsheets. The blue dashed line [---] in both spider plots indicates the best-performing co-
 472 production flowsheet, which meets all decision criteria. This flowsheet was chosen as it has the
 473 smallest internal area and, thus, provides optimum results.

474
 475 Focusing on BAU operations, where there are no IS linkages among processes, the
 476 SMR_{NH₃} cases were consistently outperformed due to higher burdens linked to all
 477 indicators. Although SMR is one of the most common and widely used methods for H₂
 478 production for MeOH and NH₃ production,⁴⁹ our results illustrate that ATR alternatives



479 produce more sustainable pathways, even if fossil-based natural gas is utilised. The
480 GHR-ATR_{BAU} is the most compelling co-production system to utilise if using a system with
481 only fossil-based fuels.

482
483 When IS linkages with CO₂ and H₂ were introduced to BAU production, there was a
484 noticeable shift towards lower GHG emissions and resource scarcity and higher efficiency
485 indicators for all the pathways as the integration of green H₂ and CO₂ reuse reduces the
486 dependency of the fossil-based fuels without losing MeOH and NH₃ productivity. The
487 most attractive co-production scheme using IS and green H₂ was the GHR-ATR_{Hyd}
488 system while ATR-ATR_{Hyd} flowsheets show strong competitiveness as burden-shifting is
489 reduced. Implementation of the GHR-ATR_{Hyd} system can lead to high process and
490 resource efficiency and there would be a reduction in the overall GHG emissions
491 compared to traditional systems where SMR technology is used. However, if existing
492 industrial plants were retrofitted with these technologies, significant capital expenditure
493 and the development of hydrogen production plants would be required and hence these
494 are limitations to the implementation of the system. It should be noted that this system
495 has shown to be best-performing co-production system compared to other systems, but
496 these findings are valid only at the capacities considered in the study. Therefore, lower
497 scale production systems may not show the same findings. Overall, our results illustrate
498 the need for cleaner supply chains (*e.g. renewable energy*) within co-production schemes
499 with IS as pathways to sustainable, large-scale production of MeOH and NH₃.

500
501 To achieve higher levels of IS and sustainability, companies must be willing to work
502 together to develop these co-production systems. Although IS can be adopted using a
503 top-down approach, it is recommended that companies employ a bottom-up approach
504 where there is self-organisation of the IS exchanges amongst the plants. A recent
505 example of self-organisation of IS for the co-production of MeOH and NH₃ is the
506 partnership between KBR and Johnson Matthey.⁴⁰ This exemplifies that companies can
507 successfully collaborate to achieve lower emissions and higher sustainability levels for
508 their companies. As with all IS relationships, there are challenges involved which include
509 technology readiness and maturity, economic factors and policy development.⁵⁰



510 However, if the companies have common goals of increasing sustainability levels and
 511 have the financial resources, these relationships can be nurtured and can flourish.
 512 Further work can therefore be undertaken utilising supply chain optimisation of the co-
 513 production schemes with techno-economic analyses to highlight the viability of IS
 514 integration and hybridisation within conventional large-scale chemical production.

515
 516 **Table 2** Life Cycle Inventories for BAU and IS integrated (*Hyd*) MeOH-NH₃ co-production cases.

517 Functional unit (FU) = 1 kg NH₃.

Technology	GHR-	SMR-	ATR-	GHR-	SMR-	ATR-	GHR-	SMR-	ATR-	GHR-	SMR-	ATR-
	SMR	SMR	SMR	ATR	ATR	ATR	SMR	SMR	SMR	ATR	ATR	ATR
	BAU	BAU	BAU	BAU	BAU	BAU	Hyd	Hyd	Hyd	Hyd	Hyd	Hyd
INPUTS- Materials												
Natural Gas^a	2.37	2.65	2.55	1.96	2.24	2.14	2.14	2.37	2.29	1.73	1.97	1.88
[kg]												
Water [kg]	1.11	1.81	0.88	1.61	2.31	1.38	1.07	1.66	0.88	1.57	2.16	1.38
Captured CO₂^b [kg]	-	-	-	-	-	-	-	1.41				
Green H₂ [kg]	-	-	-	-	-	-	0.089	0.089	0.089	0.089	0.089	0.089
INPUTS- Energy												
Electricity^c	1.10	0.20	0.27	1.35	0.45	0.52	1.07	0.31	0.37	1.31	0.56	0.62
[kWh]												
Heating^d	4.69	11.22	5.37	-	6.53	0.68	4.69	10.15	5.26	-	5.46	0.57
[kWh]												
Cooling	6.49	9.09	8.09	5.66	8.26	7.26	6.37	8.55	7.70	5.54	7.71	6.87
[kWh]												
OUTPUTS- MATERIALS												
MeOH [kg]	2.71	2.71	2.71	2.71	2.71	2.71	2.71	2.71	2.71	2.71	2.71	2.71
NH₃ [kg]	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Process CO₂	1.23	0.34	1.23	1.47	0.58	1.47	0.56	-	0.56	0.80	0.06	0.80
[kg]												
Other CO₂	1.22	2.88	1.71	0.19	1.85	0.68	1.26	2.64	1.67	0.23	1.61	0.64
[kg]												
CO-PRODUCT ALLOCATION^e												
MeOH	0.716	0.716	0.716	0.716	0.716	0.716	0.716	0.716	0.716	0.716	0.716	0.716



NH₃	0.284	0.284	0.284	0.284	0.284	0.284	0.284	0.284	0.284	0.284	0.284	0.284
KPIs^f												
Energy	66.93	61.51	63.72	79.59	72.05	75.12	67.31	62.68	64.58	80.14	73.65	76.32
Efficiency												
[%]												
Resource	31.28	35.00	33.71	25.89	29.61	28.31	31.13	34.24	33.16	25.74	28.85	27.76
Efficiency												
[MJ/kg_{products}]												

518 ^aTotal Natural gas required both as feedstock and utility heating purposes; ^bCaptured CO₂ from Natural Gas Power
519 Plant; ^cNet Electricity consumed considering total power generated within flowsheets; ^dNet Heating consumed
520 considering total heat produced from purge gas, NH₃ boil-off and total heat required by natural gas; ^eEconomic
521 allocation considering MeOH price = USD 0.679/kg,⁵¹ NH₃ price = USD 0.73/kg;⁵² Energy and Resource efficiencies
522 evaluated at LHV_{natgas} = 49 MJ/kg;⁵³ LHV_{MeOH} = 22.7 MJ/kg;⁵⁴ LHV_{NH₃} = 18.8 MJ/kg;⁵⁵ LHV_{H₂} = 120.2 MJ/kg.⁵³
523

524 4. Conclusion

525 The inherent flexibility of IS-integrated co-production systems, which allow for seamless
526 incorporation of renewable energy sources, positions them as pivotal players in the
527 transition toward sustainable industrial practices. Our study underscores the
528 transformative potential of IS in reshaping production within the existing MeOH and NH₃
529 industries. By integrating green H₂ produced through electrolysis and utilising CO₂ from
530 NH₃ synthesis, we have demonstrated a viable pathway for significantly reducing the
531 carbon footprint of these essential chemical industries. A detailed analysis revealed that
532 the application of IS, mainly through the ATR_{NH₃} configurations, has shown superior
533 performance in energy efficiency and reduced resource intensity compared to
534 conventional SMR_{NH₃} systems. In contrast, IS-integrated flowsheets for MeOH
535 demonstrate significant reductions in natural gas use and heating requirements albeit with
536 an 8% increase in electricity consumption due to E-methanol production. These changes
537 result in an average 28% reduction in total CO₂ emissions across IS cases compared to
538 BAU operations. Notably, the trade-offs between electrification and heating offer
539 substantial benefits for low-carbon NH₃ production, with the GHR-ATR_{Hyd} configuration
540 achieving a noteworthy reduction in natural gas consumption and CO₂ emissions,
541 highlighting its potential as a leading approach for low-carbon chemical manufacturing.



542 General trends indicate that EE increases and RI decreases in the order of GHR > ATR
543 > SMR, with ATR_{NH_3} outperforming SMR_{NH_3} in most metrics. Specifically, the GHR-
544 ATR_{BAU} configuration emerges as the most energetically favourable. While IS promotes
545 efficient energy use, it is crucial to recognise that the GHR- ATR_{BAU} systems excel beyond
546 other configurations, except for its hybrid variant GHR- ATR_{Hyd} . This underscores the
547 necessity for comprehensive energy analysis and trade-off assessments in co-production
548 schemes. In BAU co-production setups, the primary hotspots are linked to natural gas
549 consumption and direct CO_2 emissions, with similar trends observed in hybrid systems,
550 albeit with slightly lower impacts. GHG impacts improve in the sequence GHR- ATR_{Hyd} >
551 $ATR-ATR_{Hyd}$ > $SMR-ATR_{Hyd}$ > GHR- SMR_{BAU} > $ATR-SMR_{BAU}$ > $SMR-SMR_{BAU}$, aligning
552 with energy and resource efficiency results. Although the benefits of IS are primarily
553 realised through green H_2 integration, the inherent flexibility of IS-integrated co-production
554 flowsheets supports greater E-methanol integration as renewable electricity scales up,
555 enabling more sustainable MeOH and NH_3 production.

556 Looking ahead, future work offers significant opportunities to optimize IS-integrated
557 systems and advance their sustainability. Building on the demonstrated environmental
558 benefits of the IS pathway, key areas of focus include integrating GHR ammonia systems
559 to explore additional low-carbon co-production schemes and conducting techno-
560 economic analyses to assess their scalability and financial feasibility. Supply chain
561 optimization processes can also be employed to determine the optimal mix of
562 technologies and address logistical challenges, while incorporating life cycle costing will
563 provide a comprehensive assessment of long-term economic and environmental impacts.
564 Furthermore, identifying and addressing potential technical bottlenecks, such as process
565 inefficiencies or material compatibility issues, will be critical. These efforts, combined with
566 strategies to scale and commercialize IS systems, will help bridge the gap between
567 research and industrial application, ultimately supporting broader absolute sustainability
568 goals.

569 Overall, ATR configurations demonstrate superior performance across human health and
570 ecosystem quality, whereas GHR and SMR technologies show less favourable outcomes.
571 Despite potential burden shifting, the overall impact remains positive, with the GHR-



572 ATR_{Hyd} approach emerging as the most favourable production method compared to
573 current BAU processes - advancing decarbonisation efforts within the MeOH and NH₃
574 industries. Ultimately, this study demonstrates that IS is a viable strategy for the cleaner
575 co-production of MeOH and NH₃, offering a transferable model for sustainable chemical
576 production in other carbon-intensive industries, advocating for a promising pathway
577 toward achieving net-zero emissions and defossilising chemical sectors.



578 **Appendix A. Supplementary data**

579 All specific data supporting this article have been included as part of the Supplementary
580 Information.

581 **Conflicts of interest**

582 There are no conflicts to declare.

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Towards Flexible Large-Scale Environmentally Sustainable Methanol and Ammonia Production using Industrial Symbiosis

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Data Availability Statement

All specific data supporting this article have been included as part of the Supplementary Information.

