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Enhancing the cycle-life of initial-anode-free lithium-metal batteries by pre-lithiation in Mn-based Li-rich spinel cathodes†

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Anode-free lithium metal batteries (AF-LMBs) are attracting growing attention due to the burgeoning pursuit of high energy density. However, the poor reversibility of lithium-ion plating/stripping on the Cu anode triggers multiple issues, including rapid capacity loss, active lithium loss, and short lifetime. Herein, a cathode pre-lithiation strategy combined with a fluorine-containing electrolyte is introduced to achieve long-lifetime AF-LMBs. Furthermore, contact pre-lithiation, a more advanced and convenient strategy, has been introduced to precisely control the lithiation degree by adjusting the contact time. It has been demonstrated that over-lithiated $\text{Li}_{1.3}\text{Mn}_2\text{O}_4$ can deliver additional lithium ions during the charging process, thus exhibiting 94.4% capacity retention after 40 cycles.



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research interests are focused on the development of electrochemical energy storage devices, surface/interfacial electrochemistry, and operando spectroscopic characterization.

Introduction

Rechargeable Li-ion batteries (LIBs) have developed into the most commonly used electrochemical energy storage devices.^{1–4} Nowadays, with the urgent requirement of achieving maximum energy density, lithium metal batteries (LMBs) have been spotlighted as next-generation energy storage devices.^{5–8} Compared with traditional LMBs, anode-free lithium metal batteries (AF-LMBs) have a higher theoretical energy density.^{9–12} However, owing to the lack of lithium compensation, the poor reversibility of lithium-ion plating/stripping, and non-uniform lithium deposition on the Cu anode, AF-LMBs face the tremendous challenge of rapid capacity fading, which hinders their practical implementation.^{9,13–15} In the last few years, numerous strategies (such as optimizing electrolytes, modifying current collectors, constructing artificial solid electrolyte interphase (SEI) layers, and pre-lithiation strategies) have been proposed to extend the lifetime of AF-LMBs.^{16–18} Among these strategies, pre-lithiation strategies can effectively compensate for the irreversible lithium loss during the first few cycles, improve the initial coulombic efficiency (ICE), and thus obtain better cycle performance. However, anode pre-lithiation strategies cannot apply to AF-LMBs because Li-ions cannot intercalate into the Cu anode, different from other anodes (*i.e.*, carbon-, Si- and graphite-based anodes).^{19,20}

Currently, efforts have also been made to pre-install additional lithium sources into the cathode which can be classified as adding Li-containing additives and forming an over-lithiated cathode.^{21,22} Li-containing additives in the cathode can effectively mitigate the lithium loss, however, sacrificial salts ($\text{Li}_2\text{C}_4\text{O}_4$, $\text{Li}_2\text{C}_2\text{O}_4$, and Li_3N , *etc.*) would generate gases (*i.e.*, CO,

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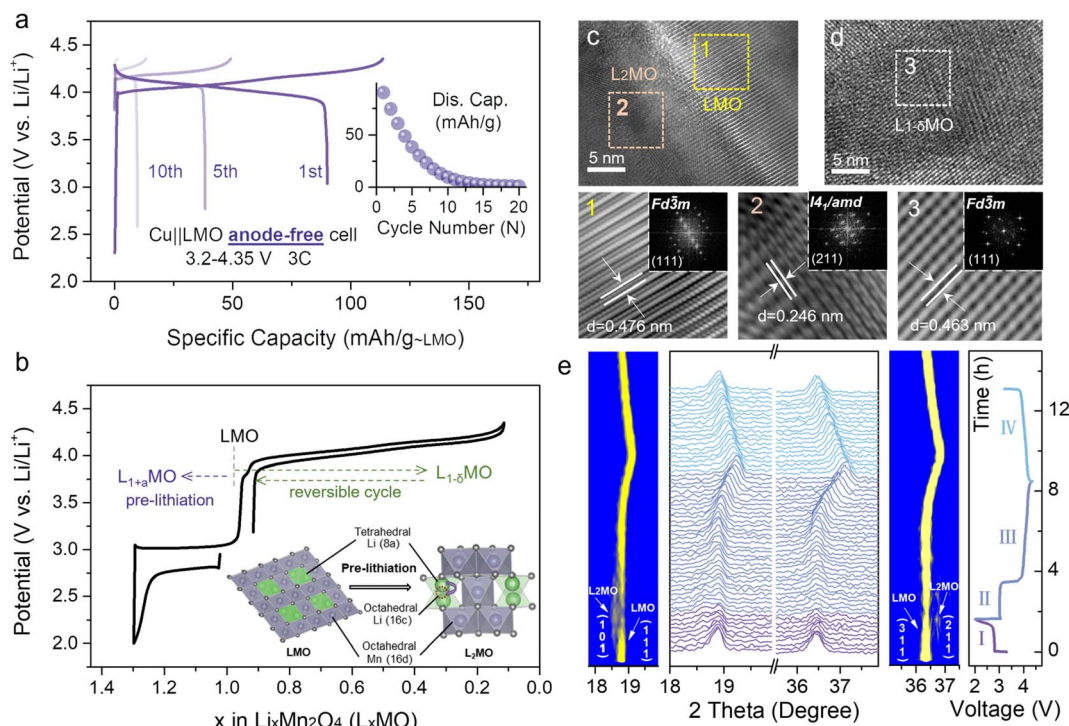


Fig. 1 (a) Charge–discharge curves of the Cu||LMO anode-free cell in the voltage range from 3.2 to 4.35 V at 3C rate. (b) The charge/discharge profiles of the Li||LMO half-cell ($L_x\text{MO}$ ($0 \leq x \leq 2$)). Insets are the schematic illustration of the reversible phase transition between LMO and $L_2\text{MO}$. High-resolution transmission electron microscopy (HRTEM) images of the LMO (c) discharged to 2 V and (d) recharged to 4.35 V, and the corresponding (inverse) fast Fourier transformation (FFT) patterns. (e) Two-dimensional contour map of *in situ* X-ray diffraction (XRD) diffraction patterns for the (101), (111), (311), and (211) reflections, and the corresponding galvanostatic charge–discharge curve of the Li||LMO half-cell.

CO_2 , or N_2) at the specific voltage after the first charge, which would affect the electrode stability, the energy density of the system, and the whole cycling environment, hindering the practical application.^{23,24} The over-lithiated cathode can release additional Li-ions during the first charge, which are stored in unoccupied crystallographic sites, to offset the active lithium consumed to form the SEI and the lithium loss in the subsequent cycles.^{25–28} Notably, the over-lithiated cathode strategy does not introduce inactive ingredients, making it more convenient for practical applications than additives.

LiMn_2O_4 (LMO) is a non-toxic and environmentally friendly cathode material with low cost and outstanding rate performance. Meanwhile, over-lithiated $\text{Li}_{1+x}\text{Mn}_2\text{O}_4$ ($L_{1+x}\text{MO}$, $0 \leq x \leq 1$) obtained by over-lithiation of LiMn_2O_4 was proposed as a lithium reservoir compound to provide an additional lithium source to overcome the capacity loss, and considered as a promising cathode material for AF-LMBs.²⁹ Over-lithiated cathodes on AF-LMBs can improve the ICE and prolong the lifetime, but the lifetime has still been threatened by the undesirable average coulombic efficiency (ACE). To achieve desirable ACE, the strategy of optimizing electrolytes has been applied. Electrolyte engineering will modify the interface chemistry of AF-LMBs by introducing fluorine-containing additives to obtain high capacity retention (CR). Therefore, combining over-lithiated cathodes with optimized electrolytes can extend the lifespan of AF-LMBs to the best.

In this work, the Cu|| $L_{1.3}\text{MO}$ AF-LMB was constructed using the Cu anode and over-lithiated $\text{Li}_{1.3}\text{Mn}_2\text{O}_4$ ($L_{1.3}\text{MO}$) cathode obtained from conventional LMO (Fig. S1 and Table S1†), combined with a fluorine-containing electrolyte to prolong the AF-LMB lifetime. Additional lithium can be provided by the I_{41}/amd type $\text{Li}_2\text{Mn}_2\text{O}_4$ ($L_2\text{MO}$) during the first charge, and thus offset the lithium consumption. The crystal structure of the cathode material after pre-lithiation has been studied by *in situ* X-ray diffraction (XRD). In addition, the transition between LMO and $L_2\text{MO}$ is reversible, which has been demonstrated by *ex situ* X-ray absorption structure (XAS) analysis. Considering that electrochemical pre-lithiation cannot be used in practical applications, we propose a contact pre-lithiation method, which can precisely control the lithiation degree by adjusting the contact time. At the same time, benefiting from the over-lithiated cathode and optimized electrolyte, a Cu|| $L_{1.3}\text{MO}$ anode-free cell with a high ICE of 99% can still achieve a capacity retention of 94.4% after 40 cycles at 0.5C discharge.

Results and discussion

The electrochemical performance of the Cu||LMO anode-free coin-cell shows a rapid capacity loss during different cycles without excess lithium (Fig. 1a). As for the typical anode-free cell, disappointing initial coulombic efficiency (ICE) is attributed to the lithiophilic organic–inorganic solid electrolyte interphase (SEI) and Li dendrite formation on the Cu anode,

and undesirable average coulombic efficiency (ACE) which is triggered by non-uniform Li plating/stripping on the lithiophobic Cu anode (Fig. S2†).^{5,25,30} However, the ICE and ACE of the Li||LMO half-cell (Fig. S3†) upon cycling with different numbers reached superior values, about 96.3% and 99%, respectively, indicating that the poor cycling stability of the Cu||LMO AF-LMB results from the Cu anode. To date, various strategies for optimizing anode-free cells have been reported in several literature reports. Electrolyte optimization is an effective strategy to increase the lifetime because it can improve the ACE by promoting lithium morphology and lithium plating/stripping on the Cu anode.^{16,31} In addition, to improve the ICE of anode-free cells, pre-lithiation strategies have been applied to extend the lifespan, which can provide additional lithium-ions to compensate for the irreversible Li loss during the initial cycles. Herein, we use a strategy gained from the aforementioned considerations by combining optimized electrolytes with cathode pre-lithiation to reduce active lithium loss and supplement the irreversible capacity loss, extending the lifetime of anode-free cells.

From the point-of-view of specific energy, environmental pollution (toxicity), and cost, a spinel LMO cathode is one of the most promising cathodes for lithium-ion batteries (LIBs) owing to the low toxicity of Mn sources, abundant reserves, high energy density, and excellent rate performance. LMO compounds have the unoccupied octahedral site (16c) and the formula can be denoted as $[\text{Li}^+]_{8a}[\text{Mn}^{3+}\text{-Mn}^{4+}]_{16d}[\square]_{16c}[\text{O}_4]_{32e}$ (\square represents the octahedral vacancy).³² The $[\text{Mn}_2]_{16d}[\square]_{16c}[\text{O}_4]_{32e}$ skeleton is a three-dimensional network of tetrahedral and octahedral coplanar structures, which benefit fast lithium-ion diffusion. Additional lithium ions can intercalate into the empty 16c octahedral sites in the LMO structure, allowing LMO to transform into $\text{Li}_2\text{Mn}_2\text{O}_4$ (L_2MO) and enabling the application of pre-lithiation strategies.

Fig. 1b displays the charge–discharge curves of the Li||LMO half-cell, related to the pre-lithiation process, and the schematic illustration of the reversible phase transition between LMO and L_2MO . Li-ions at the 8a site continuously insert into empty 16c octahedral sites during the first discharge process, and then the cubic spinel converts to a tetragonal spinel L_2MO .^{1,32} Besides, high-resolution transmission electron microscopy (HRTEM) and *in situ* X-ray diffraction (XRD) were carried out to visually demonstrate the phase transition between LMO and L_2MO during the whole charge–discharge cycling process (Fig. 1c–e). Fig. 1e shows the evolution of XRD patterns and the corresponding zoom in the contour plot of the main peak (111) and (311) throughout the entire four regions (the specific reaction equations are shown in Fig. S4†), clearly demonstrating the two-phase transition process.³³ In region I, during the first discharge process, the characteristic peaks (111) and (311) of LMO gradually divide into two peaks, and new peaks (101) and (211) which are related to the L_2MO form, respectively, indicating one Li-ion is intercalated into the empty octahedral site of cubic LMO to transform partial LMO into tetragonal L_2MO , resulting in the coexistence of LMO and L_2MO .³⁴ Region II (recharge to 3.9 V) is the reverse process of region I, involving a phase transition from L_2MO (tetragonal) to LMO (cubic), and all the

characteristic reflections of L_2MO gradually disappear. In region III (recharge to 4.35 V), on further de-intercalation of Li-ions from the transformed LMO (cubic), the (111) and (311) peaks of LMO are observed to shift to higher degrees, inducing a solid–solution reaction to form cubic-spinel-like Li-deficient $\text{Li}_{1-\delta}\text{Mn}_2\text{O}_4$ ($0 \leq \delta \leq 1$).³³ When re-discharged to 3.2 V (region IV), all the characteristic reflections of LMO shifted back to the initial position, indicating that L_2MO reversibly transforms into LMO. In Fig. 1c, the lattice fringes of over-lithiated LMO reveal the (111) plane of LMO and (211) plane of L_2MO with interlayer spacings of 0.476 nm (region 1, yellow) and 0.246 nm (region 2, orange), respectively, indicating the coexistence of LMO and L_2MO . Furthermore, the Li-deficient LMO after charge to 4.35 V remains a cubic-spinel structure (Fig. 1d, region 3, white), which is similar to the initial cubic-spinel LMO (Fig. S5†), implying that partial pre-lithiation will not affect the LMO structure. HRTEM results are consistent with *in situ* XRD. Meanwhile, L_2MO , formed by first discharge to 2 V, will release additional Li-ions to the anode during the subsequent cycles. By controlling the re-discharge cut-off voltage, partial Li-ions can be stored on the anode to prolong the lifetime of anode-free cells without sacrificing the energy density (Fig. 1b).

Intercalation of too many Li-ions into the LMO structure will affect the structural stability, and therefore, it is necessary to precisely control the lithiation degree of cathodes. When the lithiation degree exceeds 30%, the structure of the LMO will be damaged (Fig. S6†). Based on the above considerations, the molar percentage of L_2MO in the L_{1+x}MO cathode was kept below 30% in the subsequent tests. When the initial discharge cut-off voltage is set to 2 V, $\text{L}_{1.3}\text{MO}$ is obtained (Fig. S7, S8 and Table S2†). Fig. 2a (gray line) displays the whole electrochemical lithiation charge–discharge curves of the Li|| $\text{L}_{1.3}\text{MO}$ half-cell (denoted as cell-B). To explore the effect of structural stability after over-lithiation, the electrochemical performance of the Li|| $\text{L}_{1.3}\text{MO}$ half-cell was further compared with that of the typical Li||LMO half-cell (denoted as cell-A, Fig. S9†) shown in Fig. 2b (3.2–4.35 V, at 1C (1C = 148 mA g⁻¹)). Notably, cell-B released an outstanding discharge capacity of 115.6 mA h g⁻¹ with 99.46% ICE, ascribed to the electrochemical pre-lithiation in the initial discharge process. Furthermore, cell-B exhibits superior capacity retention and cycling stability after 500 cycles, consistent with or even better than that of cell-A, indicating that partial pre-lithiation will not affect the structural stability of LMO and the reversible phase transformation between LMO and L_2MO (cyclic voltammetry curves confirmed this conclusion again, Fig. S10†). However, due to the typical Jahn–Teller distortion and manganese disproportionation reaction, the LMO cathodes exhibit unstable long-term stability in the voltage range from 2 V to 4.35 V (Fig. S11†).

The analysis of the cathode structure will deliver valuable information for further comprehending the prominent electrochemical performance.³⁵ The X-ray absorption structure (XAS) technique, especially X-ray absorption near edge structure (XANES) and extended X-ray absorption fine structure (EXAFS), is suitable for obtaining information regarding the electronic and local structure of cathode materials.³⁶ The *ex situ* XAS spectra at the Mn K-edge have been photon-energy-calibrated,

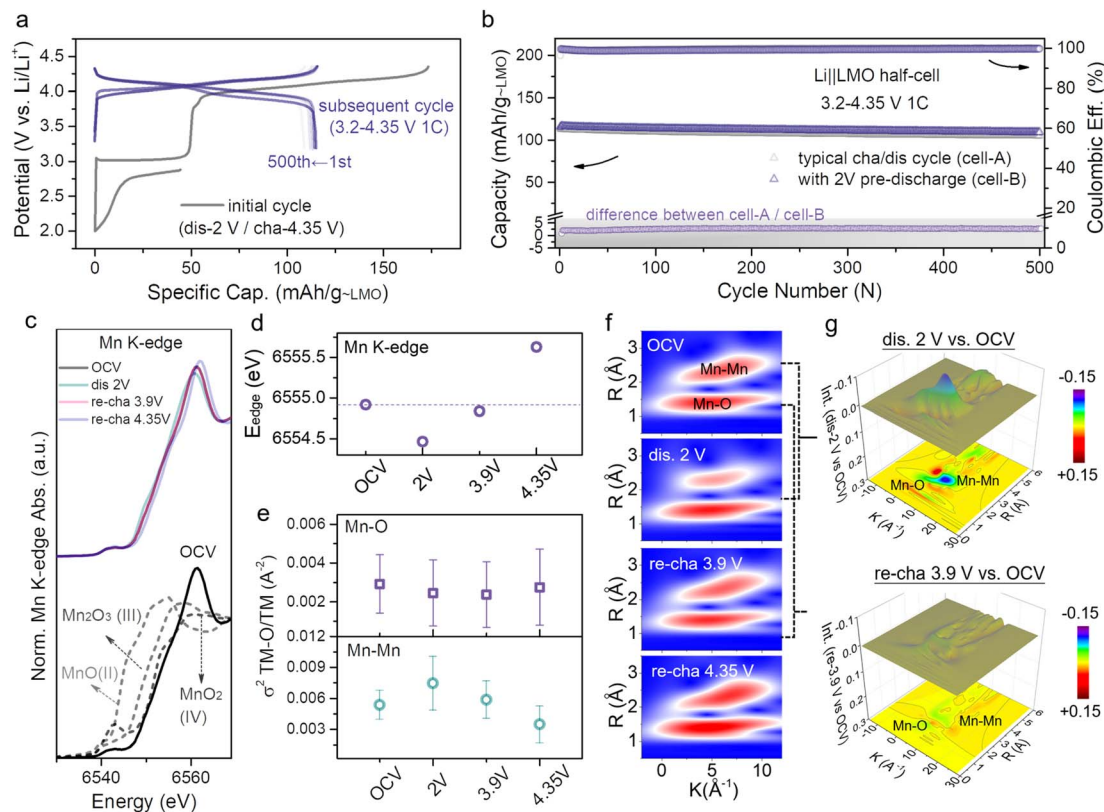


Fig. 2 (a) Voltage profiles of the Li||L_{1.3}MO half-cell that was initially discharged to 2 V and then cycled in the voltage range of 3.2–4.35 V (denoted as cell-B). (b) Cycling performances of cell-A (Fig. S9†) and cell-B, along with the difference of discharge capacity between cell-A and cell-B. (c) XANES spectra, and (d) edge positions at the Mn K-edge of the LMO electrodes at different voltage states. (e) Debye–Waller factor σ^2 , and (f) WT-EXAFS spectra of the Mn–O/Mn bond of the LMO at different states. (g) Color 3D WT-EXAFS spectra showing the differences between WT-EXAFS spectra of the Mn–O bond and Mn–Mn bond (first discharge to 2 V vs. OCV (top) and re-charge to 3.9 V vs. OCV (bottom)).

absorbance-normalized, and then used to capture the internal structural evolution of LMO after pre-lithiation. Fig. 2c and d provide information about the valence state variation of Mn during the whole charge–discharge process at four specific potentials (open circuit voltage (OCV), dis 2 V, re-cha 3.9 V and re-cha 4.35 V; dis: discharge, re-cha: re-charge), and the corresponding point position in the charge–discharge curve is shown in Fig. S12.† The XANES spectra at the OCV state by contrast with several manganese oxides standards (MnO, Mn₂O₃, and MnO₂) are stacked in the Fig. 2c bottom for reference. The edge position of the OCV state discloses the coexistence of Mn³⁺ and Mn⁴⁺ in LMO. With the continual intercalation of Li-ions, upon discharge to 2 V, the edge position of Mn shifted from 6654.9 eV to lower energy (6554.5 eV) as a result of the reduction of Mn⁴⁺ to lower valence manganese, inducing the formation of a new tetragonal phase L₂MO to result in the coexistence of LMO and L₂MO. The Mn edge position backward shifted to the initial position while recharging to 3.9 V. When reaching a higher voltage (re-cha 4.35 V) owing to excessive deintercalation of Li-ions, the edge position shifted to higher energy (6555.6 eV), resulting in a solid–solution reaction accompanied by the oxidation of Mn³⁺ to Mn⁴⁺. The changes in the Mn K-edge position indicated the reversibility of the LMO structure after pre-lithiation.

In addition, EXAFS spectra (Fig. S13†) provide information about bond length, coordination number, and the Debye–Waller factor (σ^2) of the coordination atoms for the Mn atom, such as O and Mn. Fig. S14† presents Fourier transform (FT) magnitude and the relevant fitting result of Mn K-edge EXAFS spectra in the OCV state, corresponding to a model of dealing EXAFS data. The two shells at ≈ 1.5 and 2.5 Å correspond to the Mn–O and Mn–Mn interactions. The σ^2 provides a measure of the structural disorder in a material, as shown in Fig. 2e. The σ^2 value of Mn–Mn increased and the bond strength (R) of Mn–Mn weakened (Fig. S13†) while discharging to 2 V, suggesting that the intercalation of Li-ions in octahedral vacancies results in the transformation of the LiO₄ tetrahedron into LiO₆ octahedra, which affects the Mn–Mn interaction so that the Mn–Mn coordination and system structure disorder become intensified, giving rise to the two-phase transition from LMO to L₂MO. During the process of recharging to 3.9 V accompanied by the deintercalation of Li-ions, the Mn–Mn σ^2 value recovered to the initial value along with a slight deviation leading to the local structure being ordered, indicating the high reversibility of the Li-ion intercalation/deintercalation and LMO structure after pre-lithiation, which was consistent with the results of XANES. With the further deintercalation of Li-ions, the σ^2 value of Mn–Mn decreased and the Mn–Mn distance became shorter

(Fig. S13[†]), suggesting that the LMO structure became more ordered. In the LMO structure, the Mn–O distance does not vary much with the complete discharge–charge process due to the Mn atoms being coordinated by 6 adjacent O atoms at equal distances. To further explore more intuitive changes of the surrounding coordination environments of transition metal after a whole Li-ion (de)intercalation process, wavelet transform (WT) analysis of Mn K-edge spectra is further performed. Fig. 2f exhibits two different regions: Mn–O (first shell) and Mn–Mn (second shell). The strength of Mn–Mn at dis 2 V is weakened compared with the OCV state, owing to the covalent effect of Li-ions intercalating into vacancies on the two-phase transition. Notably, the strength difference between dis 2 V and OCV is quite obvious (blue) as seen from the color 3D WT-EXAFS spectra in Fig. 2g. In addition, along with the lithium-ions deintercalated from the octahedral sites, when re-charging to 3.9 V, the strength of Mn–Mn goes back to the strength of Mn–Mn at the initial OCV state with a slight difference, consistent with the results in Fig. 2g (yellow). The strength variability of Mn–Mn suggests that the covalent effect has no effect on structural reversibility.

Based on the aforementioned results, the cathode pre-lithiation strategy has been applied to anode-free cells. However, only utilizing the cathode pre-lithiation strategy to improve ICE (Fig. S15a[†]) or using optimized electrolytes to

improve ACE (Fig. S15b[†]) still results in rapid capacity loss, and the lifetime of the anode-free cell cannot extend to the best. To get the maximum energy density and long-term stable anode-free devices, the cathode pre-lithiation strategy combined with a fluorine-containing electrolyte was applied to achieve long-lifetime anode-free cells. Depending on the structural properties of LMO, extra Li-ions can be stored in the LMO structure. The lithiation degree can be determined by the cut-off potential. An anode-free cell consisting of an over-lithiated $L_{1.3}MO$ cathode and a Cu anode outperforms the $Cu||LMO$ anode-free cell (Fig. 3a and b) by delivering a higher initial discharge specific capacity of 112 mA h g^{-1} , with an outstanding capacity retention of 93.1% after 40 cycles (Fig. 3c, S16 and S17[†]). The ICE of the anode-free cell increases from 84.4% to 98.8%, due to the pre-lithiation strategy, which stores extra Li-ions in the LMO structure, which can offset the irreversible loss of active lithium in the subsequent cycles. Meanwhile, electrolyte optimization promotes the reversibility of lithium plating/stripping, which contributes to the long lifespan of anode-free cells. More importantly, $L_{1.3}MO$ is outstanding in rate performance (Fig. S18[†]), which makes it possible to realize anode-free cells with high current density. When discharged at 1C rate, the ICE of the $Cu||L_{1.3}MO$ anode-free cell (Fig. S19b[†]) is 98%, with a high capacity retention of 83.3% after 40 cycles (Fig. 3d), certainly surpassing the $Cu||LMO$ anode-free cell (Fig. S19a[†]). Therefore, the outstanding electrochemical performance of the $L_{1.3}MO$ cathode undoubtedly demonstrates its great potential for anode-free cells.

Electrochemical pre-lithiation has been widely used in laboratories, however, the complex assembly/disassembly process hinders its practical applications. To date, some alternative strategies have been proposed. First, lithium metal powder can be mixed into the electrode for pre-lithiation; nevertheless, this strategy is relatively risky to cause short-circuit.²¹ Second, the lithiation degree of ultra-thin lithium films can be controlled by their thickness, but their cost makes them impractical for large-scale practical applications.²⁶ Moreover, there is a piece of bad news, massively reported strategies have been applied to common anodes rather than Cu anodes, and most of these strategies cannot be applied to Cu anodes. In this work, contact pre-lithiation, a more advanced and convenient strategy, has been introduced for application to the cathode, and the schematic is displayed in Fig. 4a. When the un lithiated LMO cathode comes into direct contact with lithium metal through the pre-prepared electrolyte, the spontaneous pre-lithiation process will be initiated due to the potential difference between LMO and lithium metal (lithium metal has a much lower potential than LMO). In the pre-lithiation process, the lithium metal transforms into Li-ions, and then gradually intercalates into LMO octahedral vacancies. To inspect the feasibility of contact pre-lithiation and electrochemical pre-lithiation, *in situ* XRD was conducted (Fig. 4b and c). For electrochemical pre-lithiation, during the discharge process of the plateau around 2.7 V, the main peak (111) gradually divided into two, and a new diffraction peak (101) related to L_2MO appeared, indicating the formation of L_2MO . A similar tendency was observed in the *in situ* XRD patterns of contact pre-lithiation

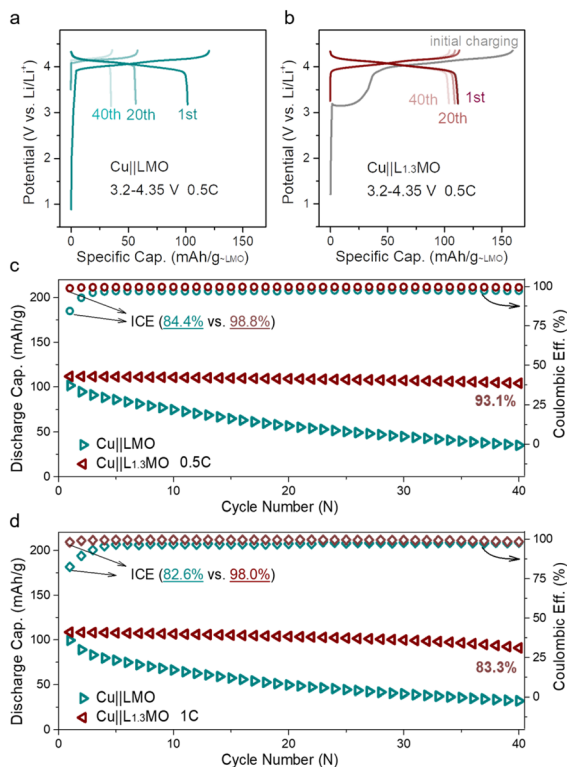


Fig. 3 Charge–discharge curves of (a) $Cu||LMO$ and (b) $Cu||L_{1.3}MO$ anode-free coin cells, and (c) corresponding cycling performance and CE of (a) and (b) at 0.5C discharge rate. (d) Cycling performance and CE of $Cu||LMO$ (Fig. S19a[†]) and $Cu||L_{1.3}MO$ (Fig. S19b[†]) at 1C discharge rate. ($L_{1.3}MO$ cathodes were prepared *via* the electrochemical pre-lithiation method).

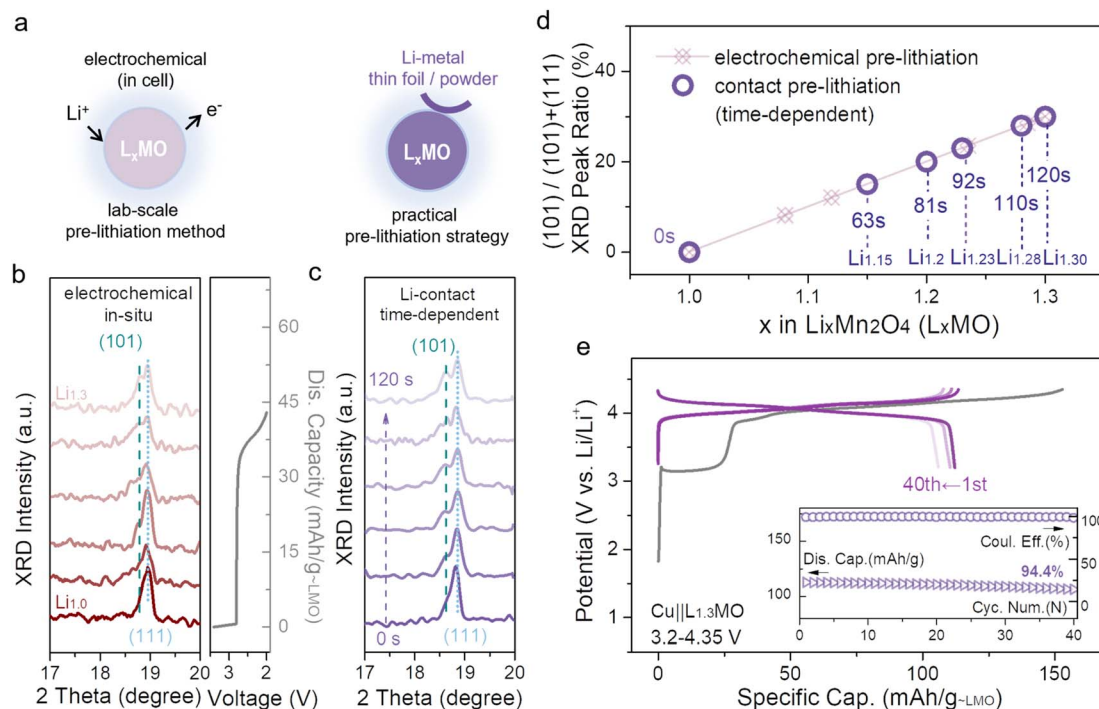


Fig. 4 (a) Schematic illustration of electrochemical pre-lithiation (left) and contact pre-lithiation (right). (b) *In situ* XRD patterns of the Li||LMO half-cell discharged to 2 V, and the corresponding galvanostatic charge–discharge curve (according to electrochemical pre-lithiation). (c) *In situ* XRD patterns of contact pre-lithiation which depends on contact time were obtained to observe the change of the main peak (111). (d) The ratio of the (101) peak area corresponds to different x values in $L_x\text{Mn}_2\text{O}_4$ ($0 \leq x \leq 2$) (according to *in situ* XRD patterns in (b) and (c)). (e) Typical galvanostatic charge/discharge curves of the $\text{Cu}||\text{L}_{1.3}\text{MO}$ (2 min) anode-free coin cell at 0.5C discharge rate, and the inset represents the corresponding cycling performance.

(Fig. 4c), and as the contact time increased, the (101) peak also appeared, confirming that contact pre-lithiation is reliable. More importantly, the lithiation degree (x value, ($0 \leq x \leq 2$)) can be precisely controlled by controlling the contact time (Fig. S20†), and the integrity of the cathode can be maintained during the pre-lithiation process. Notably, by calculating the proportion of the (101) peak area, when the contact time extended to 2 min, the same over-lithiation degree was achieved using contact pre-lithiation and electrochemical pre-lithiation (Fig. 4d). Furthermore, over-lithiated $\text{L}_{1.3}\text{MO}$ was achieved *via* contact pre-lithiation of LMO for 2 min, and then a $\text{Cu}||\text{L}_{1.3}\text{MO}$ anode-free cell was constructed (Fig. 4e). The electrochemical performance of the $\text{Cu}||\text{L}_{1.3}\text{MO}$ anode-free cell prepared by contact pre-lithiation is tantamount to the electrode prepared by electrochemical pre-lithiation, confirming that contact pre-lithiation has no effect on the LMO structure. In addition, the $\text{Cu}||\text{L}_{1.3}\text{MO}$ anode-free cell with a high ICE of 99% exhibits a high capacity retention of 94.4% after 40 cycles (Fig. 4e), exhibiting its great potential for practical applications.

Conclusions

In summary, a cathode strategy combined with optimized electrolytes has been successfully proposed to achieve a long life-span of AF-LMBs. The variation of the crystal structure after pre-lithiation and the reversible phase transition between conventional $Fd\bar{3}m$ type LiMn_2O_4 and $I4_1/amd$ type $\text{Li}_2\text{Mn}_2\text{O}_4$

have been demonstrated by *in situ* XRD, HRTEM, and *ex situ* XAS. Additional lithium ions are intercalated into the vacancies in the LiMn_2O_4 structure to form over-lithiated $\text{Li}_2\text{Mn}_2\text{O}_4$, and then $\text{Li}_2\text{Mn}_2\text{O}_4$ delivers additional lithium ions during the first charge process to offset active lithium loss and prolong the life-span of AF-LMBs. Furthermore, contact pre-lithiation, a more advanced and convenient strategy at the engineering level, has been introduced to precisely control the lithiation degree by controlling the contact time. $\text{Cu}||\text{L}_{1.3}\text{Mn}_2\text{O}_4$ AF-LMBs have been constructed by the application of contact pre-lithiation combined with a fluorine-containing electrolyte and exhibit a high capacity retention of 94.4% after 40 cycles. We believe that this could spark a storm of related studies for the design of AMF-LMBs.

Author contributions

L. C., C. W., X. K. and Y. Q. contributed to the design of the research and performed the experimental data analysis. L. C. conducted the materials synthesis, electrochemical studies and cell performance studies. C. C. and Y. L. conducted the XAS experiments and the analysis of XAS results. G. Z., Y. T., and B. Z. helped to conduct the XRD experiment and FAULTS simulation. X. W. and T. L. conducted the LSV and SEM experiments. S. Z. conducted the HR-TEM experiment. H. Z. and Y. Y. drew the schematics. X. K., Y. L. and Y. Q. supervised the work. All

authors discussed the results, co-wrote and commented on the manuscript.

Conflicts of interest

There are no conflicts to declare.

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