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# ARTICLE



## Recent Developments in the Catalytic Hydrogenation of CO<sub>2</sub> to Formic acid/Formate using Heterogeneous Catalysts

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The conversion of  $CO_2$  into value added chemicals is one of the fascinating strategies to mitigate the level of  $CO_2$  in the atmosphere. Specifically, the hydrogenation of  $CO_2$  into formic acid/formate has received a great deal of attention since the product is a valuable basic chemical as well as a promising energy storage material. However due to the kinetic and thermodynamic limitations of this conversion, developing an efficient catalytic system has become desirable. Therefore various approaches have been implemented for the development of both homogeneous and heterogeneous catalysts. In this context, the recent advances in the hydrogenation of  $CO_2$  to formic acid/formate using heterogeneous catalysts as well as theoretical investigations are presented.

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#### 1. Introduction

In recent years, climate change and increasing global temperatures due to the anthropogenic emission of  $CO_2$  into the atmosphere have caused increasing concern. The concentration of  $CO_2$  in the atmosphere has reached unprecedented levels (~400 ppm), mainly due to the utilization of carbon-rich fossil fuels, such as coal, oil and natural gas.<sup>1-2</sup> Thus, reducing the emission of  $CO_2$ , utilizing the abundant  $CO_2$  in the atmosphere and recycling  $CO_2$  have attracted much attention.<sup>3-6</sup> Recently, "Lima call for climate action" targeted a



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the development of multifunctional COF materials.

near-zero anthropogenic emission of CO<sub>2</sub> by the end of the century, highlighting the concern over atmospheric CO<sub>2</sub> levels.<sup>7-8</sup> Consequently, research into renewable fuels, CO<sub>2</sub> storage and CO<sub>2</sub> utilization has gained increased attention in the scientific and technological community.<sup>9-12</sup>

 $CO_2$  is emerging as an attractive C1 feedstock for producing various chemicals owing to the fact that it is safe, abundant, nontoxic, economical and renewable. Such  $CO_2$ -based products are not only profitable, but are also alternatives to those derived from petroleum resources, and could therefore lessen petroleum dependence in society.<sup>13-17</sup> However, very few industrial processes, largely limited to those involving urea, salicylic acid and carbonate synthesis, utilize  $CO_2$  as a raw material.<sup>18</sup>

One important chemical, out of diverse chemical products derived based on  $CO_2$  as a C1 feedstock, is formic acid, which is a valuable basic chemical used as preservative, antibacterial agent, insecticide and also as de-icing agent in various



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industries.<sup>19-20</sup> In addition, it plays a major role in the synthetic chemistry as an acid, a reductant and a precursor for syntheses. Moreover, it is being considered as a hydrogen storage material in energy industries. Even though formic acid has a relatively low H<sub>2</sub> content (4.4 wt%), it is easy to store and transport.<sup>21</sup> Recently, formic acid has emerged as a promising fuel source in direct liquid fuel cell systems due to its excellent oxidation kinetics, high cell potential and less fuel crossover problems.<sup>22</sup> Thus, the myriad applications of formic acid as well as CO<sub>2</sub> utilization attracts the hydrogenation of CO<sub>2</sub> to formic acid/formates in the scientific and technological community to a greater extent.

Currently 800,000 T of formic acid is produced per year in the industries using toxic carbon monoxide and methanol.<sup>23</sup> According to Barcow and coworker's, this process could emit ca. 3076 kg of  $CO_2$  for the production of 1 T of formic acid, whereas only 100 kg of  $CO_2$  could be emitted, if the same is produced by  $CO_2$  hydrogenation process.<sup>24</sup> Hence,  $CO_2$ -based production has enormous potential to reduce the environmental impact when compared with conventional CObased method.

The hydrogenation of  $CO_2$  to formic acid involves the conversion of gases substances into liquid products and hence the reaction is entropically disfavored. Thus, the reaction is endergonic in the gas phase ( $\Delta G^{\circ}_{298} = 32.9 \text{ kJ mol}^{-1}$ ) and is exergonic in the aqueous (solvation) phase ( $\Delta G^{\circ}_{298} = -9.5 \text{ kJ} \text{ mol}^{-1}$ ). In addition, the equilibrium can be shifted towards the product side using certain bases, such as ammonia (NH<sub>3</sub>) and triethylamine (NEt<sub>3</sub>) (eqs. 1-3).<sup>25</sup> Moreover, the chemical equilibrium of  $CO_2$ /bicarbonate (HCO<sub>3</sub><sup>-1</sup>)/carbonate (CO<sub>3</sub><sup>2-</sup>) is influenced by many parameters, such as temperature, CO<sub>2</sub> pressure, kind of base, and solution pH. Thus, the actual form of the substrate in this reaction is ambiguous. Henceforth, the term 'hydrogenation of  $CO_2$ ' being used in this review and elsewhere may actually involve  $HCO_3^{-1}/CO_3^{-2-}$  as the real substrate.

Since the discovery of phosphine-based Ru complexes by Inoue *et al.*,<sup>26</sup> excellent progress has been achieved in the development of homogeneous catalysts.<sup>27-32</sup> In particular,

extensive studies on homogeneous Ir, Ru, and Rh complexes have been reported, and recently, half-sandwich Ir derivatives and Ru/Ir-pincer complexes have shown tremendous catalytic activities, with a maximum turnover number (TON) of 3,500,000 and a maximum turnover frequency (TOF) of 1,100,000  $h^{-1}$ .<sup>33-40</sup>

Despite the homogeneous catalysts exhibiting excellent catalytic efficiencies for the hydrogenation of  $CO_2$  to formate, industries are reluctant to use them for large-scale production, owing to the difficulty in catalyst separation from the final reaction mixture.<sup>41</sup> Importantly, these homogeneous catalysts also promotes the decomposition of generated formate back into  $CO_2$  and  $H_2$  during the product separation step(s).<sup>23,42-43</sup> Because of such limitations, diverse heterogeneous catalysts which have strong merit in separation were reported.

While many reviews and books have been focused on CO2 hydrogenation to formate using homogeneous catalysts,44-47 summarization of heterogeneous catalysts on  $CO_2$ hydrogenation are not available yet. Therefore, for the first time, the progress that has been achieved in the development of heterogeneous catalysts for this conversion is presented here. In order to explore the prospective design for highly active and industrially viable heterogeneous catalysts we have segmented this review based on the type of catalysts and the catalyst supports employed. The organization of this review is as follows; it has categorized into three major sections excluding introduction and conclusion. After this introduction, the second section provides the application of heterogeneous metal catalysts. This section is subdivided into two parts based on the type of metal catalysts employed: section 2.1 explores the performances of bulk metal catalysts; section 2.2 presents the catalytic efficiencies of supported metal catalysts. The third section addresses the application of heterogenized molecular catalysts. This section is further classified into two parts based on the kind of heterogenization processes followed; section 3.1 deal with the efficiencies of metal complexes heterogenized by grafting methods; section 3.2 explores the performances of metal complexes heterogenized by incorporating into the support's pore wall. Since



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	$\Delta G^{\circ}  \Delta H^{\circ}  \Delta S^{\circ}$
	(kJ mol <sup>-1</sup> ) (kJ mol <sup>-1</sup> ) (J mol <sup>-1</sup> K <sup>-1</sup> )
HCO <sub>2</sub> H (I)	32.9 -31.2 -216 (1)

 $CO_2(g) + H_2(g) + NH_3(aq) \longrightarrow HCO_2^{-}(aq) + NH_4^{+}(aq) -9.5 -84.3 -250$  (2)

 $CO_2(aq) + H_2(aq) + NH_3(aq) = HCO_2(aq) + NH_4^+(aq) -35.4 -59.8$ 

covalent organic framework (COF) based supports have only been utilized in the literature, we entitled this section as "Heterogenized COFs catalyst". The section four briefly explores the theoretical investigations on this topic and in the final section, we briefly summarized the status and perspectives of this field.

 $CO_2(g) + H_2(g)$ 

#### 2. Heterogeneous Metal Catalysts

#### 2.1 Bulk Metal Catalysts

The research on hydrogenation of CO<sub>2</sub> to formate began in 1935 by Adkins et al. using RANEY nickel (Ra-Ni) catalyst and they reported 57 % yield at 80-150  $^\circ\mathrm{C}$  under high pressure (20-40 MPa) in Ethanol (EtOH)/Phenol solvent system (Table 1, entry 1).<sup>48</sup> Even though the reaction was not catalytic (TON <1), it initiated a new field of research which is the conversion of relatively cheap and abundant CO<sub>2</sub> into value added chemicals. After a while, Stalder et al. employed Pd black as a catalyst for the conversion (entry 2) and observed catalytic conversion (TON 2.1) in 1 M aqueous NaHCO<sub>3</sub> solution after long reaction times (53 h).<sup>49</sup> Takahashi et al. used a mixture of Fe and Ni powder as a catalyst under hydrothermal conditions (300 °C) using water (H<sub>2</sub>O) as a hydrogen source; however, the yield of formate was very low (TON 0.022).<sup>50</sup> Later, Fachinetti et al. broadened their search to Group 8-11 metal blacks.<sup>51</sup> Initially they screened metals that promote the reverse reaction that is decomposition of formate salts to  $CO_2$  and  $H_2$ , as they necessarily promote the hydrogenation of CO<sub>2</sub> to formate. Transition metals (Group 8-11), such as Fe, Co, Ni, Cu, Ru, Rh, Pd, Ag, Ir, Pt and Au were screened for the decomposition of formic acid-NEt<sub>3</sub> (HCOOH/NEt<sub>3</sub>) adducts to CO<sub>2</sub> and H<sub>2</sub> at 40 °C, and only Au metal blacks showed gas evolution, indicating that only Au metal had the potential to promote the hydrogenation of CO<sub>2</sub> to formate. Since then, Au black was examined as a catalyst for the hydrogenation of  $CO_2$  to formate at 40 °C in NEt<sub>3</sub> solution, and the results showed that Au black fairly converted CO<sub>2</sub> to formate. However, deactivation of the catalyst was observed during the reaction, which was due to the aggregation of catalytic metal particles during the reaction, leading to the number of active sites on the surface of the catalyst being reduced. This result clearly explains the low catalytic efficiencies of bulk metals and also the inevitability of a support to stabilize metal blacks.

#### 2.2 Supported Metal Catalysts

Since heterogeneous catalytic reactions are surface reactions, they typically follow the following steps: (1) the adsorption of reactants onto the surface of the catalyst; (2) surface reaction of adsorbed reactants with the catalyst; and (3) desorption of

products from the surface of the catalyst.<sup>52</sup> Since the number of metal atoms on the surface of a bulk metal is extremely small compared to the number of metal atoms in the interior, a large number of active metal atoms are not exposed to the reactants, which makes bulk metals economically inefficient to use in catalytic processes. Moreover, as these bulk metals often aggregate under reaction conditions, the number of active metal atoms on the surface of the catalyst is reduced further. To overcome these problems, catalytically active metals are often dispersed on solid supports.

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(3)

Since the Au blacks aggregated under reaction conditions, Fachinetti *et al.* employed titanium dioxide (TiO<sub>2</sub>) supported Au particles (1 wt% Au) for this conversion.<sup>51</sup> The supported Au particles (AUROlite<sup>\*</sup>) showed superior catalytic conversion than unsupported Au particles, and attained a TON of 855 at 40 °C under 18 MPa total pressure in NEt<sub>3</sub> solution for 3 days (entry 3). Importantly, 1.3 kg of HCOOH/NEt<sub>3</sub> adduct with an acid to amine ratio of 1.7 was obtained after 37 days of continuous production. This result showed that, unlike bulk Au black, the supported Au particles were very stable during the reaction conditions. However, owing to the Au-catalyzed reverse water gas shift reaction, the accumulation of CO (63 mmol) was observed, which consequently slowed the reaction.<sup>53</sup>

Recently Pidko and co-workers employed both supported and unsupported Au nanoparticles [Au NP(s)] as a catalyst for this reaction.<sup>54</sup> They also observed the superior catalytic efficiency of supported Au NPs than unsupported Au NPs. They employed a series of supports namely, Al<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, ZnO, CeO<sub>2</sub>, MgAl-HT (hydrotalcite), MgCr-HT and CuCr<sub>2</sub>O<sub>4</sub>, to stabilize the Au NPs and studied their catalytic efficiencies (entries 4-10). Of the various supports employed, the Au NP supported on Al<sub>2</sub>O<sub>3</sub> (Au NP/Al<sub>2</sub>O<sub>3</sub>) has showed better catalytic performance (TON 215) (entry 4). Notably, Au NP/Al<sub>2</sub>O<sub>3</sub> exhibited a twofold higher catalytic efficiency than the titania-supported Au NP (Au NP/TiO<sub>2</sub>) (entries 4 and 5). This superior performance of Au NP/Al<sub>2</sub>O<sub>3</sub> is believed to be the synergetic effect of Au NPs and Al<sub>2</sub>O<sub>3</sub> support. The temperature dependent TOF values and the kinetic modeling results revealed that the Au NP/Al<sub>2</sub>O<sub>3</sub> has a near-zero apparent activation energy (1.2 kcal mol<sup>-1</sup>). Based on the spectroscopic data and previous studies, they proposed a plausible mechanism in which the Au-H species, formed from the heterolytic dissociation of H<sub>2</sub>, react with the surface bicarbonate species and form Au-formate intermediate. This surface formate species would migrate to the more stable alumina surface and subsequently formates are released from the catalytic cycle.

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Previously, Stalder *et al.* studied the catalytic efficiency of a formate under ca. 0.1 MPa  $H_2$  pressure.<sup>49</sup> Three types of series of supported Pd species for the conversion of NaHCO<sub>3</sub> to

Table 1. Comparison of catalytic systems for the hydrogenation of	CO <sub>2</sub> to formic acid/formate
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En	Catalyst	Temperat	p(H <sub>2</sub> )/p(CO <sub>2</sub> )	Solvent	Additive/ base	Time	TON/Final formate	TOF	Re
tr		ure (°C)	(MPa)			(h)	concentration (M)	(h⁻¹)	f
у 1	Ra-Ni	100	4-14/6	EtOH/ Phenol	2,2,6,6-Tetra- Me-4-OH piperidine	6	-/0.31	<1	48
2	Pd black	25	0.1/0	H <sub>2</sub> O	NaHCO <sub>3</sub>	53	2.1/0.19	<1	49
3	AUROlite	40	9/9	NEt <sub>3</sub>	NEt <sub>3</sub>	52	855	16.4	51
4	Au NP/Al <sub>2</sub> O <sub>3</sub>	70	20/20	EtOH	NEt <sub>3</sub>	20	215/0.20	11	53
5	Au NP/TiO <sub>2</sub>	70	20/20	EtOH	NEt <sub>3</sub>	20	111/0.09	5.5	54
6	Au NP/ZnO	70	20/20	EtOH	NEt <sub>3</sub>	20	2/<0.01	<1	54
7	Au NP/CeO <sub>2</sub>	70	20/20	EtOH	NEt <sub>3</sub>	20	8/<0.01	<1	54
8	Au NP/MgAl- HT	70	20/20	EtOH	$NEt_3$	20	91/0.01	4.5	54
9	Au NP/MgCr- HT	70	20/20	EtOH	NEt <sub>3</sub>	20	52/<0.01	2.6	54
10	Au NP/CuCr <sub>2</sub> O <sub>4</sub>	70	20/20	EtOH	NEt <sub>3</sub>	20	6/<0.01	<1	54
11	$Pd/BaSO_4$	25	0.1/0	H <sub>2</sub> O	NaHCO <sub>3</sub>	50	19/0.09	<1	49
12	$Pd/\gamma - Al_2O_3$	25	0.1/0	H <sub>2</sub> O	NaHCO <sub>3</sub>	53	50/0.23	<1	49
13	Pd/C	25	0.17/0	H <sub>2</sub> O	NaHCO <sub>3</sub>	46	115/0.54	2.5	49
14	Pd/AC	20	2.75/0	H <sub>2</sub> O	NaHCO <sub>3</sub>	1	527/0.28	527	55
15	Pd/AC	20	2.75/0	H <sub>2</sub> O	KHCO₃	1	567/0.30	567	55
16	Pd/AC	20	2.75/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	1	782/0.42	782	55
17	Pd/AC	20	2.75/0	H <sub>2</sub> O	Na <sub>2</sub> CO <sub>3</sub>	1	<1/<0.01	<1	55
18	Pd/AC	20	2.75/0	H <sub>2</sub> O	K <sub>2</sub> CO <sub>3</sub>	1	<1/<0.01	<1	55
19	Pd/AC	20	2.75/0	H <sub>2</sub> O	(NH <sub>4</sub> ) <sub>2</sub> CO <sub>3</sub>	1	278/0.15	278	55
20	Pd/AC	20	2.75/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	15	1769/0.95	118	55
21	Pd/AC	20	5.52/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	2	1672/0.90	836	55
22	$Pd/Al_2O_3$	20	2.75/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	1	278/0.08	278	55
23	$Pd/CaCo_3$	20	2.75/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	1	20/<0.01	20	55
24	Pd/BaSO <sub>4</sub>	20	2.75/0	H <sub>2</sub> O	NH <sub>4</sub> HCO <sub>3</sub>	1	212/0.02	212	55
25	Pd/AC	20	2.75/0	EtOH/ H <sub>2</sub> O (7/3)	$NH_2CO_2NH_4$	8	845/0.91	105	56
26	Pd/r-GO (1 wt%)	100	4/0	H <sub>2</sub> O	KHCO <sub>3</sub>	32	7088/4.53	221	57
27	Pd/r-GO (2 wt%)	100	4/0	H <sub>2</sub> O	KHCO <sub>3</sub>	10	2117/4.06	211	57
28	Pd/r-GO (5 wt%)	100	4/0	H <sub>2</sub> O	KHCO <sub>3</sub>	10	1658/3.18	165	57
29	PdNi/CNT-GR	40	25/25	H <sub>2</sub> O	nil	15	6.4/0.02	<1	58
30	Ru/MgO	80	5/8.5	EtOH	NEt <sub>3</sub>	1	0	-	58
31	Ru/AC	80	5/8.5	EtOH	NEt <sub>3</sub>	1	10/0.05	10	58
32	$Ru/\gamma-AI_2O_3$	80	5/8.5	EtOH	NEt <sub>3</sub>	1	91/0.455	91	58

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33         Ru/y-ALO <sub>2</sub> (n))         80         5/8.5         ELOH         NEL <sub>5</sub> 1         731/0.68         721         60           34         3         80         5/4/9.3         ELOH         PPhy/NEL <sub>5</sub> 1         1022/0.40         1022         62           35         4         80         4/12         ELOH         PPhy/NEL <sub>5</sub> 1         656/0.52         65         63           36         5         80         5.4/9.3         ELOH         PPhy/NEL <sub>5</sub> 1         723/0.28         723         66           39         8         80         4/12         ELOH         PPhy/NEL <sub>5</sub> 1         858/0.59         68         63           41         10         80         5/8         ELOH         PPhy/NEL <sub>5</sub> 1         868/0.59         68         63           42         11         80         5/8         ELOH         PPhy/NEL <sub>5</sub> 1         143/0.34         141         60           43         80         5/8         ELOH         ASPhy/NEL <sub>5</sub> 1         110/0.65         70           54         13         80         5/8         ELOH         ASPhy/NEL <sub>5</sub> 1 <th1< th=""><th>En tr</th><th>Catalyst</th><th>Temperat ure (°C)</th><th>p(H<sub>2</sub>)/p(CO<sub>2</sub>) (MPa)</th><th>Solvent</th><th>Additive/ base</th><th>Time (h)</th><th>TON/Final formate concentration (M)</th><th>TOF (h⁻¹)</th><th>Re f</th><th></th></th1<>	En tr	Catalyst	Temperat ure (°C)	p(H <sub>2</sub> )/p(CO <sub>2</sub> ) (MPa)	Solvent	Additive/ base	Time (h)	TON/Final formate concentration (M)	TOF (h⁻¹)	Re f	
35         4         80         4/12         EtOH         PPh/NEt         1         656/0.52         656         63           36         5         80         5/8         EtOH         PPh/NEt         1         151/0.36         151         65           37         6         80         5/4/9.3         EtOH         PPh/NEt         1         723/0.28         723         66           38         7         80         5/4/9.3         EtOH         PPh/NEt         1         537/0.11         537         66           39         8         80         4/12         EtOH         PPh/NEt         1         886/0.69         88         63           41         10         80         5/8         EtOH         PPh/NEt         1         143/0.34         143         65           43         5         80         5/8         EtOH         App/NEt         1         171/0.66         29         65           44         5         80         5/4/9.3         EtOH         Asph/NEt         1         171/0.06         70           53         80         5/4/9.3         EtOH         Asph/NEt         1         171/0.06         70 <td><u>у</u> 33</td> <td><math>Ru/\gamma-Al_2O_3(n))</math></td> <td>80</td> <td>5/8.5</td> <td>EtOH</td> <td>NEt<sub>3</sub></td> <td>1</td> <td>731/0.68</td> <td>731</td> <td>60</td> <td></td>	<u>у</u> 33	$Ru/\gamma-Al_2O_3(n))$	80	5/8.5	EtOH	NEt <sub>3</sub>	1	731/0.68	731	60	
36         5         80         5/8         EtOH         PPh/NEts         1         151/0.36         151         65           37         6         80         5.4/9.3         EtOH         PPhy/NEts         1         723/0.28         723         66           39         8         80         4/12         EtOH         PPhy/NEts         1         138/1.10         138/4         63           40         9         80         4/12         EtOH         PPhy/NEts         1         138/1.10         138/4         63           40         9         80         4/12         EtOH         PPhy/NEts         1         138/1.10         138         65           41         10         80         5/8         EtOH         PPhy/NEts         1         143/0.34         143         65           42         11         80         5/8         EtOH         APhy/NEts         1         191/0.45         191         66           44         5         80         5.4/9.3         EtOH         APhy/NEts         1         171/0.06         70           51         16         60         2/2         H <sub>2</sub> O         NEts         2         100/0.13 <td>34</td> <td>3</td> <td>80</td> <td>5.4/9.3</td> <td>EtOH</td> <td>PPh<sub>3</sub>/NEt<sub>3</sub></td> <td>1</td> <td>1022/0.40</td> <td>1022</td> <td>62</td> <td>,</td>	34	3	80	5.4/9.3	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	1022/0.40	1022	62	,
37         6         80         5.4/9.3         EtOH         PPhy/NEt3         1         723/0.28         723         66           38         7         80         5.4/9.3         EtOH         PPhs/NEt3         1         537/0.21         537         66           39         8         80         4/12         EtOH         PPhs/NEt3         1         1384/1.10         1384         63           40         9         80         4/12         EtOH         PPhy/NEt3         1         1384/1.10         1384         63           41         10         80         5/8         EtOH         PPhy/NEt3         1         13/0.45         191         65           42         11         80         5/8         EtOH         ApPh/NEt3         1         12/0.06         29         65           44         5         80         5/8         EtOH         APPhy/NEt3         1         17/0.06         171         66           44         5         80         5/8         EtOH         APPhy/NEt3         1         17/0.06         171         66           47         12         60         2/2         H20         NEt3         2	35	4	80	4/12	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	656/0.52	656	63	
38780 $5.4/9.3$ EtOH $PPh_y/NEt_3$ 1 $537/0.21$ $537$ 6639880 $4/12$ EtOH $PPh_y/NEt_3$ 1 $1384/1.10$ $1384$ $63$ 40980 $4/12$ EtOH $PPh_y/NEt_3$ 1 $1384/1.10$ $1384$ $63$ 411080 $5/8$ EtOH $PPh_y/NEt_3$ 1 $15/0.18$ $75$ $65$ 421180 $5/8$ EtOH $PPh_y/NEt_3$ 1 $191/0.45$ $65$ 43580 $5/8$ EtOH $ApPh_y/NEt_3$ 1 $191/0.45$ $65$ 44580 $5/8$ EtOH $ApPh_y/NEt_3$ 1 $171/0.06$ $71$ $66$ 45380 $5.4/9.3$ EtOH $ApPh_y/NEt_3$ 1 $171/0.06$ $71$ $66$ 46380 $5.4/9.3$ EtOH $AsPh_y/NEt_3$ 1 $171/0.06$ $71$ $66$ 4712 $60$ $2/2$ $H_50$ $NEt_3$ 2 $1300/0.13$ $620$ $70$ 4813 $60$ $2/2$ $H_50$ $NEt_3$ 2 $1300/0.13$ $620$ $70$ 5015 $60$ $2/2$ $H_50$ $NEt_3$ 1 $0$ $0$ $70$ 5116 $02/2$ $H_50$ $NEt_3$ 1 $100/0.11$ $100$ $70$ 5312 $60$ $2/2$ $H_50$ $NEt_3$ 1 $130/0.13$ $80$ $70$ 5412 <td< td=""><td>36</td><td>5</td><td>80</td><td>5/8</td><td>EtOH</td><td>PPh<sub>3</sub>/NEt<sub>3</sub></td><td>1</td><td>151/0.36</td><td>151</td><td>65</td><td></td></td<>	36	5	80	5/8	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	151/0.36	151	65	
39         8         80         4/12         EtOH         PPhy/NEt,         1         1384/1.10         1384         63           40         9         80         4/12         EtOH         PPhy/NEt,         1         868/0.59         868         63           41         10         80         5/8         EtOH         PPhy/NEt,         1         143/0.34         143         65           42         11         80         5/8         EtOH         Appe/NEt,         1         143/0.34         143         65           43         5         80         5/8         EtOH         Appe/NEt,         1         171/0.06         171         66           44         5         80         5.4/9.3         EtOH         APph/NEt,         1         171/0.06         171         66           45         3         80         5.4/9.3         EtOH         APph/NEt,         1         171/0.06         70           46         3         60         2/2         H <sub>2</sub> O         NEt,         2         100/0.01         55         70           47         12         60         2/2         H <sub>2</sub> O         NEt,         2         200/0.02	37	6	80	5.4/9.3	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	723/0.28	723	66	
$40$ 9 $80$ $4/12$ EtOHPPh/NEt, PPh/NEt, I1 $868/0.69$ $868$ $63$ $41$ 10 $80$ $5/8$ EtOHPPh/NEt, I1 $75/0.18$ $75$ $65$ $42$ 11 $80$ $5/8$ EtOH $PPh/NEt_3$ 1 $143/0.34$ $143$ $65$ $43$ 5 $80$ $5/8$ EtOH $dppe/NEt_3$ 1 $191/0.45$ $191$ $65$ $44$ 5 $80$ $5/8$ EtOH $ASPh_3/NEt_3$ 1 $179/0.07$ $179$ $66$ $45$ 3 $80$ $5.4/9.3$ EtOH $NPh_3/NEt_3$ 1 $171/0.06$ $70$ $46$ 3 $80$ $5.4/9.3$ EtOH $ASPh_3/NEt_3$ 1 $170/0.01$ $55$ $70$ $47$ 12 $60$ $2/2$ $H_20$ $NEt_3$ 2 $110/0.01$ $55$ $70$ $48$ 13 $60$ $2/2$ $H_20$ $NEt_3$ 1 $0$ $0$ $70$ $50$ 15 $60$ $2/2$ $H_20$ $NEt_3$ 1 $80/0.08$ $880$ $70$ $51$ 16 $60$ $2/2$ $H_20$ $NEt_3$ 1 $80/0.08$ $880$ $70$ $52$ 12 $60$ $2/2$ $H_20$ $NEt_3$ 1 $80/0.08$ $880$ $70$ $53$ 12 $90$ $2/2$ $H_20$ $NEt_3$ 1 $100/0.11$ $1100$ $70$ $54$ 12 $120$ $2/2$ $H_20$ $NEt_3$ 1 $38/0.04$	38	7	80	5.4/9.3	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	537/0.21	537	66	
41       10       80 $5/8$ EtOH       PPhy/NEt3       1 $75/0.18$ $75$ $65$ 42       11       80 $5/8$ EtOH       PPhy/NEt3       1 $143/0.34$ $143$ $65$ 43       5       80 $5/8$ EtOH $Asph_y/NEt_3$ 1 $29/0.06$ $29$ $65$ 44       5       80 $5/8$ EtOH $Asph_y/NEt_3$ 1 $29/0.06$ $29$ $65$ 45       3       80 $5/49.3$ EtOH $Asph_y/NEt_3$ 1 $17/0.06$ $171$ $66$ 46       3       80 $5/49.3$ EtOH $Asph_y/NEt_3$ 1 $171/0.06$ $171$ $66$ 47       12 $60$ $2/2$ $H_yO$ $NEt_3$ 2 $100/0.11$ $57$ $67$ 48       13 $60$ $2/2$ $H_yO$ $NEt_3$ 1 $80/0.08$ $880$ $70$ 51       16 $60$ $2/2$ $H_yO$ $NEt_3$ 1 $80/0.04$ $20$ $70$	39	8	80	4/12	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	1384/1.10	1384	63	
42       11       80       5/8       EtOH       PPhy/NEt,       1       143/0.34       143       65         43       5       80       5/8       EtOH       dppe/NEt3       1       191/0.45       191       65         44       5       80       5/8       EtOH       AsPh3/NEt3       1       29/0.66       29       65         45       3       80       5/4/9.3       EtOH       AsPh3/NEt3       1       171/0.06       171       66         46       3       80       5/4/9.3       EtOH       AsPh3/NEt3       1       171/0.06       171       66         47       12       60       2/2       H30       NEt3       2       1300/0.13       620       70         48       13       60       2/2       H30       NEt3       2       100/0.01       50       70         50       15       60       2/2       H30       NEt3       1       100/0.01       100       70         51       16       60       2/2       H30       NEt3       1       100/0.01       100       70         52       12       60       2/2       H30       NEt3 <td>40</td> <td>9</td> <td>80</td> <td>4/12</td> <td>EtOH</td> <td>PPh<sub>3</sub>/NEt<sub>3</sub></td> <td>1</td> <td>868/0.69</td> <td>868</td> <td>63</td> <td></td>	40	9	80	4/12	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	868/0.69	868	63	
$43$ 580 $5/8$ EtOH $dppe/NE_5$ 1 $191/0.45$ $191$ $65$ $44$ 580 $5/8$ EtOH $AsPh_3/NEt_3$ 1 $29/0.06$ $29$ $65$ $45$ 380 $5.4/9.3$ EtOH $NPh_3/NEt_3$ 1 $179/0.07$ $179$ $66$ $46$ 380 $5.4/9.3$ EtOH $AsPh_3/NEt_3$ 1 $171/0.06$ $171$ $66$ $47$ 12 $60$ $2/2$ $H_20$ $NEt_3$ 2 $1300/0.13$ $620$ $70$ $48$ 13 $60$ $2/2$ $H_20$ $NEt_3$ 2 $400/0.04$ $200$ $70$ $49$ 14 $60$ $2/2$ $H_20$ $NEt_3$ 1 $0$ $0$ $70$ $50$ 15 $60$ $2/2$ $H_20$ $NEt_3$ 1 $800/0.08$ $880$ $70$ $51$ 16 $60$ $2/2$ $H_20$ $NEt_3$ 1 $800/0.08$ $880$ $70$ $52$ 12 $60$ $2/2$ $H_20$ $NEt_3$ 1 $1100/0.11$ $1100$ $70$ $54$ 12 $120$ $2/2$ $H_20$ $NEt_3$ 1 $1100/0.11$ $1100$ $70$ $55$ 12 $60$ $2/2$ $H_20$ $NEt_3$ 1 $1100/0.11$ $1100$ $70$ $56$ 17 $120$ $2/2$ $H_20$ $NEt_3$ 1 $38/0.01$ $38$ $71$ $57$ 18 $120$ $2/2$ $H_20$ $NEt_3$ 1 $132/0.02$ <t< td=""><td>41</td><td>10</td><td>80</td><td>5/8</td><td>EtOH</td><td>PPh<sub>3</sub>/NEt<sub>3</sub></td><td>1</td><td>75/0.18</td><td>75</td><td>65</td><td></td></t<>	41	10	80	5/8	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	75/0.18	75	65	
44       5       80       5/8       EtOH       AsPh <sub>3</sub> /NEt <sub>3</sub> 1       29/0.06       29       65         45       3       80       5.4/9.3       EtOH       NPh <sub>3</sub> /NEt <sub>3</sub> 1       179/0.07       179       66         46       3       80       5.4/9.3       EtOH       AsPh <sub>3</sub> /NEt <sub>3</sub> 1       171/0.06       171       66         47       12       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       1300/0.13       620       70         48       13       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       100/0.01       55       70         49       14       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       400/0.04       200       70         50       15       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       0       0       70         51       16       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       1100/0.11       30       70         52       12       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       130/0.23       10       70         54       12       120       2/2       H <sub>2</sub> O	42	11	80	5/8	EtOH	PPh <sub>3</sub> /NEt <sub>3</sub>	1	143/0.34	143	65	
$45$ $3$ $80$ $5.4/9.3$ $EtOH$ $NPh_3/NEt_3$ $1$ $179/0.07$ $179$ $66$ $46$ $3$ $80$ $5.4/9.3$ $EtOH$ $AsPh_3/NEt_3$ $1$ $171/0.06$ $171$ $66$ $47$ $12$ $60$ $2/2$ $H_1O$ $NEt_3$ $2$ $1300/0.13$ $620$ $70$ $48$ $13$ $60$ $2/2$ $H_1O$ $NEt_3$ $2$ $100/0.01$ $55$ $70$ $49$ $14$ $60$ $2/2$ $H_2O$ $NEt_3$ $2$ $400/0.04$ $200$ $70$ $50$ $15$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $0$ $0$ $70$ $51$ $16$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $880/0.88$ $880$ $70$ $52$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $53$ $12$ $90$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $54$ $12$ $90$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $55$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $55$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $20$ $2300/0.27$ $140$ $70$ $56$ $17$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $132/0.2$ $132$ $71$ $57$ $18$ $120$ $2/2$ <	43	5	80	5/8	EtOH	dppe/NEt <sub>3</sub>	1	191/0.45	191	65	
$46$ $3$ $80$ $5.4/9.3$ $EtOH$ $AsPh_3/NEt_3$ $1$ $171/0.06$ $171$ $66$ $47$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $2$ $1300/0.13$ $620$ $70$ $48$ $13$ $60$ $2/2$ $H_5O$ $NEt_3$ $2$ $110/0.01$ $55$ $70$ $49$ $14$ $60$ $2/2$ $H_5O$ $NEt_3$ $2$ $400/0.04$ $200$ $70$ $50$ $15$ $60$ $2/2$ $H_5O$ $NEt_3$ $1$ $0$ $0$ $70$ $51$ $16$ $60$ $2/2$ $H_5O$ $NEt_3$ $1$ $0$ $0$ $70$ $52$ $12$ $60$ $2/2$ $H_5O$ $NEt_3$ $1$ $880/0.08$ $880$ $70$ $53$ $12$ $90$ $2/2$ $H_5O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $54$ $12$ $120$ $2/2$ $H_5O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $55$ $12$ $60$ $2/2$ $H_5O$ $NEt_3$ $1$ $130/0.2$ $120$ $70$ $56$ $17$ $120$ $2/2$ $H_5O$ $NEt_3$ $1$ $132/0.02$ $132$ $71$ $57$ $18$ $120$ $2/2$ $H_5O$ $NEt_3$ $1$ $132/0.02$ $132$ $71$ $57$ $18$ $120$ $2/2$ $H_5O$ $NEt_3$ $1$ $132/0.02$ $132$ $71$ $57$ $18$ $120$ $2/2$ $H_5O$ <t< td=""><td>44</td><td>5</td><td>80</td><td>5/8</td><td>EtOH</td><td>AsPh<sub>3</sub>/NEt<sub>3</sub></td><td>1</td><td>29/0.06</td><td>29</td><td>65</td><td></td></t<>	44	5	80	5/8	EtOH	AsPh <sub>3</sub> /NEt <sub>3</sub>	1	29/0.06	29	65	
471260 $2/2$ $H_2O$ NEt_321300/0.1362070481360 $2/2$ $H_2O$ NEt_32110/0.015570491460 $2/2$ $H_2O$ NEt_32400/0.0420070501560 $2/2$ $H_2O$ NEt_310070511660 $2/2$ $H_2O$ NEt_31880/0.013570521260 $2/2$ $H_2O$ NEt_311100/0.111100705412120 $2/2$ $H_2O$ NEt_322300/0.23120070551260 $2/2$ $H_2O$ NEt_3202700/0.27140705617120 $2/2$ $H_2O$ NEt_3138/<0.01	45	3	80	5.4/9.3	EtOH	NPh <sub>3</sub> /NEt <sub>3</sub>	1	179/0.07	179	66	
48       13       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       110/0.01       55       70         49       14       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       400/0.04       200       70         50       15       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       0       0       70         51       16       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       880/0.88       880       70         52       12       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       1100/0.11       1100       70         53       12       90       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       2300/0.23       1200       70         54       12       120       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       100/0.11       100       70         55       12       60       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       248/0.04       248       71         56       17       120       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 1       132/0.02       132       71         57       18       120       2/2       H <sub>2</sub> O       NEt <sub>3</sub> <	46	3	80	5.4/9.3	EtOH	AsPh <sub>3</sub> /NEt <sub>3</sub>	1	171/0.06	171	66	
$49$ 1460 $2/2$ $H_2O$ Net $L_2O$ 2 $400/0.04$ 20070501560 $2/2$ $H_2O$ NEt_310070511660 $2/2$ $H_2O$ NEt_32 $70/<0.01$ 3570521260 $2/2$ $H_2O$ NEt_31880/0.0888070531290 $2/2$ $H_2O$ NEt_311100/0.111100705412120 $2/2$ $H_2O$ NEt_322300/0.23120070551260 $2/2$ $H_2O$ NEt_3202700/0.27140705617120 $2/2$ $H_2O$ NEt_31248/0.04248715718120 $2/2$ $H_2O$ NEt_3138/<0.01	47	12	60	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	2	1300/0.13	620	70	
$50$ $15$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $0$ $0$ $70$ $51$ $16$ $60$ $2/2$ $H_2O$ $NEt_3$ $2$ $70/<0.01$ $35$ $70$ $52$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $880/0.08$ $880$ $70$ $53$ $12$ $90$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $54$ $12$ $120$ $2/2$ $H_2O$ $NEt_3$ $2$ $2300/0.23$ $1200$ $70$ $55$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $248/0.04$ $248$ $70$ $56$ $17$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/<0.01$ $38$ $71$ $57$ $18$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/<0.01$ $38$ $71$ $58$ $19$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/<0.01$ $38$ $71$ $59$ $20$ $40$ $6/6$ $NEt_3$ $PEt_3$ $1$ $132/0.02$ $132$ $71$ $59$ $20$ $60$ $6/6$ $NEt_3$ $PPh_3$ $24$ $255$ $1$ $79$ $61$ $21$ $150$ $2.7/1.3$ $D_2O$ $NEt_3$ $24$ $205/0.34$ $3.9$ $80$ $64$ $21$ $150$ $3.5/0.5$ $D_2O$ $NEt_3$ $24$ $79/0.27$ $3.2$ $80$ $64$ $21$ $150$ $3.5/0.5$ $D_2O$	48	13	60	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	2	110/0.01	55	70	
$51$ $16$ $60$ $2/2$ $H_2O$ $NEt_3$ $2$ $70/c0.01$ $35$ $70$ $52$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $880/0.08$ $880$ $70$ $53$ $12$ $90$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $54$ $12$ $120$ $2/2$ $H_2O$ $NEt_3$ $2$ $2300/0.23$ $1200$ $70$ $55$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $20$ $2700/0.27$ $140$ $70$ $56$ $17$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/c0.01$ $38$ $71$ $57$ $18$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/c0.01$ $38$ $71$ $58$ $19$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/c0.01$ $38$ $71$ $59$ $20$ $400$ $6/6$ $NEt_3$ $NEt_3$ $1$ $132/0.02$ $132$ $71$ $59$ $20$ $400$ $6/6$ $NEt_3$ $PPh_3$ $24$ $255$ $1$ $79$ $61$ $21$ $150$ $2.7/1.3$ $D_2O$ $NEt_3$ $24$ $2054$ $94$ $79$ $61$ $21$ $150$ $3.5/0.5$ $D_2O$ $NEt_3$ $24$ $79/0.34$ $3.9$ $80$ $64$ $21$ $150$ $3.5/0.5$ $D_2O$ $NEt_3$ $24$ $79/0.34$ $3.9$ $80$ $64$ $23$ $120$ $2/2$ <	49	14	60	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	2	400/0.04	200	70	
$52$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $1$ $880/0.08$ $880$ $70$ $53$ $12$ $90$ $2/2$ $H_2O$ $NEt_3$ $1$ $1100/0.11$ $1100$ $70$ $54$ $12$ $120$ $2/2$ $H_2O$ $NEt_3$ $2$ $2300/0.23$ $1200$ $70$ $55$ $12$ $60$ $2/2$ $H_2O$ $NEt_3$ $20$ $2700/0.27$ $140$ $70$ $56$ $17$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $248/0.04$ $248$ $71$ $57$ $18$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/<0.01$ $38$ $71$ $58$ $19$ $120$ $2/2$ $H_2O$ $NEt_3$ $1$ $38/<0.01$ $38$ $71$ $59$ $20$ $40$ $6/6$ $NEt_3$ $PE_3$ $1$ $132/0.02$ $132$ $71$ $60$ $20$ $60$ $6/6$ $NEt_3$ $PE_3$ $24$ $255$ $1$ $79$ $61$ $21$ $150$ $2.7/1.3$ $D_2O$ $NEt_3$ $24$ $81/0.28$ $3.3$ $80$ $62$ $21$ $150$ $3.71$ $D_2O$ $NEt_3$ $24$ $95/0.34$ $3.9$ $80$ $64$ $21$ $150$ $3.5/0.5$ $D_2O$ $NEt_3$ $24$ $50/0.06$ $250$ $81$ $66$ $23$ $120$ $2/2$ $H_2O$ $NEt_3$ $2$ $500/0.66$ $250$ $81$ $66$ $23$ $120$ $2/2$ <	50	15	60	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	1	0	0	70	
531290 $2/2$ $H_2O$ NEt_311100/0.111100705412120 $2/2$ $H_2O$ NEt_322300/0.23120070551260 $2/2$ $H_2O$ NEt_3202700/0.27140705617120 $2/2$ $H_2O$ NEt_31248/0.04248715718120 $2/2$ $H_2O$ NEt_3138/<0.01	51	16	60	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	2	70/<0.01	35	70	
54         12         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 2         2300/0.23         1200         70           55         12         60         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 20         2700/0.27         140         70           56         17         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         248/0.04         248         71           57         18         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         38/<0.01	52	12	60	2/2	H₂O	NEt <sub>3</sub>	1	880/0.08	880	70	
55         12         60         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 20         2700/0.27         140         70           56         17         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         248/0.04         248         71           57         18         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         38/<0.01	53	12	90	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	1	1100/0.11	1100	70	
56         17         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         248/0.04         248         71           57         18         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         38/<0.01	54	12	120	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	2	2300/0.23	1200	70	
57       18       120       2/2       H2O       NEt3       1       38/<0.01	55	12	60			NEt <sub>3</sub>	20	2700/0.27	140	70	
58         19         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 1         132/0.02         132         71           59         20         40         6/6         NEt <sub>3</sub> NEt <sub>3</sub> 24         25         1         79           60         20         60         6/6         NEt <sub>3</sub> PPh <sub>3</sub> 24         2254         94         79           61         21         150         2/2         D <sub>2</sub> O         NEt <sub>3</sub> 24         81/0.28         3.3         80           62         21         150         2.7/1.3         D <sub>2</sub> O         NEt <sub>3</sub> 24         95/0.34         3.9         80           63         21         150         3.71         D <sub>2</sub> O         NEt <sub>3</sub> 24         95/0.34         3.9         80           64         21         150         3.5/0.5         D <sub>2</sub> O         NEt <sub>3</sub> 24         95/0.34         3.9         80           65         23         80         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 2         500/0.06         250         81           66         23         120         2/2         H <sub>2</sub> O         NEt <sub>3</sub> 2         2700/0	56	17	120	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	1	248/0.04	248	71	
59       20       40       6/6       NEt <sub>3</sub> NEt <sub>3</sub> 24       25       1       79         60       20       60       6/6       NEt <sub>3</sub> PPh <sub>3</sub> 24       2254       94       79         61       21       150       2/2       D <sub>2</sub> O       NEt <sub>3</sub> 24       81/0.28       3.3       80         62       21       150       2.7/1.3       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         63       21       150       3.1       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         64       21       150       3.5/0.5       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         65       23       80       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         66       23       120       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       160       81         67       23       160       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       500/0.61       166       81         68       23       200       2/2       H <sub>2</sub> O <t< td=""><td>57</td><td>18</td><td>120</td><td>2/2</td><td>H<sub>2</sub>O</td><td>NEt<sub>3</sub></td><td>1</td><td>38/&lt;0.01</td><td>38</td><td>71</td><td></td></t<>	57	18	120	2/2	H <sub>2</sub> O	NEt <sub>3</sub>	1	38/<0.01	38	71	
59       20       40       6/6       NEt <sub>3</sub> NEt <sub>3</sub> 24       25       1       79         60       20       60       6/6       NEt <sub>3</sub> PPh <sub>3</sub> 24       2254       94       79         61       21       150       2/2       D <sub>2</sub> O       NEt <sub>3</sub> 24       81/0.28       3.3       80         62       21       150       2.7/1.3       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         63       21       150       3.1       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         64       21       150       3.1       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         65       23       80       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         66       23       150       3.5/0.5       D <sub>2</sub> O       NEt <sub>3</sub> 24       95/0.34       3.9       80         67       23       80       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       500/0.06       250       81         67       23       160       2/2       H <sub>2</sub> O <td< td=""><td></td><td></td><td>120</td><td></td><td></td><td></td><td></td><td></td><td></td><td>71</td><td></td></td<>			120							71	
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63       21       150       3/1       D2O       NEt3       24       95/0.34       3.9       80         64       21       150       3.5/0.5       D2O       NEt3       24       77/0.27       3.2       80         65       23       80       2/2       H2O       NEt3       2       500/0.06       250       81         66       23       120       2/2       H2O       NEt3       2       3320/0.40       1660       81         67       23       160       2/2       H2O       NEt3       2       2700/0.33       1350       81         68       23       200       2/2       H2O       NEt3       2       1320/0.16       660       81         69       23       120       4/4       H2O       NEt3       2       5000/0.61       2500       81			150							80	
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68       23       200       2/2       H <sub>2</sub> O       NEt <sub>3</sub> 2       1320/0.16       660       81         69       23       120       4/4       H <sub>2</sub> O       NEt <sub>3</sub> 2       5000/0.61       2500       81										81	
69 <b>23</b> 120 4/4 H <sub>2</sub> O NEt <sub>3</sub> 2 5000/0.61 2500 81										81	
/0 <b>23</b> 120 $4/4$ H <sub>2</sub> O NEt <sub>2</sub> 0.25 1300/0.15 5300 81	70	23	120	4/4	H <sub>2</sub> O	NEt <sub>3</sub>	0.25	1300/0.15	5300	81	

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En tr y	Catalyst	Temperat ure (°C)	p(H <sub>2</sub> )/p(CO <sub>2</sub> ) (MPa)	Solvent	Additive/ base	Time (h)	TON/Final formate concentration (M)	TOF (h⁻¹)	Re f
71	25	120	4/4	H <sub>2</sub> O	NEt <sub>3</sub>	0.5	750/0.01	1500	82
72	25	120	4/4	H <sub>2</sub> O	NEt <sub>3</sub>	10	6400/0.14	640	82

supports, namely BaSO<sub>4</sub>,  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and carbon were employed, and all the supported Pd catalysts (Pd/BaSO<sub>4</sub>, Pd/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> and Pd/C) showed better activity than unsupported Pd black under similar reaction conditions, again revealing the importance of catalyst supports (entries 2, 11-13). Among the supported catalysts, Pd/C showed the maximum TON (115) at 25 °C (entries 11-13). Additionally, Ni, Ru, Rh and Pt metals supported on  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> also catalyzed the reaction, but to a lesser extent than Pd.

Recently, Su *et al.* employed a porous carbon material (activated carbon) as a support (Pd/AC) and systematically studied the conversion of various bicarbonate salts to formates under relatively high  $H_2$  pressures (0.69-5.52 MPa).<sup>55</sup> The Pd/AC showed a higher TOF (527 h<sup>-1</sup>) than the Pd/C (TOF 2.5 h<sup>-1</sup>), indicating the benefit of porous catalyst

supports for the reaction (entries 13 and 14). In addition, various carbonates (Na<sub>2</sub>CO<sub>3</sub>, K<sub>2</sub>CO<sub>3</sub> and (NH<sub>4</sub>)<sub>2</sub>CO<sub>3</sub>) and bicarbonates (NaHCO<sub>3</sub>, KHCO<sub>3</sub> and NH<sub>4</sub>HCO<sub>3</sub>) were screened and it was found that the hydrogenation of carbonate salts was much more difficult than the bicarbonate salts (entries 14-19). This is because the protonation of carbonate ions was the rate limiting step at this temperature. Of the bicarbonate salts screened, NH<sub>4</sub>HCO<sub>3</sub> gave higher yield (42.4 %, TON 782) than NaHCO<sub>3</sub> (28.6 %, TON 527) and KHCO<sub>3</sub> (30.8 %, TON 567) (entries 14-16). The high yield of formate from NH<sub>4</sub>HCO<sub>3</sub> salt was thought to be caused by higher equilibrium concentration of HCO<sub>3</sub><sup>-</sup> ions (0.92 M) over CO<sub>3</sub><sup>2-</sup> ions than that of KHCO<sub>3</sub> (0.89 M) or NaHCO<sub>3</sub> salts (0.61 M).

However, the yield of formate was decreased at higher temperatures because Pd/AC promoted the decomposition of



Chart 1. Representative structures of catalysts 1-11

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ammonium formate back into CO<sub>2</sub>, H<sub>2</sub> and NH<sub>3</sub> to a large extent at higher temperatures. Therefore, maximum activity was obtained at high H<sub>2</sub> pressure (5.52 MPa) and long reaction time (entries 20 and 21). In addition, various catalyst supports (BaSO<sub>4</sub>, CaCO<sub>3</sub> and  $\gamma$ -Al<sub>2</sub>O<sub>3</sub>) were also screened and it was found that Pd/AC exhibited better catalytic performance than the others (entries 16, 22-24). This was attributed to the hydrophobic nature of activated carbon, which results in the accumulation of  $H_2$  on the surface of the support. In addition to the above salts (NaHCO<sub>3</sub>, KHCO<sub>3</sub> and  $NH_4HCO_3$ ), ammonium carbamate salt ( $NH_2CO_2NH_4$ ) was also studied.<sup>56</sup> It was shown that the activities of these salts were depend on the solvents employed. For example, in pure H<sub>2</sub>O solution, NaHCO<sub>3</sub> (0.5 M) showed the maximum yield of 23 % but in pure EtOH solution, NH<sub>2</sub>CO<sub>2</sub>NH<sub>4</sub> (0.5 M) exhibited the maximum yield of 40 %. The yield of  $NH_2CO_2NH_4$  was improved to 44 % in EtOH-H<sub>2</sub>O mixture (7:3), and it was expected due to the formation of ethyl carbamate salt in the EtOH-H<sub>2</sub>O mixture. The Pd/AC showed the maximum TON of 845 using NH<sub>2</sub>CO<sub>2</sub>NH<sub>4</sub> salt at 20 °C under 2.75 MPa H<sub>2</sub> pressure (entry 25). Furthermore, the catalytic efficiency of Pd/AC was maintained over repeated recycling.

Yong Cao and co-workers evaluated the catalytic performance of Pd nanoparticles supported on reduced graphitic oxide nanosheets (Pd/r-GO).<sup>57</sup> They obtained the highest TON (7088) using 1 wt% Pd/r-GO after a long reaction period (32 h) at 100 °C under 4 MPa H<sub>2</sub> pressure (entry 26). However, the catalytic efficiency was gradually decreased while increasing the Pd loading (entries 26 and 28), and this was attributed to the large lattice strain of Pd nanoparticles in 1 wt% Pd/r-GO than in 2 and 5 wt% Pd/r-GO.

Very recently, Nguyen et al. studied the catalytic performance of PdNi alloy supported on Carbon Nanotube-Graphene (PdNi/CNT-GR) composite for the direct synthesis of formic acid by CO<sub>2</sub> hydrogenation (without any base).<sup>58</sup> To prevent the stacking of GR and the bundling of CNTs, which usually occurs themselves, CNT-GR composite has been utilized as a support to expose the entire surface areas of CNTs and GR for the catalysis. Interestingly, the bimetallic PdNi/CNT-GR (Pd<sub>3</sub>Ni<sub>7</sub>/CNT-GR; Pd-30 %, Ni-70 %) produced substantial amount of formic acid (1.92 mmol- TON 6.4) at 40 °C under 5 MPa total pressure (entry 29). However, a little amount of acetic acid generation was also observed. By comparing with the efficiency of mono-metallic Ni supported on CNT-GR (Ni/CNT-GR) and Pd supported on CNT-GR (Pd/CNT-GR), it was inferred that the synergic effect of Pd-Ni actually responsible for its catalytic activity.

Hao *et al.* hypothesized that the hydroxyl groups on the surface of a support may enhance the adsorption of CO<sub>2</sub> and the catalytic efficiency of a catalyst.<sup>59</sup> To test the hypothesis, ruthenium hydroxide was supported on three different supports; (1) MgO which do not have hydroxyl groups (Ru/MgO); (2) activated carbon which have a limited number of hydroxyl groups on the surface (Ru/AC); and (3)  $\gamma$ -alumina, which have abundant hydroxyl groups on the surface (Ru/AC); and roup roduce formate and Ru/AC showed little activity (TON 10), and Ru/ $\gamma$ -





Chart 2. Representative structures of catalysts 12-16

Al<sub>2</sub>O<sub>3</sub> showed higher catalytic activity (TON 91) (entries 30-32). Unlike Pd/AC and Pd/Al<sub>2</sub>O<sub>3</sub>, Ru/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> exhibited higher catalytic efficiency than Ru/AC. This might be due to the synergic effect of metal and support. Moreover, they observed that presence of RuO<sub>2</sub> on the surface of catalyst (formed during catalyst preparation) lowers the efficiency of the catalyst. Later, Liu *et al.* employed  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> nanorods ( $\gamma$ -Al<sub>2</sub>O<sub>3</sub>(n)) to support the ruthenium hydroxide species (Ru/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>(n)) owing to the high surface area, abundant hydroxyl groups, and its increased interaction with ruthenium species.<sup>60-61</sup> As expected, the catalytic efficiency of Ru/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub>(n) (TON 731) was higher than Ru/ $\gamma$ -Al<sub>2</sub>O<sub>3</sub> under similar reaction conditions (entries 32-33).

#### 3. Heterogenized Molecular Catalysts

metal catalysts Heterogeneous demonstrated the possibilities to the separation of catalysts from reaction mixtures and continuous use for repeated runs. However, the catalytic efficiencies of these catalysts were poor; for example, the maximum TOF obtained using these metalbased heterogeneous catalysts was 836 h<sup>-1</sup> (entry 21).<sup>55</sup> Since these catalysts are mainly made from precious metals (Ru, Pd, Au, etc.), achieving high catalytic efficiency is essential for their economical use. Conversely, homogeneous metal complexes have shown tremendous catalytic efficiencies (TONs up to 3,500,000,  $^{38}$  TOFs up to 1,100,000 h<sup>-1</sup>), $^{40}$  but are difficult to separate from reaction mixtures. Therefore, much research on the development of heterogeneous catalysts with high catalytic efficiencies has been undertaken. In this context, strategies involving the heterogenization of homogeneous metal complexes have been developed. These strategies seek to develop materials that combine the activity



Chart 3. Representative structures of catalysts 17-19

and selectivity of homogeneous metal catalysts with the advantages of heterogeneous catalysts, i.e., recyclability and easy seclusion from reaction mixtures. Such heterogenization processes, also called 'immobilization', have been performed to produce heterogenized catalysts for  $CO_2$  hydrogenation to formate.

#### 3.1 Grafted Molecular Catalysts

Krocher et al. was prepared silica tethered Ru complexes (1 and 2) through the covalent bond between the ligand and support for the synthesis of dimethylformamide from  $CO_2$ (Chart 1).<sup>62</sup> Later, Zheng and co-workers immobilized the Ru complexes on the surface of supports through the coordination bond between the donor ligand of the support and the metal ion (Chart 1, 3-11).63-67 They extensively studied the effect of various supports (silica, MCM-41 and polystyrene (PS)) and surface-bound donor ligands (amine (-NR<sub>2</sub>), nitrile (-CN) and thiol (-SH)) for the hydrogenation of CO<sub>2</sub> to formate. To study the effect of supports on reactivity, both inorganic and organic supports have been considered. For the inorganic supports, only silica based supports (silica and MCM-41) were employed which might be due to the ease of functionalization through their surface OH-groups and their rigid structure. Among the inorganic supports, MCM-41 supported catalyst (3) showed higher activity than silica supported catalyst (4) (entries 34 and 35). The high surface area (852  $m^2 g^{-1}$ ) and uniform pores (3.5 nm) of MCM-41 were responsible for this result, indicating that the porous catalysts together with large surface area would be the possible candidates for better catalytic efficiency. Regarding the organic supports, only PS was investigated. The catalytic efficiency of PS supported catalyst (5) was found to be very low (TOF-151 h<sup>-1</sup>) under similar reaction conditions (entries 34 and 36). Considering the amine (3), nitrile (6) and thiol (7) functionalities on the surface of support, the amine functionalized catalyst (3) exhibited better activity than 6 and 7 (entries 34, 37 and 38). This might be due to the strong electron donating ability of amine groups to metal ion than those of nitrile and thiol groups. Of the primary (4), secondary (8) and tertiary amine (9) functionalized complexes, the secondary amine functionalized complex (8) showed highest TOF (1384  $h^{-1}$ ) (entries 35, 39 and 40). This again reveals that the strong electron donating ligands increases the efficiency of the catalyst as secondary amine is better electron donor than primary and tertiary amines. Similar trend was obtained while considering catalysts 5, 10 and 11 (entries 35, 41 and 42). Conversely, recycling experiments of 3, 6 and 7 showed that catalysts 3 and 6 deactivated more significantly than catalyst 7. This may be the better back donating ability of thiol group than the nitrile and amine functional groups; thus, the bond between metal and thiol donor ligand of the support remains stronger.

Furthermore, these Ru complexes produced the formate only in the presence of external ligands/additives (PPh<sub>3</sub>, AsPh<sub>3</sub>, NPh<sub>3</sub> and Ph<sub>2</sub>P(CH<sub>2</sub>)<sub>2</sub>PPh<sub>2</sub> (dppe)), suggesting the in situ formed active catalyst contained external ligand as one of the ligands (Chart 1, showed the expected active catalyst (**4A**) for catalyst **4**).<sup>64</sup> They have also studied the outcome of the reaction with various additives and observed that the bidentate ligand, dppe, exhibited higher catalytic efficiency than the monodentate ligands (entry 34, 36, 43-46). This was attributed to the smaller bite angle of the dppe ligand (313.082°, 313.418°) than the PPh<sub>3</sub> ligand (314.76°), which consequently reduces the steric hindrance of dppe ligand with the Ru ion. Therefore, the coordination of dppe with metal ions was more favorable than PPh<sub>3</sub>, which led to the higher activity of dppe containing catalysts.<sup>67</sup>

In 2008, Zhang et al. employed ionic liquid (IL) as a reusable base to isolate formic acid from formate.<sup>68</sup> In light of Zheng and co-workers results, 63-67 they have employed silica supported Ru complex ["Si"-(CH<sub>2</sub>)<sub>3</sub>NH(CSCH<sub>3</sub>)-{RuCl<sub>3</sub>(PPh<sub>3</sub>)}] as a catalyst for this purpose. The catalyst in combination with amine functionalized IL promoted the CO2 hydrogenation with a maximum TOF of 103 h<sup>-1</sup>. Almost 1:1 molar ratio of formic acid to IL (used) was observed, indicating the complete consumption of the added IL. They also prepared diamine-functionalized IL to improve the efficiency of CO<sub>2</sub> hydrogenation.<sup>69</sup> The maximum TOF of 920  $h^{-1}$  was obtained at relatively high temperature (80 °C) and pressure (18 MPa total pressure). As expected, the molar ratio of formic acid to IL was reached up to 2:1. Notably, the free formic acid was separated from the IL with the aid of N<sub>2</sub> flow at 130 °C and the catalyst and IL were reused for several runs. These unique features of this method offer the opportunity to apply the reaction in commercial process.

Hicks and co-workers further functionalized the amine groups of the mesoporous silica into imine groups by Schiff base reaction with o-(diphenylphosphino)benzaldehyde, and immobilized Ir complexes through an imine-phosphine coordination bond (**12**).<sup>70</sup> For comparison, monodentate phosphine complexes (**13** and **14**), amine precatalyst **15** and the homogeneous counterpart (**16**) were synthesized (Chart

2). X-ray photoelectron Spectroscopy (XPS) measurements of 12 and 16 showed that the environment of Ir in 12 (61.6 eV) and 16 (61.8 eV) are similar. Among the catalysts screened (12, 13, 14, 15 and 16), only phosphine containing catalysts (12, 13, 14 and 16) were showed activity in CO<sub>2</sub> hydrogenation to formate (entries 47-50). Catalyst 12 exhibited a higher TON (1300) than 13 (110) and 14 (400) (entries 47-49). Moreover, 12 showed almost 20 times higher efficiency than unsupported catalyst (16), revealing the increased stability and activity upon heterogenization of homogeneous complexes (entries 47 and 51). The catalytic efficiency was increased with temperature, and the highest TOF of 1200 h<sup>-1</sup> was attained at 120 °C (entries 52-54). Timedependent formate production studies showed that formate production increased with time, and the catalyst exhibited the maximum TON (2700) and afforded a maximum concentration of formate (0.270 M) at 60 °C after 20 h (entries 47, 52 and 55). Catalyst 12 was recycled at minimum time intervals (0.5 h) under mild conditions and obtained the average TON of 70.

Hicks and co-workers also employed polyethyleneimine (PEI), an aliphatic amine-based organic polymer containing primary, secondary and tertiary amine groups, as a support to immobilize the Ir complexes.<sup>71</sup> It was expected that this amine-based support would be multifunctional, acting as CO<sub>2</sub> capturing material, formate stabilizer and catalyst support. Hence, the catalyst **17** was prepared by tethering complex **16** on this PEI (Chart 3). They compared the activity of **17** with an imine containing catalyst **(18)** and a phosphine containing catalyst **(19)** and found that **17** exhibited better activity than **18** and **19** (entries 56-58). However, it is noteworthy that the efficiency of **17** is poor when compared to **12** (entries 54 and

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56), indicating the weakness of PEI supports. Additionally, it was found that varying the amount of Ir loading [Ir-25 % (PEI-PN/Ir-25), Ir-65 % (PEI-PN/Ir-65) and Ir-95 % (PEI-PN/Ir-95)] on the PEI backbone affected the efficiency of catalyst; PEI-PN/Ir-65 exhibited better efficiency (TOF 310 h<sup>-1</sup>) than PEI-PN/Ir-25 (TOF 94  $h^{-1}$ ) and PEI-PN/Ir-95 (TOF 122  $h^{-1}$ ). XPS and TEM measurements revealed the existence of agglomerated Ir nanoparticles on the surface of PEI-PN/Ir-25 and PEI-PN/Ir-95, whereas no such agglomerated Ir nanoparticles were observed in PEI-PN/Ir-65. Consequently, they suggested that the Ir nanoparticles are catalytically inactive for the hydrogenation of CO<sub>2</sub> to formate. In addition, the efficiency of catalysts was also affected by the PEI molecular weight (PEI-MW). Moreover, recycling experiments demonstrated that the efficiency of catalysts decreases continuously, especially for low PEI-MW catalyst, owing to the increased solubility and formation of inactive Ir species. Furthermore, the catalysts exhibited poor activity in the absence of external base, suggesting that the amines present in the backbone of PEI no longer significantly stabilize the formate under these conditions.

#### 3.2 Heterogenized COF Catalysts

Since the Ir/Ru complexes heterogenized on conventional silica, PS and aliphatic polymer supports demonstrated low catalytic activity and stability,<sup>63-71</sup> the research on new strategies/supports to immobilize the homogeneous complexes are inevitable. Thus, porous organic polymers have been used as catalyst supports owing to their high surface area, well-defined porosity, ease of use and the diverse number of synthetic routes.<sup>72</sup> Specifically, crystalline microporous organic polymers with ordered porous



Chart 4. Structural representation of catalysts 20 and 21

structures – so called 'covalent organic frameworks' (COFs) – have drawn particular attention due to their low density, high thermal stability, large surface area, tunable pore size and structure, and versatile covalent combination of building blocks.<sup>73</sup> These polymeric materials have used as gas storage materials, catalyst supports and photonic band gap materials.<sup>74-78</sup> Consequently, COFs like Troger's base-derived microporous organic polymers (TB-MOPs),<sup>79</sup> graphitic carbon nitrides (g-C<sub>3</sub>N<sub>4</sub>),<sup>80</sup> triazine-based covalent organic frameworks (CTFs)<sup>81</sup> and heptazine-based covalent organic frameworks (HBFs)<sup>82</sup> have been employed as catalyst supports for CO<sub>2</sub> hydrogenation to formate.

Liu and co-workers prepared a TB-MOP supported Ru(III) catalyst (**20**) through the coordination bond between the N atoms of the TB-MOP and the Ru(III) ions (Chart 4).<sup>79</sup> The microporous structure of **20** was confirmed by Brunauer-Emmett-Teller (BET) measurements. The catalyst **20** exhibited the substantial catalytic efficiency (TON-2254) in the presence of PPh<sub>3</sub> ligands at 40 °C under 12 MPa total pressure (entry 60). However, in the absence of PPh<sub>3</sub> ligands the TON was decreased to 25 (entries 59 and 60), suggesting the active catalyst could be similar to that proposed by Zheng and co-workers<sup>64</sup>.

Later, Lee *et al.* demonstrated the catalytic performance of Pd nanoparticles supported on mesoporous  $g-C_3N_4$  (**21**) (Chart 4).<sup>80</sup> The TON for **21** in 20 % NEt<sub>3</sub>-Deuterium oxide (D<sub>2</sub>O) solution was found to be 81 at 150 °C under  $p(H_2)/p(CO_2) = 1$  (entry 61). Interestingly, the relative ratio of gas pressures  $[p(H_2)/p(CO_2)]$  affected the outcome of the



Chart 5. Structural representation of catalysts 22 and 23

reaction; TON was increased to 106 at  $p(H_2)/p(CO_2) = 2$  (entries 61 and 62). However, TON was reduced on increasing the ratio further (entries 62 and 64).

Over the past ten years, homogeneous [IrCp\*(N-N)X]Y complexes (N-N represents bipyridine (bpy), phenonthroline and pyrimidine derivatives, Cp\*-1,2,3,4,5-pentamethyl cyclopentadiene,  $X-CI/H_2O$ ,  $Y-CI/SO_4^{2-}$ ) have shown tremendous catalytic activities and selectivities.83-85 The highest TON (222,000) and maximum TOF (53,800 h<sup>-1</sup>) were obtained with these catalysts by Himeda et al.<sup>35,83</sup> Since these catalysts are proton-responsive and pH-switchable, their catalytic activity and H<sub>2</sub>O solubility can be tuned by pH of the solution. Thus, at the end of the CO<sub>2</sub> hydrogenation (a decrease in the pH of the solution leaded by reaction equilibrium), the catalyst can be precipitated because of its low solubility in weak acidic solution (pH 5.5).<sup>86</sup> However, this unique property is only observed for the Ir-phenonthroline derivative. Recently, Yoon and co-workers developed a new strategy to heterogenize the homogeneous [IrCp\*(bpy)Cl]Cl complex (22) (Chart 5).<sup>81</sup> They employed a bpy incorporated CTF (bpy-CTF) as a support owing to its high thermal stability, large pore volumes and high surface areas. The bpy-CTF has the potential to form complexes with metal precursors (Chart 5). They hypothesized that the complex resulting from the reaction of [IrCp\*Cl<sub>2</sub>]<sub>2</sub> and bpy-CTF would have a similar coordination environment as that of complex 22. As they hypothesized, the heterogenized complex, bpy-CTF-[IrCp\*Cl]Cl (**23**), was synthesized and thoroughly characterized to prove its exact coordination environment as that of complex 22. Scanning electron microscopy (SEM) measurements of 23 illustrated the uniform distribution of Ir and Cl atoms throughout the complex, suggesting the uniform metalation of Ir ions onto bpy moieties. In addition, Energy dispersive X-ray spectroscopy (EDS) as well as XPS measurements revealed that the atomic ratio of Ir and Cl was close to 1:2. Moreover, XPS measurements of both 22 and 23 showed that they have exactly same EBE value for Ir  $4f_{7/2}$ (62.1 eV), reiterating the similar coordination environment of Ir in both the catalysts. Inductively coupled plasma mass spectrometry (ICP-MS) analysis of 23 showed that it has relatively high Ir content (4.7 wt%) in the framework, indicating every sixth CTF ring unit contains one {IrCp\*} unit. The temperature-dependent catalytic performance of 23

The temperature-dependent catalytic performance of **23** showed that the activity increased with temperature up to 120 °C, thereafter decreased as the temperature increased further (entries 65 and 68). This is attributed to the exothermic nature of the reaction. However, the catalytic activity increased with pressure and attained a maximum TON of 5,000 at 120 °C under 8 MPa total pressure (entry 69). The time-dependent formate generation studies revealed that the reaction attained equilibrium (0.6-0.7 M formate concentration) within a relatively short reaction time (2 h). In addition, under relatively mild conditions, catalyst **23** showed the highest ever initial TOF of 5,300 h<sup>-1</sup> for the conversion of CO<sub>2</sub> to formate using heterogeneous catalysts (entry 70). Moreover, catalyst **23** was recycled over five runs without



Chart 6. Structural representation of catalysts 24 and 25

significant loss of activity and on each recycling ca. 92  $\,\%$  catalytic activity was maintained.

Vey recently, Yoon and co-workers have also heterogenized the [IrCp\*(N-N)X]Y complex using  $g-C_3N_4$  (24) and HBF (25) supports (Chart 6).<sup>82</sup> The uniform metalation as well as the ratio of Ir to Cl (1:2) were confirmed by SEM and EDS measurements, respectively. ICP-MS analysis of 25 showed very less Ir content (0.86 wt%) in the framework. The catalyst 25 exhibited an initial TOF of 1500 h<sup>-1</sup> and TON of 6400 at 120 °C under 8 MPa total pressure (entries 71 and 72). The catalyst was recycled without significant loss of activity and stability, and on each recycling ca. 90 % catalytic activity was maintained with an average TON of 4000.

#### 4. Theoretical Investigations

Even though the research on development of efficient catalyst is progressive, understanding the complete reaction mechanism through the experimental research is rather difficult and time consuming. This is due to the fact that finding substrate-catalyst interactions, energies of molecules involved, transition states and intermediates structure, and activation barriers for the process is quite difficult.<sup>87</sup> To overcome these limitations, theoretical calculations have become powerful tools to investigate the reaction pathway.<sup>88</sup> Moreover, the key structure-activity relationship for the rational design of suitable and efficient catalyst could be gained through this study.

Synthesis of formic acid and methanol from  $CO_2$  and  $H_2$  involves formate as one of the intermediate. Hence, many reports discussed the reaction pathway for the formation of formic acid, free formate anion and catalyst bound formate from  $CO_2$  and  $H_2$ .<sup>89-91</sup> However, the calculations involving only

formic acid formation using heterogeneous catalysts are presented in here.  $^{\rm 92-97}$ 

Peng et al. theoretically explored CO<sub>2</sub> hydrogenation to formic acid on Ni(111) surfaces.<sup>92</sup> They investigated the reaction mechanism via two routes, namely formate intermediate route (HCOO\*\*) in which CO<sub>2</sub> can be hydrogenated at its carbon atom and carboxyl intermediate route (COOH\*) in which  $\mathrm{CO}_2$  can be hydrogenated at its oxygen atom, using Ni(111) surfaces. Their calculations showed that for the formation of HCOO\*\* a lower activation energy (14.3 kcal mol<sup>-1</sup>) is required than for the COOH<sup>\*</sup> (19.1 kcal mol<sup>-1</sup>). This result clearly suggests that the HCOO\*\* route is more favorable than COOH\* route. Previously, Vesselli et al. concluded that the COOH\* route preferably produce CO and H<sub>2</sub>O instead of formic acid by Ni(110) surface. <sup>93</sup> Peng et al. also studied the second hydrogenation step, that is the formation of formic acid from HCOO\*\*, and found that it has very high activation barrier (14.3 kcal mol<sup>-1</sup>), suggesting this might be the rate-determining step for formic acid production.<sup>92</sup> Overall, the reaction is highly endothermic (12.9 kcal mol<sup>-1</sup>). Moreover, they also extensively studied to reduce such a high activation barrier and concluded that if subsurface H [absorbed in the subsurface of Ni(111)] involve in the second hydrogenation step, the activation barrier could be lowered and can make the overall reaction exothermic (-16.3 kcal mol<sup>-1</sup>). Similar results were obtained for Ni(110) surfaces.<sup>94</sup>

Limtrakul and co-workers theoretically investigated the reaction mechanism of hydrogenation of  $CO_2$  to formic acid catalyzed by Cu-alkoxide-functionalized metal organic framework (Cu-MOF-5).<sup>95</sup> Two different reaction pathways

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are proposed, namely concerted and stepwise mechanisms. In both the pathways, reactants  $(CO_2 \text{ and } H_2)$  are initially adsorbed on the Cu-MOF-5 catalyst and form the coadsorption complex. For the concerted mechanism, the reaction is proposed to take place in a single step with the active site of catalyst not assisting the H<sub>2</sub> splitting. In the transition state of this pathway, the adsorbed CO<sub>2</sub> is simultaneously hydrogenated at the C and O atom to form formic acid. The activation barrier for this pathway is calculated to be 67.2 kcal mol<sup>-1</sup>. For the stepwise mechanism, in which a part of the active site assists the H<sub>2</sub> splitting, the reaction occurs via two steps involving a formate intermediate. The first step, which is the formation formate intermediate, is found to be the rate-determining step with the activation energy of 24.2 kcal mol<sup>-1</sup>. The more facile second step, in which the proton is transferred to the formate intermediate, has a smaller activation barrier (18.3 kcal mol<sup>-1</sup>). Because of the smaller activation barriers associated with this pathway (24.2 vs 67.2 kcal mol<sup>-1</sup>), it, therefore, seems to be more favored over the concerted one. Furthermore, the catalytic effect of Cu-MOF-5 is also compared with the gas-phase uncatalyzed reaction in which the reaction takes place in one step with a barrier of 73.0 kcal mol<sup>-1</sup>. Therefore, this investigation clearly infers the two important design strategies for efficient catalysts for this reaction. (1). the catalysts would adsorb the reactants. (2). it would assist the H<sub>2</sub> splitting.

Since the frustrated Lewis pairs (FLPs) are capable of activating CO<sub>2</sub> and heterolytically dissociating H<sub>2</sub>, Ye et al. theoretically demonstrated the reaction mechanism of hydrogenation of CO<sub>2</sub> to formic acid catalyzed by Lewis pairfunctionalized metal organic framework (UiO-66-P-BF<sub>2</sub>).<sup>96</sup> They investigated the reaction in two different approaches. In the first approach, H<sub>2</sub> is activated initially by dissociative adsorption, and then reacting with physisorbed CO2 to produce formic acid. In this pathway, the addition of hydridic and protic hydrogens (chemisorbed H atoms) to C and O of physisorbed CO<sub>2</sub> respectively, occurs in a concerted fashion with the activation barrier of 10.8 kcal mol<sup>-1</sup>. In the second approach, CO<sub>2</sub> is activated initially by chemisorptions, and then reacting with physisorbed H<sub>2</sub>. However, in this approach, the undesired formyl and hydroxyl moieties were produced with high activation barrier rather than the desired formic acid product. This is because the CO<sub>2</sub> bound too strongly with the FLP of UiO-66-P-BF<sub>2</sub> through chemisorption. Hence, for the UiO-66-P-BF<sub>2</sub> catalyst to work in practice, one would have to expose the material first to H<sub>2</sub> and then to CO<sub>2</sub> to avoid the competing reaction and potential poisoning of the catalyst. This requirement would prohibit its practical use. Therefore, the designed catalyst should weakly bind with CO<sub>2</sub> through FLP (P-BF<sub>2</sub>) and at the same time it would provide a binding site that selectively dissociates H<sub>2</sub>.

Limtrakul and co-workers also explored the catalytic reaction pathway of Cu embedded in the surface of graphene (Cu/dG) for the  $CO_2$  hydrogenation to formic acid.<sup>97</sup> Initially, they studied the properties of Cu/dG through their calculations and found that the catalyst Cu/dG binds more

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strongly with H<sub>2</sub> (adsorption energy = -6.12 kcal mol<sup>-1</sup>) than  $CO_2$  (adsorption energy = -5.1 kcal mol<sup>-1</sup>). In addition, the Cu/dG is more selective for the adsorption of H<sub>2</sub> molecule rather than the CO<sub>2</sub> molecule. They investigated the course of the reaction via two paths. In the first path, the reaction takes place in two steps. In the initial step, the first hydrogenation of  $CO_2$  takes place, without activating the  $H_2$ molecule, through the highest activation barrier (34.6 kcal mol<sup>-1</sup>) and produces the unstable H-Cu-COOH intermediate. In the later step, the second hydrogenation takes place through the H-transfer from the Cu atom to the carbon of the -COOH moiety via three membered ring with the activation barrier of 4.0 kcal mol<sup>-1</sup>. Finally, formic acid is released from the Cu/dG catalyst with the activation energy of 20.1 kcal  $mol^{-1}$ . For the second route, the H<sub>2</sub> molecule is activated by dissociating H<sub>2</sub> molecule to Cu-H and C-H (from grapheme carbon) moieties in the first step with the highest energy barrier of 19.7 kcal mol<sup>-1</sup>. In the second step, the insertion of CO<sub>2</sub> into the Cu-H species to form the formate intermediate (HCOO-Cu/H-dG) is much more favorable (-14.6 kcal mol<sup>-1</sup>) and requires the activation energy of 13.6 kcal mol<sup>-1</sup>. Finally, the protonation of formate intermediate preferably takes place with the second  $H_2$  molecule (11.6 kcal mol<sup>-1</sup>). Therefore this study infers that the H<sub>2</sub> activated route would be more facile than the inactivated H<sub>2</sub> route.

#### 5. Summary and Conclusions

Diverse forms of heterogeneous catalysts for the conversion of  $CO_2$  into formate have evolved to meet the requirements for industrial application. The following features have emerged as being important for achieving this challenging goal. The heterogeneous catalyst should be sufficiently active to generate enough formate within relatively short period of reaction time. Catalyst's support framework should be sufficiently robust to prevent deleterious decomposition of catalytic active site in harsh reaction condition (pH = 13). The catalysts should be easily separated from reaction mixture at the end of reaction and recycled. Most of these requirements are fulfilled by heterogenization of homogeneous Ir complexes by incorporating onto the pore of the covalent organic frameworks.

Although the field has gone through a rapid progression phase, more work must be carried out to achieve remaining important goals of the development of catalysts for the conversion of  $CO_2$  into formate. The first is to obtain a system having the extreme stability over repeated recycle. Another is to generate the catalyst with cheap transition metal ion(s).

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